**Tableau Equations** 

$$\begin{bmatrix}
\mathbf{0} & \mathbf{0} & \mathbf{S} \\
-\mathbf{S}^{T} & \mathbf{I} & \mathbf{0} \\
\mathbf{0} & \mathbf{M}_{0}\mathbf{p} + \mathbf{M}_{1} & \mathbf{N}_{0}\mathbf{p} + \mathbf{N}_{1}
\end{bmatrix}
\begin{bmatrix}
\mathbf{e}(t) \\
\mathbf{v}(t) \\
\mathbf{i}(t)
\end{bmatrix} = \begin{bmatrix}
\mathbf{0} \\
\mathbf{0} \\
\mathbf{u}_{s}(t)
\end{bmatrix}$$

$$\begin{bmatrix} \mathbf{0} & \mathbf{0} & \mathbf{Q} \\ -\mathbf{Q}^T & \mathbf{I} & \mathbf{0} \\ \mathbf{0} & \mathbf{M}_0 \mathbf{p} + \mathbf{M}_1 & \mathbf{N}_0 \mathbf{p} + \mathbf{N}_1 \end{bmatrix} \begin{bmatrix} \mathbf{v}_t(t) \\ \mathbf{v}(t) \\ \mathbf{i}(t) \end{bmatrix} = \begin{bmatrix} \mathbf{0} \\ \mathbf{0} \\ \mathbf{u}_s(t) \end{bmatrix}$$

$$\begin{bmatrix} -\mathbf{B}^T & \mathbf{0} & \mathbf{I} \\ \mathbf{0} & \mathbf{B} & \mathbf{0} \\ \mathbf{0} & \mathbf{M}_0 \mathbf{p} + \mathbf{M}_1 & \mathbf{N}_0 \mathbf{p} + \mathbf{N}_1 \end{bmatrix} \begin{bmatrix} \mathbf{i}_L(t) \\ \mathbf{v}(t) \\ \mathbf{i}(t) \end{bmatrix} = \begin{bmatrix} \mathbf{0} \\ \mathbf{0} \\ \mathbf{u}_s(t) \end{bmatrix}$$

# R L C V-I Relations in Laplace Domain

$$i = C\frac{dv}{dt} \qquad v = L\frac{di}{dt} \qquad v = iR$$

$$V(s) = \left(\frac{1}{Cs}\right)I(s) + \frac{v(0^{-})}{s}, \quad V(s) = LsI(s) - Li(0^{-}), \quad V(s) = RI(s)$$

# The Origin of Initial Conditions

$$\int_{a}^{x} \frac{df(t)}{dt} dt = f(x) - f(a) \qquad f(x) = \int_{a}^{x} \frac{df(t)}{dt} dt + f(a)$$

# SOLUTION TO FIRST ORDER LINEAR DIFFERNTUIAL EQUATION

$$\tau \frac{dx}{dt} + x(t) = B$$
  $x(t) = Ae^{\left(-\frac{t}{\tau}\right)} + B$ 

#### TRANSMISISON LINES

$$v(x,t) = v_o + v_1 \left( t - \frac{x}{u_p} \right) + v_2 \left( t + \frac{x}{u_p} \right) \qquad \text{forward backward wave decomposition}$$
 
$$i(x,t) = i_o + i_1 \left( t - \frac{x}{u_p} \right) + i_2 \left( t + \frac{x}{u_p} \right) \qquad \text{forward backward wave decomposition}$$
 
$$i_1(x,t) - i_1(x,t_o) = \frac{1}{Z_0} (v_1(x,t) - v_1(x,t_o))$$
 
$$i_2(x,t) - i_2(x,t_o) = -\frac{1}{Z_0} (v_2(x,t) - v_2(x,t_o))$$

$$i(x,t) = i_o + i_1 \left(t - \frac{x}{u_p}\right) + i_2 \left(t + \frac{x}{u_p}\right)$$
 forward backward wave decomposition

$$i_1(x,t) - i_1(x,t_o) = \frac{1}{Z_o} (v_1(x,t) - v_1(x,t_o))$$

$$i_2(x,t) - i_2(x,t_o) = -\frac{1}{Z_0} (v_2(x,t) - v_2(x,t_o))$$

Voltage Reflection Coefficient for a lossless line at an impedance R

$$\rho = \frac{R - Z_0}{R + Z_0}$$

Transfer of an impedance Z from x=0 to x=1 on a lossless transmission line in the frequency domain.

$$Z_{l} = Z_{0} \left( \frac{Z \cos(\beta l) + jZ_{0} \sin(\beta l)}{Z_{0} \cos(\beta l) + jZ \sin(\beta l)} \right)$$

Transfer of source with impedance  $Z_{S}$  at x=0 to x=l on a lossless transmission line in the frequency domain.

$$V_{SE} = \frac{Z_0 V_S}{Z_0 \cos(\beta l) + j Z_S \sin(\beta l)}$$

$$V_x = V_+ e^{-jbx} + V_- e^{jbx}$$

$$\beta = \omega \sqrt{LC} \qquad Z_0 = \sqrt{\frac{L}{C}} \qquad u_p = \frac{1}{\sqrt{LC}}$$

$$\rho(s) = \frac{Z(s) - Z_0(s)}{Z(s) + Z_0(s)}$$
 Reflection coefficient at an impedance Z(s)

## **Uniform Loaded Line Equations Approximations**

Load  $C_x$  at spacing  $l_x$ . Unloaded line capacitance  $C_0$  F/m

$$a = \left(1 + \frac{C_x}{l_x C_0}\right) = \left(1 + \frac{Z_0 C_x}{T_x^{Unloaded}}\right)$$

$$au_d^{Loaded} = au_d^{Unloaded} \sqrt{a} \qquad Z_0^{Loaded} = rac{Z_0^{Unloaded}}{\sqrt{a}}$$

## Approximate Second Order Modelling of Loaded Lossless Line

**Backward or Source** 

end damping

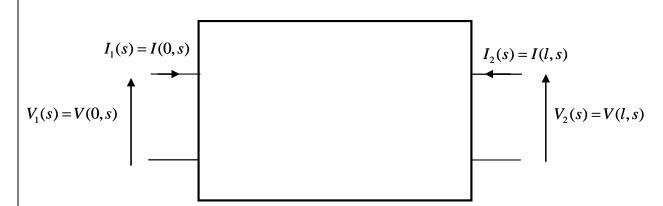
$$\omega_{n} = \frac{1}{\sqrt{Z_{0}C_{L}T_{d}}}, \ \xi = \frac{R_{S}\left(Z_{0}C_{L} + T_{d}\right)}{2Z_{0}\sqrt{Z_{0}C_{L}T_{d}}} \approx \frac{R_{S}}{2Z_{0}}\sqrt{\frac{Z_{0}C_{L}}{T_{d}}}$$

**Forward or Destination** 

end damping

$$\omega_n = \frac{1}{\sqrt{Z_0 C_L T_d}}, \ \xi = \frac{Z_0}{2R_L} \sqrt{\frac{T_d}{Z_0 C_L}}$$

#### **Two Port Model of Transmission Line**



$$\begin{bmatrix} V_2(s) \\ -I_2(s) \end{bmatrix} = \begin{bmatrix} \cosh(\gamma(s)l) & -Z_0(s)\sinh(\gamma(s)l) \\ -\frac{1}{Z_0(s)}\sinh(\gamma(s)l) & \cosh(\gamma(s)l) \end{bmatrix} \begin{bmatrix} V_1(s) \\ I_1(s) \end{bmatrix}$$

$$Z_0(s) = \sqrt{\frac{(R+sL)}{(G+sC)}} \qquad \gamma(s) \triangleq \sqrt{(R+sL)(G+sC)}$$

#### INCIDENCE MATRIX CONVENTION

 $\begin{cases} +1 \text{ edge } k \text{ leaves vertex } i \\ -1 \text{ edge } k \text{ enters vertex } i \\ 0 \text{ edge } k \text{ does not touch vertex } i \end{cases}$ 

- 1. Given a connected digraph **G**, a *loop* **L** is defined to be a connected subgraph of **G** in which precisely two edges (branches) are incident with each node.
- 2. Any loop formed by branches of a circuit is called a *mesh* iff the loop encloses no other branches, or wires in its interior.
- 3. Given a connected digraph **G**, a subset of branches **C** of **G** is called a *cut* set iff the following two conditions are satisfied:
  - the removal of all the branches of the cut set results in a digraph that is not a connected digraph, and
  - the removal of all but any one branch of G leaves the digraph connected.
- 4. A (spanning) *tree* T of a connected graph G is a subgraph which satisfies three fundamental properties:
  - It is connected.
  - It contains all connected vertices of G.
  - It has no loops (circuits).
- 5. Given a tree **T**, the edges of **G** can be partitioned into two disjoint sets:
  - Edges which belong to T, called tree branches or twigs for short
  - Edges which do not belong to T, called links or chords or cotrees branches.
- 6. Every twig of **T** together with some links defines a unique cut set, called the *fundamental cut set* associated with the twig.
- 7. Every link of **T** and the unique path on the tree between its two nodes constitutes a unique loop, called the *fundamental loop* associated with the link.
- 8. If S is the incidence for a given connected digraph G contained with one node used as the datum, a theorem due to Kirchoff states that the number of spanning trees is given by  $\det(\mathbf{SS}^T)$ .

# **LAPLACE TRANSFORMS**

F(s)	f(t), t>0
$Y(s) = \int_0^\infty \exp(-st) y(t) dt$	y(t)
Y(s)	$y(t) = \frac{1}{j2\pi} \int_{c-j\infty}^{c+j\infty} \exp(st) Y(s) ds$
$s^{n} Y(s) - s^{n-1} [y(0)]$ $-s^{n-2} [y'(0)] - \dots - s [y^{(n-2)}(0)]$ $-[y^{(n-1)}(0)]$	y <sup>(n)</sup> (t)
(1/s) F(s)	$\int_0^t Y(\tau) d\tau$
F(s)G(s)	$\int_0^t f(t-\tau)g(\tau)d\tau$
$\frac{1}{\alpha}F\left(\frac{s}{\alpha}\right)$	f (\alpha t)
$F(s - \alpha)$	$\exp(-\alpha t) f(t)$
1	$\delta(t)$
$\exp(-\alpha s),  \alpha \ge 0$	$\delta(t-\alpha)$
1/s	u(t)
$\frac{1}{s} \exp(-\alpha s)$	$u(t-\alpha)$
$\frac{1}{s^n},  n = 1, 2, 3, \dots$	$\frac{t^{n-1}}{(n-1)!}$
$\frac{1}{\left(s+\alpha\right)^{n}} \ ,  n=1,2,3,\dots$	$\left[\frac{t^{n-1}}{(n-1)!}\right] \exp\left(-\alpha t\right)$
$\frac{\alpha}{s(s+\alpha)}$	$1 - \exp(-\alpha t)$
$\frac{1}{(s+\alpha)(s+\beta)},  \beta \neq \alpha$	$\frac{1}{(\beta-\alpha)} \left[ \exp(-\alpha t) - \exp(-\beta t) \right]$

$\frac{s}{(s+\alpha)(s+\beta)},  \beta \neq \alpha$	$\frac{1}{(\alpha - \beta)} [\alpha \exp(-\alpha t) - \beta \exp(-\beta t)]$
$\frac{\alpha}{s^2 + \alpha^2}$	$\sin(\alpha t)$
$\frac{s}{s^2 + \alpha^2}$	cos(αt)
$\frac{s^2 - \alpha^2}{\left[s^2 + \alpha^2\right]^2}$	t cos(αt)
$\frac{\alpha}{s^2(s+\alpha)}$	$t - \frac{1}{\alpha} \left[ 1 - \exp\left(-\alpha t\right) \right]$
$\frac{s+\lambda}{(s+\alpha)^2+\beta^2}$	$\exp\left(-\alpha t\right)\left\{\cos(\beta t) + \left[\frac{\lambda - \alpha}{\beta}\right]\sin(\beta t)\right\}$
$\frac{s+\alpha}{s^2+\beta^2}$	$\frac{\sqrt{\alpha^2 + \beta^2}}{\beta} \sin(\beta t + \phi),  \phi = \arctan\left(\frac{\beta}{\alpha}\right)$

$$f(0^+) = \lim_{s \to \infty} sF(s)$$
  $f(\infty) = \lim_{s \to 0} sF(s)$ 

# **DIFFERENTIATION**

$$\frac{d(g(h(x)))}{dx} = \frac{d(g(h(x)))}{dh} \frac{d(h(x))}{dx}$$

$$\frac{d}{dx} (f(x) \cdot g(x)) = f(x) \cdot g'(x) + g(x) \cdot f'(x)$$

$$\frac{d}{dx} \left(\frac{f(x)}{g(x)}\right) = \frac{g(x) \cdot f'(x) - f(x) \cdot g'(x)}{(g(x))^2}$$

$$\frac{d}{dx} (x^n) = nx^{n-1}$$

$$\frac{d}{dx} (\ln x) = \frac{1}{x}$$

$$\frac{d}{dx} (\sin x) = \cos x$$

$$\frac{d}{dx} (\cos x) = -\sin x$$

$$\frac{d}{dx} (\tan x) = \sec^2 x$$

$$\frac{d}{dx}(\cot x) = -\csc^2 x$$

$$\frac{d}{dx}(\sec x) = \sec x \tan x$$

$$\frac{d}{dx}(\arcsin x) = \frac{1}{\sqrt{1 - x^2}}$$

$$\frac{d}{dx}(\arctan x) = \frac{1}{1 + x^2}$$

$$\frac{d}{dx}(\arcsin x) = \frac{1}{1 + x^2}$$

$$\frac{d}{dx}(\sinh x) = \cosh x$$

### INTEGRATION

$$\int x^{n} dx = \frac{1}{n+1} x^{n+1} + c, \quad n \neq -1$$

$$\int \frac{1}{x} dx = \ln|x| + c$$

$$\int a^{x} dx = \frac{1}{\ln a} a^{x} + c$$

$$\int \cos x dx = \sin x + c$$

$$\int \frac{dx}{1+x^{2}} = \arctan x + c$$

$$\int \frac{dx}{\sqrt{1-x^{2}}} = \arcsin x + c$$

$$\int \frac{dx}{\sqrt{1-x^{2}}} = \arcsin x + c$$

$$\int \frac{dx}{ax^2 + bx + c} = \begin{cases}
\frac{1}{\sqrt{b^2 - 4ac}} \ln \left( \frac{2ax + b - \sqrt{b^2 - 4ac}}{2ax + b + \sqrt{b^2 - 4ac}} \right), b^2 - 4ac \ge 0 \\
\frac{2}{\sqrt{4ac - b^2}} \tan^{-1} \left( \frac{2ax + b}{\sqrt{4ac - b^2}} \right), b^2 - 4ac < 0
\end{cases}$$