

Generic 2D Inverse Kinematics for Rovers

Miro Voellmy, 2019-04-09

Robot Model

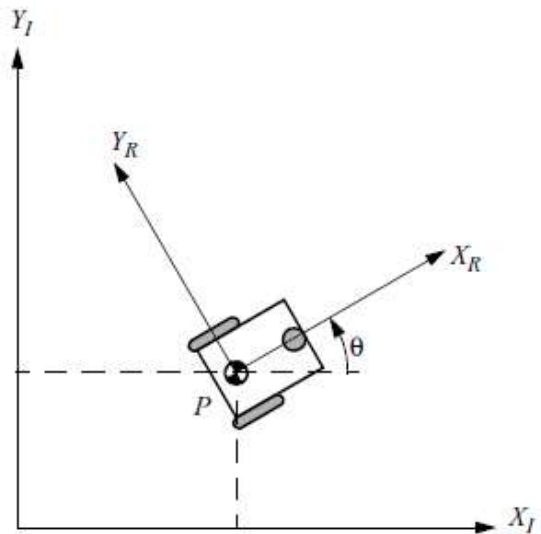


Figure 3.1
The global reference frame and the robot local reference frame.

Position and orientation of rover in world

$$\xi_I = \begin{bmatrix} x \\ y \\ \theta \end{bmatrix}$$

Linear and angular velocities of rover in world

$$\dot{\xi}_I = \begin{bmatrix} \dot{x} \\ \dot{y} \\ \dot{\theta} \end{bmatrix} = f(l, r, \theta, \phi_1, \phi_2)$$

Transformation from world to rover

$$R(\theta) = \begin{bmatrix} \cos \theta & \sin \theta & 0 \\ -\sin \theta & \cos \theta & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

Velocities transformed from world to rover

$$\dot{\xi}_R = R\left(\frac{\pi}{2}\right)\dot{\xi}_I$$

Figures and equations from

Introduction to Autonomous Mobile Robots, Siegwart, Nourbakhsh, Scaramuzza

<https://mitpress.mit.edu/books/introduction-autonomous-mobile-robots-second-edition>

Steered Wheel Constraints

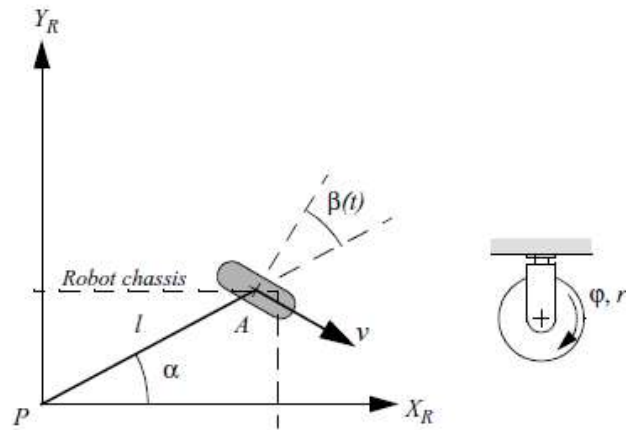


Figure 3.5
A steered standard wheel and its parameters.

Rolling Constraint

$$\begin{bmatrix} \sin(\alpha + \beta) & -\cos(\alpha + \beta) & (-l) \cos \beta \end{bmatrix} R(\theta) \dot{\xi}_I - r \dot{\phi} = 0 \quad (3.15)$$

No Sliding Constraint

$$\begin{bmatrix} \cos(\alpha + \beta) & \sin(\alpha + \beta) & l \sin \beta \end{bmatrix} R(\theta) \dot{\xi}_I = 0 \quad (3.16)$$

Equations 3.15 & 3.16 are used to first compute the steering angle β with (3.16) and then the wheel speed $\dot{\phi}$ with (3.15) for each wheel.

We want to steer the rover with respect to the rover frame. Therefore:

$$\theta = 0 \quad \text{and} \quad R(0) = I_3$$

$$\dot{\xi}_R = R(0) \dot{\xi}_I = \begin{bmatrix} \dot{x}_R \\ \dot{y}_R \\ \dot{\theta}_R \end{bmatrix}$$

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Steer Wheel Constraints

The equations (3.15, 3.16) simplify to:

$$\sin(\alpha + \beta) \dot{x}_R - \cos(\alpha + \beta) \dot{y}_R - l \cos(\beta) \dot{\theta}_R = r \dot{\phi}$$

$$\cos(\alpha + \beta) \dot{x}_R + \sin(\alpha + \beta) \dot{y}_R + l \sin(\beta) \dot{\theta}_R = 0$$

Solving for β using [1]:

$$\beta = \text{atan2}(-(\sin(\alpha) \dot{y}_R + \cos(\alpha) \dot{x}_R), l \dot{\theta}_R + \cos(\alpha) \dot{y}_R - \sin(\alpha) \dot{x}_R)$$

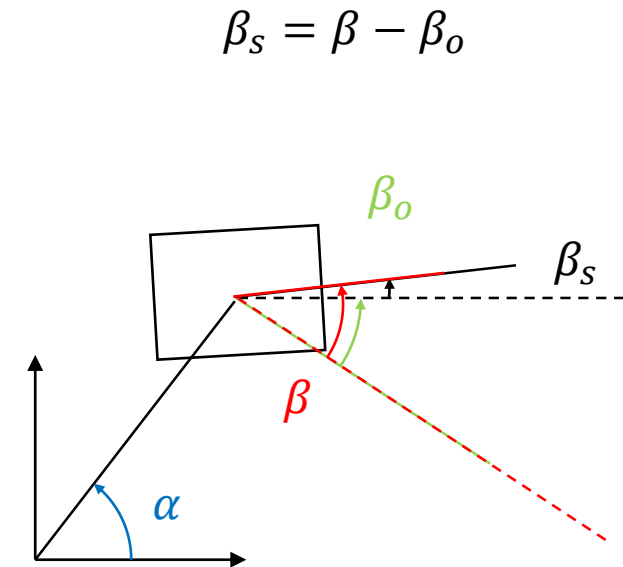
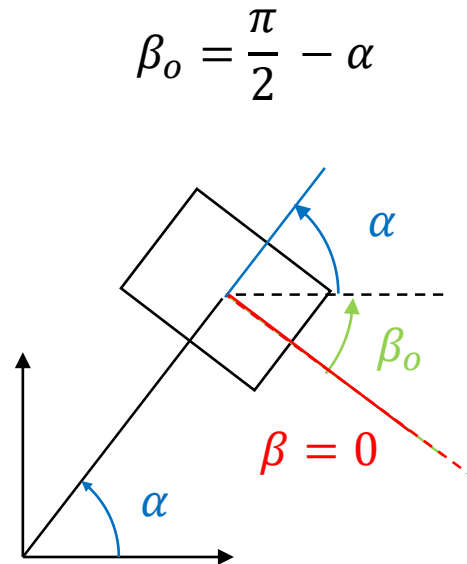
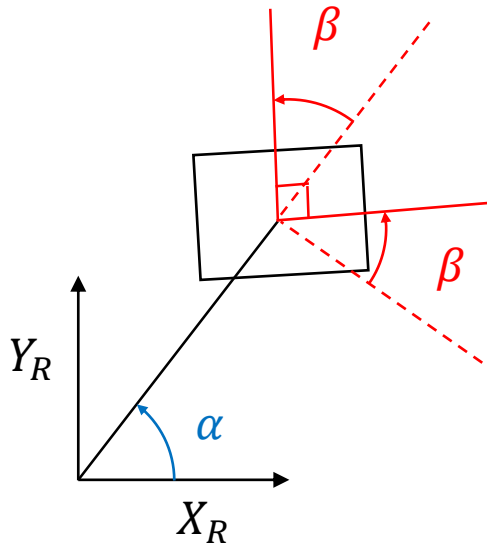
And $\dot{\phi}$ with β now known:

$$\dot{\phi} = \frac{\sin(\alpha + \beta) \dot{x}_R - \cos(\alpha + \beta) \dot{y}_R - l \cos(\beta) \dot{\theta}_R}{r}$$

Steering Angle Corrections

As shown in figure 3.5, β defines the wheel angle in respect the rover origin-normal.

For practical purposes the angle β_s in respect to the forward direction x is required.



Steering Angle Requirements

β_s should be set to minimize the wheel steering from its current position β_{curr} .

The wheel steering also has to stay within the motor limits:

$$-100^\circ \leq \beta_s \leq +100^\circ$$

Whenever β_s is changed by factors of 180° the sign of the wheel velocity $\dot{\varphi}$ has to be flipped.

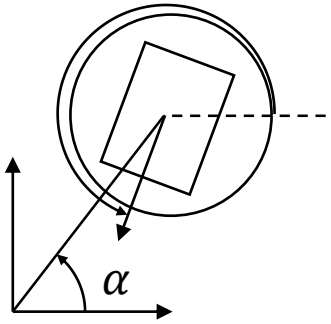
$$\dot{\varphi} = -\dot{\varphi}$$

Steering Angle Correction Procedure

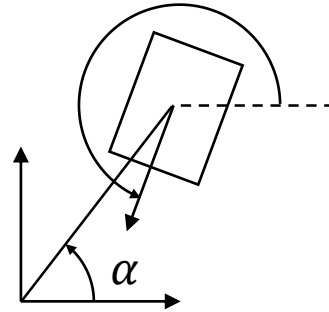
1. Limit β_s to $-360^\circ \leq \beta_s \leq +360^\circ$
2. Limit β_s to $-180^\circ \leq \beta_s \leq +180^\circ$
 - Flip $\dot{\phi}$ if applied
3. Limit β_s to motor limits $-100^\circ \leq \beta_s \leq +100^\circ$
 - Flip $\dot{\phi}$ if applied
4. If there are alternative configurations possible:
$$-100^\circ \leq \beta_s \pm 180^\circ \leq +100^\circ$$
5. Set β_s to closest one to β_{curr}
 - Flip $\dot{\phi}$ if applied

Steering Angle Correction Example

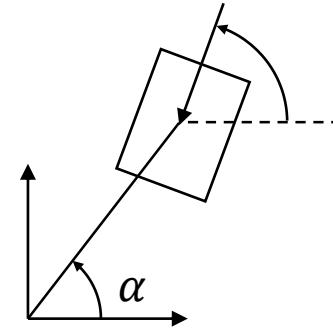
0. $\beta_s = 620^\circ$ $\dot{\varphi} = \frac{10^\circ}{s}$



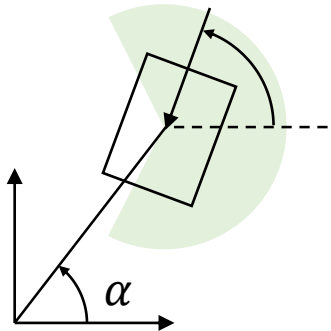
1. $\beta_s = 260^\circ$ $\dot{\varphi} = \frac{10^\circ}{s}$



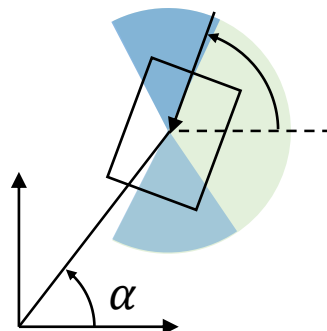
2. $\beta_s = 80^\circ$ $\dot{\varphi} = -\frac{10^\circ}{s}$



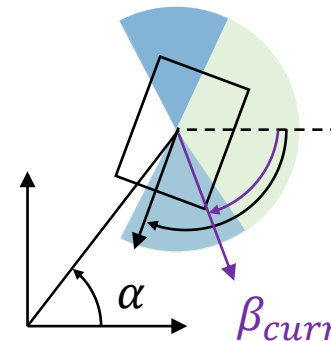
3. $\beta_s = 80^\circ$ $\dot{\varphi} = -\frac{10^\circ}{s}$



4. $\beta_s = 80^\circ$ $\dot{\varphi} = -\frac{10^\circ}{s}$



5. $\beta_s = 100^\circ$ $\dot{\varphi} = \frac{10^\circ}{s}$



Sources

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