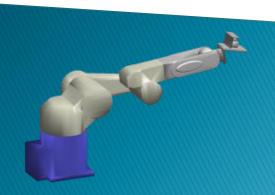
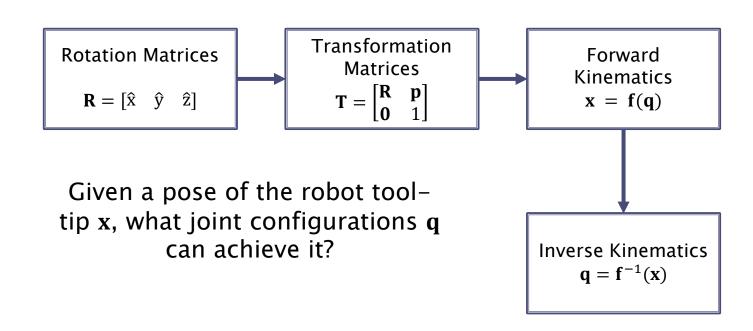
5.1 Inverse Kinematics

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Roadmap

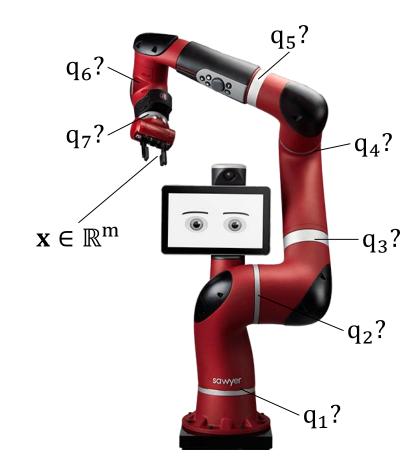


The Inverse Kinematics Problem

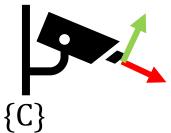
Given a *desired* end-effector pose $x \in \mathbb{R}^m$...

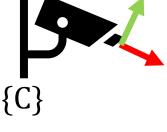
... find a set of joint positions $\mathbf{q} \in \mathbb{R}^n$ that satisfies the forward kinematics $\mathbf{x} = \mathbf{f}(\mathbf{q})$ (or some equivalent).

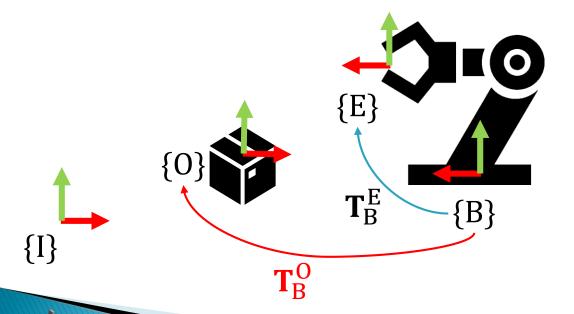
In other words, solve $q = f^{-1}(x)$.



Motivation for Forward Kinematics







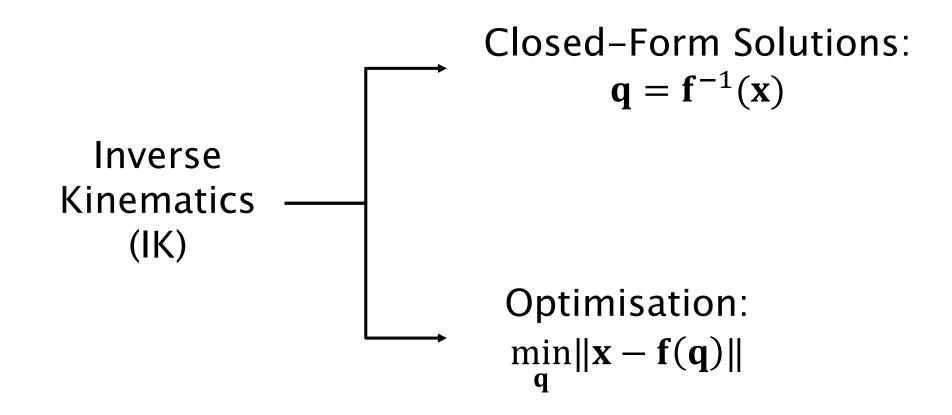
Desired end-effector transform to grasp object:

$$T_{\text{desired}} = T_{\text{B}}^{\text{O}}$$

Need to find a joint configuration **q** to reach the object:

$$T_{B}^{E}(q) = T_{desired}$$

Two Approaches to Inverse Kinematics



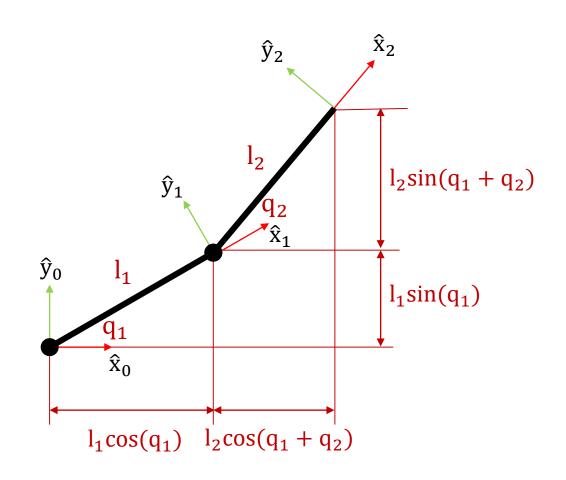
Forward kinematics:

$$x = f(q)$$

$$\begin{bmatrix} x \\ y \end{bmatrix} = \begin{bmatrix} l_1 \cos(q_1) + l_2 \cos(q_1 + q_2) \\ l_1 \sin(q_1) + l_2 \sin(q_1 + q_2) \end{bmatrix}$$

Inverse Kinematics:

$$\begin{bmatrix} \mathbf{q}_1 \\ \mathbf{q}_2 \end{bmatrix} = \mathbf{f}^{-1}(\mathbf{x})?$$



Pythagoras's Theorem:

$$d^2 = x^2 + y^2$$

Law of Cosines:

$$d^2 = l_1^2 + l_2^2 - 2l_1l_2\cos(\alpha)$$

$$\cos(\alpha) = \frac{l_1^2 + l_2^2 - d^2}{2l_1 l_2}$$

But also,

$$q_2 = \pi - \alpha$$

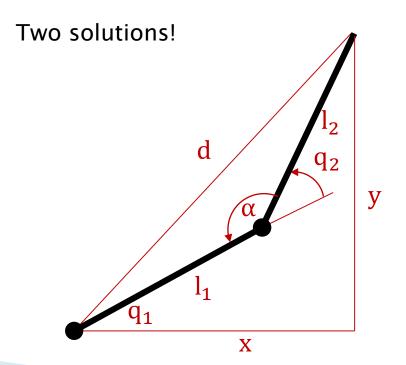
$$cos(q_2) = cos(\pi - \alpha)$$

$$= cos(\pi) cos(\alpha) + sin(\pi) sin(\alpha)$$

$$= -cos(\alpha)$$

$$= \frac{d_2 - l_1^2 - l_2^2}{2l_1 l_2}$$

$$q_{2} = \begin{cases} \pi - \cos^{-1}\left(\frac{l_{1}^{2} + l_{2}^{2} - x^{2} - y^{2}}{2l_{1}l_{2}}\right) \\ \cos^{-1}\left(\frac{x^{2} + y^{2} - l_{1}^{2} - l_{2}^{2}}{2l_{1}l_{2}}\right) \end{cases}$$



Using tangent rule:

$$tan(q_1 + \beta) = \frac{y}{x}$$

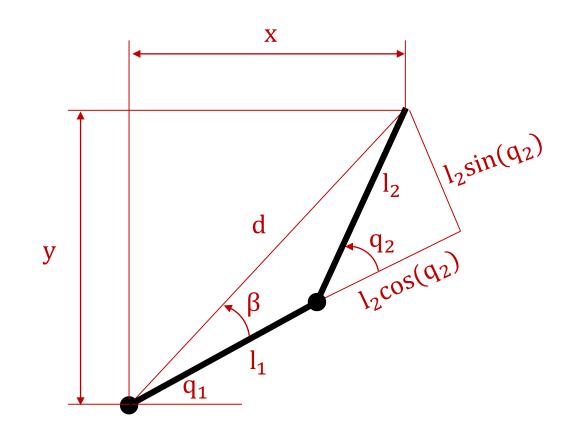
$$q_1 = tan^{-1} \left(\frac{y}{x}\right) - \beta$$

Using Law of Cosines:

$$\beta = \tan^{-1} \left(\frac{l_2 \sin(q_2)}{l_1 + l_2 \cos(q_2)} \right)$$

Hence:

$$q_1 = \tan^{-1}\left(\frac{y}{x}\right) - \tan^{-1}\left(\frac{l_2\sin(q_2)}{l_1 + l_2\cos(q_2)}\right)$$

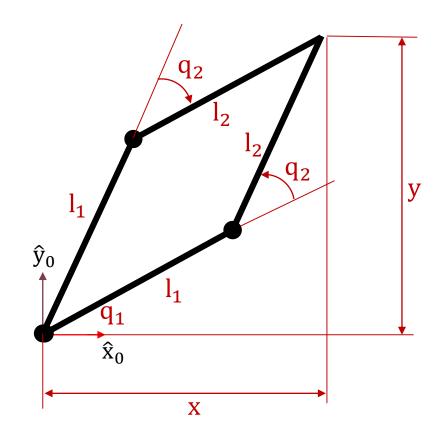


There are **2 distinct joint configurations** $\mathbf{q} \in \mathbb{R}^2$ for a given end-effector pose $\mathbf{x} \in \mathbb{R}^2$.

$$\mathbf{q} = \begin{bmatrix} \tan^{-1} \left(\frac{x}{y} \right) - \tan^{-1} \left(\frac{l_2 \sin(q_2)}{l_1 + l_2 \cos(q_2)} \right) \\ \pi - \cos^{-1} \left(\frac{l_1^2 + l_2^2 - x^2 - y^2}{2l_1 l_2} \right) \end{bmatrix}$$

Or

$$\mathbf{q} = \begin{bmatrix} \tan^{-1} \left(\frac{x}{y} \right) - \tan^{-1} \left(\frac{l_2 \sin(q_2)}{l_1 + l_2 \cos(q_2)} \right) \\ \cos^{-1} \left(\frac{x^2 + y^2 - l_1^2 - l_2^2}{2l_1 l_2} \right) \end{bmatrix}$$

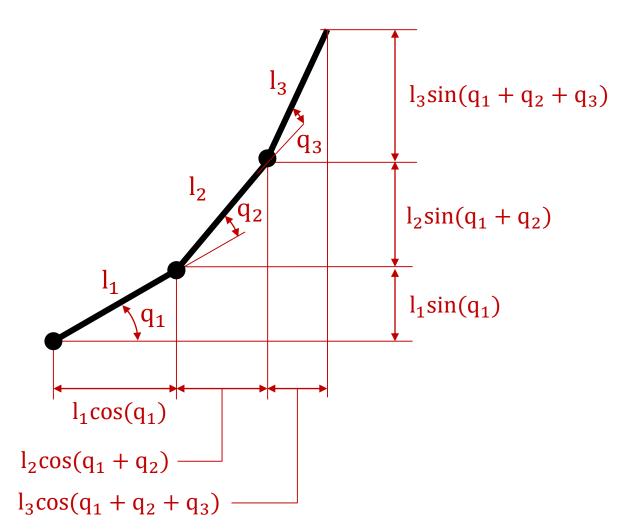


Forward kinematics:

$$\begin{bmatrix} x \\ y \end{bmatrix} = \begin{bmatrix} l_1c_1 + l_2c_{12} + l_3c_{123} \\ l_1s_1 + l_2s_{12} + l_3s_{123} \end{bmatrix}$$

Where:

- $c_1 = \cos(q_1)$
- $c_{12} = \cos(q_1 + q_2)$
- $c_{123} = \cos(q_1 + q_2 + q_3)$
- $s_{12} = \sin(q_1 + q_2)$
- $s_{123} = \sin(q_1 + q_2 + q_3)$



Task space:

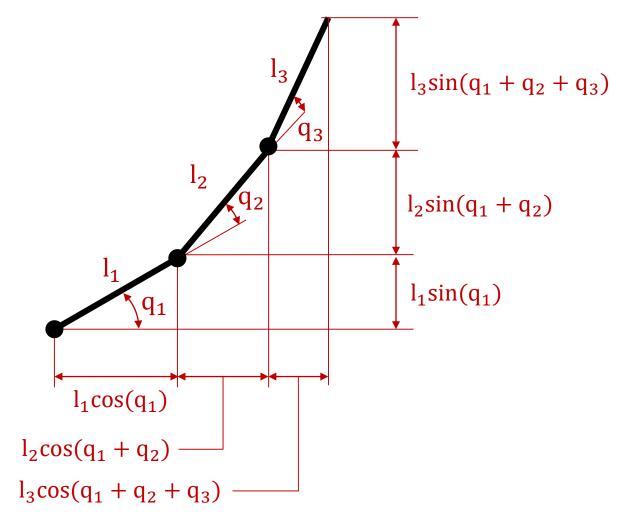
$$\mathbf{x} = \begin{bmatrix} \mathbf{x} \\ \mathbf{y} \end{bmatrix} \in \mathbb{R}^2$$

Joint/control space:

$$\mathbf{q} = \begin{bmatrix} q_1 \\ q_2 \\ q_3 \end{bmatrix} \in \mathbb{R}^3$$

$$m = 2 < n = 3$$
.

This system is underdetermined and thus has infinitely many solutions.



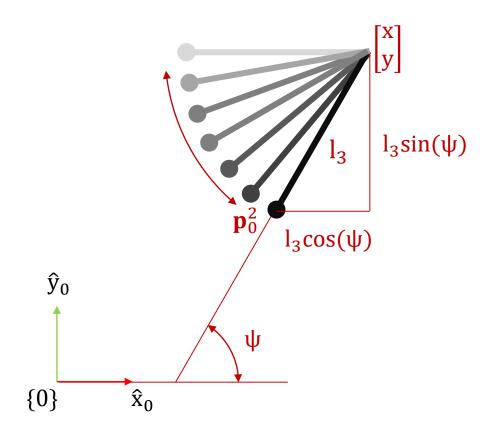
Since we have infinite joint solutions, the end-effector orientation ψ can be set (almost) arbitrarily.

Then the position of the 2nd link frame is:

$$\mathbf{p}_0^2 = \begin{bmatrix} \mathbf{x} - \mathbf{l}_3 \cos(\psi) \\ \mathbf{y} - \mathbf{l}_3 \sin(\psi) \end{bmatrix}$$

Then we can use inverse kinematics to solve the first 2 joints:

$$\begin{bmatrix} \mathbf{q}_1 \\ \mathbf{q}_2 \end{bmatrix} = \mathbf{f}^{-1}(\mathbf{p}_0^2)$$



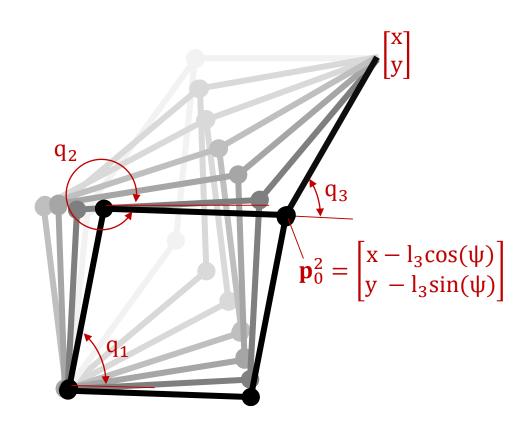
Given ψ and \mathbf{p}_0^2 , then the first 2 joint angles of the manipulator are:

$$q_{2} = \begin{cases} \pi - \cos^{-1} \left(\frac{l_{1}^{2} + l_{2}^{2} - (\mathbf{p}_{0}^{2})^{T} \mathbf{p}_{0}^{2}}{2l_{1}l_{2}} \right) \\ \cos^{-1} \left(\frac{(\mathbf{p}_{0}^{2})^{T} \mathbf{p}_{0}^{2} - l_{1}^{2} - l_{2}^{2}}{2l_{1}l_{2}} \right) \end{cases}$$

$$q_{1} = \tan^{-1} \left(\frac{x_{2}}{y_{2}} \right) - \tan^{-1} \left(\frac{l_{2} \sin(q_{2})}{l_{1} + l_{2} \cos(q_{2})} \right)$$

The 3rd joint is:

$$q_3 = \psi - (q_1 + q_2)$$



Insights in to the Inverse Kinematics Problem

For task space $\mathbf{x} \in \mathbb{R}^{m}$ and joint space $\mathbf{q} \in \mathbb{R}^{n}$:

- If m = n (same no. of joints to task space) there are finite joint configurations to achieve the endeffector pose*
- If n > m, (more joints than task space) there are infinite joint configurations to achieve the endeffector pose*

A robot with more degrees of freedom in the control space than required by the task space is said to be **redundant**.

Advantages of redundancy:

- Avoid joint limits
- Avoid collisions with obstacles
- Minimize joint velocities, torque, energy consumption...

^{*} Actually, this is not 100% correct, but it is a good heuristic!

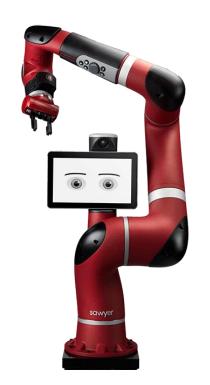
Inverse Kinematics for Complex Robot Arms

Very difficult, and sometimes an analytical solution may not even exist.

Certain robot geometry can be exploited, e.g. wrist-type robots.

Alternatively, we can use mathematical optimization to solve IK.

We can let computers do the work for us.



 $\mathbf{q} \in \mathbb{R}^7$

Summary of Inverse Kinematics

- Given a desired end-effector pose $x \in \mathbb{R}^m$, find a feasible joint configuration $q = f^{-1}(x) \in \mathbb{R}^n$
- Two approaches:
 - Closed–form solutions
 - Optimization
- \blacktriangleright Finite solutions for m = n
- ▶ Infinite solutions for m < n