

CONSTRAINING THE HIGH DENSITY NUCLEAR SYMMETRY ENERGY WITH PIONS

By

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ABSTRACT

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ACKNOWLEDGEMENTS

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TABLE OF CONTENTS

LIST OF TABLES	vii
LIST OF FIGURES	viii
CHAPTER 1 EXPERIMENT	1
1.1 Energy loss in material	1
1.2 Time Projection Chambers	1
1.3 Pad Response Function	1
1.3.1 Experimental Pad Response Function	3
1.4 S π RIT TPC Overview	5
1.4.1 Enclosure	8
1.4.2 Voltage Step Down	9
1.4.3 Field Cage	9
1.4.4 Voltage Step Down	10
1.4.5 Pad Plane	13
1.4.6 Wire Planes	13
1.4.7 Electronics	16
1.4.8 Considerations when constructing a TPC	17
1.4.9 Gas Properties	18
1.5 Ancillary Detectors	19
1.5.1 Kyoto Multiplicity Trigger	19
1.5.2 Krakow KATANA Veto and Multiplicity Array	20
1.5.3 Active Veto Array	21
1.6 Radio Isotope Beam Factory (RIBF) Facility	21
1.7 Experimental Setup	22
1.8 Data Acquisition (DAQ)	23
1.9 Trigger Condition	24
1.10 Collision Data Taken	27
CHAPTER 4 DATA ANALYSIS I: CALIBRATION AND CORRECTIONS	25
4.1 Software	25
4.1.1 Pulse Shape Algorithm	28
4.2 Calibrations and Corrections	28
4.2.1 Gating grid noise subtraction	28
4.2.2 Cocktail calibration	29
4.2.3 Electronics calibration	31
4.2.4 Anode gain calibration	32
4.2.5 Extending the dynamic range of the Electronics	33
4.2.6 Method of Desaturation	36
4.2.7 Space Charge Corrections	41
4.3 Monte Carlo Simulation	51

4.3.1	Drift Task	52
4.3.2	Pad Response Task	54
4.3.3	Electronics Task	54
4.3.4	Simulating Saturation	56
4.4	Monte Carlo Track Embedding	60
4.4.1	MC and Data Comparison	65
4.5	Aligning TPC	66
4.6	CoBo timing correction	66
4.7	Efficiency Corrections	67
APPENDIX	69
BIBLIOGRAPHY	72

LIST OF TABLES

Table 1.1	An overview of the properties of the S π RIT TPC	7
Table 1.2	Wire plane properties	13
Table 1.3	Summary of range of GET electronics settings.	17
Table 1.4	19
Table 1.5	Primary and secondary beam properties produced in the S π RIT TPC experimental campaigns.	23
Table 4.1	Summary of expected cocktail.	29
Table 4.2	Summary of expected cocktail.	29
Table 4.3	Summary of expected cocktail.	29
Table 4.4	Summary of expected cocktail.	31
Table 4.5	Average energy loss of each beam.	42
Table 4.6	An overview of the properties of the TPC	53
Table .1	List of runs for the analysis.	70

LIST OF FIGURES

Figure 1.1 A cartoon illustration of the charge distribution resulting from an electron avalanche on one wire and the projections of the distribution onto the two axis $\rho(x)$ onto the x-axis and $\rho(z)$ onto the z-axis. The orientation of the wire planes is flipped upside down to display the perspective better.	3
Figure 1.2 Experimental pad response function of many events for a crossing angle of $85^\circ < \theta \leq 90^\circ$	4
Figure 1.3 PRF response from π^- data.	5
Figure 1.4 Parameters N_0 and σ as a function of the crossing angle θ with the 4 th order polynomial fits.	6
Figure 1.5 Overview of the S π RIT TPC	8
Figure 1.6 FC overview	10
Figure 1.7 FC overview 2	11
Figure 1.8 Schematic of the electric connections relevant to the Field Cage system.	12
Figure 1.9 Schematic of the TPC system	13
Figure 1.11 On and off configurations of the gating grid.	15
Figure 1.12 Number of electrons produced in a single avalanche on an anode wire. Two different voltages were simulated using Garfield++ at 1470 V and 1214 V. The expected Polya distribution fit is also given in yellow.	16
Figure 1.13 Drift velocity of electrons in P10 gas.	18
Figure 1.14 Exploded views of Kyoto and KATANA arrays.	20
Figure 1.15 Overview of the RIBF, BigRIPS, and SAMURAI beamline.	22
Figure 1.16 Drawing of the experimental setup with the TPC inside of the SAMURAI magnet at 0° configuration.	24
Figure 1.17 KATANA trigger box logic.	25
Figure 1.18 Master trigger logic.	25

Figure 4.1	Cartoon graphic of a top down view of a fit to a track passing through several pads. The bolded pads and the charges q_i represent the hits belonging to that pad and the clusters of the track representing the average position of the track. The three clusters at the bottom are clustered in the x-direction and for the upper three clustered in the z-direction. The estimate of the position of the avalanche is given by the track fit and the position from the center to each pad to the \bar{x} position is given as λ_i .	27
Figure 4.2	Calibration of electronics	32
Figure 4.3	Calibration of low high.	33
Figure 4.4	The expected dE/dx lines of different particles are given in red as calculated by Geant4. The approximate dynamic range of the TPC is shown by the vertical bar for the gain setting used in the experiment. Anything outside of this region would be saturated to some degree.	35
Figure 4.5	A typical case of a saturating event. The red pulses represent the time bucket signal for each collected charge. The pads directly underneath the avalanche point, q_2' and q_3' , are saturated while pads farther away, q_1 and q_4 are not saturated.	37
Figure 4.6	Pad plane projection for a cocktail event in the TPC.	38
Figure 4.7	Pad plane projection for a collision event in the TPC. Highlighted by red arrows are two regions of anode wires which had a reduced voltage of 1214 V. The voltage of the rest of the TPC anode wires are 1460 V. The reduction in voltage reduces the gain by a factor of about 10.	39
Figure 4.8	The left panel shows the high gain stopping power vs low gain when the method of desaturation was not applied. In the right panel the desaturation technique was applied to the high gain region. The low gain does not suffer from saturation and represents the true dE/dx value.	40
Figure 4.9	Uncorrected (left panel) and desaturated (right panel) cocktail data.	40
Figure 4.10	Uncorrected (left panel) and desaturated (right panel) collision data at polar angles of $\theta < 40^\circ$ and azimuthal angles between $-80^\circ < \phi < 80^\circ$	41
Figure 4.11	Location of space charge in ^{132}Sn	42
Figure 4.12	Beam path of the experiments	43
Figure 4.13	ΔV_x distribution for left-going and right-going tracks in the TPC for the	45
Figure 4.14	ΔV_{LR} as a function of the beam rate.	46

Figure 4.15 Space charge relation	47
Figure 4.16 Shift of tracks	48
Figure 4.19 A summary of all the effects modeled in the TPC MC simulation.	52
Figure 4.20 PRF response of Monte Carlo simulation of π^-	55
Figure 4.21 Standard pulse	56
Figure 4.22 Pole zero correction	57
Figure 4.23 Geant4 simulation of ^{108}Sn beam at 270 MeV/A in P10 gas. Notice the extent of the delta electrons in the vertical direction as compared to the horizontal extent.	58
Figure 4.24 Tagging the saturated pads.	59
Figure 4.25 Flow of embedding implementation in the software.	62
Figure 4.26 A 200 MeV/c π^- embedded into a nuclear collision type event. The embedded track identified by the software is highlighted by the solid green line.	62
Figure 4.27 A 200 MeV/c π^- embedded into a nuclear collision type event. The embedded track identified by the software is highlighted by the solid green line.	63
Figure 4.28 Comparison of MC to data.	65
Figure 4.29 Comparison of MC to data.	66
Figure 4.30 TBW	67
Figure 4.31	68

CHAPTER 1

EXPERIMENT

1.1 Energy loss in material

The average energy loss in a material can be described by the Bethe-Bloch equation,

$$\frac{dE}{dx} = \frac{4\pi N Z^2 e^4}{mc^2 \beta^2} \left(\ln \frac{2mc^2 \beta^2 \gamma^2}{I} - \beta^2 \right). \quad (1.1)$$

Where N is the number density of electrons in the medium, e the elementary charge, mc^2 is the rest mass of the electron, Z is the charge of the traversing particle, I is the mean excitation energy of the medium, and β is the velocity of the particle. There is a large variation in energy loss around this mean value, with a long high energy loss tail. A full description of the energy loss distribution can be described in CITE HERE.

1.2 Time Projection Chambers

1.3 Pad Response Function

Each electron avalanche produces an two-dimensional image charge on the pad plane, as shown in the cartoon in Fig. 1.1, where the projection of the charge distribution onto the x and z axis of this distribution are labeled as $\rho(x)$ and $\rho(z)$ respectively. If $\rho(x, z)$ represents the charge distribution on the pad-plane, the total charge observed on each pad, Q , is given as,

$$Q(x_o, z_o) = \int_{z_o - \frac{l}{2}}^{z_o + \frac{l}{2}} \int_{x_o - \frac{w}{2}}^{x_o + \frac{w}{2}} \rho(x, z) dx dz, \quad (1.2)$$

where x_o and z_o represent the x and z coordinates of the center of each pad, w is the width, and l is the length. This function is commonly referred to as the Pad Response Function (PRF). The total charge observed for this track is a superposition of PRFs of each avalanches on all the anode wires. It is the use of this PRF that allows for sub-millimeter accuracy in the position resolution

of the TPC [1]. Typically in a TPC, hits are grouped into clusters and it is practical to cluster in only one direction. The PRF can be expressed in a way that is independent of the location of the avalanche. If the true position of the avalanche is (x'_o, z'_o) , and the charge distribution can be written in a position independent way

$$Q(\lambda_x) = \int_{z_o - \frac{l}{2}}^{z_o + \frac{l}{2}} \int_{x_o - \frac{w}{2}}^{x_o + \frac{w}{2}} \rho(\lambda_x, \lambda_z) dx dz, \quad (1.3)$$

and the PRF for row clustering can be written as,

$$Q(\lambda_z) = \int_{z_o - \frac{l}{2}}^{z_o + \frac{l}{2}} \int_{x_o - \frac{w}{2}}^{x_o + \frac{w}{2}} \rho(\lambda_x, \lambda_z) dx dz. \quad (1.4)$$

The direction most perpendicular to the track's direction of travel provides the most accurate position resolution. Clustering in the S π RIT TPC is done for several pads containing charge in the direction most perpendicular to the track's direction of travel.

In this example the clustering direction would be along the x axis, as illustrated by the bolded pads. By choosing to cluster only in one direction, we have not included the charge in adjacent pads along the z axis resulting from the tails of $\rho(z)$. Therefore the charge not included in the bolded pads will be incorporated into adjacent clusters, introducing small correlations in charge between neighboring clusters.

Gatti [2] derived a semi-empirical formula for the charge distribution in a simple multi-wire TPC given as,

$$\begin{aligned} PRF_{\text{Gatti}}(\lambda) = & \frac{K_1}{K_2 \sqrt{K_3}} [\arctan(\sqrt{K_3} \tanh[K_2(\frac{\lambda}{h} + \frac{w}{2h})]) \\ & - \arctan(\sqrt{K_3} \tanh[K_2(\frac{\lambda}{h} - \frac{w}{2h})])] \end{aligned} \quad (1.5)$$

where w is the width of the pad, h is the distance of the anode plane to the pad plane, and λ is the distance of the pad center to the avalanche point. It is a single parameter equation where the two parameters $K_1 = \frac{K_2 \sqrt{K_3}}{4 \arctan(\sqrt{K_3})}$ and $K_2 = \frac{\pi}{2} \left(1 - \frac{\sqrt{K_3}}{2}\right)$ depend on the parameter K_3 , which is a function of the ratio of the anode wire diameter to the distance of the anode wires to the pad plane. K_3 can be looked up in a graph in [1] and [2].

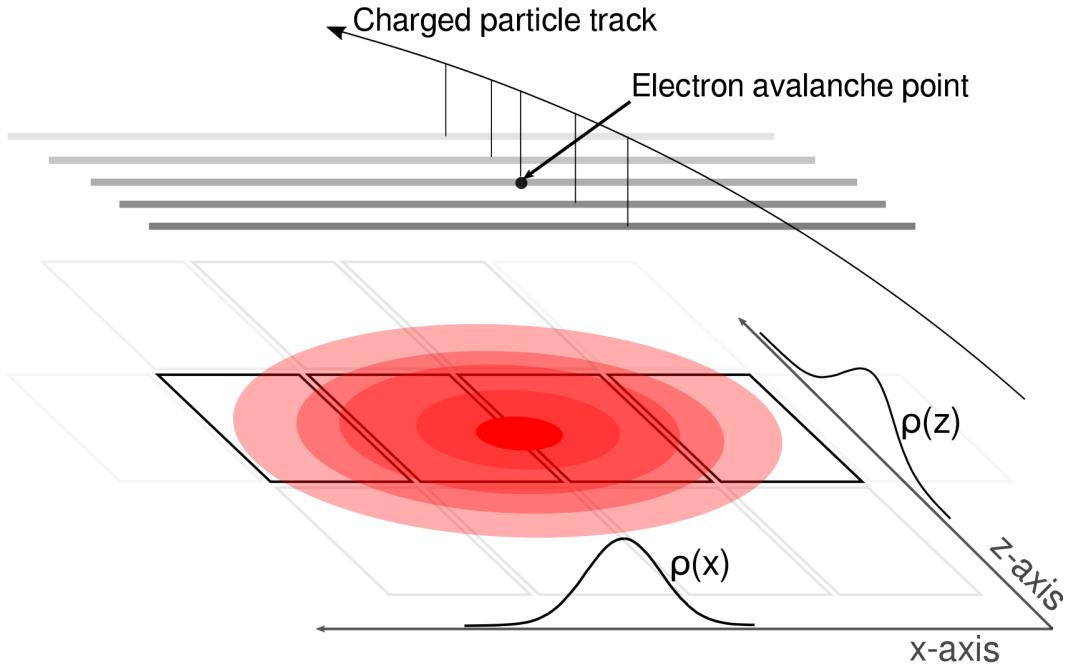


Figure 1.1: A cartoon illustration of the charge distribution resulting from an electron avalanche on one wire and the projections of the distribution onto the two axis $\rho(x)$ onto the x-axis and $\rho(z)$ onto the z-axis. The orientation of the wire planes is flipped upside down to display the perspective better.

1.3.1 Experimental Pad Response Function

The correlations we introduced by only clustering along one direction do not play a significant role in the particle identification, but cause deviations from the expected Gatti distribution. Also, analytic PRFs only exist for classical multi-wire TPCs. For these reasons it is useful to experimentally measure the PRF and fit it with an empirical function, typically a Gaussian, to describe its behavior.

As in Fig. 4.1, we postulate that the PRF is a function of the total charge deposited in a cluster $Q = \sum_i q_i$, and the difference in position of the center of the i^{th} pad, x_i , to the mean position $\bar{x} = \sum_i x_i q_i / Q$, defined as $\lambda_i = x_i - \bar{x}$. The PRF is simply defined as the charge fraction of each pad as a function of λ , as shown in Equation 1.6.

$$PRF(\lambda_i) = \frac{q_i(\lambda_i)}{Q} \quad (1.6)$$

Averaging over many events in the experimental data, the resulting PRF for the S π RIT TPC

is shown in Fig. 1.2. Here we see the deviations from the expected analytic Gatti distribution (black curve), whereas fitting with a two parameter Gaussian function (red curve) gives a better description of the data, Eq. 1.7, with the two parameters being the normalization coefficient, N_0 , width σ , and with a mean value assumed to be 0.

$$PRF_{\text{Gaus}}(\lambda) = N_0 e^{\frac{-\lambda^2}{2\sigma^2}} \quad (1.7)$$

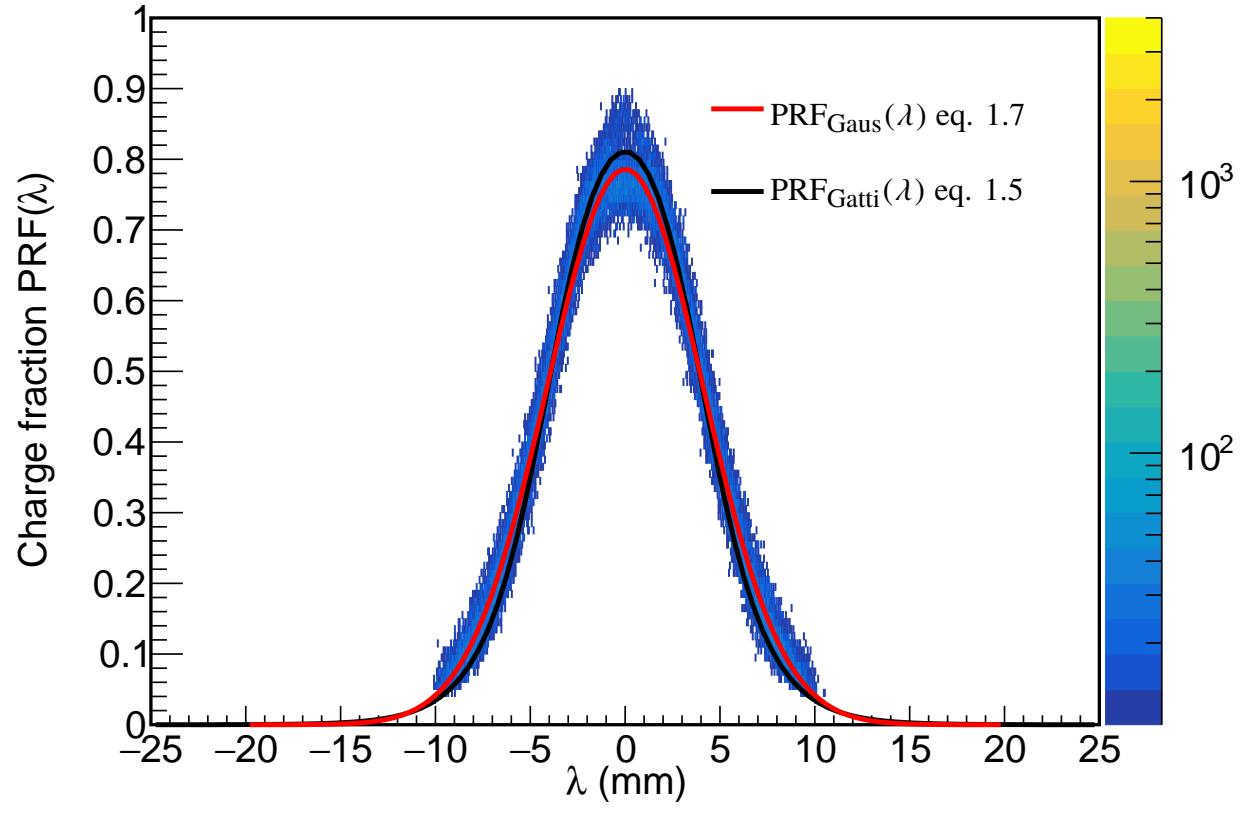


Figure 1.2: Experimental pad response function of many events for a crossing angle of $85^\circ < \theta \leq 90^\circ$.

The shape of the PRF depends on the crossing angle of the track [2]. Plotted in Fig. 1.3 is the PRF of π^- tracks vs. the crossing angle θ . The PRF gets wider starting from 90° and going to 45° ; if we did not switch clustering directions the PRF would become wider until it was a uniform distribution and there was no position resolution. Since we switch the clustering direction from x

to the z direction at 45° , the opposite trend is seen where the PRF becomes narrower as the position resolution gets better going from 45° to 0° .

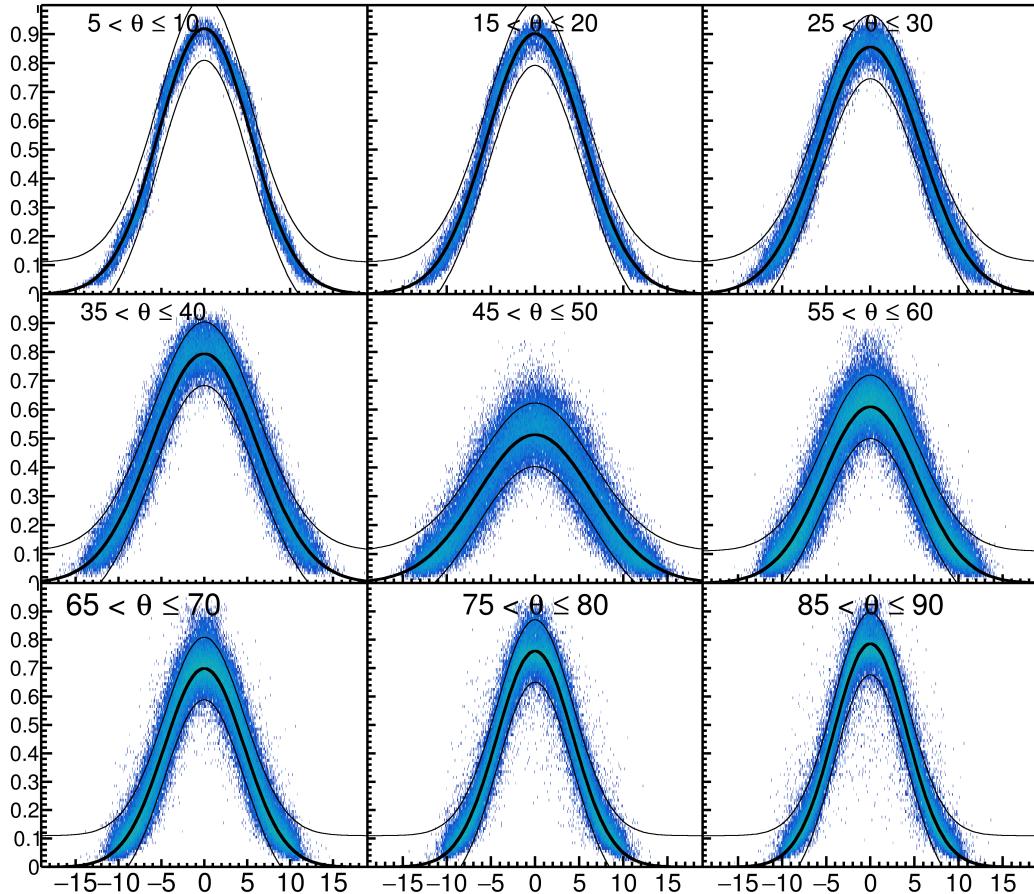


Figure 1.3: PRF response from π^- data.

Fits were performed to the experimental data with 5° width bins from $0^\circ < \theta \leq 90^\circ$. The two parameters of the Gaussian fits are plotted versus θ in Fig. 1.4; a 4^{th} order polynomial fit between these points allowed for interpolating between θ .

1.4 S π RIT TPC Overview

The Samurai Pion-Reconstruction and Ion Tracker Time Projection Chamber (S π RI TPC) is a Multi-Wire Proportional Counter developed to measure pions and other light charge particles

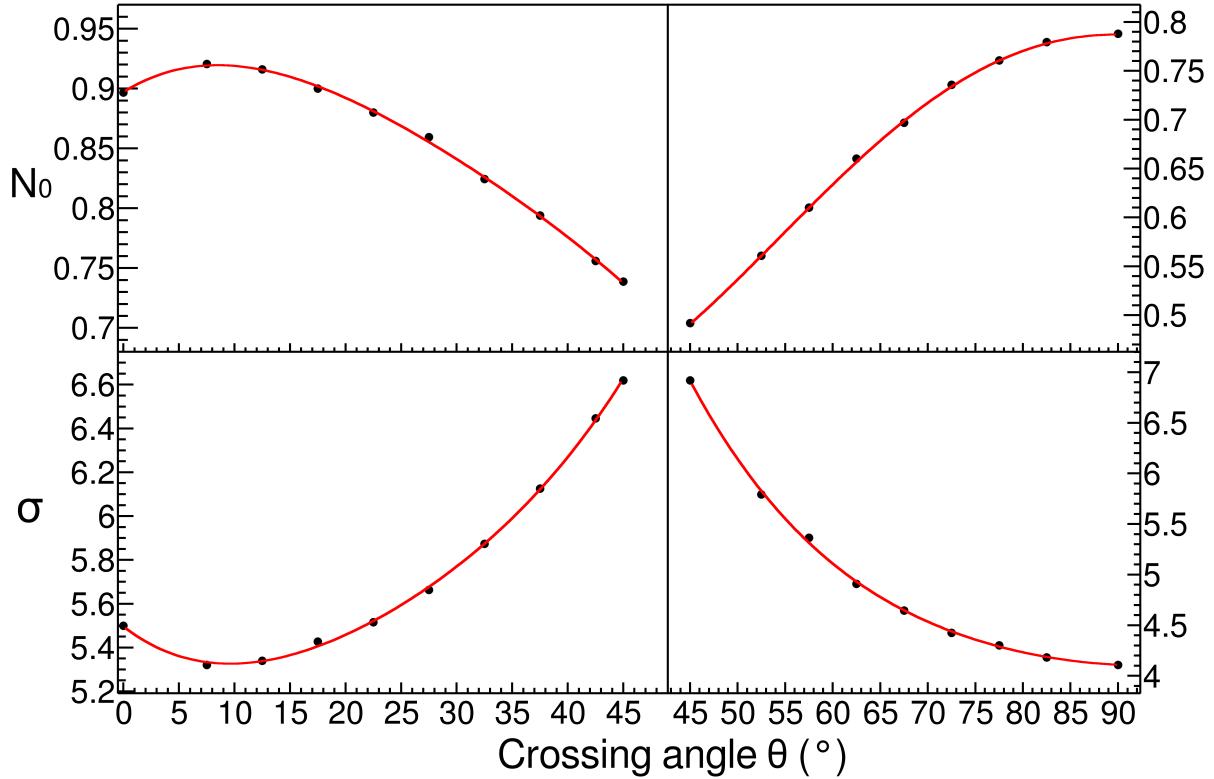


Figure 1.4: Parameters N_0 and σ as a function of the crossing angle θ with the 4^{th} order polynomial fits.

resulting from radioactive heavy ion collisions in a fixed target experiments. The TPC is enclosed in a thin aluminum sheet walls all around in order to minimize neutron scattering and to allow for light charged particles to reach the arrays of scintillating bars detectors on the sides and downstream of the TPC. The S π RI TPC was developed to fit inside the Samurai dipole magnet used at the Rare Isotope Beam Factory (RIBF) at RIKEN in Wako-shi, Japan [3]; the dipole gap limited the vertical space of the TPC. More detail and specifications of the Samurai dipole magnet are given in [4].

A target ladder allowed for up to 5 fixed targets to be mounted. A ACME worm gear allowed for the x-axis motion for changing the targets during the experiment, without needing to open or move the TPC. The motion of this worm gear was translated through the target motion feed-through by several brass gears and non-magnetic gear boxes. The motion of the target ladder could be controlled by hand or by operation of the drill. The targets were mounted on stand-offs on the target

S π RIT TPC Overview	
Pad plane area	1.3 m x .9 m
Pad size	1.2 cm x .8 cm
Number of pads	12096 (112 x 108)
Gas composition	90% Ar + 10% CH ₄
Multiplicity limit	200
dE/dx range	Z=1-8, π , p,d,t,He,Li-O
Drift length	50 cm

Table 1.1: An overview of the properties of the S π RIT TPC

ladder and also had z-axis motion. This allowed for the targets to be positioned as close as possible to the thin window of the field cage, maximizing the geometric acceptance.

The electronics were mounted to the aluminum top plate. Several aluminum ribs were mounted to the top of the plate to bring structural rigidity. A flatness within 150 μ m was achieved across the whole top plate as measured by a laser position system. The charge sensitive pads of the pad plane were etched into several circuit boards were recessed and glued to the bottom portion of the top plate. Vias through the pad plane circuit boards brought the signal traces from the pads to surface mount pads on the other side of the boards. Several holes cut through the top plate allowed for the interface cables of the electronics to be connected to these surface pads.

Just below the pad plane were a set of three wire planes; the gating grid, ground, and anode wire planes. The detailed function of these wires will be explained later but they served to separate the boundary between the drift volume and the avalanche volume.

The front and sides of the field cage were assembled from 8 independent rigid circuit boards. The downstream window served as the downstream wall of the field cage all though it was a large polycarbonate frame in which a removable kapton window could be installed. This thin window minimized the scattering of exiting neutrons and charged particles for downstream detectors.

The voltage step down takes the high voltage of the cathode and steps the voltage down through a set of copper rings and a resistor chain, minimizing the chance for sparking.

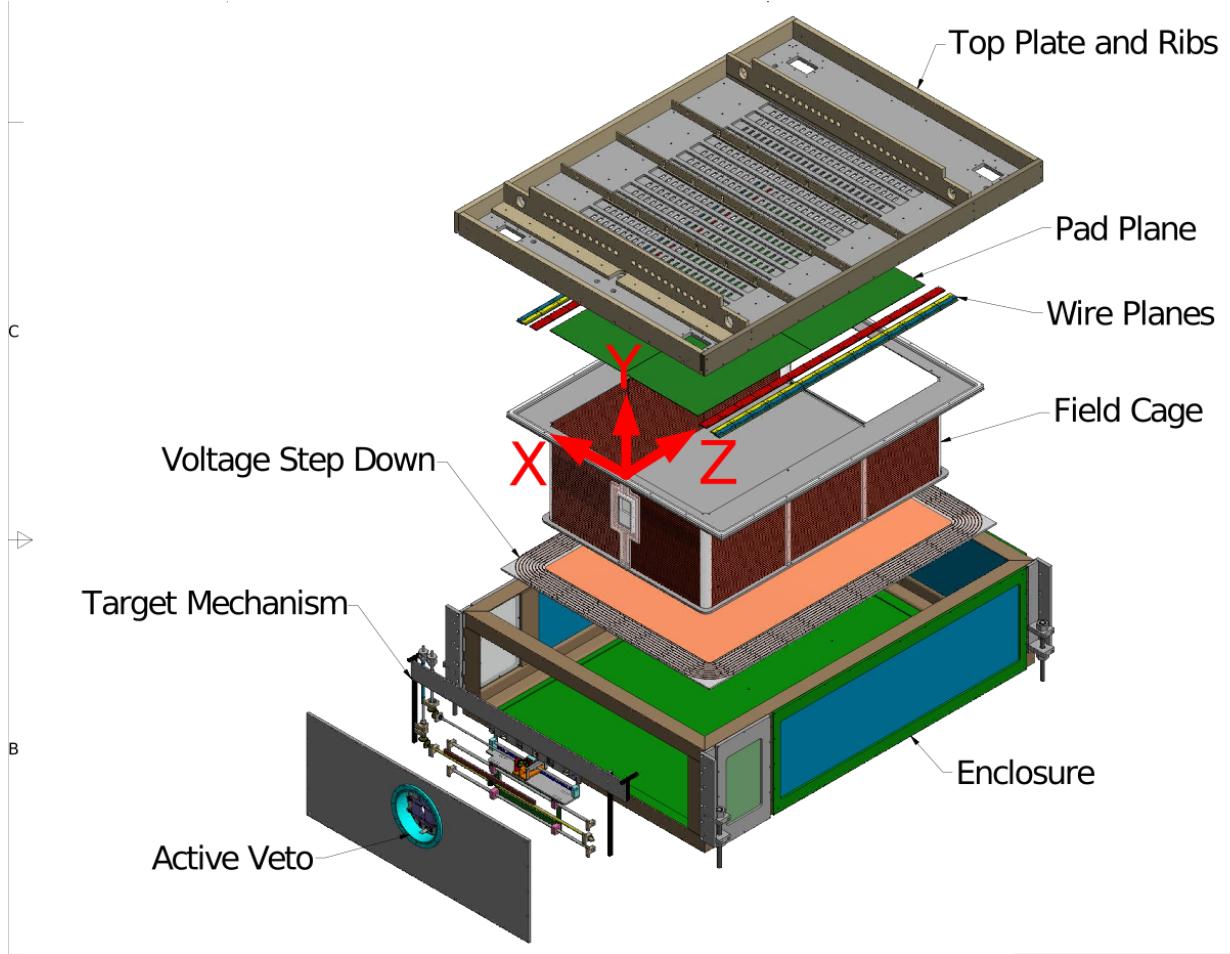


Figure 1.5: Overview of the S̳RIT TPC

1.4.1 Enclosure

The skeleton of the enclosure is composed of a rigid aluminum angle-iron frame. All walls are constructed of a aluminum frame with think sheet metal. All materials were made to be as thin to allow charged particles and neutrons to exit the TPC without scattering too much. This allows for a trigger to be created by placing detectors on the sides and downstream of the TPC. The enclosure itself is made to be gas tight with respects to the outside and the field cage. This is to allow for the possibility to run a different gas inside the enclosure than the field cage. Although, in this set of experiments we ran the same gas in the field cage and enclosure volume.

1.4.2 Voltage Step Down

The gap between the field cage's cathode and the ground of the enclosure is quite small. To prevent electric breakdown in the gas between this gap a series of concentric copper rings safely stepped down the voltage to ground; where each ring was separated by a resistor. There were 7 concentric rings with a $10\text{ M}\Omega$ resistors in between, creating a resistor chain which steps down the voltage each ring by approximately 1000 V.

1.4.3 Field Cage

ADD info how to calculate cathode voltage from HW supply.

The field cage holds the detector gas and sets up a uniform electric field in which electrons can drift upwards toward the anode wires. It was designed to hang from the top plate and therefore needed to be of a lightweight construction. Also the materials needed to be thin to allow for light charged particle and neutrons to pass through without significant scattering for ancillary detectors. Therefore instead of a downstream wall, a large thin exit window was constructed. The cathode was constructed of an aluminum honeycomb laminate. Two sheets of ??? aluminum were bonded to a core of aluminum honeycomb structure providing a lightweight yet rigid structure for the cathode.

The field cage was constructed from several panels of printed circuit boards (PCBs). The epoxy in the common PCB substrate FR4 contains bromine which is not suitable for the long term operation of a TPC, as the bromine will eventually cause gain reduction of the wires [CITE]. The halogen free material chosen was Cryogenic-G10. We built the TPC with the option to run explosive gases such hydrogen, thus we decided to have field cage an isolated volume from the rest of the TPC enclosure. While the risk of a high voltage spark was minimized using the voltage step down, the risk of sparking when using an explosive gas could be further minimized by isolating the detector volume from the enclosure volume thereby allowing you to run an insulating gas between the field cage while running the explosive gas inside the detector volume only.

The front of the field cage was made of two PCBs and each side was constructed of three PCBs.

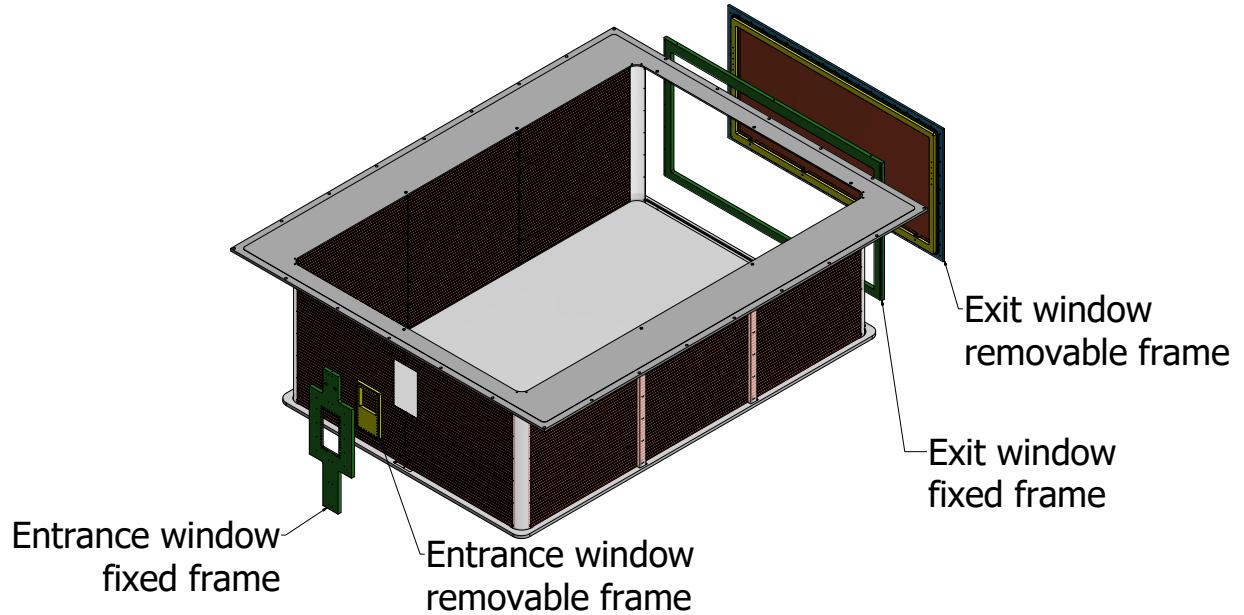


Figure 1.6: FC overview

The exit window was a $10\mu\text{m}$ thick Kapton window with evaporated aluminum strips on the inside and outside; mounted on a polycarbonate frame.

$$V_n = V_{cath} \frac{R_p + (50 - n)R}{49 \cdot R + R_p} \quad (1.8)$$

$$R_p = 49 \cdot R \left(\frac{\frac{y_{g.g.} - y_{cath}}{y_{TP} - y_{cath}} \frac{V_{cath} - V_{gg}}{V_{cath}}}{} - 1 \right) \quad (1.9)$$

1.4.4 Voltage Step Down

Figure ?? shows a cartoon drawing of the electrode geometry of the field cage walls. The basic idea of the field cage is to set up a constant electric field in the field cage volume to allow for a constant drift, in the presence of gas, for electrons. To accomplish this the field cage is composed

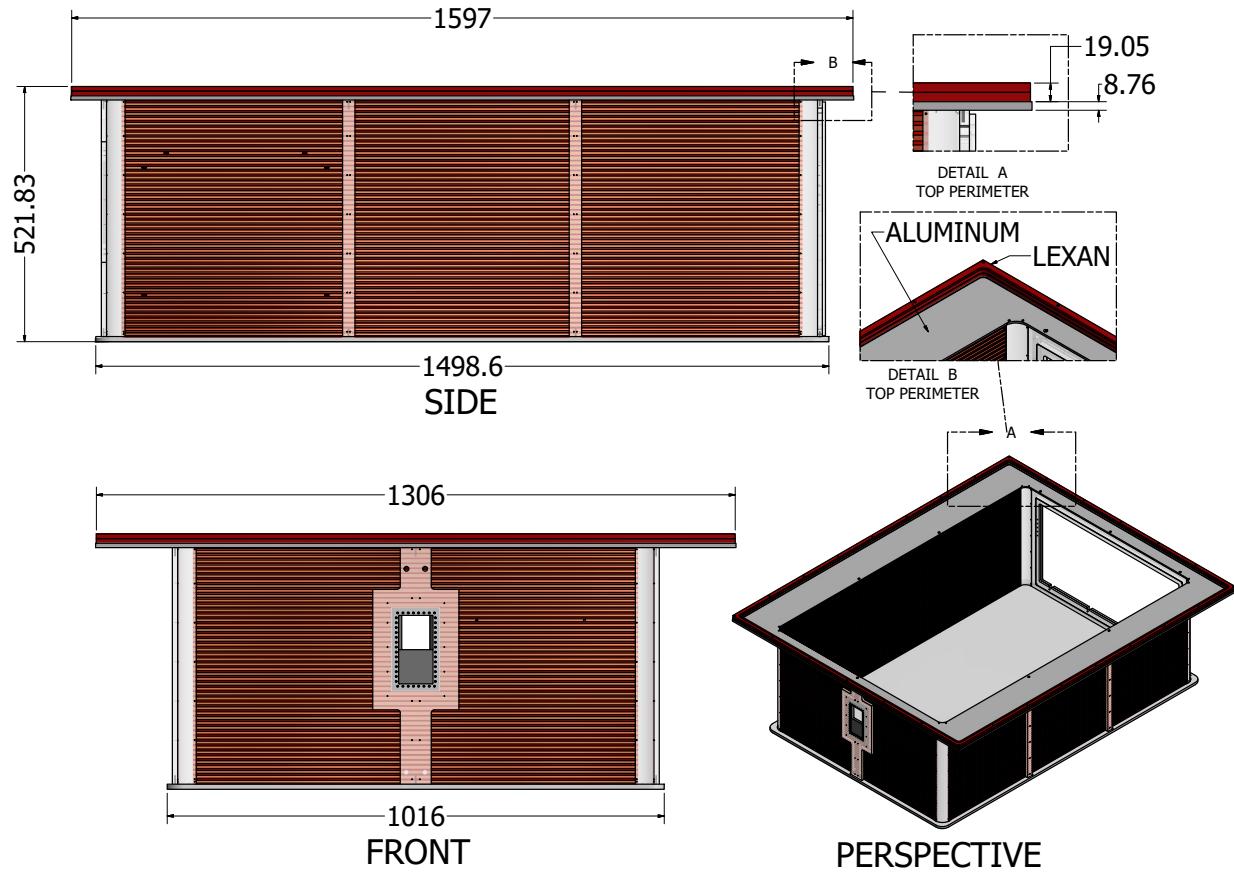


Figure 1.7: FC overview 2

of a set of copper strips which are set at a defined voltage by a resistor chain for a fixed distance between strips; setting up a constant electric field.

The cathode itself is connected to the HV supply through a $10\text{ M}\Omega$ resistor and has an effective capacitance to ground of 4 nF , C_{VSD} . The field cage is made of 50 inside copper strips and 49 outside copper strips; the strip thickness is exaggerated in the figure to show the detail. The first inside strip is connected to the cathode which is connected by an effective $5\text{ M}\Omega$ resistor, R , to the next inside strip and the first outside strip. The resistor chain creates a voltage divider in which each strip is separated by a constant difference voltage at a fixed distance setting up a constant electric field. The last strip of the field cage is composed of partially a small inner strip on the PCB board and the aluminum top perimeter piece which holds the field cage together with the top plate of the

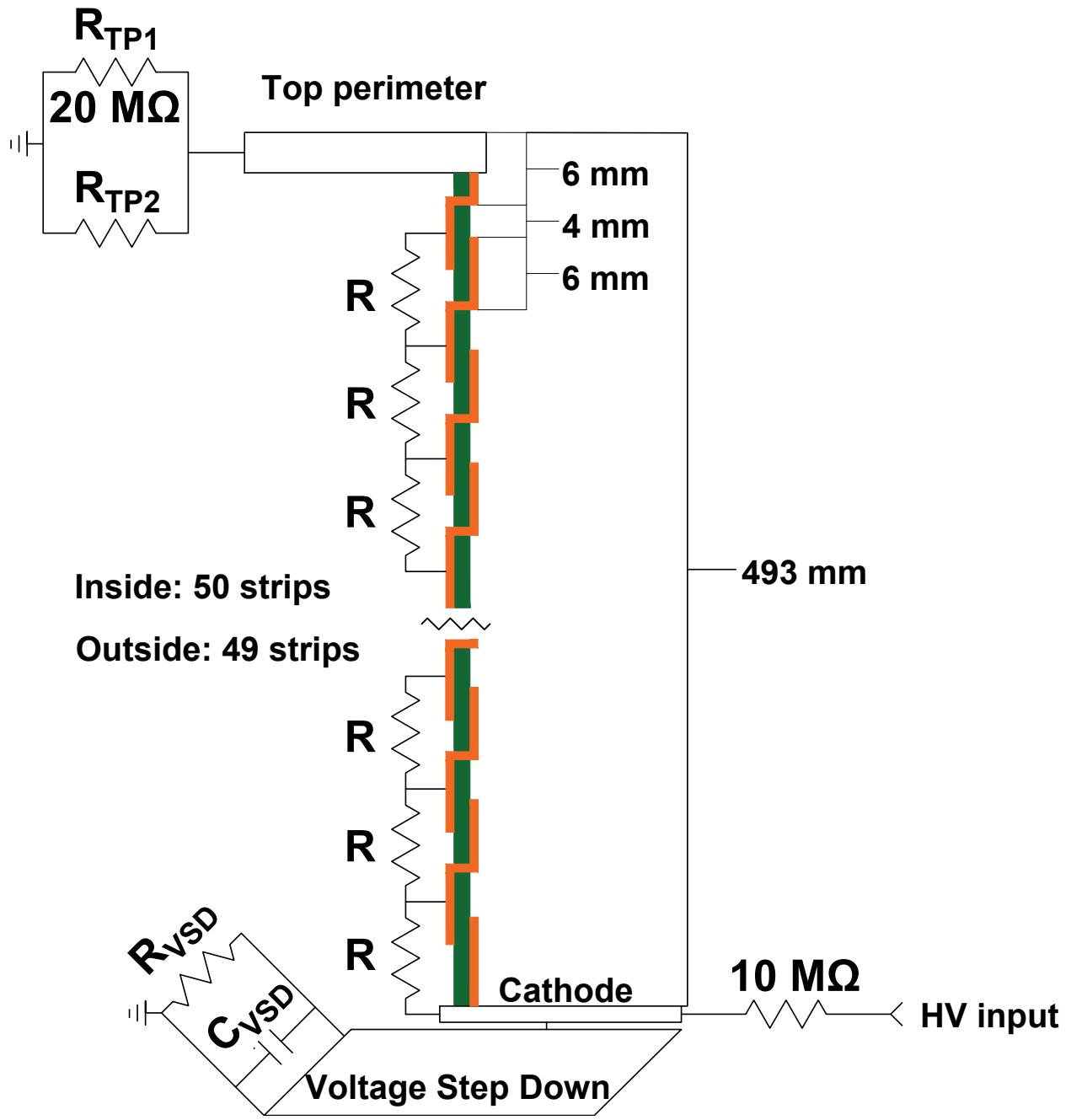


Figure 1.8: Schematic of the electric connections relevant to the Field Cage system.

TPC. Together their thickness is equal to the 6 mm strip width of the other strips. The top perimeter is connected to electrical ground through a $20 \text{ M}\Omega$ resistor with the option to place an additional resistor in parallel to tune the voltage of the top perimeter.

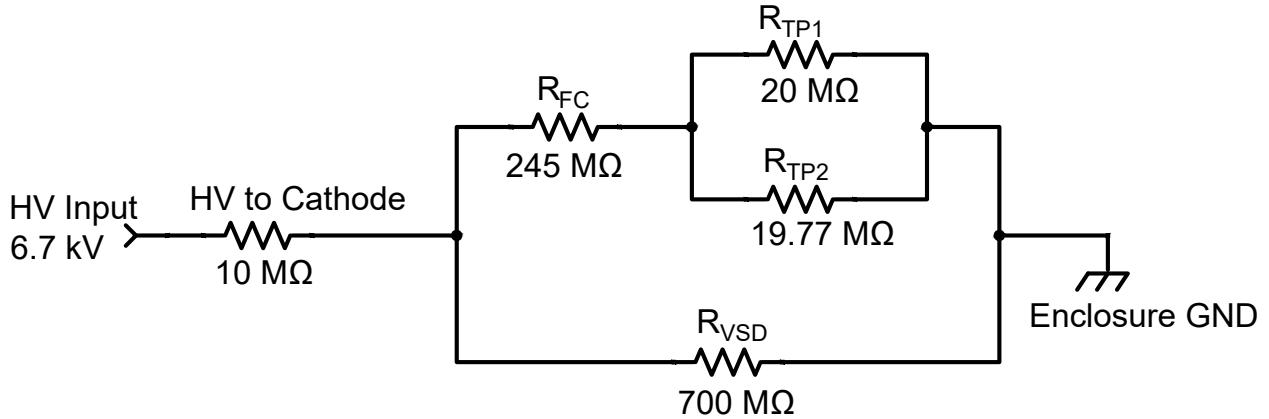


Figure 1.9: Schematic of the TPC system

GET electronics settings

Plane	Material	Diameter μm	Pitch mm	Distance to pad-plane	Tension N	Voltage V
Anode	Au-plated W	20	4		4	0.5
Ground	BeCu	75	1		8	1.2
Gating	BeCu	75	1		14	1.2

Table 1.2: Wire plane properties

1.4.5 Pad Plane

The pad-plane is a multi-layer circuit board which is segmented into 11.5 mm x 7.5 mm charge sensitive pads; arranged in an array of 108 x 112 pads in the x and z-directions respectively making 12096 pads in total. There is an insulating gap of 0.5 mm on each side separating the pads. The effective area covered by the pads is 1344 mm x 864 mm. There is a via and trace coming from each pad to the opposite side of the pad plane and is arranged in a surface pads which may be readout by a surface mount SAMTEC connector CITE HERE. Add figure of close up of pad plane

1.4.6 Wire Planes

There are three wire planes that sit underneath the pad-plane. The wire plane closest to the pad-plane (4 mm), is the anode wire. The next plane (12 mm), is the ground plane or frisch grid, and the last plane (14 mm), is the gating grid. The gating grid is the first plane that electrons meet as

they drift upward towards the anode plane. The gating grid is operated as a gate either allowing electrons and ions through or blocking them entirely. The ground plane shields the inside volume of the TPC from the high voltages of the anode wires where the avalanche process of the electron takes place.

The ground plane is the least interesting plane and is shorted to the enclosure ground by a BNC terminator on the outside of the TPC. If we would like to calibrate the electronics of the TPC we typically inject a pulser into one end of the ground plane and terminate the other end with a 50Ω termination.

In the open configuration the gating grid is transparent to electrons coming from the TPC volume and also allows for ions to move from the avalanche region into the TPC volume. It functions as the gate of the TPC where we only open the gating grid when an event meets the selection trigger criteria; minimizing the excessive exposure to the un-reacted beams which would quickly build up enormous amounts of space charge. We close the TPC after reading out approximately one TPC volume – about $10\mu\text{s}$ – of space to prevent the back-flow of ions from the avalanche region of that event. Since ions move with a velocity much slower than that of electrons, the ions only move several μm in the time the gate is open; this allows for electrons to pass through while preventing the back-flow of ions into the FC volume. Figure 1.11 shows a Garfield simulation of the gating grid in both the on and off configurations. In the on configuration, all the wires share the same average voltage, $V_{g.g.}$, which is optimized for the case of 100% electron transparency. In the off configuration the reference voltage $V_{g.g.}$ remains the same, but alternating wires get an offset voltage of $\pm\Delta V$, so that the electric field between wires is great enough to block incoming electrons; opening the grid from this closed bi-polar mode is simply done by removing the offset voltage and allowing the two wires to connect and equilibrate their charges back to the reference voltage.

The anode wires are typically biased to 10^3 V and are very thin, about $20\mu\text{m}$ in diameter. This creates a very high electric field very close to the anode wire in which the electron gains significant kinetic energy producing electrons until it terminates on the anode wire. The amount of electrons it produces depends on the anode wire voltage and the gas properties. The absolute gas gain was

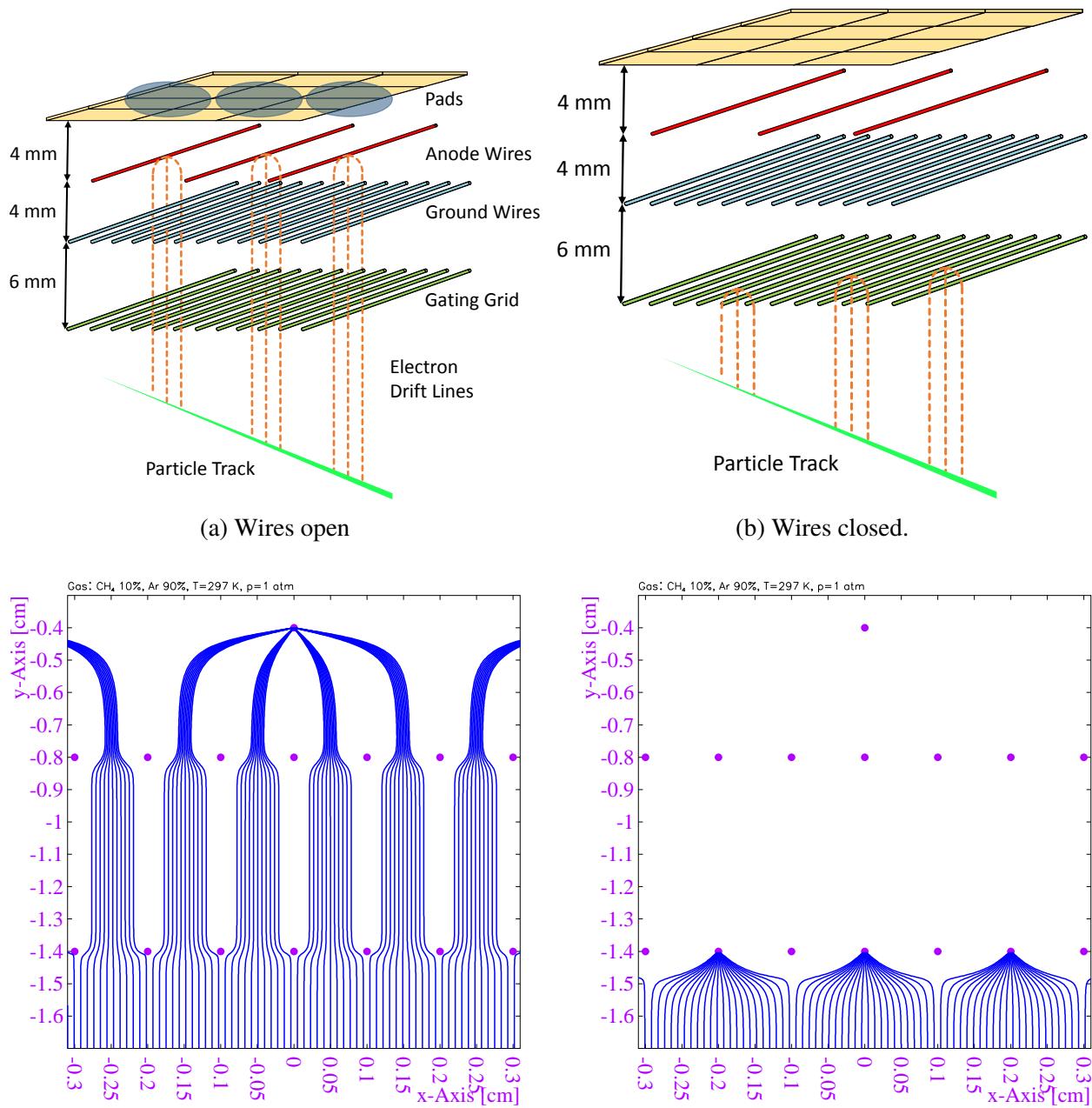


Figure 1.11: On and off configurations of the gating grid.

not experimentally measured but was simulated by a Garfield simulation. During the experiment the anode wires were biased to two different voltages. We will refer to the voltage 1460 V as the “high voltage” and 1214 V as the “low voltage”. Only two sections were biased with the lower voltage setting due to concerns of a high current issue. Figure 1.12 shows the expected number of electrons distributions for electrons produced in a avalanche process of an electron creating a

single avalanche. The distribution follows a Polya distribution as expected and the MC data in the simulation was fit with a Polya function [1].

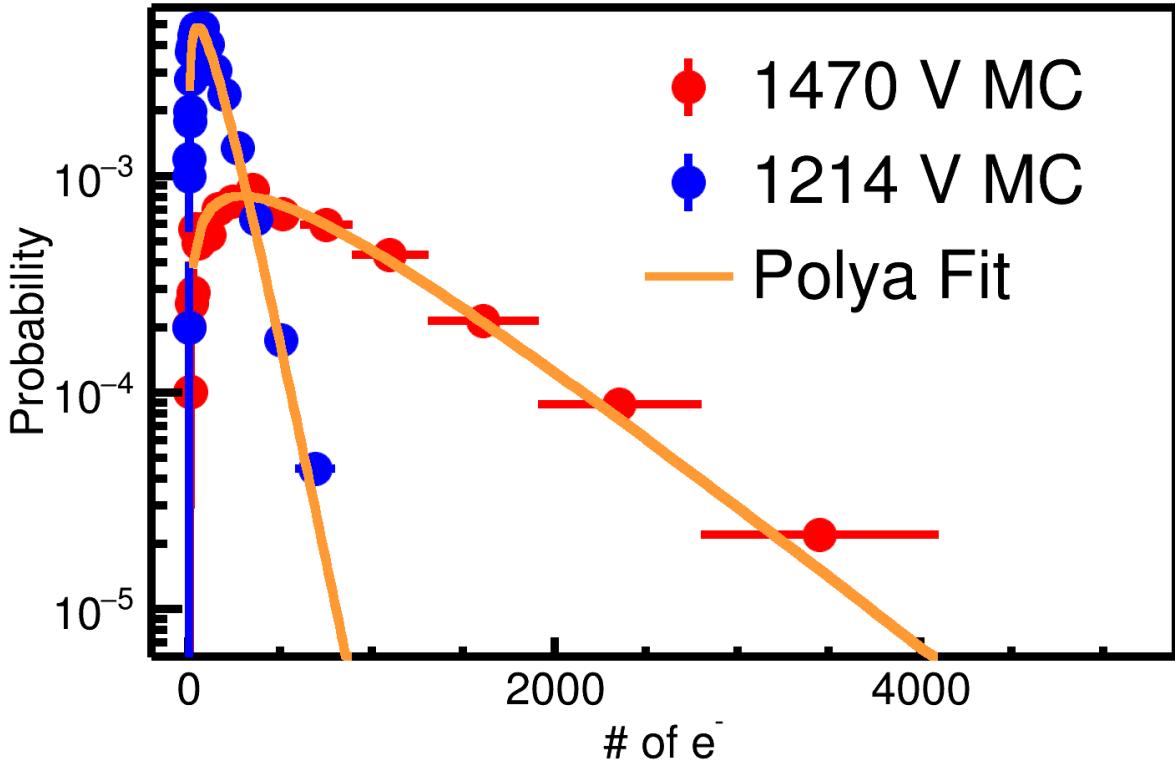


Figure 1.12: Number of electrons produced in a single avalanche on an anode wire. Two different voltages were simulated using Garfield++ at 1470 V and 1214 V. The expected Polya distribution fit is also given in yellow.

1.4.7 Electronics

Signals in the S π RIT TPC are amplified and digitized by the recently developed Generic Electronics for TPCs (GET) [5]. Short cables transmit the signals from the pads to the inputs of the AGET chips. Each AGET chip services 64 pads (63 pads are connected in our case), contains a pre-amplifier, and a Switched Capacitor Array (SCA), with a maximum of 512 time buckets with an adjustable sampling frequency of 1 to 100 MHz. Four AGET chips are mounted on one AsAd (ASIC and ADC) motherboard. The gain of each AGET can be configured as 0.12, 0.24, 1.0, or 10 pC over the whole dynamic range, and the ADCs on each AsAd board provides 12 bit resolution. The peaking

GET electronics settings	
ADC bit range	14 bits
Sampling frequency	1-100 MHz
Dynamic range	.12, .24, 1.0, 10pC
Peaking time	69,117,232,501,720,1014 ns
Time bucket range	512

Table 1.3: Summary of range of GET electronics settings.

times of the shaping amplifiers can be set to 69, 117, 232, 501, 720, or 1014 ns. In this experiment, the gain was set to the highest setting, 0.12 pC, the peaking time 117 ns, and the sampling frequency 25 MHz (resulting in 40 ns time buckets). The Aget 2.0, asad 2.1, and cobo 1.0 firmware versions were used. The variations in the electronics were calibrated by measuring the response of each channel to a injected reference pulse, covering the full dynamic range of each channel.

1.4.8 Considerations when constructing a TPC

Several considerations went into the construction of the S π RI TPC which I wish to summarize and document here. All materials and glues of the TPC were selected as low out-gassing materials. Several materials (that are common place in nuclear labs), such as vacuum grease, viton o-rings, all out-gas organic chemicals into the counter gas which damage the TPC by permanently lowering the gain over time. The organic molecules responsible are difficult to identify exactly, but lists of good and bad materials are well known in the literature from experiments. If a material we wished to use was not on these lists we placed the material in a clean chamber with the counter gas and flowed this counter gas through a small proportional counter making sure the gain did not drop at high collection rates when exposed to a high rate alpha Americium source.

Sparking Two volumes of gas.

1.4.9 Gas Properties

The gas used inside of the field cage was a mixture of 90% Ar and 10% Methane (CH_4) by volume –so called P10– gas, operated just under atmospheric pressure (1 atm). The gas was continually flowed through the field cage and exited into the enclosure volume, finally passing through a bubbler to atmosphere. The gas purity was monitored with an oxygen and water monitor which are the two most concerning contaminants. The water never exceed ??? ppm and the oxygen level never exceeded ??? ppm. Figure 1.13 shows the drift velocity of P10 gas at 1 atm as a function of electric field value in V cm^{-1} . Operating near the peak value of the drift velocity curve minimizes the change in the drift velocity as the effective field slightly changes due to slight variations in the pressure. The electric field in the experiment was 125 V cm^{-1} at 760 Torr, giving a reduced electric field $0.17 \text{ V cm}^{-1} \text{ Torr}^{-1}$.

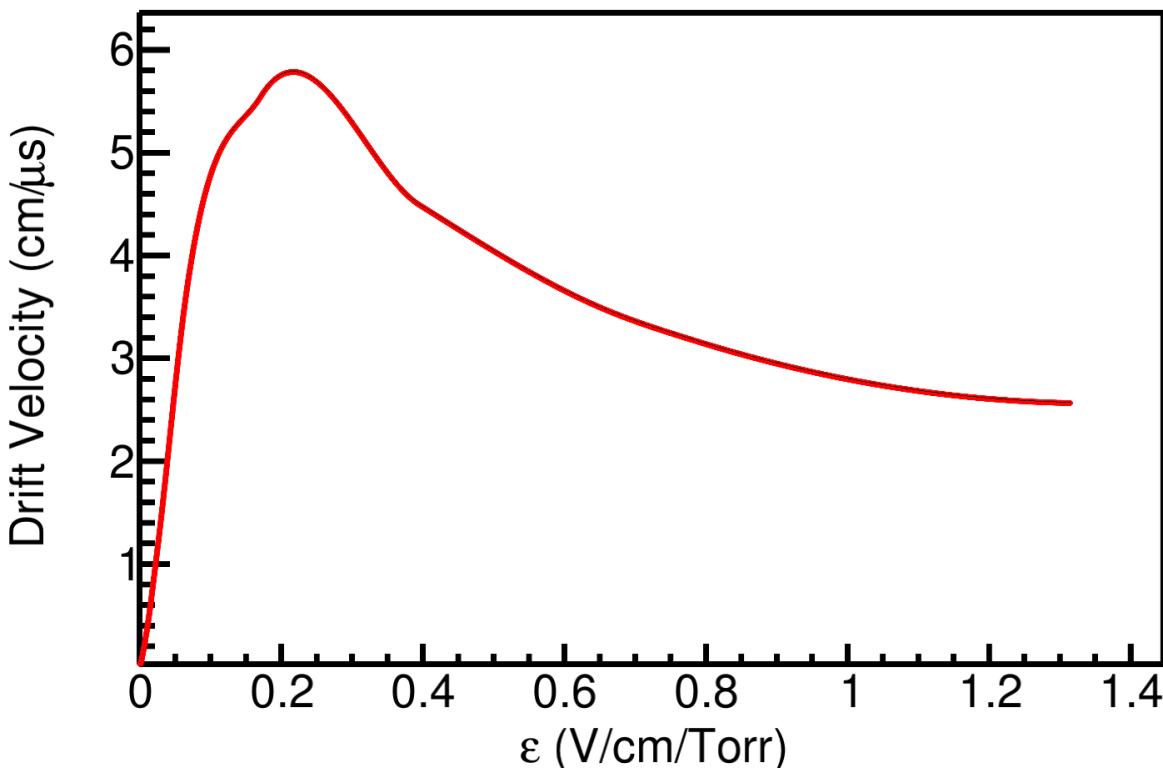


Figure 1.13: Drift velocity of electrons in P10 gas.

The general formula for the drift velocity, $d\vec{x}/dt$, of an electron in the presence of electric and

magnetic fields, \vec{E} and \vec{B} , can be expressed in the Langevin equation as,

$$\frac{d\vec{x}}{dt} = \frac{\mu}{1 + (\omega\tau)^2} \left(\vec{E} + \omega\tau \frac{\vec{E} \times \vec{B}}{|\vec{B}|} + \omega^2 \tau^2 \frac{\vec{E} \cdot \vec{B}}{|\vec{B}|^2} \vec{B} \right), \quad (1.10)$$

where μ is the signed drift velocity, ω is the cyclotron frequency, and τ is the collision parameter for a particular gas [1].

Several properties of the gas were also simulated in Garfield such as the longitudinal and transverse diffusion, σ_t and σ_l respectively, and the electron and ion drift velocities, v_d and v_i respectively for the experimental electric field of 125 V cm^{-1} ; summarized in Table 1.4.

Gas properties	σ_t (cm $^{-1/2}$)	σ_l (cm $^{-1/2}$)	v_d (cm μs^{-1})	v_i (cm μs^{-1})	G_h	G_l
	0.024	0.034	5.43	2.05×10^{-4}	903	150

Table 1.4

1.5 Ancillary Detectors

1.5.1 Kyoto Multiplicity Trigger

The Kyoto Multiplicity Array consists of two arrays of plastic scintillating bars on each side of the TPC, each consisting of 30 bars. The entire TPC structure was designed so that light charged particles could easily pass through the field cage and side walls of the TPC enclosure. In this way the number of tracks passing through the sides of the TPC could be measured by this array. In heavy ion collisions the more central a nuclear collision is, the more nucleons participate in the collision, resulting in more measured tracks. It is this correlation between the number of tracks and centrality of the collision that makes the Kyoto Array sensitive to the centrality of events. It is more likely that in very central collisions more tracks are going to the peripheral angles and measured by the Kyoto array. In the experiment the trigger selection criteria was $n_{Kyoto} > 4$, where n_{Kyoto} is the total number of tracks measured by both arrays.

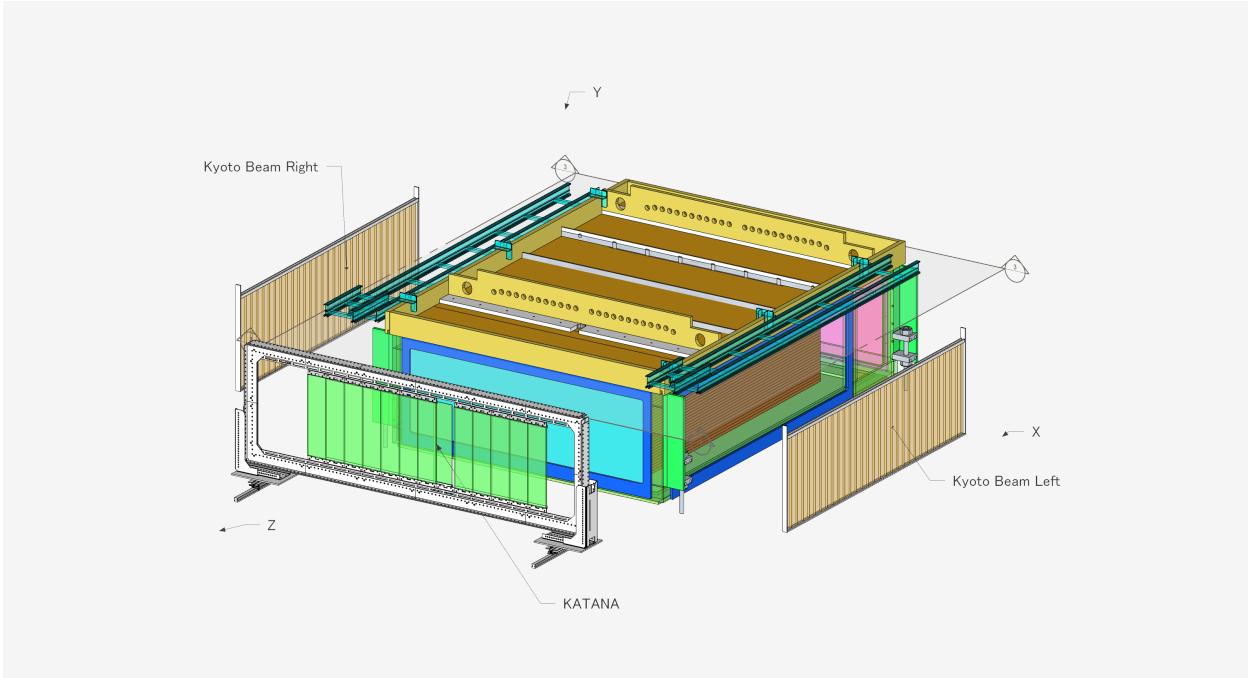


Figure 1.14: Exploded views of Kyoto and KATANA arrays.

1.5.2 Krakow KATANA Veto and Multiplicity Array

The Krakow KATANA array consists of 12 plastic scintillating bars mounted to the downstream wall of the TPC enclosure. Three of the 12 bars were thin and operated as a beam veto in the event the beam did not make a nuclear collision with the target; this was a majority of the time. The 9 other bars operated as an additional multiplicity array similar to the Kyoto array. Since most of the particles are focus forward in a cone in the laboratory frame, it was found the condition on the Kyoto array was sufficient to trigger on central events; thus the KATANA array was used in primarily the beam veto mode. This was accomplished by positioning the array so that the expected position of the beam exiting the TPC would be centered on the three thin paddles. The threshold of the veto paddles were set so that the charge of a particle, Z , was $Z > 20$. This allowed the selection of very central events and we did not trigger on very peripheral or no collision events.

1.5.3 Active Veto Array

The beam was tuned by two sets of quadropole magnets, STQ 1 and STQ2, so that the beam spot was focused on the TPC target location. Because of the inherent angular dispersion of the beam there were incoming beam events which significantly deviated from the target location. To veto these type of events an active veto array was set at the entrance of the TPC consisting of four small scintillating bars arranged to be slightly larger than the target size. The threshold was set so that any beam particle which passed through any of the bars it would send a trigger signal to not trigger the system since the beam path would not be on target but on some other material inside the TPC.

1.6 Radio Isotope Beam Factory (RIBF) Facility

The primary and secondary beams were produced at the Radioactive Isotope Beam Factory (RIFB) facility at RIKEN, in Wako-shi, Japan. The RIBF facility starts with two primary beam types, ^{132}Xe and ^{238}U , which produced by an ion-source and accelerated to progressively higher kinetic energies by 1 linear accelerator (RILAC), and 4 different cyclotrons (RRC, fRC, IRC, and SRC), reaching a primary beam energy of 345 MeVA.

After the SCR, the primary beams impinge on a rotating 3 mm Be target which produces many different species by fragmentation. These fragments are then separated by the BigRIPS spectrometer which is tuned to the particular secondary fragment of interest. This is accomplished through several dipole magnets, slits, and wedge degraders. The resulting secondary beam is not pure and the purity depends on the primary beam and target beam desired.

In these set of experiments several beams were produced with varying intensities and purities. Table 1.5 summarizes the average qualities of the 4 secondary beams produced in the two experimental campaigns.

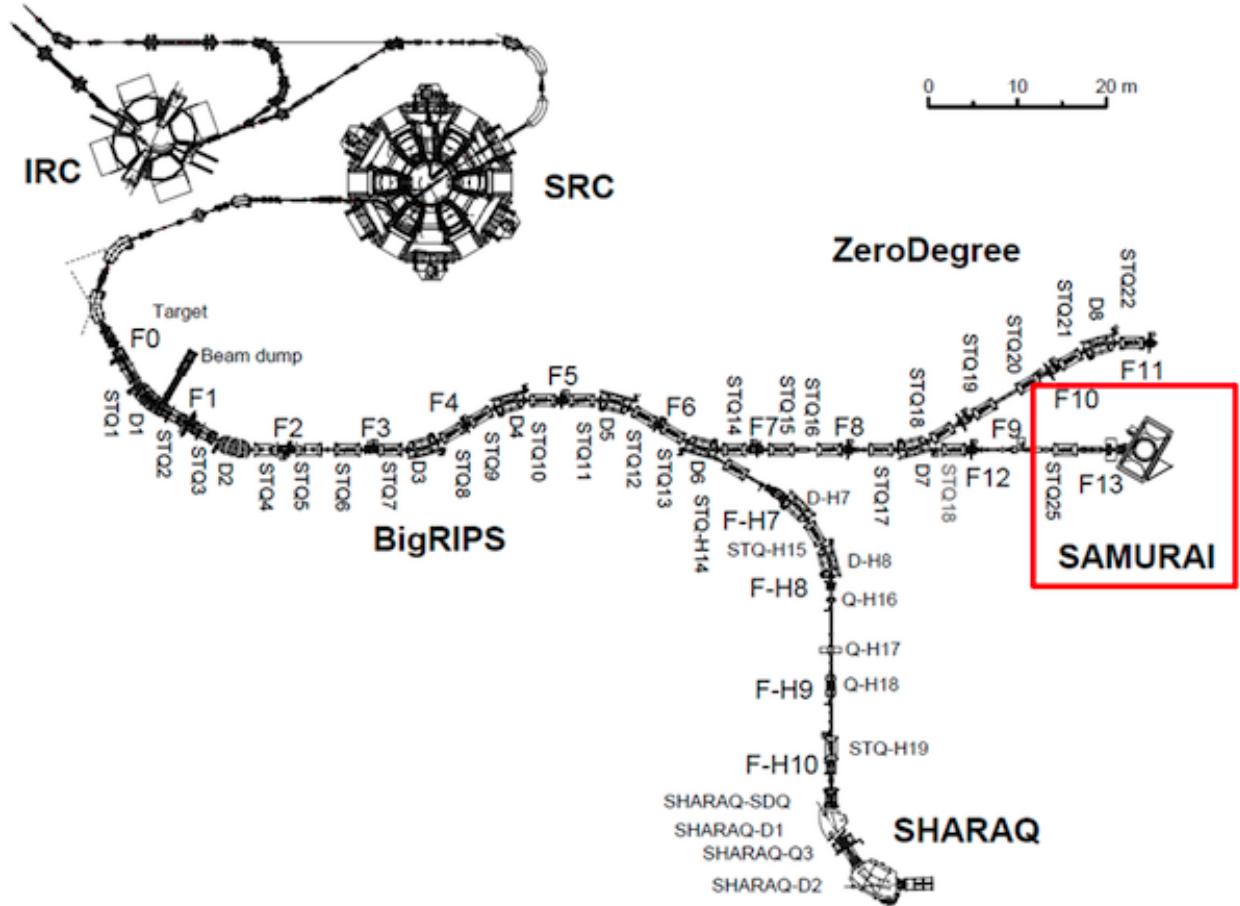


Figure 1.15: Overview of the RIBF, BigRIPS, and SAMURAI beamline.

1.7 Experimental Setup

The S π RIT TPC was designed to fit exactly into the dipole gap of the dipole magnet at the end of the BigRIPS beam line. Figure 1.16 shows a drawing of the S π RIT TPC inside of the SAMURAI magnet chamber which was rotated to the 0° configuration. Typically the SAMURAI (Superconducting Analyzer for Multi-particles from Radioisotope beams) is operated under vacuum as a large-acceptance multi-particle spectrometer for radioactive-beam experiments. This magnet can reach magnetic fields up to 3 T at the center of the pole gap. The space between the magnetic pole faces is further complicated by large bolts which protrude from the pole faces. These bolts secure the vacuum chamber to the magnet which is not practically removable; though the inside of the magnet was not operated under vacuum. This required an extensive rail system and support

Primary Beam	Secondary Beam	Energy at mid target MeVA	Intensity kHz	Purity (%)
^{238}U	^{132}Sn	269.2	9.5	54
^{238}U	^{124}Sn	270.3	9.1	10
^{124}Xe	^{112}Sn	270.4	7.6	48
^{124}Xe	^{108}Sn	269.3	7.5	52

Table 1.5: Primary and secondary beam properties produced in the S π RIT TPC experimental campaigns.

frame to slowly slide in the TPC over the bolts, finally raising the TPC several cm to the final height.

The height of the TPC was roughly aligned with a self-leveling laser system to match the center of target with the center of the beam line. Once the TPC was adjusted to the final location, the position of the TPC was measured in fine detail with a photogrammetry system CITE HERE. Small highly reflective targets were placed all over the TPC both inside and out and pictures were taken with a calibrated lens and camera system. Using the commercial software provided the set of different camera perspectives reconstruct a point cloud of all the targets into 3-dimensional coordinates. Since the magnet was also measured with the same system after installation, we can match the two systems to get the absolute position of the TPC – and several of its internal components– relative to the magnet frame. The position resolution of this type of system was estimated to be around 200 μm for each coordinate, which is much more precise than needed CITE HERE or Show data.

Maybe put a position table summary here of the TPC position and definition of the coordinates system in the TPC frame and the Magnet frame

1.8 Data Acquisition (DAQ)

The Data AcQuisition (DAQ) consisted of three different systems. The RIBFDAQ system served as the master DAQ for the BigRIPS beam identificaiton DAQ, the TPC DAQ, the NeuLAND neutron wall DAQ, and the Kyoto Array DAQ systems. The TPC DAQ was handled by the NARVAL

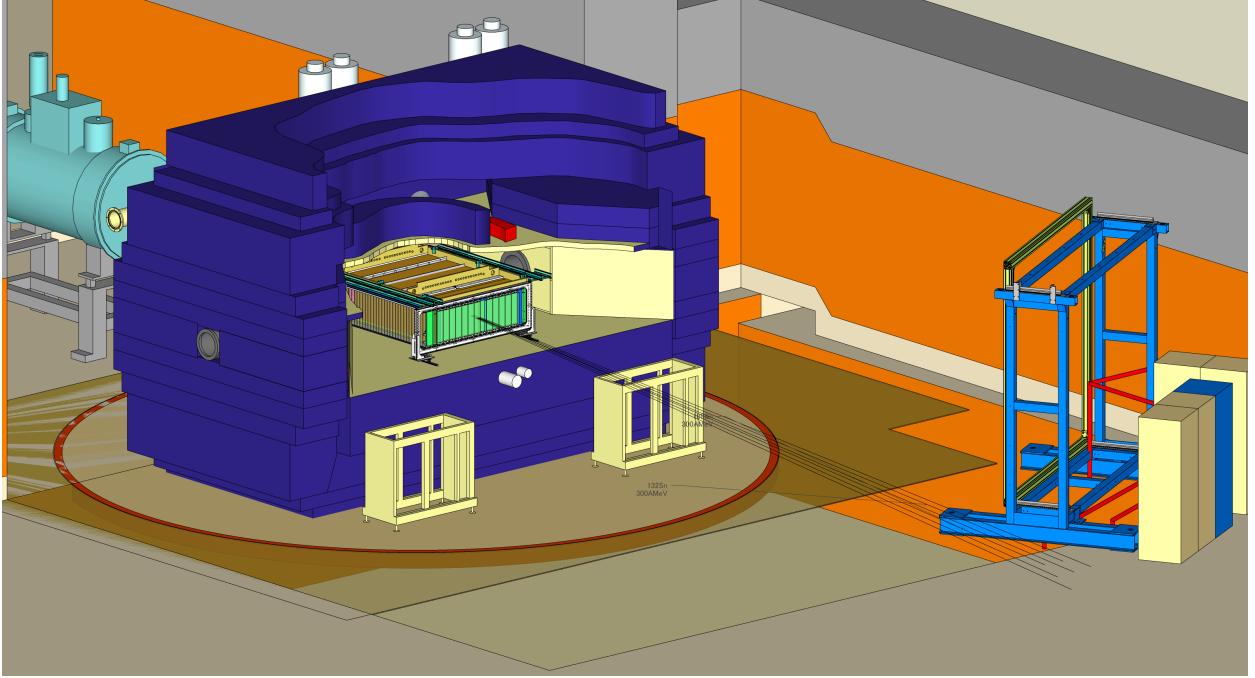


Figure 1.16: Drawing of the experimental setup with the TPC inside of the SAMURAI magnet at 0° configuration.

framework to readout the GET electronics for the S π RIT TPC. A General Trigger Operator (GTO) trigger was supplied to each DAQ synchronizing the subsystems.

1.9 Trigger Condition

Signals from all of the auxiliary detectors were combined into several logic combinations to form a trigger logic for triggering the data acquisition (DAQ) to record data. An upstream scintillating bar formed the start counter signal, triggering on any beam coming down the beam line. The active veto will trigger for any beam that is incident off the target location. The KATANA veto produces a signal if the beam passed through the TPC un-reacted, causing no nuclear collision; this produces a veto signal with a width of 4 μ s which is the approximate time it takes for the beam to drift and clear the field cage volume. The Kyoto multiplicity trigger produces a signal when the total number of tracks passing through both Kyoto arrays are greater than 4.

There were several special trigger considerations when we built the trigger for the TPC. We

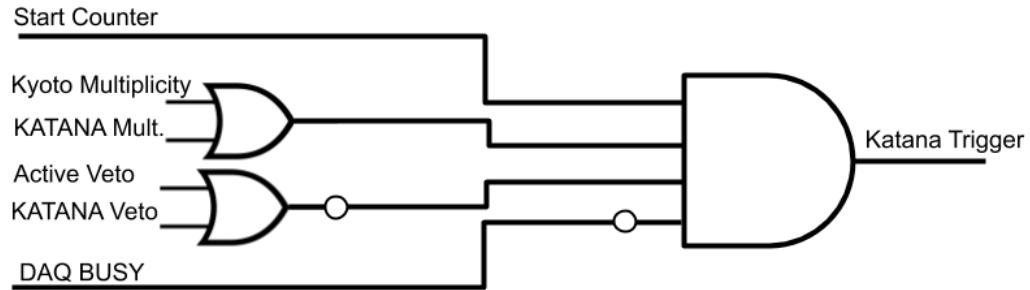


Figure 1.17: KATANA trigger box logic.

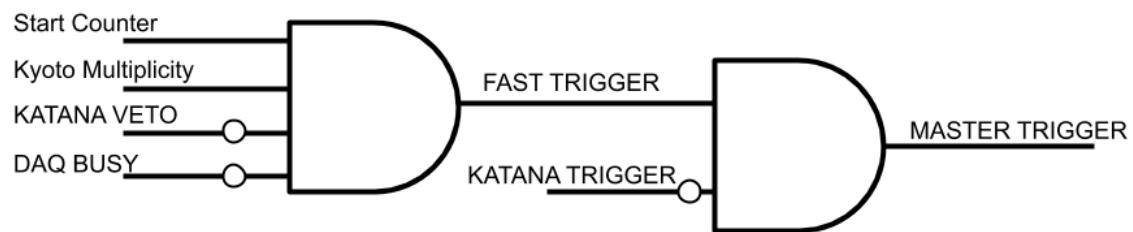
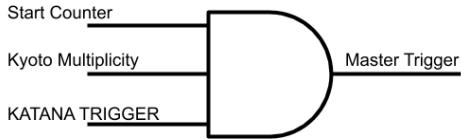
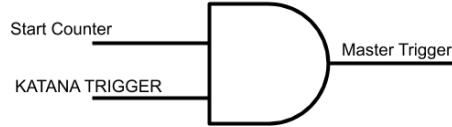


Figure 1.18: Master trigger logic.



(a) ^{124}Xe primary beam trigger.



(b) ^{238}U primary beam trigger.

required that the gating grid be opened fast to not miss any signal; as soon as there was a condition satisfying the Start Counter, Kyoto Multiplicity, the DAQ was not busy, and there was not a KATANA Veto signal. This was referred to as the Fast Trigger. If the KATANA trigger box is not satisfied –described later– this will trigger a Fast Clear signal which will not trigger the DAQ and will quickly close the gating grid. Figure 1.18 shows the logic of both of these triggers.

The master trigger for the DAQ was different for each primary beam as the experiment got progressively better. During the ^{124}Xe primary beam, the KATANA trigger box was an input into the trigger logic where as in the ^{238}U primary beam, the KATANA trigger box functioned as the trigger logic utilizing the internal trigger electronics. In either case the differences in the trigger were very minor and they both behaved practically the same except for minor details on the gating grid trigger CITE HERE JONS THESIS. Figure 1.17 summarizes the KATANA trigger box logic.

Figure 1.19a summarizes the ^{132}Xe primary beam, where the condition to produce a true KATANA trigger output was there must be a Start Counter, KATANA multiplicity, no Veto, and no DAQ busy signal. The KATANA trigger, Kyoto Multiplicity, and Start Counter together trigger the DAQ.

Where as Fig. 1.19b summarizes the ^{132}Xe primary beam, where the condition to produce a true KATANA trigger output was there must be a Start Counter, Kyoto or KATANA multiplicity, no Veto, and no DAQ busy signal. Here the KATANA trigger and the SC SUM??? together trigger the DAQ.

It is worth mentioning how the busy signals for the experiment were handled. The DAQ system

itself produces a busy signal which was combined with the busy signals from either opening or closing the gating grid. When opening the gating grid it is assumed the full volume of the TPC will be read out and therefore a 11 μs gate is produced; which is slightly more than the time it takes for all the electrons to drift in the field cage. In the case where the gating grid should be fast closed, either due to the fast clear circuit or the end of the TPC measurement, a 5 μs gate is produced to allow for the gating grid to settle to a closed configuration and clear the drift volume of any residual electrons from the beam. Both of these gates are included with the DAQ in an OR configuration which makes the overall busy signal.

1.10 Collision Data Taken

APPENDIX

APPENDIX
RUNS ANALYZED IN THIS DATA

System	#runs	Run numbers
$^{132}\text{Sn} + ^{124}\text{Sn}$	113	2841, 2843, 2844, 2845, 2846, 2848, 2849, 2850, 2851, 2852, 2855, 2856, 2857, 2858, 2859, 2860, 2861, 2875, 2877, 2878, 2879, 2880, 2881, 2882, 2883, 2884, 2887, 2888, 2889, 2890, 2891, 2892, 2893, 2894, 2896, 2898, 2899, 2900, 2901, 2902, 2903, 2904, 2905, 2907, 2914, 2916, 2917, 2919, 2920, 2921, 2922, 2924, 2925, 2926, 2927, 2929, 2930, 2931, 2932, 2933, 2934, 2935, 2936, 2939, 2940, 2941, 2942, 2943, 2944, 2945, 2946, 2948, 2955, 2956, 2958, 2959, 2960, 2961, 2962, 2964, 2965, 2966, 2968, 2969, 2970, 2971, 2972, 2973, 2975, 2976, 2977, 2978, 2979, 2980, 2981, 2982, 2983, 2984, 2985, 2986, 2988, 2989, 2990, 2991, 2992, 2993, 2997, 2999, 3000, 3002, 3003, 3007, 3039
$^{124}\text{Sn} + ^{112}\text{Sn}$	60	2542, 2543, 2544, 2546, 2547, 2548, 2552, 2553, 2554, 2555, 2556, 2557, 2558, 2559, 2560, 2562, 2563, 2564, 2565, 2566, 2567, 2568, 2569, 2570, 2571, 2572, 2573, 2574, 2575, 2578, 2579, 2580, 2581, 2582, 2583, 2584, 2585, 2586, 2587, 2588, 2589, 2590, 2591, 2592, 2593, 2594, 2595, 2596, 2597, 2598, 2599, 2600, 2601, 2617, 2618, 2619, 2620, 2621, 2622, 2623
$^{112}\text{Sn} + ^{124}\text{Sn}$	68	3059, 3061, 3062, 3065, 3066, 3068, 3069, 3071, 3074, 3075, 3076, 3077, 3078, 3080, 3081, 3082, 3083, 3084, 3085, 3087, 3088, 3089, 3090, 3091, 3092, 3093, 3094, 3095, 3097, 3098, 3102, 3103, 3138, 3139, 3140, 3141, 3142, 3143, 3144, 3145, 3146, 3148, 3149, 3150, 3151, 3152, 3153, 3154, 3155, 3156, 3157, 3158, 3159, 3165, 3166, 3167, 3168, 3169, 3170, 3171, 3172, 3177, 3179, 3180, 3181, 3182, 3183, 3184
$^{108}\text{Sn} + ^{112}\text{Sn}$	85	2272, 2273, 2274, 2275, 2276, 2283, 2284, 2285, 2286, 2288, 2289, 2291, 2310, 2311, 2314, 2315, 2320, 2322, 2323, 2324, 2325, 2331, 2332, 2333, 2334, 2335, 2336, 2337, 2340, 2341, 2362, 2363, 2368, 2369, 2370, 2371, 2372, 2373, 2374, 2375, 2378, 2379, 2380, 2381, 2382, 2383, 2384, 2385, 2386, 2387, 2388, 2389, 2391, 2392, 2393, 2394, 2395, 2396, 2397, 2398, 2399, 2400, 2401, 2402, 2429, 2432, 2433, 2434, 2437, 2438, 2439, 2440, 2442, 2453, 2461, 2462, 2463, 2501, 2502, 2503, 2505, 2506, 2507, 2508, 2509

Table .1: List of runs for the analysis.

APPENDIX
SECOND APPENDIX

BIBLIOGRAPHY

BIBLIOGRAPHY

- [1] W. Blum, W. Riegler, L. Rolandi, Particle Detection with Drift Chambers, Springer, Berlin, Heidelberg, 2008.
- [2] E. Gatti, et al., Optimum geometry for strip cathodes or grids in mwpc for avalanche localization along the anode wires, Nucl. Instr. Meth. Phys. Res. A 163 (1979) 83–92. doi:10.1016/0029-554X(79)90035-1.
- [3] Y. Yano, The ri beam factory project: A status report, Nucl. Instrum. Meth. B 261 (1-2) (2007) 1009–1013. doi:10.1016/j.nimb.2007.04.174.
- [4] T. Kobayashi, et al., Samurai spectrometer for ri beam experiments, Nucl. Instrum. Meth. B 317 (2013) 294–304. doi:10.1016/j.nimb.2013.05.089.
- [5] E. Pollacco, et al., Get: A generic and comprehensive electronics system for nuclear physics experiments, Physics Procedia 37 (2012) 1799–1804. doi:10.1016/j.phpro.2012.02.506.
- [6] M. Al-Turany, et al., The fairroot framework, J. Phys.: Conf. Ser. 396 (2). doi:10.1088/1742-6596/396/2/022001.
- [7] C. Höppner, et al., A novel generic framework for track fitting in complex detector systems, Nucl. Instrum. Meth. A 620 (2-3) (2010) 518–525. doi:10.1016/j.nima.2010.03.136.
- [8] W. Waltenberger, Rave—a detector-independent toolkit to reconstruct vertices, IEEE Transactions on Nuclear Science 58 (2) (2011) 434–444. doi:10.1109/TNS.2011.2119492.
- [9] G. Rai, et al., A tpc detector for the study of high multiplicity heavy ion collisions, IEEE Transactions on Nuclear Science 37 (2) (1990) 56–64. doi:10.1109/23.106592.
- [10] S. Collaboraiton, Samurai dipole magnet field map (2020).
URL <https://ribf.riken.jp/SAMURAI/index.php?Magnet>
- [11] G. Van Buren, et al., Correcting for distortions due to ionization in the star tpc, Nucl. Instrum. Meth. A 566 (1) (2006) 22–25. doi:10.1016/j.nima.2006.05.131.
- [12] T. Isobe, et al., Application of the generic electronics for time projection chamber (get) readout system for heavy radioactive isotope collision experiments, Nucl. Instrum. Meth. A 899 (2018) 43–48. doi:10.1016/j.nima.2018.05.022.