

CONSTRAINING THE HIGH DENSITY NUCLEAR SYMMETRY ENERGY WITH PIONS

By

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ABSTRACT

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ACKNOWLEDGEMENTS

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CHAPTER 3

EXPERIMENT

3.1 S π RIT TPC Overview

Add Overview image with labels

The Samurai Pion-Reconstruction and Ion Tracker Time Projection Chamber (S π RI TPC) is a Multi-Wire Proportional Counter developed to measure pions and other light charge particles resulting from radioactive heavy ion collisions in a fixed target experiments. The TPC is enclosed in a thin aluminum sheet walls all around in order to minimize neutron scattering and to allow for light charged particles to reach the arrays of scintillating bars detectors on the sides and downstream of the TPC. The S π RI TPC was developed to fit inside the Samurai dipole magnet used at the Rare Isotope Beam Factory (RIBF) at RIKEN in Wako-shi, Japan [1]; the dipole gap limited the vertical space of the TPC. More detail and specifications of the Samurai dipole magnet are given in [2].

A target ladder allowed for up to 5 fixed targets to be mounted. A ACME worm gear allowed for the x-axis motion for changing the targets during the experiment, without needing to open or move the TPC. The motion of this worm gear was translated through the target motion feed-through by several brass gears and non-magnetic gear boxes. The motion of the target ladder could be controlled by hand or by operation of the drill. The targets were mounted on stand-offs on the target ladder and also had z-axis motion. This allowed for the targets to be positioned as close as possible to the thin window of the field cage, maximizing the geometric acceptance.

The electronics were mounted to the aluminum top plate. Several aluminum ribs were mounted to the top of the plate to bring structural rigidity. A flatness within $150\mu\text{m}$ was achieved across the whole top plate as measured by a laser position system. The charge sensitive pads of the pad plane were etched into several circuit boards were recessed and glued to the bottom portion of the top plate. Vias through the pad plane circuit boards brought the signal traces from the pads to surface mount pads on the other side of the boards. Several holes cut through the top plate allowed for the

S π RIT TPC Overview	
Pad plane area	1.3 m x .9 m
Pad size	1.2 cm x .8 cm
Number of pads	12096 (112 x 108)
Gas composition	90% Ar + 10% CH ₄
Multiplicity limit	200
dE/dx range	Z=1-8, π , p,d,t,He,Li-O
Drift length	50 cm

Table 3.1 An overview of the properties of the S π RIT TPC

interface cables of the electronics to be connected to these surface pads.

Just below the pad plane were a set of three wire planes; the gating grid, ground, and anode wire planes. The detailed function of these wires will be explained later but they served to separate the boundary between the drift volume and the avalanche volume.

The front and sides of the field cage were assembled from 8 independent rigid circuit boards. The downstream window served as the downstream wall of the field cage all though it was was a large polycarbonate frame in which a removable kapton window could be installed. This thin window minimized the scattering of exiting neutrons and charged particles for downstream detectors.

The voltage step down takes the high voltage of the field cage cathode and steps the voltage down through a set of copper rings and a resistor chain, minimizing the chance for sparking.

3.1.1 Enclosure

3.1.2 Voltage Step Down

3.1.3 Field Cage

The field cage was designed to hang from the top plate and therefore needed to be of a lightweight construction. Also the materials needed to be thin to allow for light charged particle and neutrons to pass through without significant scattering for ancillary detectors. Therefore instead of a

downstream wall, a large thin exit window was constructed. The cathode was constructed of an aluminum honeycomb laminate. Two sheets of ??? aluminum were bonded to a core of aluminum honeycomb structure providing a lightweight yet rigid structure for the cathode.

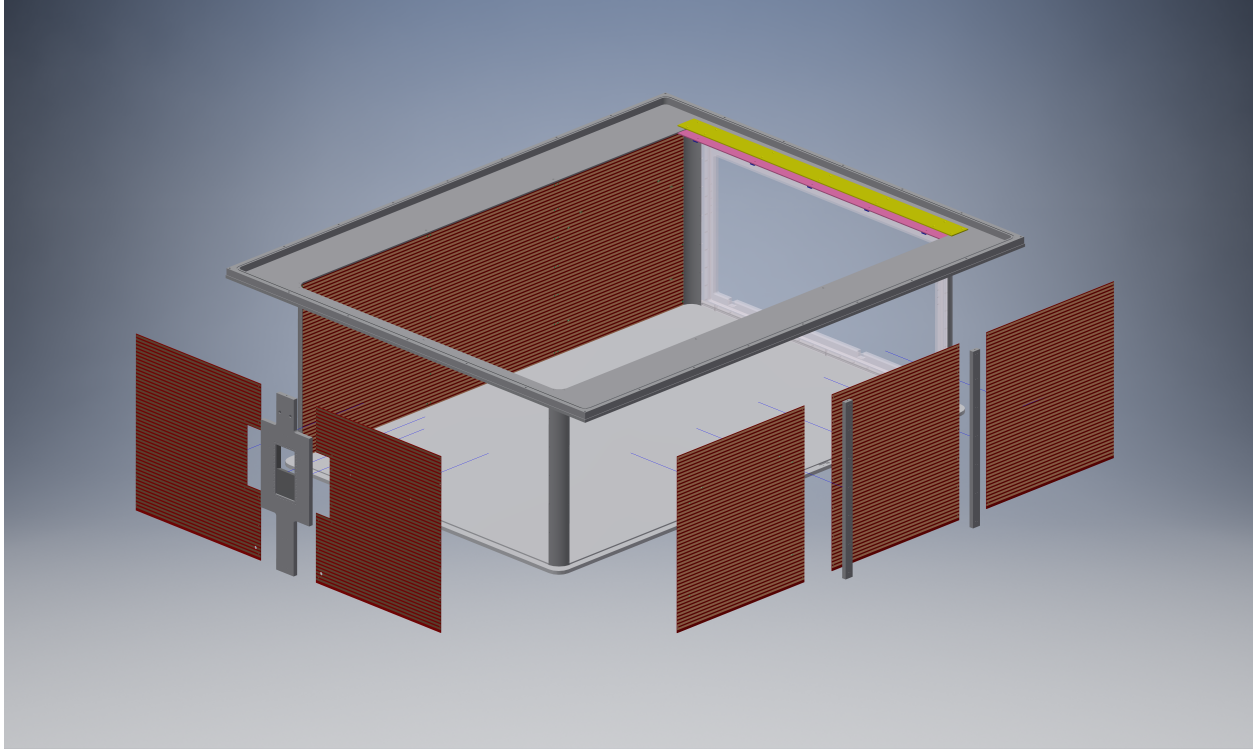


Figure 3.1 Exploded view of the S π RIT TPC

The field cage was constructed from several panels of printed circuit boards (PCBs). The epoxy in the common PCB substrate FR4 contains bromine which is not suitable for the long term operation of a TPC, as the bromine will eventually cause gain reduction of the wires [CITE]. The halogen free material chosen was Rogers ???. We built the TPC with the option to run explosive gases such hydrogen, thus we decided to have field cage an isolated volume from the rest of the TPC enclosure. While the risk of a high voltage spark was minimized using the voltage step down, the risk of sparking when using an explosive gas could be further minimized by isolating the detector volume from the enclosure volume thereby allowing you to run an insulating gas between the field cage while running the explosive gas inside the detector volume only.

The front of the field cage was made of two PCBs and each side was constructed of three PCBs.

The exit window was a $10\mu\text{m}$ thick Kapton window with evaporated aluminum strips on the inside and outside; mounted on a polycarbonate frame.

3.1.4 Voltage Step Down

To lower the risk of a high voltage spark around the cathode region a voltage step down was developed. A series of 7 concentric copper rings with 20 MOhm resistors between them steps the cathode voltage down to ground. This minimizes sharp transitions of the electric field and therefore sparking.

3.1.5 Wire Planes

Add figure of gating grid transparency closed and open configuration

3.1.6 Pad Plane

Add figure of close up of pad plane

3.1.7 Electronics

Signals in the $S\pi\text{RIT}$ TPC are amplified and digitized by the recently developed Generic Electronics for TPCs (GET) [3]. Short cables transmit the signals from the pads to the inputs of the AGET chips. Each AGET chip services 64 pads (63 pads are connected in our case), contains a pre-amplifier, and a Switched Capacitor Array (SCA), with a maximum of 512 time buckets with an adjustable sampling frequency of 1 to 100 MHz. Four AGET chips are mounted on one AsAd (ASIC and ADC) motherboard. The gain of each AGET can be configured as 0.12, 0.24, 1.0, or 10 pC over the whole dynamic range, and the ADCs on each AsAd board provides 12 bit resolution. The peaking times of the shaping amplifiers can be set to 69, 117, 232, 501, 720, or 1014 ns. In this experiment, the gain was set to the highest setting, 0.12 pC, the peaking time 117 ns, and the sampling frequency 25 MHz (resulting in 40 ns time buckets). The Aget 2.0, asad 2.1, and cobo 1.0 firmware versions

GET electronics settings	
ADC bit range	14 bits
Sampling frequency	1-100 MHz
Dynamic range	.12, .24, 1.0, 10pC
Peaking time	69,117,232,501,720,1014 ns
Time bucket range	512

Table 3.2 Summary of range of GET electronics settings.

were used. The variations in the electronics were calibrated by measuring the response of each channel to a injected reference pulse, covering the full dynamic range of each channel.

3.1.8 Considerations when constructing a TPC

Several considerations went into the construction of the $S\pi$ RI TPC which I wish to summarize and document here. All materials and glues of the TPC were selected as low out-gassing materials. Several materials (that are common place in nuclear labs), such as vacuum grease, viton o-rings, all out-gas organic chemicals into the counter gas which damage the TPC by permanently lowering the gain over time. The organic molecules responsible are difficult to identify exactly, but lists of good and bad materials are well known in the literature from experiments. If a material we wished to used was not on these lists we placed the material in a clean chamber with the counter gas and flowed this counter gas through a small proportional counter making sure the gain did not drop at high collection rates when exposed to a high rate alpha Americium source.

Sparking Two volumes of gas.

3.1.9 Gas Properties

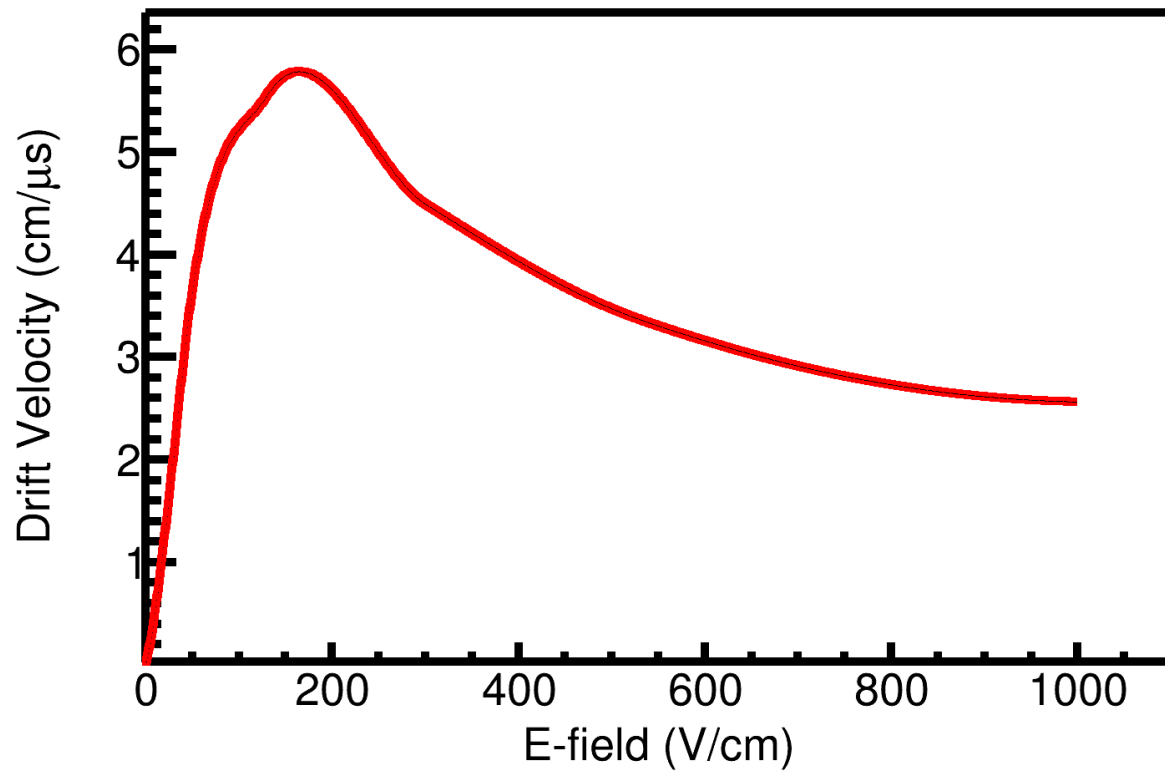


Figure 3.2 Drift velocity of electrons in P10 gas.

Gas properties	σ_t (cm ^{-1/2})	σ_l (cm ^{-1/2})	v_d (cm μs ⁻¹)	G_h	G_l
	0.024	0.034	5.43	903	150

Table 3.3

Add table for gas diffusion

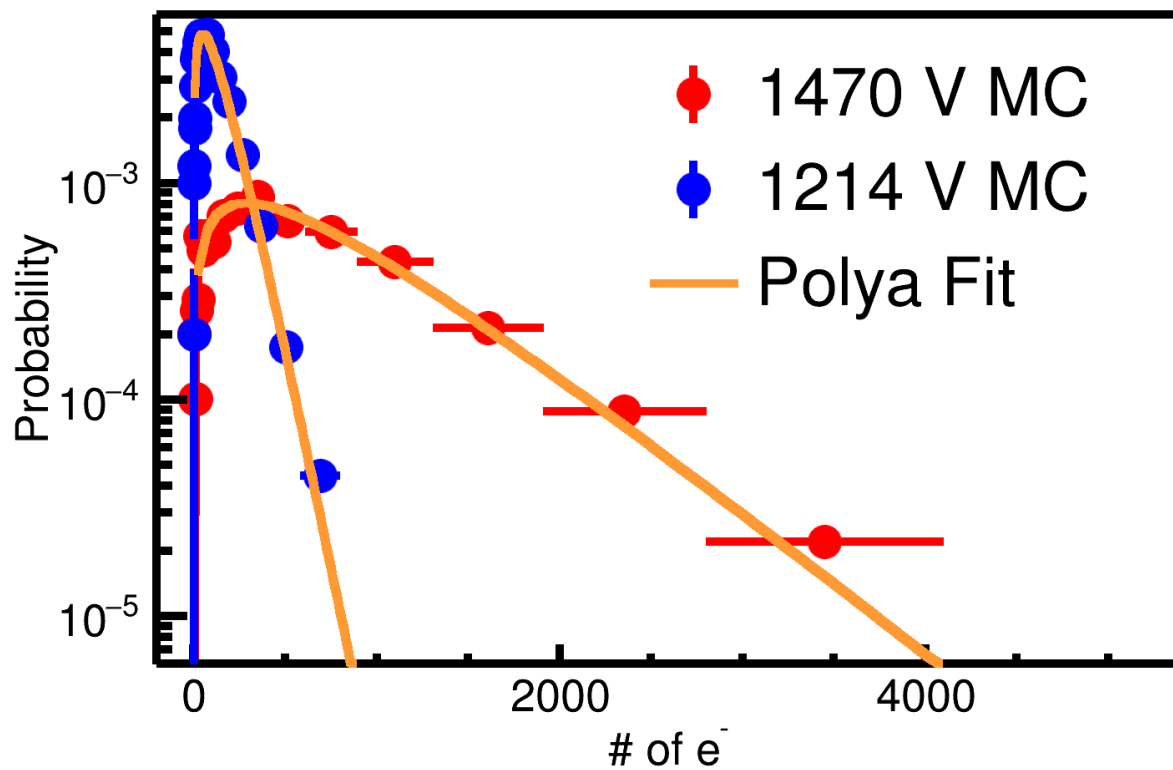


Figure 3.3 Number of electrons produced in a single avalanche on an anode wire. Two different voltages were simulated using Garfield++ at 1470 V and 1214 V. The expected Polya distribution fit is also given in yellow.

3.2 Ancillary Detectors

3.2.1 Kyoto Multiplicity Trigger

3.2.2 Krakow ?????? (KATANA)

3.3 Radio Isotope Beam Factory (RIBF) Facility

Cyclotron facility overview. Samurai line overview. Beam line element overview. Big rips beam PID. reference

3.4 $S\pi$ RIT at RIBF

Picture of setup.

SAMURAI (Superconducting Analyzer for Multi-particles from Radioisotope beams) is a large-acceptance multi-particle spectrometer for radioactive-beam experiments.

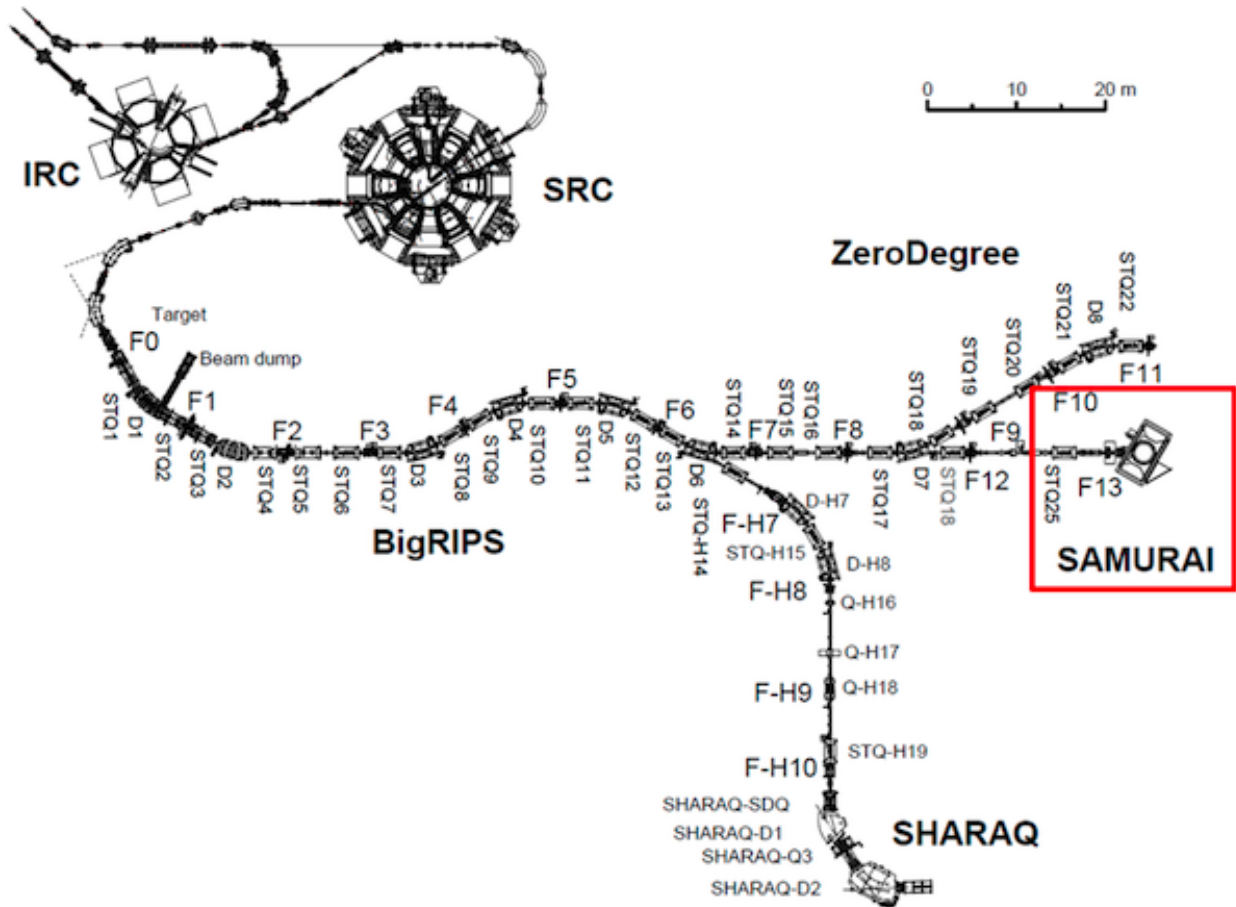


Figure 3.4 Overview of the RIBF, BigRIPS, and SAMURAI beamline.

3.5 Experimental Setup

3.6 Trigger Condition

How it was made using kyoto krakow

3.7 Collision Data Taken

CHAPTER 4

DATA ANALYSIS I: CALIBRATION AND CORRECTIONS

Need to explain pedestal subtraction GG noise subtraction

4.1 Software

The $S\pi$ RITROOT software is modular tasked based code based on the FAIRROOT package written in C++ [4]. The main tasks in the $S\pi$ RITROOT software reconstruction are:

- Decoder task
- Pulse Shape Algorithm (PSA Task)
- Helix Track Finding Algorithm
- Clustering Algorithm
- Track Fitting (GENFIT package)
- Vertex Fitting (RAVE package)

The decoder task converts the binary data file into a container class which maps the electronics channels into the corresponding pads and (x,z) coordinates.

There may be several pulses in a pad coming from two tracks passing under the same pad separated by arrival time. Using an expected pulse shape the PSA task fits the signal pulses within a pad, giving the arrival time of the drifted electrons from each particular track. The height of the fitted pulse is proportional to the total charge of that event, Q and the y-coordinate is calculated as $y = v \cdot t_0$ where v is the drift velocity and t_0 the arrival time. Combining the information from these first two tasks, (x,y,z,Q), we construct what is called a "hit".

The Helix Track Finding Algorithm finds the collection of hits belonging to one track out of all the hits in an event. The hits within a track are then reduced into clusters. A cluster's position is

the average position of the hits within a cluster, with the total charge of the cluster being the sum of the hits charges.

A tracks average position is estimated by the cluster's average position. The clusters are then fitted in the GENFIT track fitting package [5], giving the final momentum of the track. A final vertex of the event is fitted from all tracks using the package RAVE [6].

Definition of clustering A brief description of the method of clustering is illustrated in Figure 4.1. It is impractical to cluster in both the x and z-axis and we only cluster the hits along one axis. The three clusters at the bottom of Figure 4.1 are clustered along the x-axis and the upper three are along the z-axis, as shown by the bolded pads for one of the clusters in each direction.

The clustering direction depends on the angle of the track with respects to the x-axis, defined as θ . For example, a track going along the z-axis the crossing angle is defined as 90° , and a track going along the x-axis defined as 0° . In the case that the crossing angle is $45^\circ < \theta \leq 90^\circ$ the clustering direction is along the x-axis. For $0^\circ < \theta \leq 45^\circ$ it is along the z-axis.

The position along the clustering direction is calculated by weighting the individual hit's positions by their charges q_i and getting the mean value. The other direction is set to the center of the pad. For example if we are clustering along the x-axis for a cluster, the z-position is set to the center of the pad in the z-direction and vice versa.

Clustering in this way gives us better position resolution for calculating the position of each cluster. You could imagine if we calculated the clusters only along the x-axis for tracks with $\theta \approx 0^\circ$ the x-position is not well defined. By clustering in the direction most perpendicular to the track, we get a better position resolution.

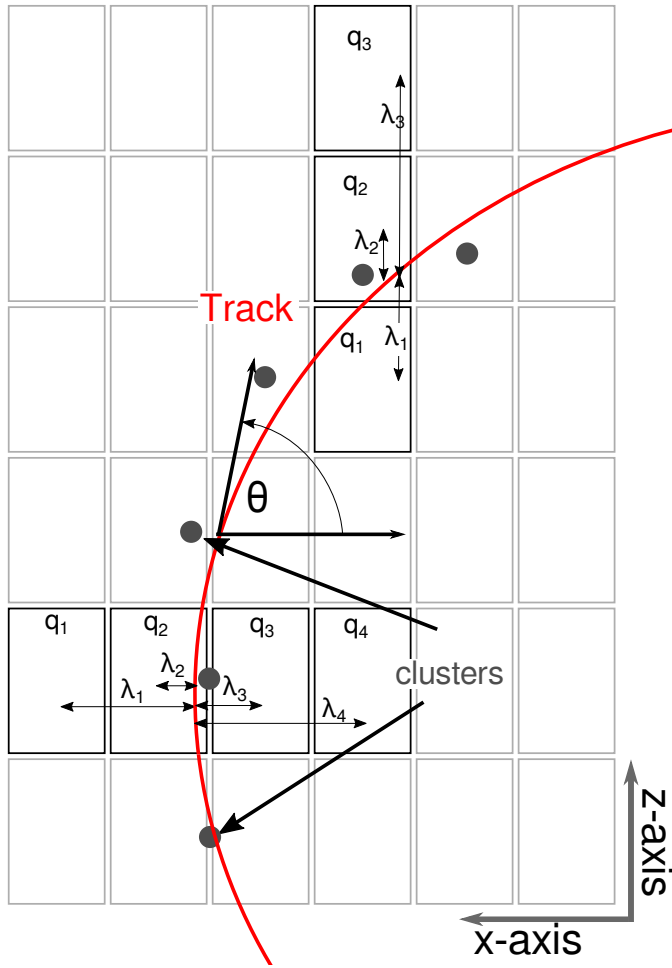


Figure 4.1 Cartoon graphic of a top down view of a fit to a track passing through several pads. The bolded pads and the charges q_i represent the hits belonging to that pad and the clusters of the track representing the average position of the track. The three clusters at the bottom are clustered in the x-direction and for the upper three clustered in the z-direction. The estimate of the position of the avalanche is given by the track fit and the position from the center to each pad to the \bar{x} position is given as λ_i .

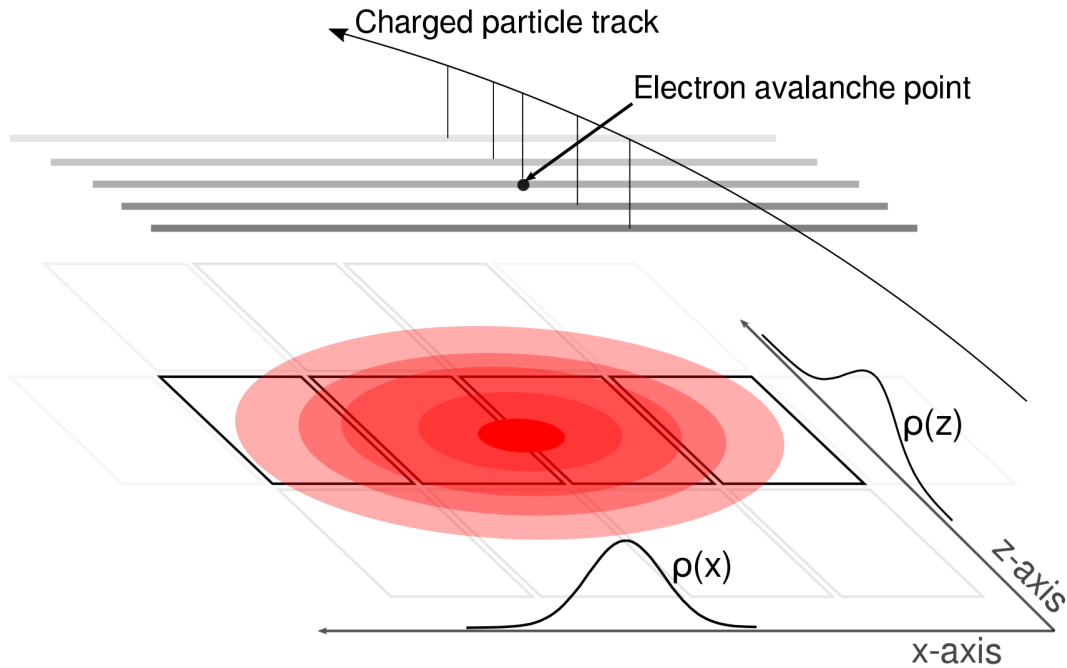


Figure 4.2 A cartoon illustration of the charge distribution resulting from an electron avalanche on one wire and the projections of the distribution onto the two axis $\rho(x)$ onto the x-axis and $\rho(z)$ onto the z-axis. The orientation of the wire planes is flipped upside down to display the perspective better.

4.2 Calibrations and Corrections

4.2.1 Cocktail calibration

Cocktail Calibration Picture of cocktail before and after ExB effect Table of LISE++ expected cocktail energies rigidity setting of dipole magnets (reference big rips line)

4.2.2 Electronics calibration

Pulse the ground grid.

Particle	100MeV				100MeV				300MeV	
	Measured									
	Raw	E×B								
p	882.8	d	d	903.5	e	e			f	f
d	817.1	d	d	898.5	e	e	1621.1		f	f
t	589.5	d	d	887	e	e	1612.4		f	f
³ He	1617.3	d	d	1795.2	e	e	3236.4		f	f
⁴ He	1405.6	d	d	1782.9	e	e	3226.4		f	f

Table 4.1 Summary of expected cocktail.

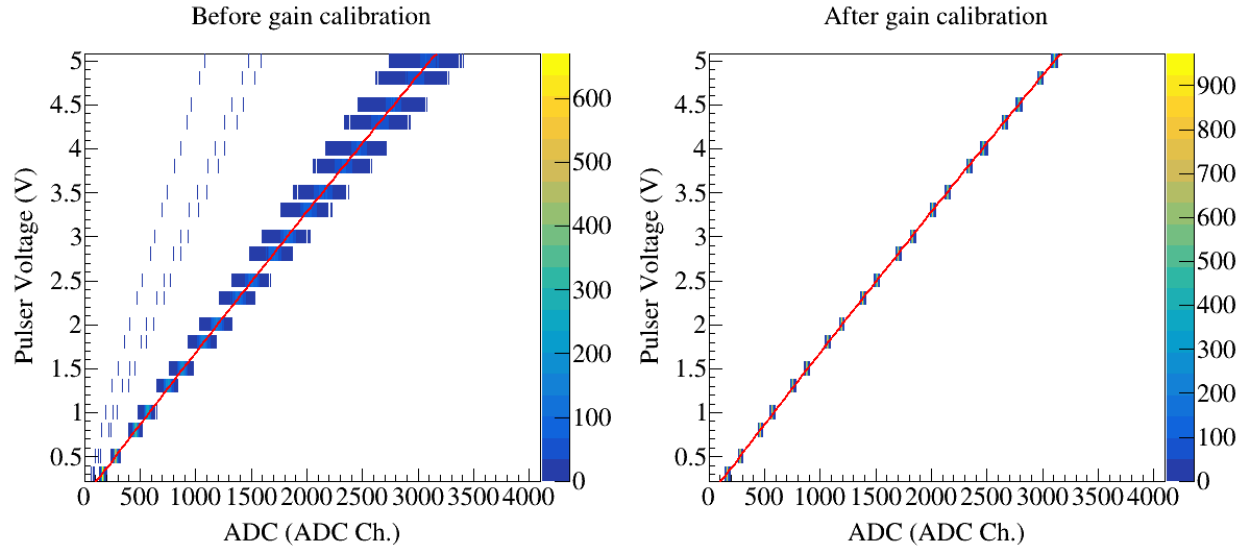


Figure 4.3 Calibration of electronics

4.2.3 Anode gain calibration

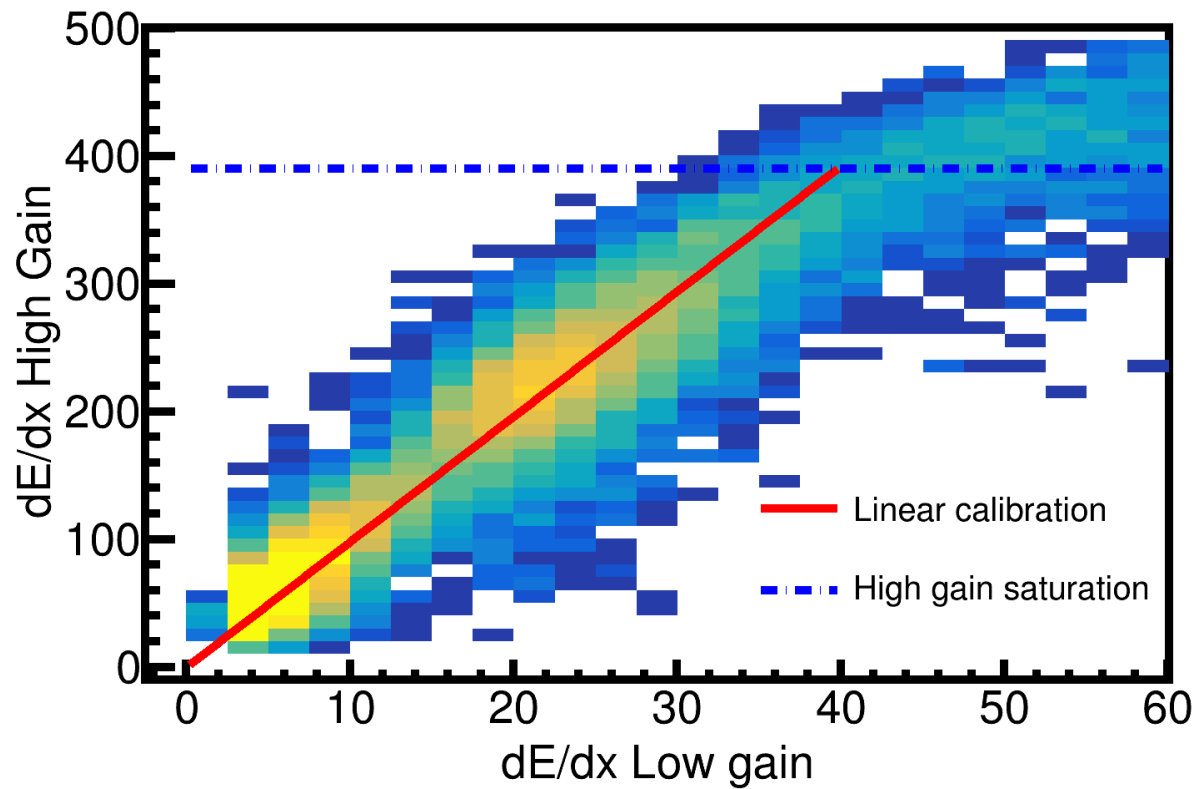


Figure 4.4 Calibration of low high.

Picture of low vs high gain channels and fit

4.2.4 Extending the dynamic range of the Electronics

Add paper here.

4.2.5 Space Charge Corrections

Overview Discuss the relevant time scales, drift lengths, magnitudes, and locations of space charge

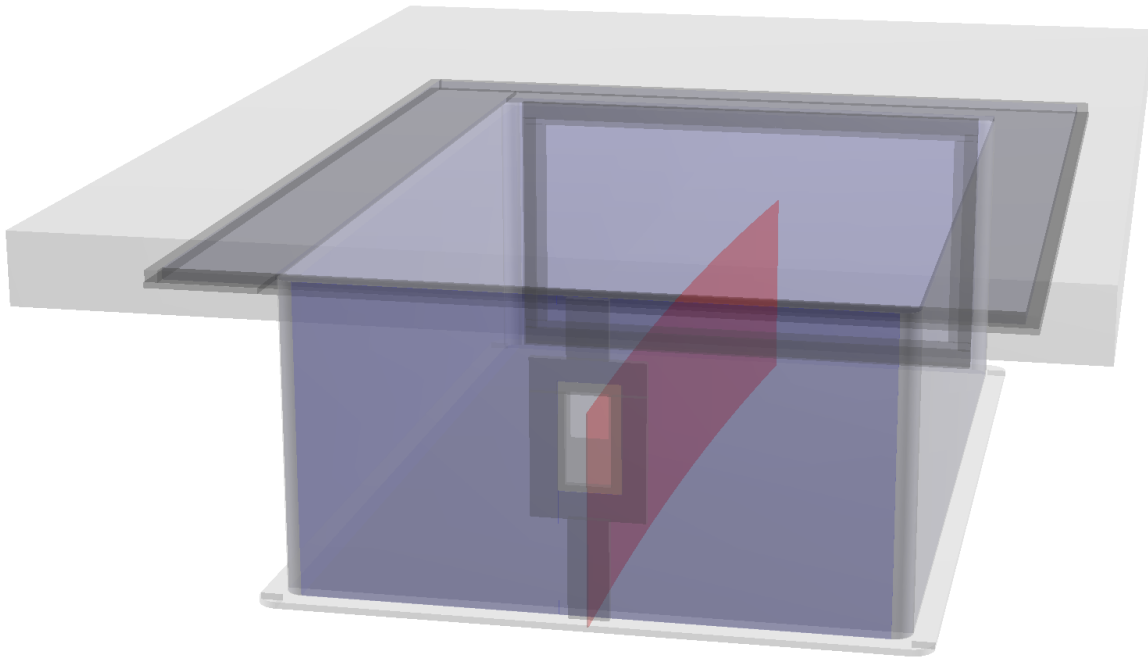


Figure 4.5 Location of space charge in ^{132}Sn

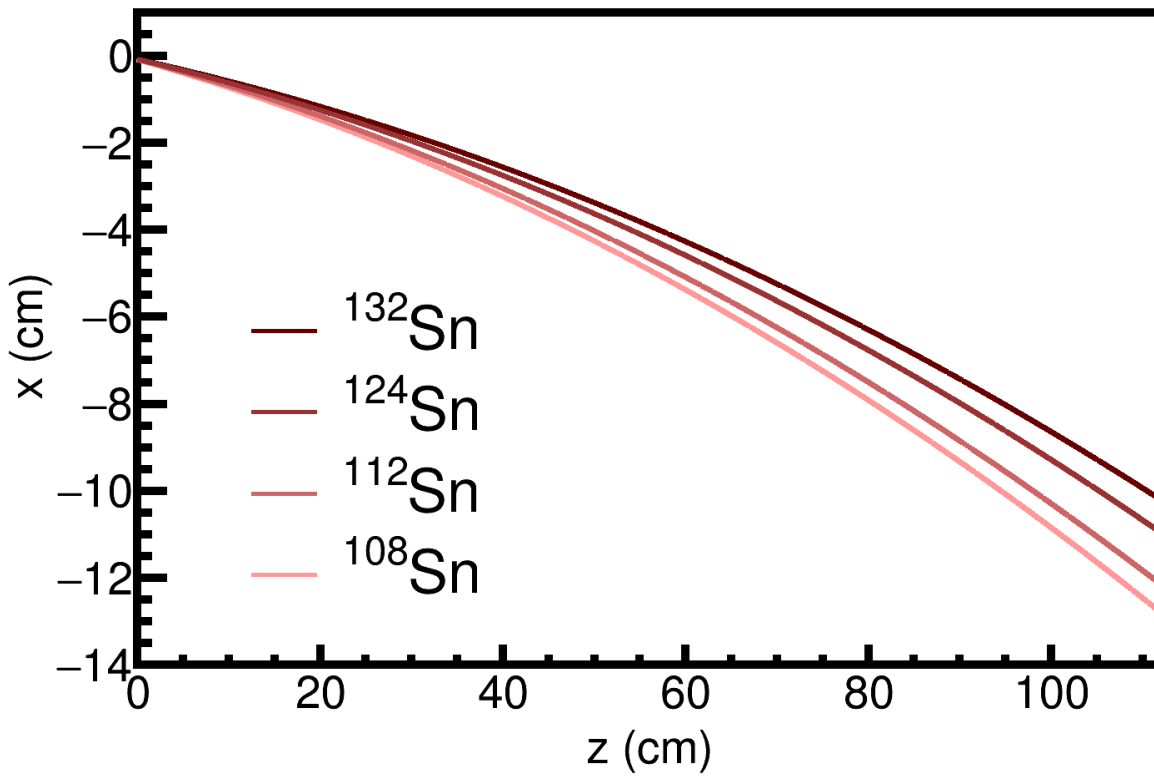


Figure 4.6 Beam path of the experiments

Figure of beam path locations for different beam types Table of energy loss tables for energies and beam types Reference appendix for poisson solver Tables for ion drift velocity in P-10 Gas reference Sauli Figure of sDAC or POCA Figure of cartoon of what is happening to tracks Figure of correction map in TPC and MC map Figure of before and after correction BDC vs reco momentum Figure of track residuals before and after?

In theory, a TPC functions with the electric and magnetic fields parallel to each other. In this way the electrons move opposite to the electric field winding tightly around the magnetic field lines, reducing transverse diffusion in the process. In practice, due to the finite size of the dipole magnet and field cage, there are transverse components to both the electric and magnetic fields. These transverse components introduce drift velocities in the transverse directions, causing a shift in the measured cluster positions of the track. Thereby introducing systematic shifts in the calculation of the momentum and the vertex calculation.

Most of the time the beam does not undergo a nuclear collision with the target and passes through the TPC drift volume. The KATANA array threshold was set to veto such events, ensuring the gating grid remain closed to prevent the large amount of charge deposited by the beam into the avalanche region. While the electron drift velocity is fast enough for the electrons produced by the unreacted beam to terminate on the closed gating grid, the drift velocities of the positive ions produced are of order 10^{-4} times slower. At higher beam rates the positive charge is allowed to pile up producing a region of positive space charge, introducing perturbations to the nominal electric field.

Since the beam comes in along the z-axis, and the drift direction of the ions is in the -y direction, we can estimate the charge density as an uniform sheet charge. The surface charge density is related to the beam rate, ion drift length, ion drift velocity, and the energy loss of the beam. Though the incoming beam comes randomly, the slow drift velocity combined with the high beam rate makes the uniform approximation valid. Tracking or estimating the beam rate as a function of time within a given run would provide a better estimate of the space charge. Or experimentally a laser system could be pulsed after each event (throughout the drift volume), giving the experimental correction map for the drift. While the potential for a laser system was implemented in the field cage design, a laser system ultimately was not developed for the $S\pi$ RIT tpc.

The beam rate within a run is roughly constant, therefore we can estimate the space charge and provide a first order correction for the space charge effect.

As mentioned in CHAPTER ???, the cocktail beam momentum was well known to within 1% as set by the BIGRips spectrometer. Also time of flight analysis of upstream and downstream scintillators also independently confirmed the beam rigidity setting. The expected momentum is given in TABLE ??? as calculated by from the beam rigidity setting of the magnet (WHICH MAGNET). The measured momenta as determined by the TPC software (given in FIG TABLE), shows a disagreement on the level of 5% too high. We noticed that if one only uses the first 90 layers (out of 112) of the TPC, the momenta is lower; one should expect the momentum to go higher as the track length is shorter (short tracks effectively are straight lines). In the cocktail beam

there is no un-reacted beam causing any significant space charge. The magnetic field map of the SAMURAI magnet has been calculated by TOSCA simulation CITE ???, and several points have been verified experimentally with a hall probe to be within XXX %. We assume that the electric field (to first order) is uniform in the y-direction. Using Garfield++ CITE ???, we can model the transverse drift of the electrons in the presence of such fields.

A grid of electrons uniformly distributed in the TPC model space were drifted to the gating grid position. The final shifts in the x and z positions was measured.

4.3 Monte Carlo Simulation

We use Geant4 as an event generator for performing Monte Carlo Simulations in the TPC. A scale model of field cage, front window, front window frame, pad plane, and aluminum top plate are modeled. The correct materials are used as well as the field cage is modeled with P-10 gas at a density of ????. By using Geant4 we can also input the magnetic field map of the SAMURAI dipole magnet (as calculated by the SAMURAI group via a TOSCA simulation). In this way any particle type may be studied and the full interactions (scattering, decay, energy loss, path taken, etc.), are accounted for. The output of this simulation is a series of energy loss points which contain the amount of energy lost in keV/cm and the position in (x, y, z) .

Separate software tasks model the converting energy loss into electrons, the drifting of electrons, the avalanche process, and the electronics response.

4.3.1 Drift Task

The drift task takes the energy loss points calculated from Geant4 and converts them into electrons, and then modeling their drift behavior in the field cage. As discussed previously the various processes[CITE To formula about drifting electronc]

A full microscopic treatment of the stochastic nature of each electron would be too cumbersome; most of the properties of the electrons are described by macroscopic quantities can be described



Figure 4.7 A summary of all the effects modeled in the TPC MC simulation.

by The charge of each MC point is converted to the total number of electrons liberated in the P-10 gas. This is a well understood property of proportional counters and is stable over a wide range of velocities and particle types [CITE BOOK]. The conversion factor of P-10 can be calculated by considering the partial volumes of each component of the gas. 4.1.

$$Number of e^- = 28 keV/cm \quad (4.1)$$

4.3.2 Pad Response Task

After the avalanche process of the previous task, the total charge of the event is split over several pads defined by the Pad Response Function (as discussed in section ???). As shown in Fig. 4.8, there are three wires that lie directly above a given pad. The z coordinate of the avalanche can only be one of these three wires, where as the x coordinate can be any value along the wire. The functional form of the software PRF (given in Eq. 4.2), was tuned to match the experimental data. Shown in Fig. 4.9, we see the tuned software PRF can match the experimental PRF from data over several crossing angles (as mentioned in Chapter ??? governs the shape of the PRF).

$$PRF(x, z) = \frac{1}{2\pi\sigma_z\sigma_x} \exp \frac{-(x-x_0)^2}{2\sigma_x^2} \exp \frac{-(z-z_0)^2}{2\sigma_z^2} \quad (4.2)$$

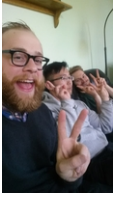


Figure 4.8 A cartoon of the wires over one pad.



Figure 4.9 Comparison of MC and data PRF

4.3.3 Electronics Task

The electronics task takes the total charge on each pad and simulates the electronics response, converting electronics into ADC channels. Accounting for the pedestal, the measured output in ADC channels (for a given gain setting) is given in Eq. 4.3.

$$1_{\text{ADC}} = \frac{ADC_{\text{Max}} - ADC_{\text{Pedestal}}}{G * f_c} \quad (4.3)$$

4.3.4 Simulating Saturation

Add figure showing saturated time bucket spectra with location of saturation identified and with pulse shape from embedding I would like to add and how it blocks it. Add Figure with 2D pad plane response with and without saturation flag

4.4 Monte Carlo Track Embedding

Add Figure of MC track embedding

Track embedding is the process of taking a simulated MC track from Geant4 and embedding its response into a real data event. After reconstructing this new embedded event we match the input MC track embedded to its corresponding final reconstructed track. By doing so we can evaluate the response of the entire TPC system to any given input value. The TPC system is composed of three major components (each which can introduce errors and or biases) the software, the detector, and the experimental setup.

As discussed in [SOFTWARE CHAPTER] the software is composed of several task, each which introduce some error. Table REF TABLE] listing some of the errors each task may introduce illustrating how difficult propagating the errors would be through each system.

The detector system itself introduces errors related to the physical processes of the measurement itself. To address this we model the TPC (and its materials) in a Geant4 simulation which provides an accurate description of various interactions of a particle traversing the materials (including the gas volume) of the TPC.

software is the most straight forward; let the software routine process an input and measure the result. Understanding the measurement requires modeling the physics involved in the theory and operations of TPC's and the electronics. The experimental setup itself is quite large and complex, several ancillary detectors such as the Kyoto multiplicity array, Krakow veto array, Active veto array, beam identification detectors, etc. Even if a full accurate model could be constructed the complex trigger logic of the DAQ system would be impossible to model. If we notice that the biases and errors of the entire experimental setup is contained in the measured experimental data. Therefore, by inputting the MC data into a real experimental event (and measuring the output of that MC track) we can estimate the errors of the experimental setup.

The software analysis routine and the bias introduced by the trigger settings of the experiment introduce systematic errors in the reconstruction of tracks

4.4.1 MC and Data Comparison

Add Figure of Pad response function for pion,proton.... for MC vs Data vs angles... Add Figure of Number of clusters of MC vs Data Add Figure of dEdx MC vs Data Add Figure of Momentum resolution MC vs Data Add Figure of track residuals? MC vs data?

4.5 Efficiency Corrections

Add Figures of efficiency vs angles in TPC polar angle plot for pions

Since the $S\pi$ RIT TPC is a fixed target experiment it's angular coverage is certainly not 4π . Because the target is several cm away from the widow of the field cage the geometric acceptance is not even 2π . The rectangular design complicates the calculation of the geometric acceptance, or the efficiency.

4.6 Beam Particle Identification

Figures of beam contaminants in our beam PID line. Table of beam purity reference to Jon's thesis paper

4.7 Solid angle coverage

APPENDIX

APPENDIX
YOUR APPENDIX

BIBLIOGRAPHY

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