Interrelationships between the Parameters

We know
$$\begin{bmatrix} V_1 \\ V_2 \end{bmatrix} = \begin{bmatrix} z_{11} & z_{12} \\ z_{21} & z_{22} \end{bmatrix} \begin{bmatrix} I_1 \\ I_2 \end{bmatrix}$$

and
$$\begin{bmatrix} I_1 \\ I_2 \end{bmatrix} = \begin{bmatrix} y_{11} & y_{12} \\ y_{21} & y_{22} \end{bmatrix} \begin{bmatrix} V_1 \\ V_2 \end{bmatrix}$$

Hence,
$$\begin{bmatrix} z_{11} & z_{12} \\ z_{21} & z_{22} \end{bmatrix} \begin{bmatrix} y_{11} & y_{12} \\ y_{21} & y_{22} \end{bmatrix} = 1$$

$$\Rightarrow \begin{bmatrix} z_{11} & z_{12} \\ z_{21} & z_{22} \end{bmatrix} = \begin{bmatrix} \frac{y_{22}}{\Delta y} & -\frac{y_{12}}{\Delta y} \\ -\frac{y_{21}}{\Delta y} & \frac{y_{11}}{\Delta y} \end{bmatrix}$$

$$y_{11} y_{22} - y_{12} y_{21}$$

Z → ABCD:

We know
$$V_1 = AV_2 - BI_2$$

$$I_1 = CV_2 - DI_2$$

Solving the equations,
$$V_1 = \frac{A}{C} I_1 + \frac{AD-BC}{C} I_2$$

and $V_2 = \frac{1}{C} I_1 + \frac{D}{C} I_2$

$$\Rightarrow Z_{11} = \frac{A}{C}, Z_{12} = \frac{AD-BC}{C}, Z_{21} = \frac{1}{C}, Z_{22} = \frac{D}{C}$$

We know
$$V_1 = h_{11} I_1 + h_{12} V_2$$

$$I_2 = h_{21} I_1 + h_{22} V_2$$
Solving the equations, $V_1 = \frac{\Delta h}{h_{22}} I_1 + \frac{h_{12}}{h_{22}} I_2$
and $V_2 = -\frac{h_{21}}{h_{22}} I_1 + \frac{1}{h_{22}} I_2$

$$\Rightarrow Z_{11} = \frac{\Delta h}{h_{22}}, Z_{12} = \frac{h_{12}}{h_{22}}, Z_{21} = -\frac{h_{21}}{h_{22}}, Z_{22} = \frac{1}{h_{22}}$$

In a similar way, we can convert the other parameters and construct the following table:

	z	y	T	h
z	$\left[egin{array}{ccc} \mathbf{z}_{11} & \mathbf{z}_{12} \ \mathbf{z}_{21} & \mathbf{z}_{22} \end{array} ight]$	$\left[\begin{array}{cc} \frac{\mathbf{y}_{22}}{\Delta\mathbf{y}} & \frac{-\mathbf{y}_{12}}{\Delta\mathbf{y}} \\ \frac{-\mathbf{y}_{21}}{\Delta\mathbf{y}} & \frac{\mathbf{y}_{11}}{\Delta\mathbf{y}} \end{array}\right]$	$\left[\begin{array}{cc} \frac{\mathbf{A}}{\mathbf{C}} & \frac{\Delta \mathbf{T}}{\mathbf{C}} \\ \frac{1}{\mathbf{C}} & \frac{\mathbf{D}}{\mathbf{C}} \end{array}\right]$	$\left[\begin{array}{cc} \frac{\Delta \mathbf{h}}{\mathbf{h}_{22}} & \frac{\mathbf{h}_{12}}{\mathbf{h}_{22}} \\ \frac{-\mathbf{h}_{21}}{\mathbf{h}_{22}} & \frac{1}{\mathbf{h}_{22}} \end{array}\right]$
y	$\left[\begin{array}{cc} \frac{\mathbf{z}_{22}}{\Delta \mathbf{z}} & \frac{-\mathbf{z}_{12}}{\Delta \mathbf{z}} \\ \frac{-\mathbf{z}_{21}}{\Delta \mathbf{z}} & \frac{\mathbf{z}_{11}}{\Delta \mathbf{z}} \end{array}\right]$	$\left[\begin{array}{cc}\mathbf{y}_{11}&\mathbf{y}_{12}\\\\\mathbf{y}_{21}&\mathbf{y}_{22}\end{array}\right]$	$\left[\begin{array}{cc} \frac{\mathbf{D}}{\mathbf{B}} & \frac{-\Delta \mathbf{T}}{\mathbf{B}} \\ \frac{-1}{\mathbf{B}} & \frac{\mathbf{A}}{\mathbf{B}} \end{array}\right]$	$\left[egin{array}{ccc} rac{1}{\mathbf{h}_{11}} & rac{-\mathbf{h}_{22}}{\mathbf{h}_{11}} \ rac{\mathbf{h}_{21}}{\mathbf{h}_{11}} & rac{\Delta \mathbf{h}}{\mathbf{h}_{11}} \end{array} ight]$
T	$\begin{bmatrix} \frac{\mathbf{z}_{11}}{\mathbf{z}_{21}} & \frac{\Delta \mathbf{z}}{\mathbf{z}_{21}} \\ \frac{1}{\mathbf{z}_{21}} & \frac{\mathbf{z}_{22}}{\mathbf{z}_{21}} \end{bmatrix}$	$\left[\begin{array}{cc} \frac{-\mathbf{y}_{22}}{\mathbf{y}_{21}} & \frac{-1}{\mathbf{y}_{21}} \\ \frac{-\Delta\mathbf{y}}{\mathbf{y}_{21}} & \frac{-\mathbf{y}_{11}}{\mathbf{y}_{21}} \end{array}\right]$	$\left[\begin{array}{cc}\mathbf{A} & \mathbf{B} \\ \mathbf{C} & \mathbf{D}\end{array}\right]$	$\left[\begin{array}{cc} \frac{-\Delta \mathbf{h}}{\mathbf{h}_{21}} & \frac{-\mathbf{h}_{11}}{\mathbf{h}_{21}} \\ \frac{-\mathbf{h}_{22}}{\mathbf{h}_{21}} & \frac{-1}{\mathbf{h}_{21}} \end{array}\right]$
h	$\left[\begin{array}{ccc} \frac{\Delta \mathbf{z}}{\mathbf{z}_{22}} & \frac{\mathbf{z}_{12}}{\mathbf{z}_{22}} \\ -\frac{\mathbf{z}_{21}}{\mathbf{z}_{22}} & \frac{1}{\mathbf{z}_{22}} \end{array}\right]$	$\left[\begin{array}{cc} \frac{1}{\mathbf{y}_{11}} & \frac{-\mathbf{y}_{12}}{\mathbf{y}_{11}} \\ \frac{\mathbf{y}_{21}}{\mathbf{y}_{11}} & \frac{\Delta\mathbf{y}}{\mathbf{y}_{11}} \end{array}\right]$	$\left[\begin{array}{cc} \frac{\mathbf{B}}{\mathbf{D}} & \frac{\Delta \mathbf{T}}{\mathbf{D}} \\ -\frac{1}{\mathbf{D}} & \frac{\mathbf{C}}{\mathbf{D}} \end{array}\right]$	$\left[\begin{array}{cc}\mathbf{h}_{11}&\mathbf{h}_{12}\\\\\mathbf{h}_{21}&\mathbf{h}_{22}\end{array}\right]$

 $\Delta \mathbf{z} = \mathbf{z}_{11}\mathbf{z}_{22} - \mathbf{z}_{12}\mathbf{z}_{21}, \Delta \mathbf{y} = \mathbf{y}_{11}\mathbf{y}_{22} - \mathbf{y}_{12}\mathbf{y}_{21}, \Delta \mathbf{h} = \mathbf{h}_{11}\mathbf{h}_{22} - \mathbf{h}_{12}\mathbf{h}_{21}, \Delta \mathbf{T} = \mathbf{A}\mathbf{D} - \mathbf{B}\mathbf{C}$

Q. The following measurements were made of a linear passive two port network.

Fill in the blanks of the table.

Sl.no
$$V_1$$
 V_2 I_1 I_2 150100-12721005072432000--4--2005--1030

A. Using
$$V_1 = Z_{11} I_1 + Z_{12} I_2$$

$$V_2 = Z_{21} I_1 + Z_{22} I_2$$

$$\begin{bmatrix} -1 & 27 \\ 7 & 24 \end{bmatrix} \begin{bmatrix} Z_{11} & Z_{21} \\ Z_{12} & Z_{22} \end{bmatrix} = \begin{bmatrix} 50 & 100 \\ 100 & 50 \end{bmatrix}$$

$$\Rightarrow$$
 $Z_{11} = \frac{500}{71}$, $Z_{12} = \frac{150}{71}$, $Z_{21} = \frac{-350}{71}$, $Z_{22} = \frac{250}{71}$

Now, filling the table:

Sl. no 3:
$$I_1 = 20 A$$
, $I_2 = 28 A$

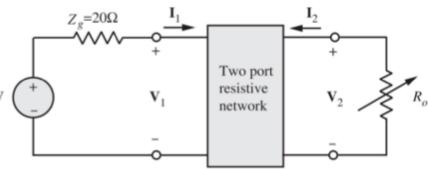
Sl. no 4: $V_1 = \frac{10000}{71} V$, $V_2 = -\frac{7000}{71} V$

Sl. no 5: $V_2 = \frac{9500}{71} V$, $V_3 = \frac{4000}{71} V$

a. The following measurements were done

on the circuit:

Determine the V_g=50V maximum power



dissipated across Ro.

Measurement 1	Measurement 2
$V_1 = 20 \text{ V}$	$V_1 = 35 \text{ V}$
$\mathbf{I}_1 = 0.8 \mathrm{A}$	$\mathbf{I}_1 = 1 \text{ A}$
$\mathbf{V}_2 = 0 \; \mathbf{V}$	$\mathbf{V}_2 = 15 \; \mathrm{V}$
$\mathbf{I}_2 = -0.4 \text{ A}$	$\mathbf{I}_2 = 0 \; \mathbf{A}$

Calculating the ABCD - parameters,

$$A = \frac{V_1}{V_2} \Big|_{I_2=0} = \frac{7}{3}, \quad B = \frac{V_1}{-I_2} \Big|_{V_2=0} = 50$$

$$C = \frac{I_1}{V_2}\Big|_{I_2=0} = \frac{1}{15}$$
, $D = \frac{I_1}{-I_2}\Big|_{V_2=0} = 2$

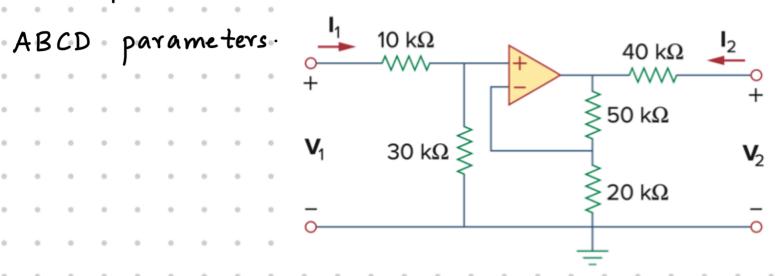
We know,

$$V_{TH} = \frac{V_g}{A + C \neq g} = \frac{50}{\frac{7}{3} + \frac{1}{15} \cdot 20} = \frac{150}{11}$$

$$Z_{TH} = \frac{B + D Z_g}{A + C Z_g} = \frac{50 + 2 \cdot 20}{\frac{7}{3} + \frac{1}{15} \cdot 20} = \frac{270}{11}$$

Hence,
$$P_{\text{max}} = \frac{V_{TH}^2}{4 Z_{TH}} \approx 1.89 W$$

Q. For the circuit shown below, calculate Z-parameters and then convert them to



Writing the KVL equations,

$$V_1 = (10 + 30) k\Omega \times I_1$$

$$V_2 = (40 \text{ kg}) I_2 + (50 + 20) \text{ kg} . 3 V_1$$

$$\Rightarrow V_2 = (105 \text{ kg}) I_1 + (40 \text{ kg}) I_2$$

Hence,
$$\begin{bmatrix} 2 \end{bmatrix} = \begin{bmatrix} 40 & 0 \\ 105 & 40 \end{bmatrix} k \Sigma$$

Converting them into ABCD parameters:

$$\begin{bmatrix} ABCD \end{bmatrix} = \begin{bmatrix} \frac{Z_{11}}{Z_{21}} & \frac{\Delta_{z}}{Z_{21}} \\ \frac{1}{Z_{21}} & \frac{Z_{22}}{Z_{21}} \end{bmatrix} = \begin{bmatrix} 0.38 & 15.24 \text{ k}\Omega \\ 9.52 \text{ m}\Omega^{1} & 0.38 \end{bmatrix}$$