

Characterizing Outburst with Microseismic Amplitude Versus Angle Analysis

Eugene Morgan¹, Cai-Ping Lu²

¹John and Willie Leone Family Department of Energy and Mineral Engineering, The Pennsylvania State University

²State Key Laboratory of Coal Resources and Safe Mining, China University of Mining and Technology

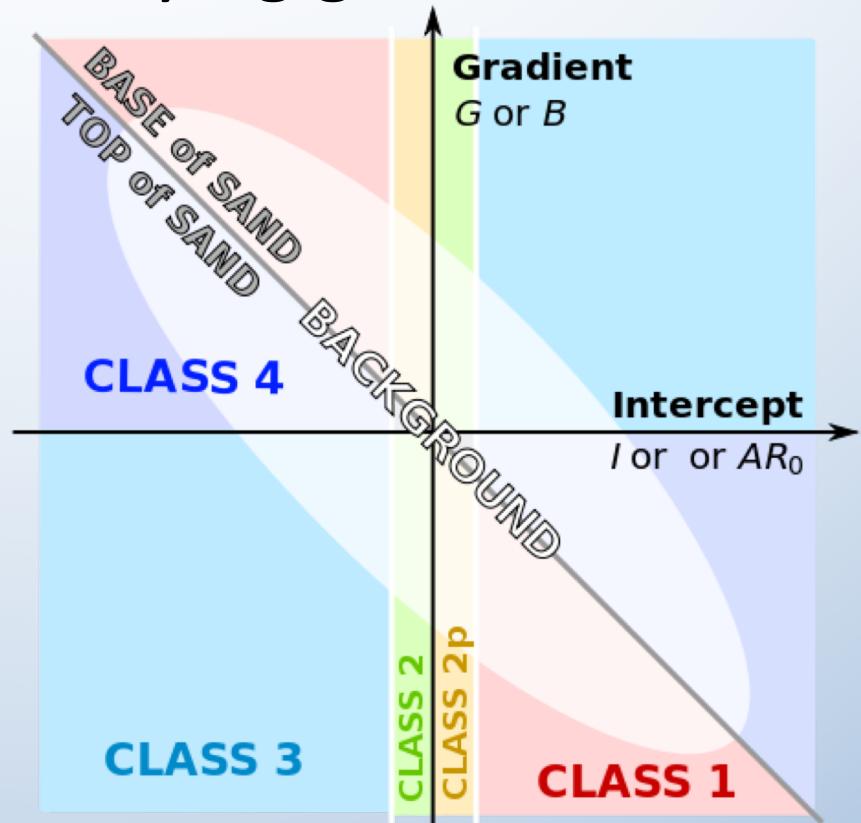
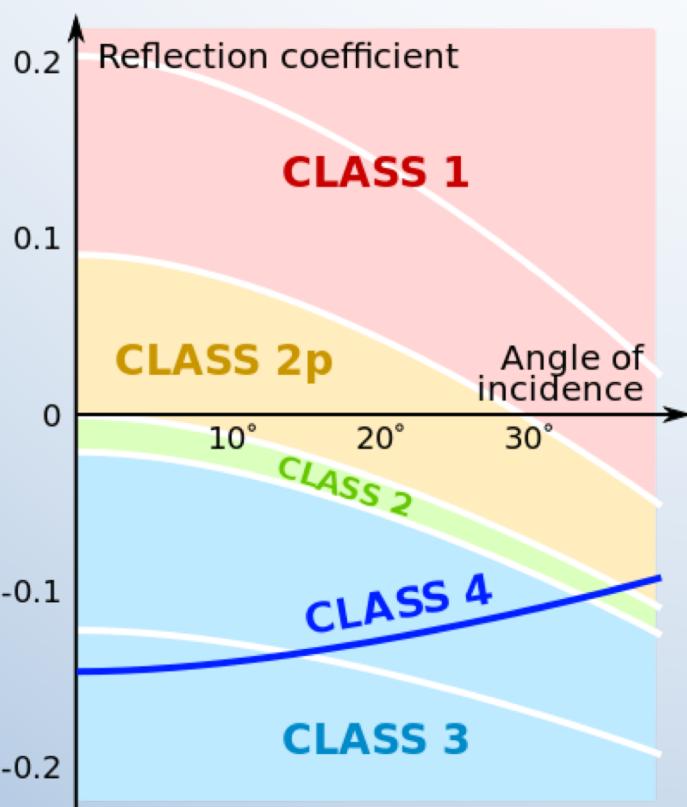


8th International Symposium on Green Mining
China University of Mining and Technology
Xuzhou, China, April 26-28, 2015



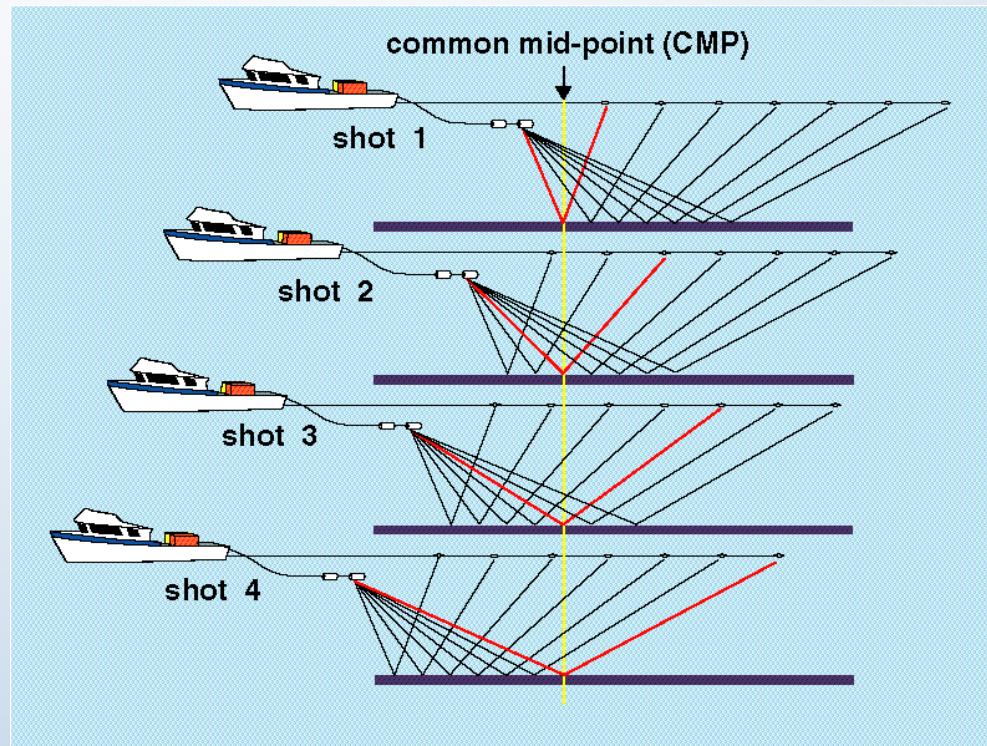
Introduction

- Amplitude Variation with Offset/Angle (AVO/AVA) analysis is a popular technique with seismic surveys for classifying gas reservoirs



Objective

- Can MS amplitude variation with angle separating sensor from source (rockburst or gas outburst) give us information about the hazardous layer?
- Can the reflection-based methods be translated for transmission waves?



Simplification of Zoeppritz Equations

Reflection Coefficient:

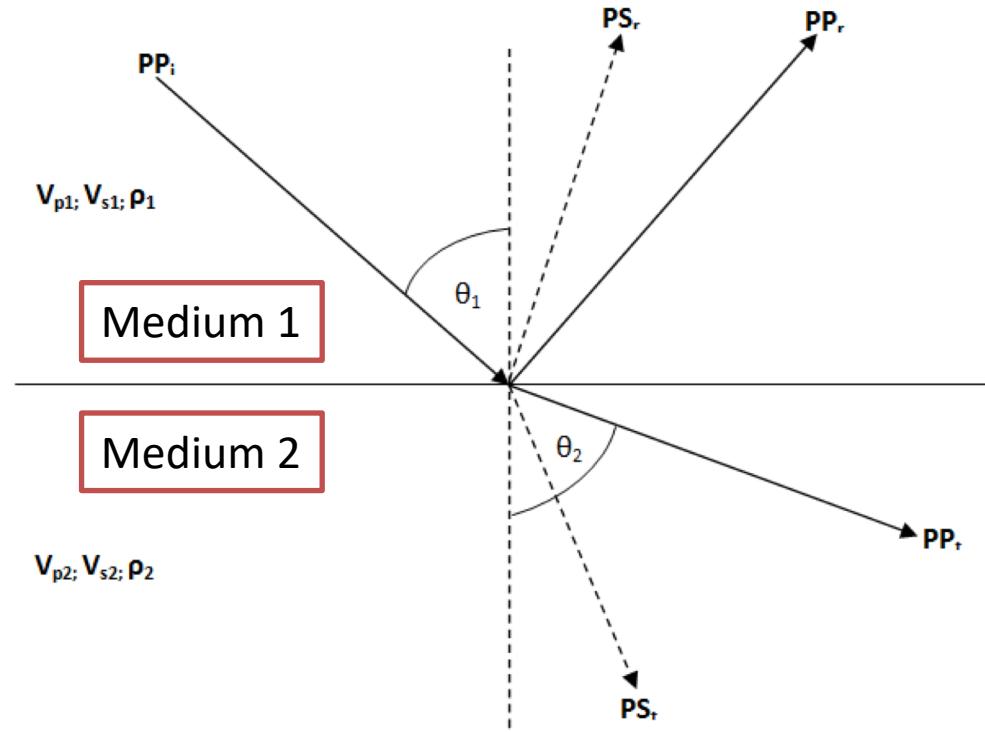
$$R_{12} = \frac{A_r}{A_i} = \frac{I_1 - I_2}{I_2 + I_1} = \frac{\rho_1 V_1 - \rho_2 V_2}{\rho_2 V_2 + \rho_1 V_1}$$

Transmission Coefficient:

$$T_{12} = \frac{A_t}{A_i} = \frac{2I_1}{I_2 + I_1} = \frac{2\rho_1 V_1}{\rho_2 V_2 + \rho_1 V_1}$$

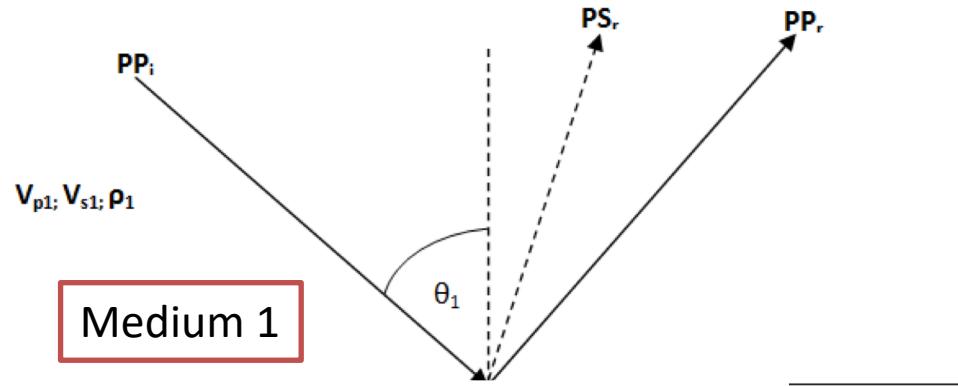
Ray Parameter (Snell's Law):

$$p = \frac{\sin \theta_1}{V_{P1}} = \frac{\sin \theta_2}{V_{P2}} = \frac{\sin \theta_{S1}}{V_{S1}} = \frac{\sin \theta_{S2}}{V_{S2}}$$



Simplification of Zoeppritz Equations

$$\begin{pmatrix} \text{PP} & \text{SP} & \text{PP} & \text{SP} \\ \text{PS} & \text{SS} & \text{PS} & \text{SS} \\ \text{PP} & \text{SP} & \text{PP} & \text{SP} \\ \text{PS} & \text{SP} & \text{PS} & \text{SP} \end{pmatrix} = \mathbf{M}^{-1} \mathbf{N}$$



$$\mathbf{M} = \begin{pmatrix} -\sin \theta_1 & -\cos \theta_{S1} & \sin \theta_2 & \cos \theta_{S2} \\ \cos \theta_1 & -\sin \theta_{S1} & \cos \theta_2 & -\sin \theta_{S2} \\ 2\rho_1 V_{S1} \sin \theta_{S1} \cos \theta_1 & \rho_1 V_{S1} (1 - 2 \sin^2 \theta_{S1}) & 2\rho_2 V_{S2} \sin \theta_{S2} \cos \theta_2 & \rho_2 V_{S2} (1 - 2 \sin^2 \theta_{S2}) \\ -\rho_1 V_{P1} (1 - 2 \sin^2 \theta_{S1}) & \rho_1 V_{S1} \sin 2\theta_{S1} & \rho_2 V_{P2} (1 - 2 \sin^2 \theta_{S2}) & -\rho_2 V_{S2} \sin 2\theta_{S2} \end{pmatrix}$$

$$\mathbf{N} = \begin{pmatrix} \sin \theta_1 & \cos \theta_{S1} & -\sin \theta_2 & -\cos \theta_{S2} \\ \cos \theta_1 & -\sin \theta_{S1} & \cos \theta_2 & -\sin \theta_{S2} \\ 2\rho_1 V_{S1} \sin \theta_{S1} \cos \theta_1 & \rho_1 V_{S1} (1 - 2 \sin^2 \theta_{S1}) & 2\rho_2 V_{S2} \sin \theta_{S2} \cos \theta_2 & \rho_2 V_{S2} (1 - 2 \sin^2 \theta_{S2}) \\ \rho_1 V_{P1} (1 - 2 \sin^2 \theta_{S1}) & -\rho_1 V_{S1} \sin 2\theta_{S1} & -\rho_2 V_{P2} (1 - 2 \sin^2 \theta_{S2}) & \rho_2 V_{S2} \sin 2\theta_{S2} \end{pmatrix}$$

Shuey's Approximation

$$R(\theta) \approx R(0) + G \sin^2 \theta$$

$$\theta = (\theta_1 + \theta_2)/2 \approx \theta_1$$

$$R(0) = \frac{1}{2} \left(\frac{\Delta V_p}{V_p} + \frac{\Delta \rho}{\rho} \right)$$

$$G = \frac{1}{2} \frac{\Delta V_p}{V_p} - 2 \frac{V_s^2}{V_p^2} \left(\frac{\Delta \rho}{\rho} + 2 \frac{\Delta V_s}{V_s} \right)$$

$$= R(0) - \frac{\Delta \rho}{\rho} \left(\frac{1}{2} + 2 \frac{V_s^2}{V_p^2} \right) - 4 \frac{V_s^2}{V_p^2} \frac{\Delta V_s}{V_s}$$

Normal-incidence reflection coefficient:

- controlled by impedance contrast

Reflection at intermediate angles between normal and critical angle:

- controlled by impedance & Poisson's ratio

$$\Delta \rho = \rho_2 - \rho_1$$

$$\rho = (\rho_2 + \rho_1)/2$$

$$\Delta V_p = V_{p2} - V_{p1}$$

$$V_p = (V_{p2} + V_{p1})/2$$

$$\Delta V_s = V_{s2} - V_{s1}$$

$$V_s = (V_{s2} + V_{s1})/2$$

This linear relationship is typically fit via Least Squares

For Transmitted P-Wave...

$$\begin{aligned} T(\theta) &= 1 - \frac{1}{2} \frac{\Delta\rho}{\rho} + \left(\frac{1}{2 \cos^2 \theta} - 1 \right) \frac{\Delta V_p}{V_p} \\ &= 1 - \left[\frac{1}{2} \left(\frac{\Delta\rho}{\rho} + \frac{\Delta V_p}{V_p} \right) \right] + \frac{1}{2} \frac{\Delta V_p}{V_p} \left(\frac{1}{\cos^2 \theta} - 1 \right) \\ &\approx \frac{2I_1}{I_2 + I_1} + \frac{V_{p2} - V_{p1}}{V_{p2} + V_{p1}} \left(\frac{1}{\cos^2 \theta} - 1 \right) \end{aligned}$$

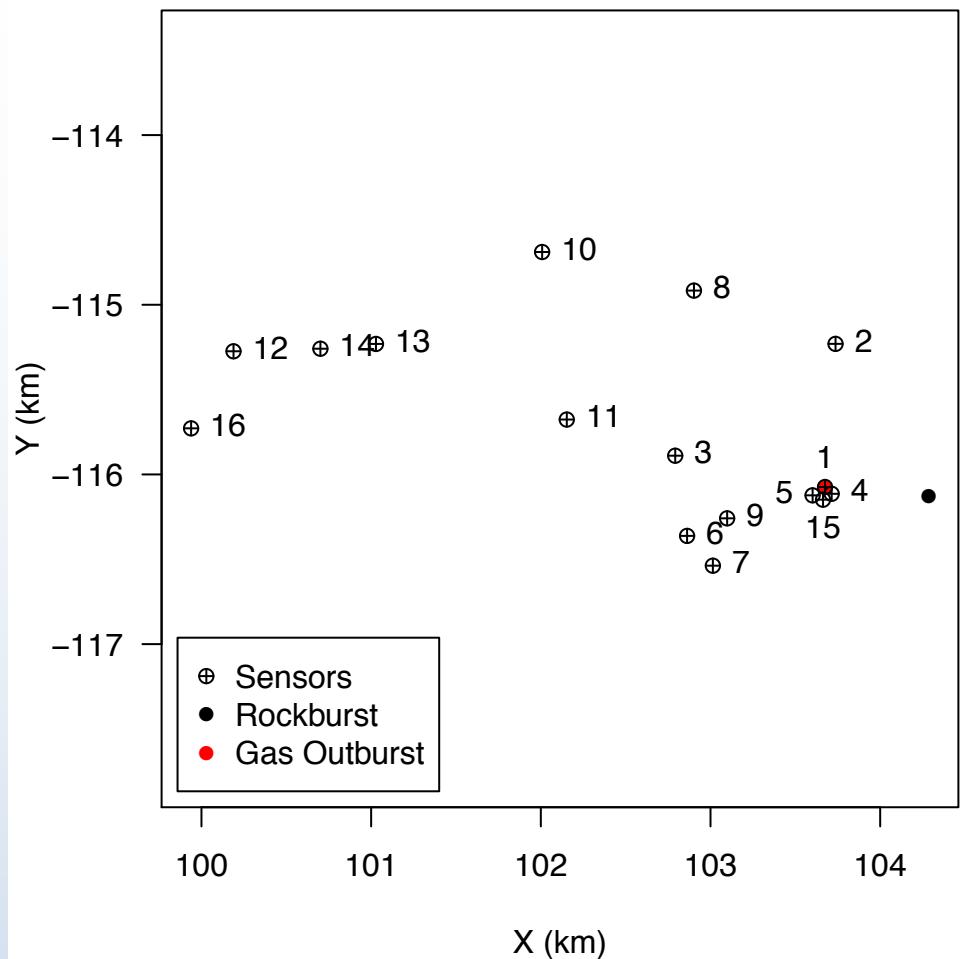
Intercept

Slope

Independent
Variable

MS Dataset

- 16 MS Sensors placed in mine
- Junde coal mine, Nov 24, 2012:
 - Rockburst at 18:24
 - Gas outburst at 20:28

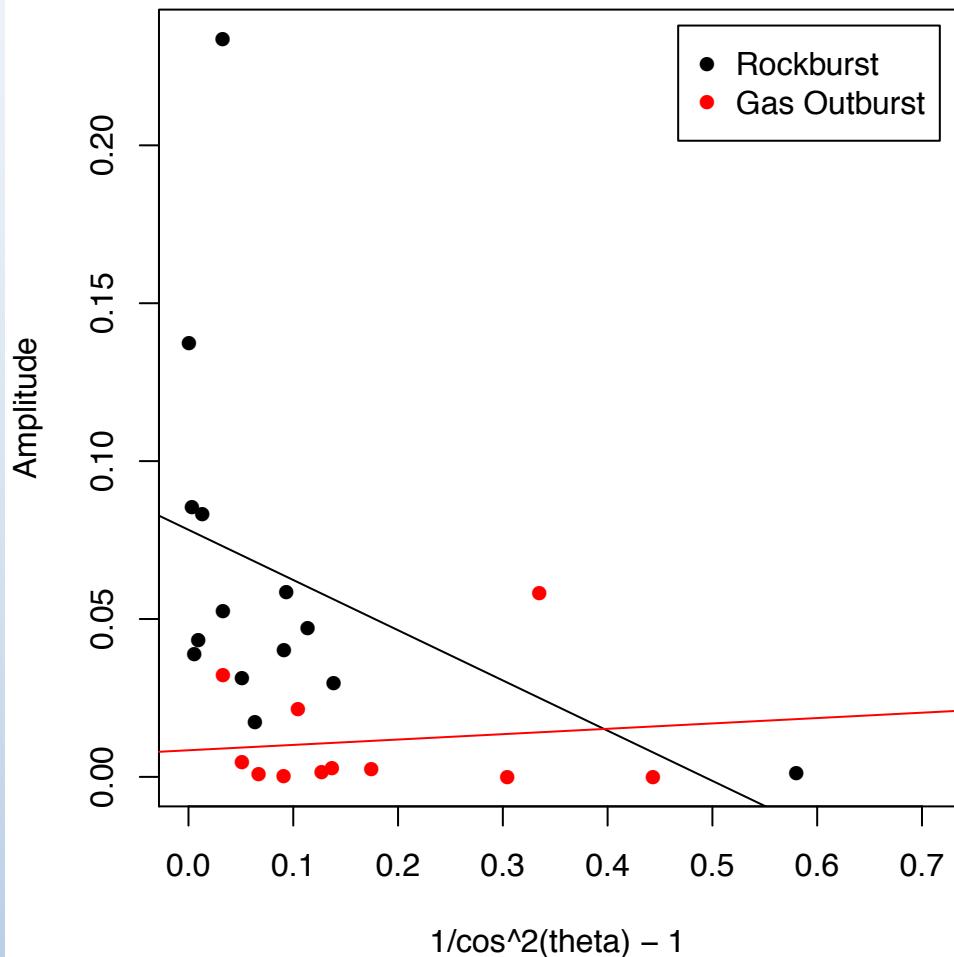


Lu, C.-P., Dou, L.-M., Zhang, N., Xue, J.-H., & Liu, G.-J. (2014). Microseismic and acoustic emission effect on gas outburst hazard triggered by shock wave: a case study. *Natural Hazards*, 73(3), 1715–1731.
doi:10.1007/s11069-014-1167-7

Some Assumptions

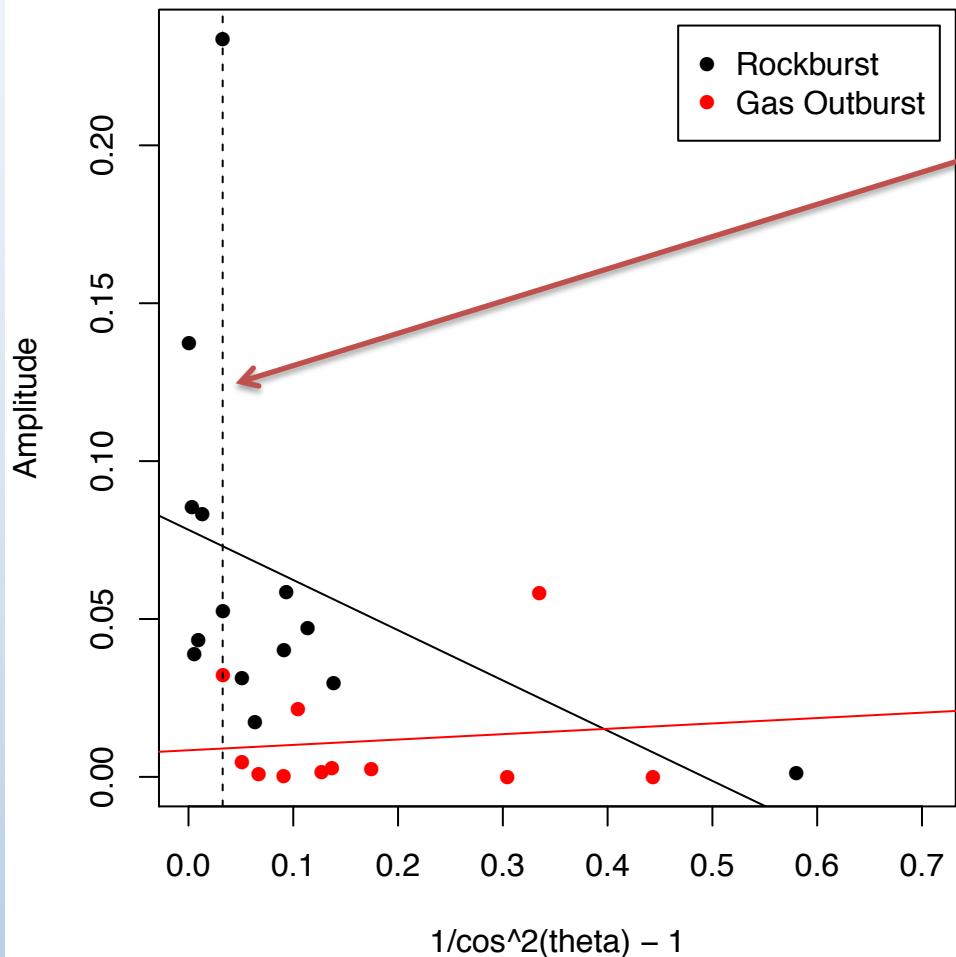
- Max. amplitude is associated with transmitted P-wave
- Coal and surrounding rock are each homogeneous and isotropic
- Critical angle = 40° : sensors outside of this omitted
- Variation in angle with respect to vertical direction is negligible
- Spherical divergence correction

Peak Amplitude vs. Angle



- **Rockburst:**
 - Significant negative slope:
 - V_p of rockburst layer greater than V_p of surrounding rock
 - Larger intercept:
 - Greater impedance of rockburst layer
- **Gas outburst:**
 - Slight positive slope
 - Slightly greater V_p of surrounding rock
 - Small intercept
 - Gas outburst in lower impedance layer

Directivity



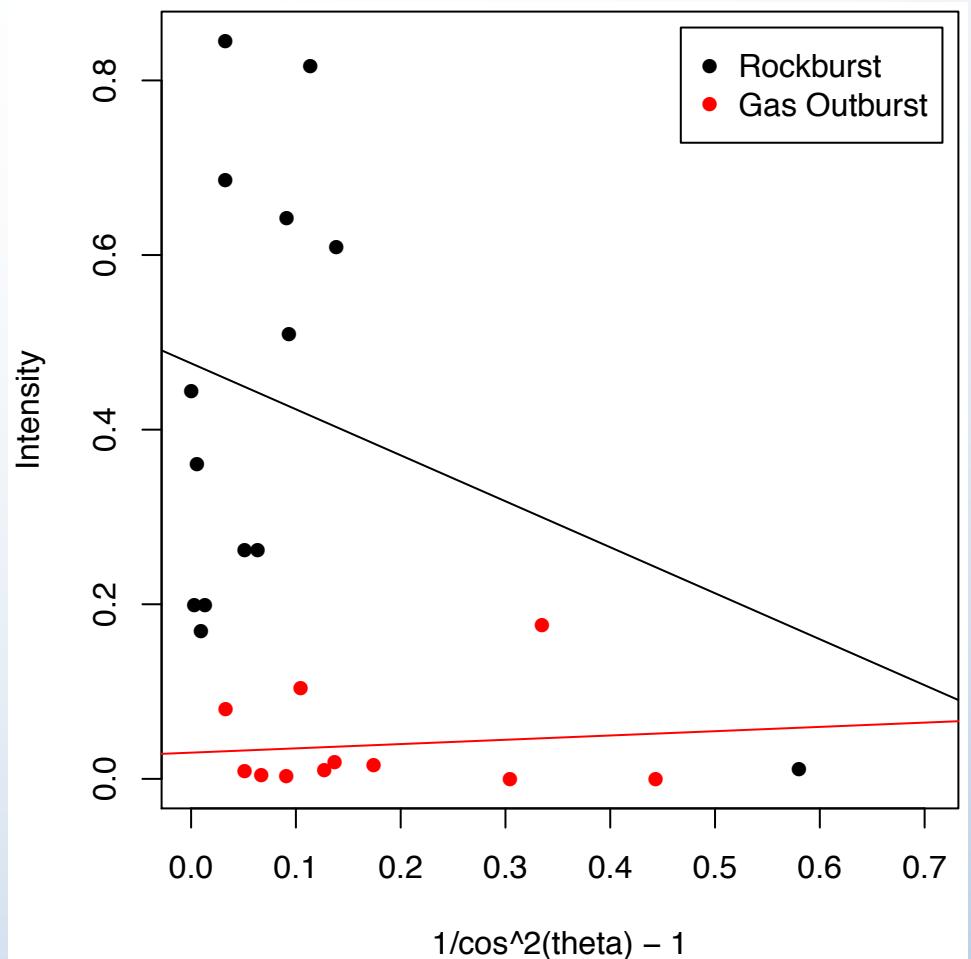
- Angle of gas outburst source from rockburst source coincides with largest rockburst amplitude
- Rockburst directs energy coaxially
- Gas outburst is isotropic

Intensity

- Calculated as:

$$\int_{0.1 \text{ Hz}}^{250 \text{ Hz}} A(f) df$$

- Implies same directivity effect



Conclusions

- Can simplify Zoeppritz equations to get transmission coefficient in linear form
 - Angle is independent variable
 - Slope is function of Vp
 - Intercept is function of Vp and density (impedance)
- AVA analysis can tell us properties of rock/gas outburst layers
 - Measure angle between MS sensors and sources
 - Pick amplitude from MS time series
- Directivity effect in rockburst may inform about location of gas outburst in future
 - Gives an indication of redistributed stresses

Thank you! Xie Xie!

Questions?