Unmanned Aerial Systems

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1 Introduction

The Unmanned Aerial System (UAS) Challenge was launched by the Institution of Mechanical Engineers (IMechE) in 2014 'with the key objectives of developing professional engineers and inspiring the next generation'[2]. The main goal is to design and build a UAS in order to autonomously deliver humanitarian aid such as medical supplies in a disaster zone. This requires a broad range of skills, from project management to airframe design to avionics system programming. To add to the challenge there is a strict weight limit and stringent safety regulations. Working together with another student, Ismail Ahmad, our goal is to follow the design and build cycle all the way through to competing at the IMechE UAS competition in June 2018.

One of the greatest individual challenges as part of the project is creating an autonomous flight system. The UAS must be capable of quickly and safely navigating to and locating a target using computer vision, dropping a payload accurately, and returning to base. This requires an understanding of the UASs flight dynamics as well as good programming and wiring capabilities. This is the aspect that I will be focusing on for my individual project, although I will be assisting with many parts of the project.

2 Design

2.1 Concept

The concept for our UAS uses a hybrid symbioisis between a *Micro Jet Engine*, henceforth refered to as MJE, and an external multi-rotor. The MJE is gimballed to always remain vertical and only provides lift, while the multirotor rotates around it providing stabilisation and control. This configuration means that standard quadcopter flight control software can be used rather than needing to come up with custom architecture.

The MJE provides a higher thrust to weight ratio than the equivalent electric motors and batteries (see Appendix C). It does this without introducing the vibration issues of a piston engine, which would seriously impact stability and control on such a lightweight design. With the current MJE and electric motors we hope to lift a payload of 3kg while remaining under the 6.9kg weight limit.

Flight control will be handled with a Pixhawk running the PX4 flight stack. This will be coupled to a companion computer running software based on the DroneKit SDK, communicating with the PixHawk using the MAVLink protocol. The companion computer is responsible for communication, waypoint navigation, and target location and tracking using computer vision. It then communicates where to go to the PixHawk.

3 Simulation: System Plausibility

3.1 Concept

One of the main concepts behind the UAS concept is the idea that, if the MJE is gimballed to remain vertical, and its thrust vector is through the center of gravity of the vehicle, it exerts no horizontal forces or moments on the rest of the vehicle. This means its effect on the stability and control of the vehicle can be ignored. In turn, this means that regular quadcopter flight control software can be used, such as the PX4 flight stack.

Being able to use PX4 firmware running on a Pixhawk is crucial. The UAS will come to cost approximately £2,500. Using home-made flight control software is therefore extremely risky. PX4, on the other hand, is a project that has been worked on by thousands of people for years, and is infinitely more reliable than anything we could put together from scratch.

Therefore, it was decided to build a simulation to test the validity of the concept that the MJE can be ignored.

3.2 Equations of Motion

The vehicle is split into two sections, the outer quadcopter frame, Quad, and the gimballed section containing the MJE, Jet. A cartesian reference frame was chosen, with the xy plane being the horizontal plane and z being height. +x is right, +y is forward, +z is up. A rotation about the x axis is pitch, about the y axis is roll, and about the z axis is yaw. These are labelled θ_x, θ_y , and θ_z for the quad and ϕ_x, ϕ_y , and ϕ_z for the jet respectively.

The gimbal is controlled by two servos, one moving the gimbal in roll and one in pitch. (There is no need for yaw control of the jet.) Note that this means $\theta_z = \phi_z$.

The multirotor uses the 'quad-x' configuration, as shown below. Note that motors 1 and 3 spin clockwise, and motors 2 and 4 spin anticlockwise.

3.2.1 Forces

Our gimbal design will transmit forces, but not moments. Thus, from a forces perspective, the vehicle is treated as a single unit. The total mass is

$$M_{TOT} = \underbrace{\rho \pi h(r_2 - r_1)}_{Frame} + 4 \cdot \underbrace{\rho \pi L r_r^2}_{Rods} + 4 \cdot \underbrace{M_M}_{Motors} + 2 \cdot \underbrace{M_G}_{Servos} + \underbrace{M_J}_{Jet}$$
 (1)

The forces acting on the system are:

$$F_x = (F_{M1} + F_{M2} + F_{M3} + F_{M4}) \cdot \sin \theta_x \cdot \cos \theta_z + F_J \cdot \sin \phi_x \cdot \cos \phi_z \tag{2}$$

$$F_y = (F_{M1} + F_{M2} + F_{M3} + F_{M4}) \cdot \sin \theta_y \cdot \cos \theta_z + F_J \cdot \sin \phi_y \cdot \cos \phi_z \tag{3}$$

$$F_z = (F_{M1} + F_{M2} + F_{M3} + F_{M4}) \cdot \cos \theta_x \cdot \cos \theta_y + F_J \cdot \cos \phi_x \cdot \cos \phi_y \tag{4}$$

3.2.2 Quad Rotation

The quad is modeled as an inner thin, hollow cylinder, the *frame*, with four cyclindrical rods, the *arms*, extending outwards. The motors are point masses on the ends of the arms. It is assumed to be constructed of aircraft-grade aluminium. This results in the following inertias about the three defined axes:

$$I_{Qx} = I_{Qy} = \underbrace{\frac{\pi \rho h_F}{12} (3(r_2^4 - r_1^4) + h_F^2(r_2^2 - r_1^2))}_{Frame} + 4 \cdot \sin 45 \cdot (\frac{M_R L_R^2}{12} + M_R(r_2 + \frac{L_R}{2})^2)$$

$$+ 4 \cdot \sin 45 \cdot M_M(r_2 + L)^2$$

$$Motors$$

$$I_{Qz} = \underbrace{\frac{\pi \rho h_F}{2} (r_2^4 - r_1^4)}_{Frame} + 4 \cdot \underbrace{\frac{M_R L_R^2}{12} + M_R(r_2 + \frac{L_R}{2})^2}_{Rods}$$

$$+ 4 \cdot \underbrace{M_M(r_2 + L)^2}_{Motors}$$

$$(5)$$

On the quad, the gimbal servos exert offset moments about the z-axis. This results in the following equations:

$$\tau_{Ox} = (-F_{M1} - F_{M2} + F_{M3} + F_{M4}) \cdot (L_R + r_2) \cdot \cos 45 \quad (7)$$

$$\tau_{Ou} = (F_{M1} - F_{M2} - F_{M3} + F_{M4}) \cdot (L_R + r_2) \cdot \cos 45 \quad (8)$$

$$\tau_{Qz} = (F_{M1} - F_{M2} + F_{M3} - F_{M4}) \cdot (L_R + r_2) \cdot \cos 45 + \tau_{Gx} \cdot r_1 + \tau_{Gy} \cdot r_1 \quad (9)$$

3.2.3 Jet Rotation

Since $\theta_z = \phi_z$, we are only interested in the rotation of the jet about the x and y axes. Since there is a rigid linkage between the servo and the gimbal, the position of the servo is proportional to the rotation of the jet.

The jet is modelled as a cylinder. However, it does not rotate about its origin in x and y, but about the appropriate servo. Including the inertia of the servos themselves (see Appendix B) results in the following inertias:

$$I_{Jx} = I_{Jy} = 3.89 \times 10^{-4} + M_J \cdot 3r_J^2 + h_J^2 + M_J l_c^2$$
 (10)

We know from Appendix B the maximum torque the servo can exert is 0.34 kg-m. The actual torque exerted is controlled by a PID controller in order to keep the jet vertical.

3.3 PID Control

8 PID controllers are needed in total: 3 position and 3 angle controllers for the quad, and 2 angle controllers for the jet gimbal. These controllers use the standard PID control logic:

$$error = setpoint - actual\ value$$

$$integral = integral + (error \times time\ period)$$

$$derivative = (error - previous\ error)/time$$

$$output = kP \times error + kI \times integral + kD \times derivative$$

where kP, kI, and kD are constants to be optimised.

3.3.1 Quad Control

In a real quadcopter, the controller sends a signal to an *electronic speed control* (ESC), which in turn sends a *pulse width modulation* (PWM) signal to the motor, controlling its speed. In this model this has been simplified, such that the controller output directly controls the force exerted by the motors.

SP_x	Quad X position controller setpoint
SP_y	Quad Y position controller setpoint
SP_z	Quad Z position controller setpoint
SP_{θ_x}	Quad X angle controller setpoint
SP_{θ_y}	Quad Y angle controller setpoint
SP_{θ_z}	Quad Z angle controller setpoint
O_x	Quad X position controller output
O_y	Quad Y position controller output
O_z	Quad Z position controller output
O_{θ_x}	Quad X angle controller output
O_{θ_u}	Quad Y angle controller output
O_{θ_z}	Quad Z angle controller output

The controllers work in sequence, with the x and y position controllers determing the setpoint of the x and y angle controllers. The Z axis controller is independent.

$$\begin{aligned} O_x &= SP_{\theta_x} \\ O_y &= SP_{\theta_y} \\ F_{M1} &= O_z - O_{\theta_x} + O_{\theta_y} + O_{\theta_z} \\ F_{M2} &= O_z - O_{\theta_x} - O_{\theta_y} - O_{\theta_z} \\ F_{M3} &= O_z + O_{\theta_x} - O_{\theta_y} + O_{\theta_z} \\ F_{M4} &= O_z + O_{\theta_x} + O_{\theta_y} - O_{\theta_z} \end{aligned} \tag{13}$$

3.3.2 Jet Gimbal Control

Servos are controlled by sending an electronic signal to tell them what position to rotate to.

 SP_{ϕ_x} Jet X angle controller setpoint SP_{ϕ_y} Jet Y angle controller setpoint O_{ϕ_x} Jet X angle controller output O_{ϕ_x} Jet Y angle controller output

$$\tau_{Jx} = O_{\phi x} \tag{15}$$

$$\tau_{Jy} = O_{\phi y} \tag{16}$$

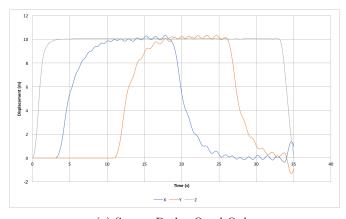
3.4 Programming

The simulation itself was written in Processing. This is a language originally based on Java that is designed for ease of programming, especially with regards to displaying graphical elements. It was chosen over using MATLAB due to the author's increased familiarity with it, and the fact that this simulation has no need of advanced mathematical capability - there are no complex differential equations or matrix operations.

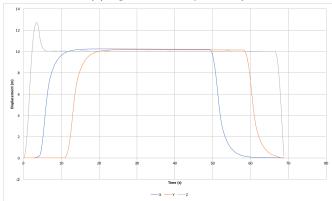
The program was built up in stages, with the physics of each stage checked before adding complexity. As far as possible, good object-oriented programming practice has been followed.

The quad section was implemented first. A controller was first tested solely in the z direction, and the response was used to calibrate PID values for the z controller. Angular controllers were then implemented, tested, and calibrated, before finally introducing x and y position controllers.

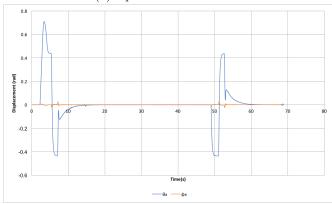
Testing involved flying a simple path: takeoff to 10m, a square path (10m north, 10m east, 10m south, 10m west), and then landing. This gave the results seen in Figure 1a. It can be seen that there is an oscilliation in x and y position. It proved difficult to eliminate, due to the not straightforward interaction of position and angle PID values. This, however proved not to be a problem. It can be seen in Figure 1b that the addition of the jet has, likely due to the added mass, damped out the oscillations in x and y position. It has also added an overshoot in z and a steady state error in x and y, but this can be corrected by fine-tuning of PID values. The flight time has also increased but this is to be expected with greater mass. In Figure 1c we can see how the quadcopter changes angle about the x axis, and how the jet initially starts to move in that direction but is quickly brought back to the vertical by the servo.







(b) Square Path - With Jet



(c) Square Path - With Jet

Figure 1

3.5 Refiment

It was realised that the mass of the quad had been implemented incorrectly (r_r had not been squared and the rod mass and motor mass had not been multiplied by 4 in equation 1). Additionally, the maximum torque of the servo had not been limited to $0.34 \mathrm{kgm}$.

These refiments decreased the stability of the drone. It is still well within acceptable parameters for rotation, and for x and y positioning, but height now has considerable steady state error and oscillation.

With sufficient PID tuning, height could be stabilised, but not without a massive initial overshoot, and slightly increasing instability in x and y. This is because as the proportion of motor control that comes from height control increases (due to increasing k_p and k_i terms), the proportion of motor control left available for the other controllers decreases.

3.6 Conclusion

It can be seen that the addition of a gimballed jet to a quadcopter does not destabilise it. The extremely simple PID controllers used in our simulation are able to cope without any difficulty, implying that a significantly more advanced flight stack such as the PX4 should have no problems. Our initial assumption that the jet can simply be ignored is, indeed, valid.

4 Simulation: Control Software

We will be controlling the PixHawk flight controller using offboard commands from an external companion computer, henceforth refered to as Pete (since CC is a rather ambigous acronym). Pete will consist of three main components: communication with the PixHawk, communication with a ground station, and target-finding computer vision.

PX4 is fully capable of Software-in-the-Loop (SITL) simulation, using either the jMAVSim or Gazebo environments. This is crucial, as it allows code to be tested with no danger to the real vehicle. Pete can commicate with the simulated vehicle using MAVLink through a UDP port; this is exactly the same as how it would connect to a real vehicle. As far as Pete's code is concerned, there is no difference between a real and a simulated vehicle except for the UDP address.

4.1 PX4 Control

Communication with the PX4 flight stack on the PixHawk is based on the DroneKit SDK. This is a platform for devoloping apps written in Python that run on a drone's companion computer. It communicates with the PixHawk using the MAVLink communication protocol.[6] The DroneCore API was also experimented with but proved significantly harder to implement and hence was abandoned.

PX4 has 12 flight modes when employed on a multirotor. We are interested in the autonomous modes, which include Hold, Return(RTL), Takeoff, Land, Mission, Follow Me, and Offboard. Of particular interest are Mission, in which 'the vehicle follows a programmed mission', and Offboard, where 'the vehicle obeys a position, velocity or attitude setpoint provided over MAVLink'.[4]

4.1.1 Implementation

The available documentation and examples for DroneKit mostly make use of the simple_goto() command. Unfortunately, as DroneKit is primarily designed to work with APM, the predecessor of PX4, this command does not work. Neither does arm_and_takeoff(), or the vehicle.groundspeed and vehicle.airspeed attributes, among others.

Additionally, it is usually assumed that one is operating in the <code>global_relative_frame</code> . There are three frames of reference available:

```
global_frame GPS coordinates, with 0 altitude at sea level
global_relative_frame GPS coordinates, with 0 altitude as ground level at the starting location
local_frame Cartesian coordinates relative to the starting location
```

local_frame is the most immediately useful to us, as it is simpler and more intuitive to use. Note that this is the North East Down (NED) frame, i.e. -10m altitude is 10m above the ground.

Custom code has had to be written to take the place of these defunct commands and allow the vehicle to be controlled in the desired manner. First of all, we want to be able to directly send a position waypoint to PX4. This is a feature that is not fully implemented in DroneKit, and so a custom command with a custom MAVLink message has been created:

```
def send_ned_position(pos_x, pos_y, pos_z):
       Move vehicle in direction based on specified velocity vectors.
       msg = vehicle.message_factory.
6
       set_position_target_local_ned_encode(
                    # time_boot_ms (not used)
           0,
                    # target system, target component
           mavutil.mavlink.MAV_FRAME_LOCAL_NED, # frame
9
           0\,b\,00\,00\,11\,11\,11\,11\,11\,10\,00\,,\ \#\ type\_mask
           pos_x, pos_y, pos_z, \# x, y, z positions
           0\,,~0\,,~0\,,~\# x, y, z velocity in m/s
           0, 0, 0, \# x, y, z acceleration (not supported yet)
13
                    # yaw, yaw_rate (not supported yet)
14
           (0, 0)
       vehicle.send_mavlink(msg)
```

Similarly, other commands have been created to suit our purposes. Some of these have been adapted from examples in the DroneKit and PX4 documentation.[6][5]

```
def arm_and_takeoff(targetAlt, accuracy=0.5):
```

```
wp = get_location_offset_meters(home, 0, 0, targetAlt)
2
      cmds.add(PX4Command(wp, "TO"))
3
      cmds.upload()
4
      time.sleep(1)
5
6
      vehicle.mode = VehicleMode("MISSION")
7
      time.sleep(1)
      print ("Vehicle mode should be MISSION: %s" % vehicle.mode.name)
9
      vehicle.armed = True
10
      while True:
          print " Altitude: ", vehicle.location.global_relative_frame
12
      .alt
          #Break and return from function just below target altitude.
          if vehicle.location.global_relative_frame.alt>=targetAlt-
14
      accuracy:
               print "Reached target altitude"
15
16
               break
          time.sleep(1)
17
18
  19
  # Go to a position relative to the home position
20
21
      targetLocation = LocationLocal(pos_x, pos_y, -pos_z)
22
23
      send_ned_position(pos_x, pos_y, -pos_z)
24
      vehicle.mode = VehicleMode("OFFBOARD")
25
      print ("Vehicle mode should be OFFBOARD: %s" % vehicle.mode.name
26
27
      while True:
28
          send_ned_position(pos_x, pos_y, -pos_z)
29
          remainingDistance = get_distance_metres_local(vehicle.
30
      location.local_frame, targetLocation)
31
          if remainingDistance<=accuracy:</pre>
               print("Arrived at target")
32
               break
33
          print "Distance to target: ", remainingDistance
34
35
          time.sleep(0.1)
36
37
  def goto_relative(pos_x, pos_y, pos_z, accuracy=0.5):
  # Go to a position relative to the current posotion
38
39
40
      currentLocation = vehicle.location.local_frame
      targetLocation = get_location_metres_local(currentLocation,
41
      pos_x, pos_y, -pos_z)
42
      send_ned_position(targetLocation.north, targetLocation.east,
43
      targetLocation.down)
      vehicle.mode = VehicleMode("OFFBOARD")
44
      print ("Vehicle mode should be OFFBOARD: %s" % vehicle.mode.name
45
46
47
      while True:
          send_ned_position(targetLocation.north, targetLocation.east
48
       targetLocation.down)
          remainingDistance = get_distance_metres_local(vehicle.
49
      location.local_frame , targetLocation)
```

```
if remaining Distance <= accuracy:
                print("Arrived at target")
               break
           print "Distance to target: ", remainingDistance
53
           time.sleep(0.1)
54
56
      setMaxXYSpeed(speed):
       vehicle.parameters['MPC_XY_VEL_MAX']=speed
       print ("Set max speed to: %s" % vehicle.parameters ['
      MPC_XY_VEL_MAX'])
59
       time.sleep(0.5)
60
  def returnToLand():
61
       vehicle.mode = VehicleMode("RTL")
       time.sleep(1)
63
       print ("Vehicle mode should be RTL: %s" % vehicle .mode.name)
64
       while vehicle.armed == True:
           print ("Waiting for landing ...")
66
           time.sleep(3)
```

arm_and_takeoff() replaces the command provided in DroneKit, and performs the same function. goto_absolute() and goto_relative() allow us to navigate to a position waypoint, simply defined as X meters north, Y meters east, and Z meters up from either the starting location or the current location. The accuracy attribute optionally allows us to change how close the vehicle must get to the waypoint to consider it to have reached it. setMaxXYSpeed() is a replacement for the vehicle groundspeed attribute present in DroneKit, which does not work as intended with PX4, and allows us to set a maximum groundspeed for the vehicle. Finally, returnToLand() has the vehicle return to it's starting location and land safely.

Altogether, this means that the communication with the PixHawk has been simplified down to a few basic commands. An example mission could consist of the following: arming and taking off, following a series of GPS coordinates, locating a target using computer vision, calculating it's offset from directly underneath the drone, using <code>goto_relative()</code> to position itself precisely over the target, droping the payload, and returning to base and landing.

5 Computer Vision

The last component of the control system is a comouter vision system capable of identifying the target. This takes the form of a red 1x1m square, incoporating an alphanumeric code in white, within a larger 2x2m white square[3]. The system would have to locate the target, calculate the offset from being centered underneath the vehicle, and to indentify the alphanumeric code.

Since an interface had already been programmed in Python, it was decided to program the computer vision in Python as well to allow for them to easily work in conjucction. To this end the OpenCV-Python library was chosen.

5.1 Square Detection

The target consists of two concentric squares and a central leter. Therefore, a good way of identifying the target is looking for concentric squares. This is called feature detection, and is the prefered computer vision approach when it is possible (which is rarely).

First, squares are recognised. This is a multi-stage process:

- 1. Convert image to grayscale
- 2. Gaussian Blur to blur the image slightly
- 3. Use Canny Edge Detection to find edges
- 4. Find complete contours
- 5. Find contours that have between 4 and 6 edges
 - An ideal square would have 4 edges, but images are rarely perfect.
- 6. Check that the contour is above a minimum size
- 7. Check that the solidity of the contour is above a threshold
 - This is done by drawing a rectangle that encloses the entire contour, and comparing the area of the rectangle to the area of the contour
 - An ideal square would have a solidity of 1
- 8. Check that the aspect ratio of the bounding rectangle is within thresholds
- 9. Contours that have passed all of these criteria must be squares

5.2 Optical Character Recognition

A Table of All Symbol Definitions

Note: values in normal text are constants, values in italics are values derived from constants. Where no value is given, that variable is a dynamic variable which changes continously.

Symbol	Definition	Value(where appropriate)
	Positions and Angles	
θ_x	Quad Pitch	
θ_y	Quad Roll	
θ_z	Quad Yaw	
ϕ_x	Jet Pitch	
ϕ_y	Jet Roll	
ϕ_z	Jet Yaw	
	Dimensions	
h_f	Quad frame height	5 mm
r_1	Quad frame inner radius	$180 \mathrm{\ mm}$
r_2	Quad frame outer radius	$200 \mathrm{\ mm}$
L_R	Quad arm length	$100 \mathrm{\ mm}$
r_r	Quad arm radius	$2~\mathrm{mm}$
r_J	Jet radius	41 mm
h_J	Jet height	150 mm
l_c	Gimbal servo connecting rod length	100 mm
	Masses	
M_{TOT}	Total Mass	
ho	Density of Quad	$2700kgm^3$
M_F	Quad frame mass	
M_R	Quad rod mass	
M_M	Motor mass	50 g
M_G	Gimbal servo mass	79 g
M_J	Jet mass	
	Inertias	
I_{Qx}	Quad inertia about x axis	
I_{Qy}	Quad inertia about y axis	
I_{Qz}	Quad inertia about z axis	
I_{Jx}	Quad inertia about x axis	
I_{Jy}	Quad inertia about y axis	
I_{Jz}	Quad inertia about z axis	
	Forces	
F_x	Sum of forces in x direction	
F_y	Sum of forces in y direction	
F_z	Sum of forces in z direction	
F_{M1}	Force from motor 1	
F_{M2}	Force from motor 2	
F_{M3}	Force from motor 3	
F_{M4}	Force from motor 4	

Symbol	Definition	Value(where appropriate)
F_J	Force from jet	
	Torques and Moments	
$ au_{Qx}$	Sum of moments on quad about x axis	
$ au_{Qy}$	Sum of moments on quad about y axis	
$ au_{Qz}$	Sum of moments on quad about z axis	
$ au_{Gx}$	Torque of jet gimbal servo about x axis	
$ au_{Gy}$	Torque of jet gimbal servo about y axis	
	PID Controllers	
SP_x	Quad X position controller setpoint	
SP_y	Quad Y position controller setpoint	
SP_z	Quad Z position controller setpoint	
SP_{θ_x}	Quad X angle controller setpoint	
SP_{θ_y}	Quad Y angle controller setpoint	
SP_{θ_z}	Quad Z angle controller setpoint	
O_x	Quad X position controller output	
O_y	Quad Y position controller output	
O_z	Quad Z position controller output	
O_{θ_x}	Quad X angle controller output	
O_{θ_y}	Quad Y angle controller output	
O_{θ_z}	Quad Z angle controller output	
SP_{ϕ_x}	Jet X angle controller setpoint	
SP_{ϕ_y}	Jet Y angle controller setpoint	
O_{ϕ_x}	Jet X angle controller output	
O_{ϕ_y}	Jet Y angle controller output	

B Servo Information

Servo information was based on a sample servo that may well end up being used on the vehicle, the Futaba BLS177SV.

Torque (at 6.6V): 34 kg-cm Speed (at 6.6V): $0.12 \text{sec}/60^{\circ}$ Weight: 79g

We can see from the data sheet that it takes the servo 0.12 seconds to rotate 60°. Assuming it takes 0.01 of those seconds to accelerate to full speed, this gives an acceleration of $873rad/s^2$. Since we know it exerts a torque of 0.34kgm, this means its inertia must be 3.89×10^{-4} .

C Thrust to Weight Ratio Calculations

References

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