



ETRiS - Geo-INQUIRE online training course , Second Day: November 7, 2023

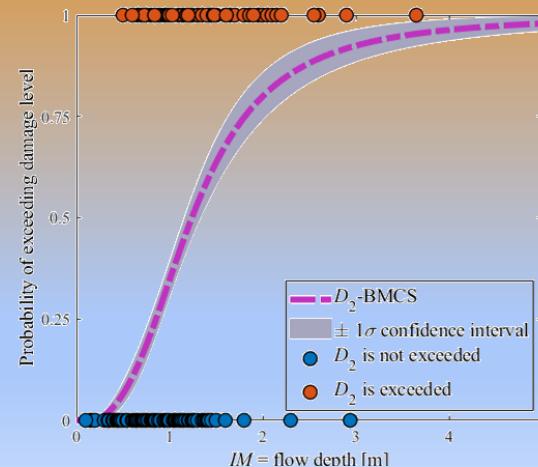
Empirical fragility and vulnerability curves for risk analysis (VA2-35-1)



University College London
INSTITUTE FOR RISK AND DISASTER
REDUCTION (IRDR)



European Tsunami Risk Service (ETRiS)



Lecture by: Hossein Ebrahimian
University of Naples Federico II (UNINA)

Moderator: Fatemeh Jalayer
University College London (UCL)

Geo-INQUIRE is funded by the European Union. Views and opinions expressed are however those of the authors only and do not necessarily reflect those of the European Union or the European Research Executive Agency. Neither the European Union nor the granting authority can be held responsible for them.



We have seen in the First Day of the Training Course:

- The forward probabilistic framework
- Damage scales
- Definition of fragility function
- Empirical fragility assessment using GLM
- Bayesian model class selection
- The definition of vulnerability function

<https://eurotsunamirisk.org/tsunamirisktoolkit/>

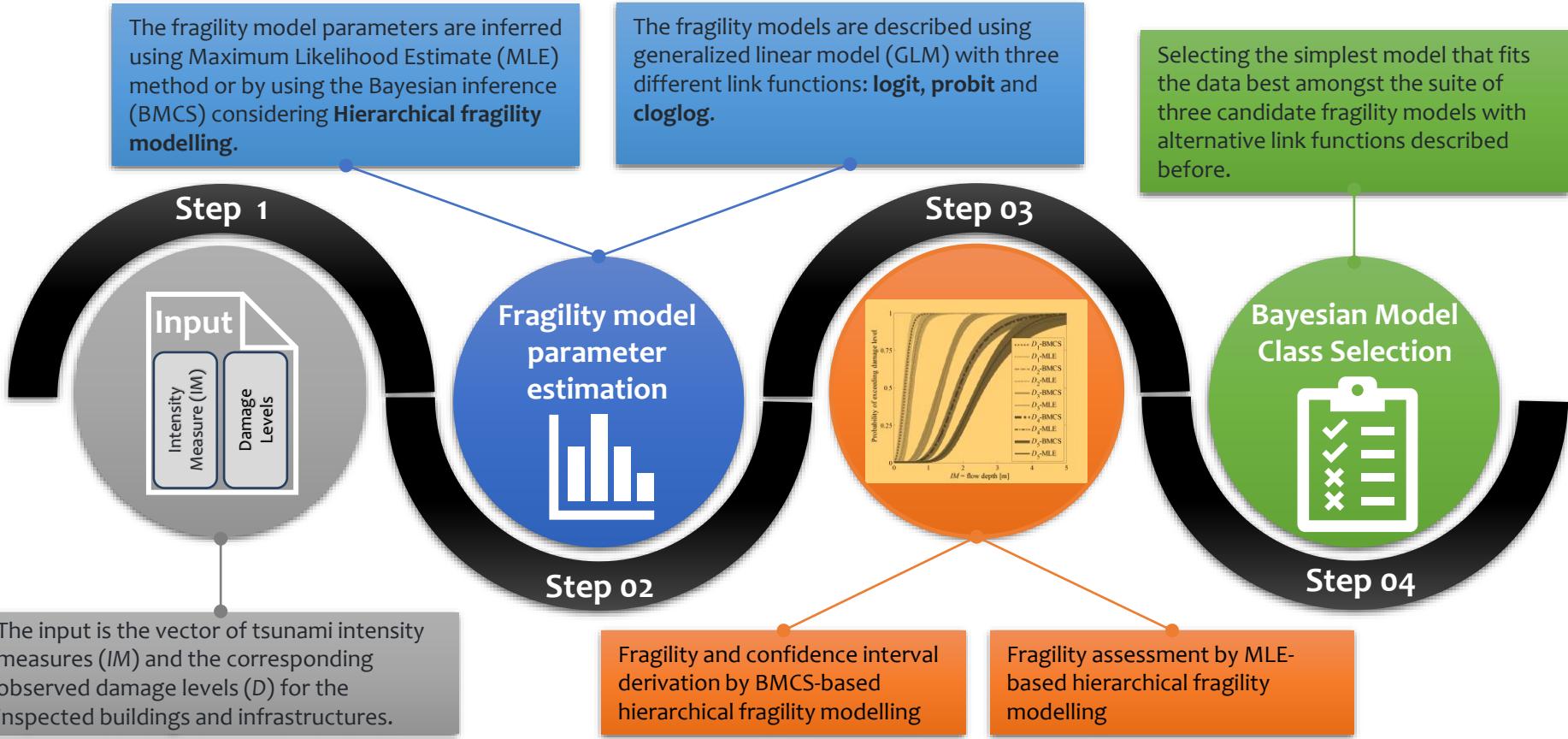
computeFrag

Will be added
to the ETRiS

If you are using computeFrag, you should cite this paper:

Jalayer, F., Ebrahimi, H., Trevlopoulos, K. and Bradley, B., 2023. Empirical tsunami fragility modelling for hierarchical damage levels. *Natural Hazards and Earth System Sciences*, 23(2), pp.909-931.

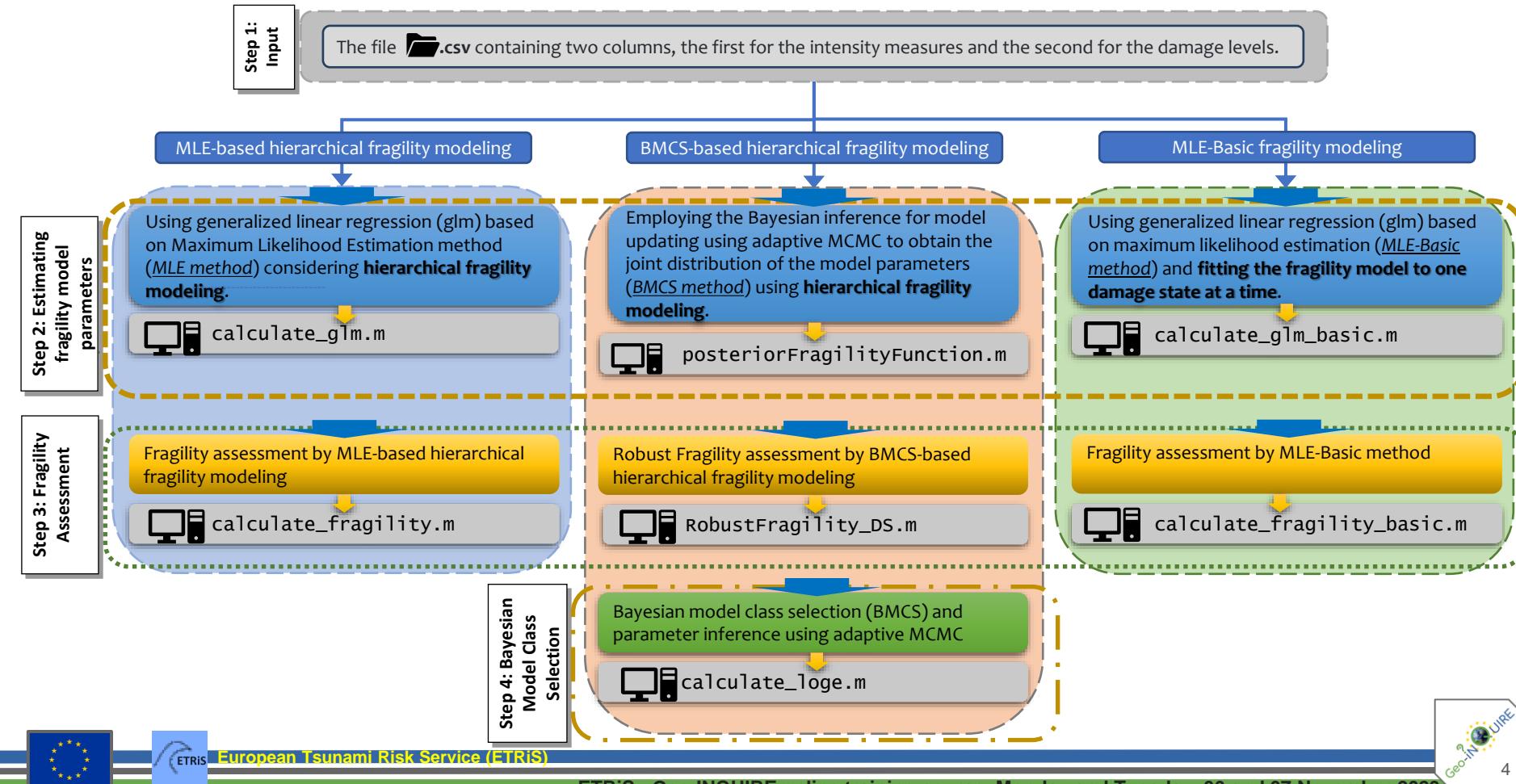
<https://doi.org/10.5194/nhess-23-909-2023>



<https://eurotsunamirisk.org/tsunamirisktoolkit/>

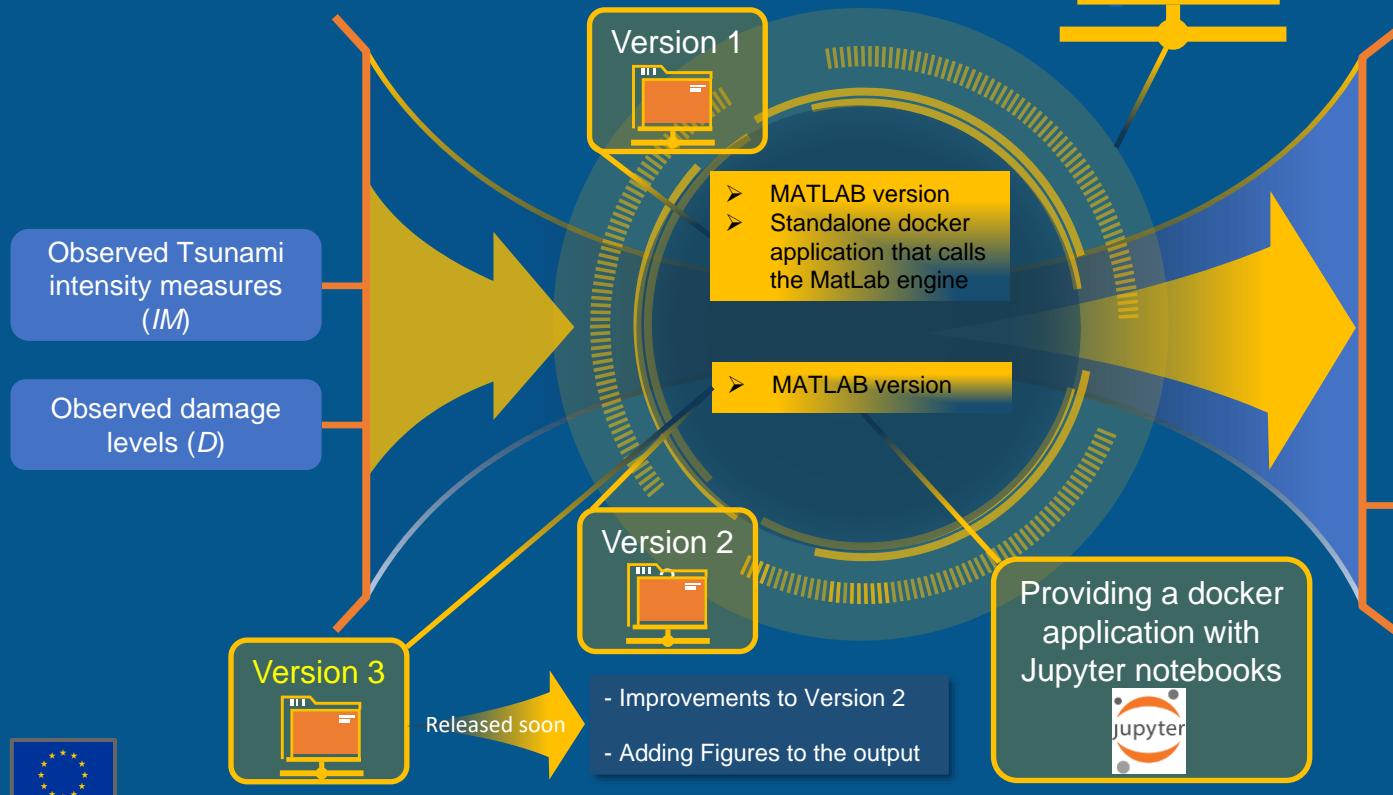


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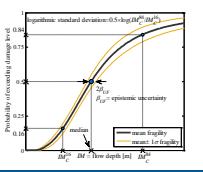


Input & Output Concept of computeFrage



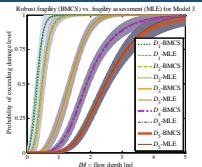
Output version 1

- BMCS-based hierarchical fragility model parameters.
- Robust fragility assessment and its confidence interval.



Output version 2

- MLE-based hierarchical fragility model parameters and fragility assessment.
- BMCS-based hierarchical fragility model parameters, Robust fragility assessment, and Bayesian model class selection.
- MLE-Basic fragility model parameters and fragility assessment.





The probability of being in a damage state DS given IM

- $P(D \geq D_j | IM)$ is the fragility function for damage level D_j .

$$P(DS_j | IM) = P[(D \geq D_j) \cdot (D < D_{j+1}) | IM]$$

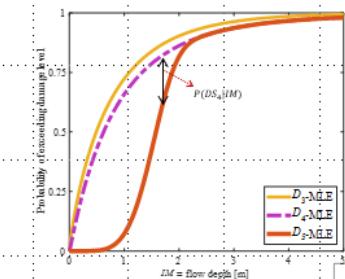
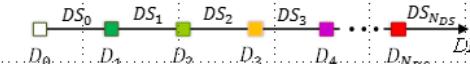
$$= \begin{cases} P(D \geq D_j | IM) - P(D \geq D_{j+1} | IM) & \text{for } 0 \leq j < N_{DS} \\ P(D \geq D_j | IM) & \text{for } j = N_{DS} \end{cases}$$

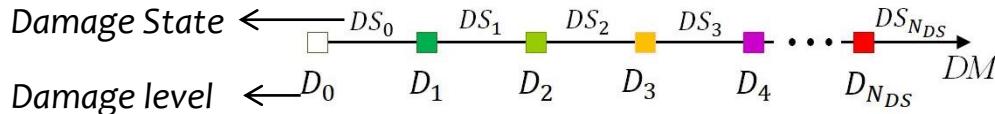
The representation of the fragility curve as $P(DS|IM)$

- The probability mass function definition is used for providing the probability of a discrete variable; e.g., being in a given damage state DS.

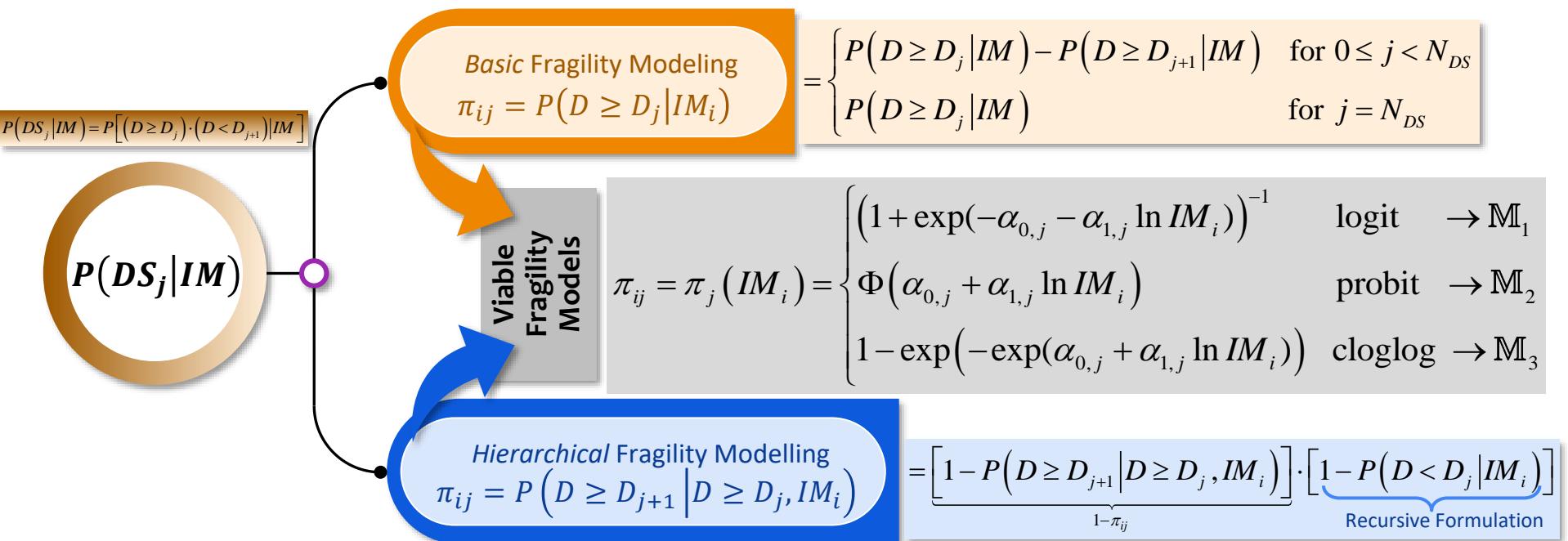
$$P(DS_j | IM = im) = P(D > D_j | IM = im) - P(D > D_{j+1} | IM = im)$$

$$P(DS_{N_{DS}} | IM = im) = P(D > D_{N_{DS}} | IM = im)$$





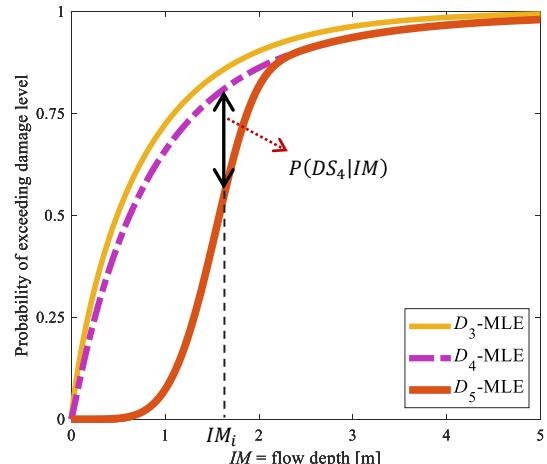
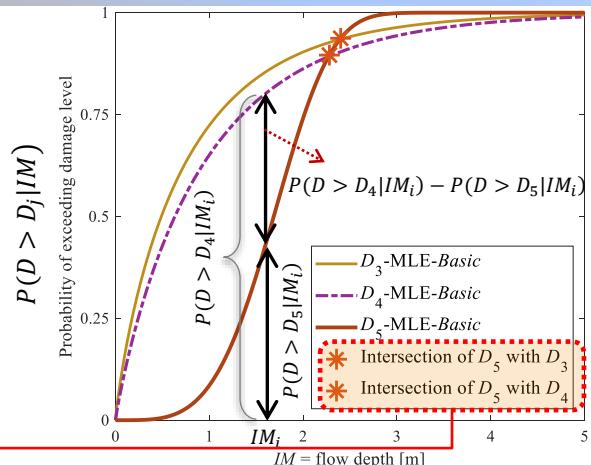
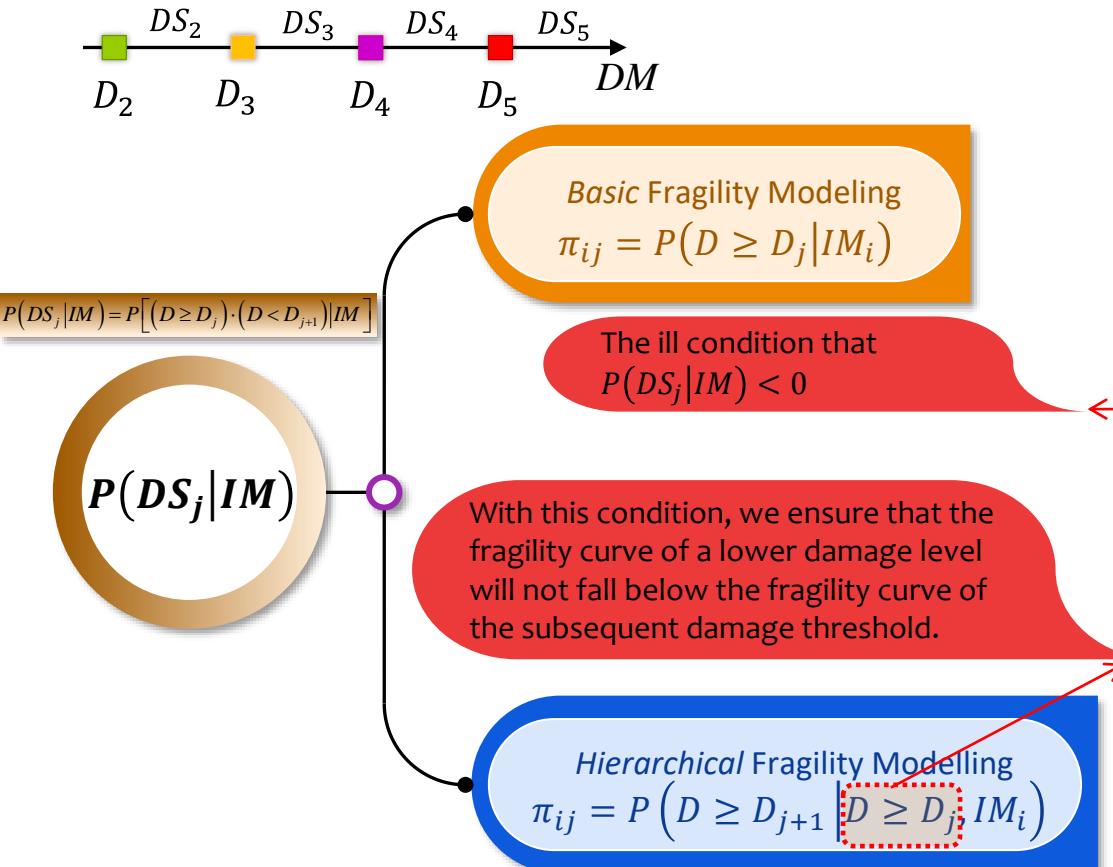
$$DS_j \equiv (D \geq D_j) \cdot (D < D_{j+1})$$



Jalayer, F., Ebrahimian, H., Trevlopoulos, K. and Bradley, B., 2023. Empirical tsunami fragility modelling for hierarchical damage levels. *Natural Hazards and Earth System Sciences*, 23(2), pp.909-931.

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Hierarchical Fragility Modelling using MLE – Parameter Estimation

$$\pi_{ij} = P(D \geq D_{j+1} | D \geq D_j, IM_i)$$

calculate_glm.m

All buildings in with observed damage $D_j \leq D < D_{j+1}$ will be assigned a probability equal to zero, while those with $D \geq D_{j+1}$ will be assigned a probability equal to one.



The vector of fragility model parameters is:

$$\theta = [\{\alpha_{0,j}, \alpha_{1,j}\}, j = 0: N_{DS} - 1]$$



theta_prior_modelk
k=1,2,3

Using MATLAB ToolBox

Basic Fragility Modelling using MLE (MLE-Basic) – Parameter Estimation

$$\pi_{ij} = P(D \geq D_j | IM_i)$$

calculate_glm_basic.m

All buildings in with observed damage $D < D_j$ will be assigned a probability equal to zero, while those with $D \geq D_j$ will be assigned a probability equal to one.



The vector of fragility model parameters is:

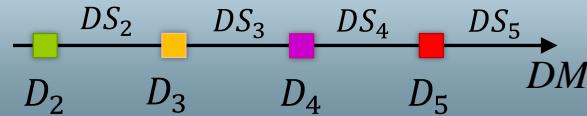
$$\theta = \{\alpha_0, \alpha_1\} \text{ for each level } D_j$$



theta_basic_modelk
k=1,2,3

01  TutorialHierarchical and Basic Fragility Modelling
using MLE by MATLAB ToolBox
– Parameter estimation

Building class 2 (Timber residential) of South Pacific 2009
Tsunami



Reese, S., Bradley, B. A., Bind, J., Smart, G., Power, W., and Sturman, J.: Empirical building fragilities from observed damage in the 2009 South Pacific tsunami, *Earth-Sci. Rev.*, 107(1-2), 156-173, 2011.

Hierarchical Fragility Modelling using Bayesian Inference

$$\pi_{ij} = P(D \geq D_{j+1} | D \geq D_j, IM_i)$$

 `posteriorFragilityFunction.m`

The adaptive MCMC procedure for drawing samples from the joint posterior $p(\boldsymbol{\theta}_k | \mathbf{D}, \mathbb{M}_k)$ of $\boldsymbol{\theta}_k$ given model \mathbb{M}_k is carried out by considering 6 chains (simulation levels), and a maximum of 2000 samples per chain.

 Samples $\{\boldsymbol{\theta}_{k,1}, \boldsymbol{\theta}_{k,2}, \dots, \boldsymbol{\theta}_{k,N_d}\}$

$$\boldsymbol{\theta} = [\{\alpha_{0,j}, \alpha_{1,j}\}, j = 0: N_{DS} - 1]$$

 `sample_theta_modelk`
`k=1,2,3`



The Posterior Distribution for Fragility Model Parameters

- The posterior distribution $p(\boldsymbol{\theta}_k | \mathbf{D}, \mathbb{M}_k)$ can be found based on Bayesian inference:

$$p(\boldsymbol{\theta}_k | \mathbf{D}, \mathbb{M}_k) = \underbrace{\frac{p(\mathbf{D} | \boldsymbol{\theta}_k, \mathbb{M}_k) p(\boldsymbol{\theta}_k | \mathbb{M}_k)}{\int_{\Omega_{\boldsymbol{\theta}_k}} p(\mathbf{D} | \boldsymbol{\theta}_k, \mathbb{M}_k) p(\boldsymbol{\theta}_k | \mathbb{M}_k) d\boldsymbol{\theta}_k}}_{\text{posterior}} = C^{-1} \underbrace{p(\mathbf{D} | \boldsymbol{\theta}_k, \mathbb{M}_k)}_{\text{likelihood}} \underbrace{p(\boldsymbol{\theta}_k | \mathbb{M}_k)}_{\text{prior}}$$

where C^{-1} is a normalizing constant.

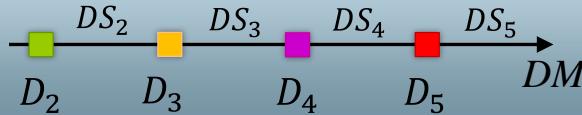


Prior: A multivariate normal distribution with zero correlation between the pairs of model parameters $\boldsymbol{\theta}_k$

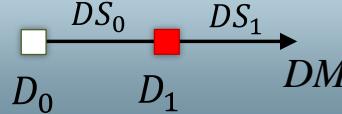
02  Tutorial

Hierarchical Fragility Modelling using Bayesian Inference by ComputeFrag - Parameter estimation

Building class 2 (Timber residential) of South Pacific 2009 Tsunami



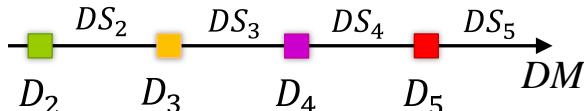
Mixed Building type (Masonry and Wood) of Dichato, Maule, 2010 Chile Tsunami



Mas, E., Koshimura, S., Suppasri, A., Matsuoka, M., Matsuyama, M., Yoshii, T., Jimenez, C., Yamazaki, F. and Imamura, F., 2012. Developing Tsunami fragility curves using remote sensing and survey data of the 2010 Chilean Tsunami in Dichato. *Natural Hazards and Earth System Sciences*, 12(8), pp.2689-2697.



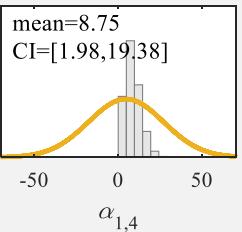
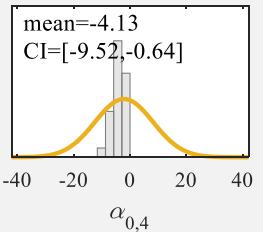
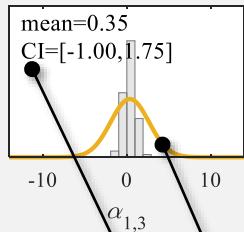
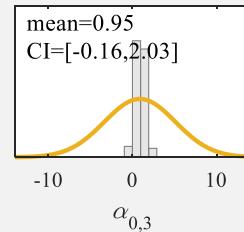
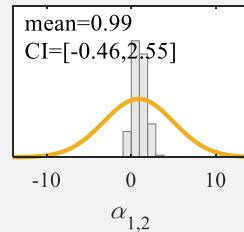
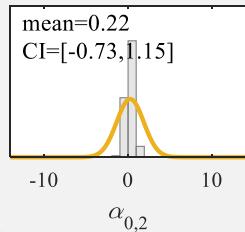
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Hierarchical Fragility Modelling using Bayesian Inference – Parameter estimation



sample_theta_model13



theta_prior_model13

0.2511
0.8625
0.8828
0.3553
-2.1409
4.6477

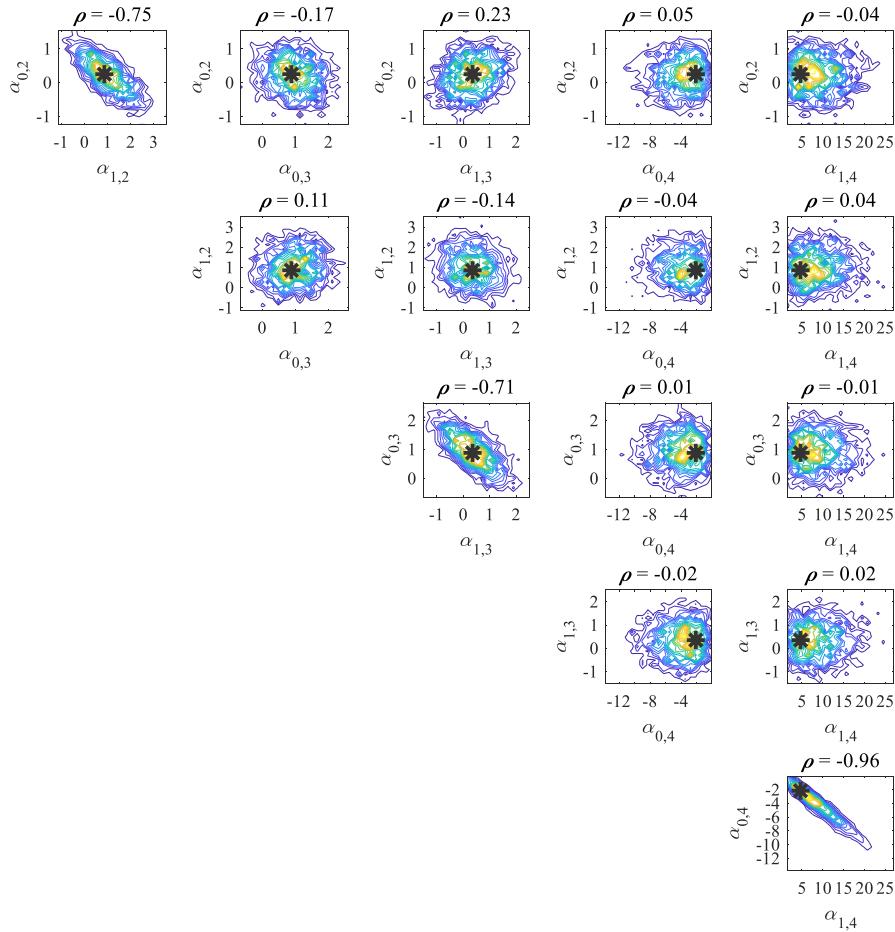
Hierarchical Fragility Modelling using MLE – Parameter estimation

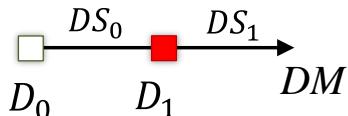
The marginal normal priors with large COV's

CI: 2% and 98% of the data based on the counted statistics



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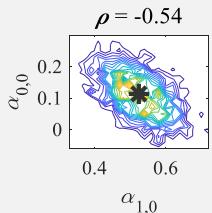
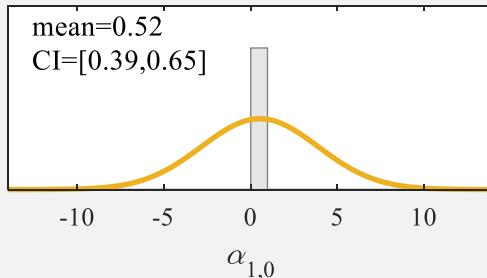
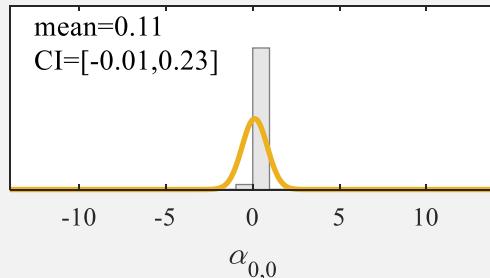




Hierarchical Fragility Modelling using Bayesian Inference – Parameter estimation



sample_theta_model12



theta_prior_model12

Hierarchical Fragility Modelling
using MLE – Parameter estimation

0.1136

0.5244



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Hierarchical Fragility Modelling using MLE of fragility model parameters

$$\boldsymbol{\theta} = \{\{\alpha_{0,j}, \alpha_{1,j}\}, j = 0: N_{DS} - 1\}$$

 calculate_fragility.m

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<https://doi.org/10.5194/nhess-23-909-2023>
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Natural Hazards and Earth System Sciences


Empirical tsunami fragility modelling for hierarchical damage levels

Fatemeh Jalayer^{1,2}, Hossein Ebrahimi², Konstantinos Tselopoulos², and Brendon Bradley³
¹Institute for Risk and Disaster Reduction, University College London, Gower Street, London WC1E 6BT, UK
²Department of Structures for Engineering and Architecture, University of Naples Federico II, Naples 80125, Italy
³Department of Civil and Natural Resources Engineering, University of Canterbury, Private Bag 4900, Christchurch 8140, New Zealand

 Fragility Curve based on the vector of IM defined

 FA_modelk, k=1,2,3



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Fragility Assessment using Generalized Regression

- The probabilities of being in different damage states can be calculated in a recursive way:

$$P(DS_j | IM_i) = \begin{cases} (1 - \pi_{ij}) \cdot \left[1 - \sum_{k=0}^{j-1} P(DS_k | IM_i) \right] & \text{for } j \geq 1 \\ 1 - \pi_{i0} \triangleq P(D \geq D_1 | IM_i) & \text{for } j = 0 \end{cases}$$

$$P(DS_{N_{DS}} | IM_i) = P(D \geq D_{N_{DS}} | IM_i) = 1 - \sum_{j=0}^{N_{DS}-1} P(DS_j | IM_i)$$

$$P(D \geq D_j | IM_i) = P(DS_j | IM_i) + P(D \geq D_{j+1} | IM_i) \quad \text{for } 0 \leq j < N_{DS}$$

**Basic Fragility Modelling using
MLE of the fragility model
parameters**
 $\theta = \{\alpha_0, \alpha_1\}$ for each level D_j

 calculate_fragility_basic.m

The fragility $\pi_{ij} = P(D \geq D_j | IM_i)$ is obtained by using a generalized linear regression model according with “logit”, “probit” or “cloglog” link function fitted to the damage data (M_k where $k = 1:3$)

 Fragility Curve based on the vector of IM defined

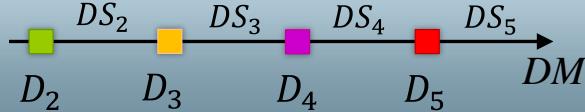
 FA_basic_modelk
k=1,2,3

03

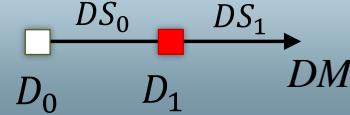
Tutorial

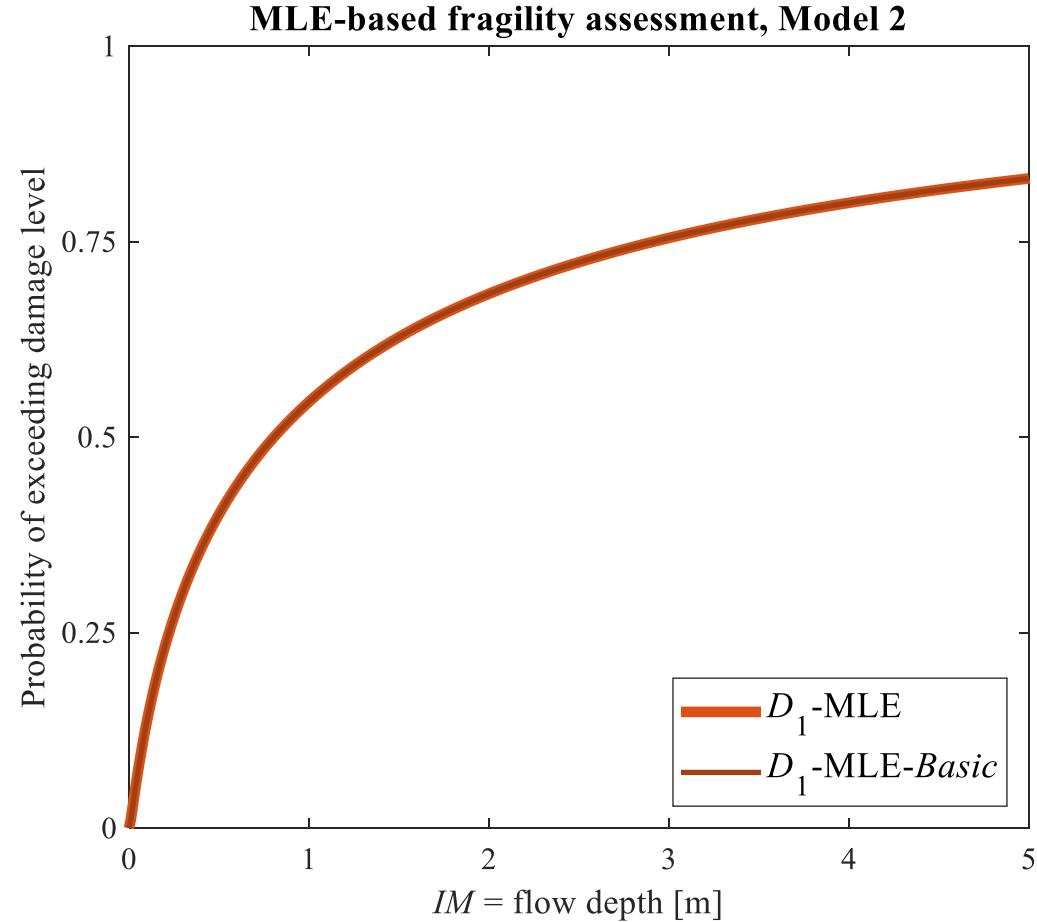
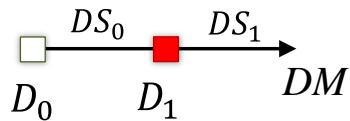
Hierarchical and Basic Fragility Assessment
using MLE of fragility model parameters

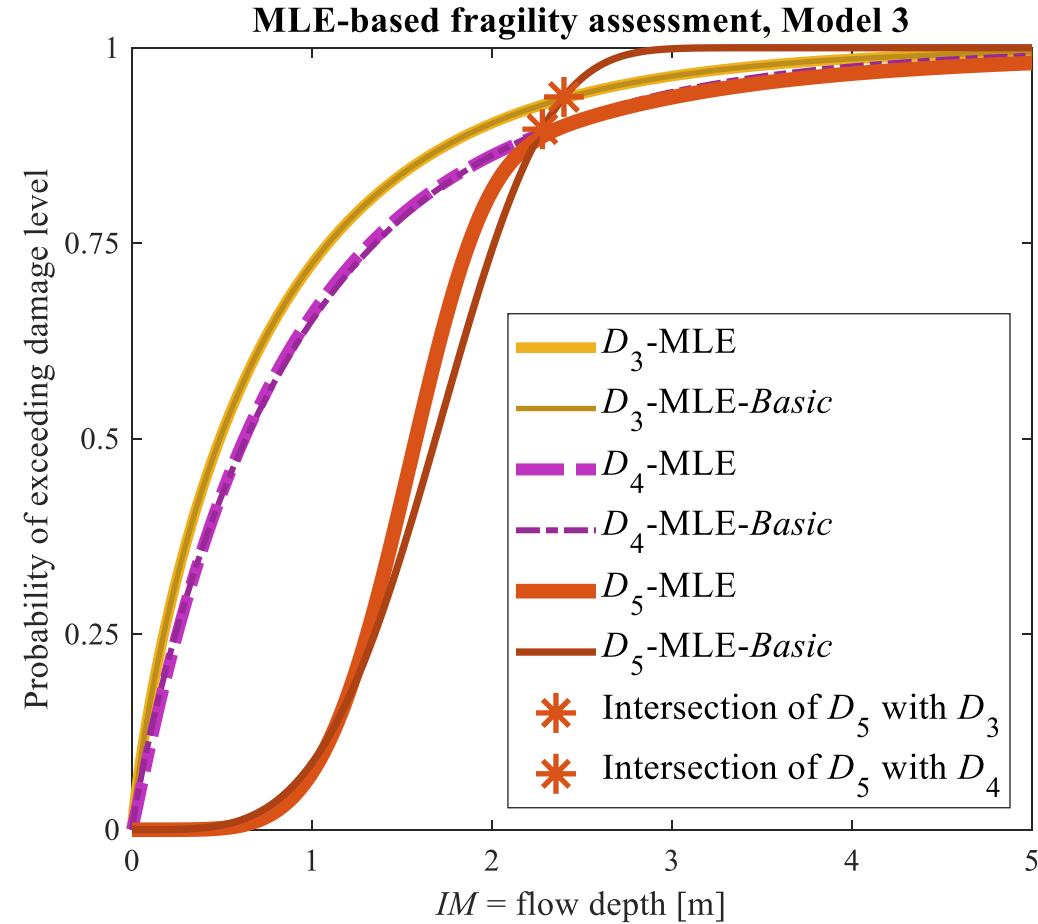
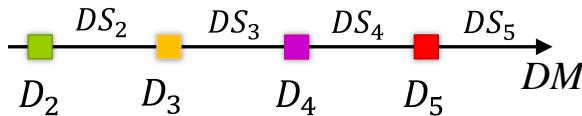
Building class 2 (Timber residential) of South Pacific 2009
Tsunami



Mixed Building type (Masonry and Wood) of Dichato, Maule,
2010 Chile Tsunami







RobustFragility_DS.m

Hierarchical Fragility Modelling using Bayesian Inference for the fragility model parameters

$$\{\theta_{k,1}, \theta_{k,2}, \dots, \theta_{k,N_d}\}$$

$$\theta = [\{\alpha_{0,j}, \alpha_{1,j}\}, j = 0:N_{DS} - 1]$$

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Christchurch 8140, New Zealand

 Fragility Curve and its confidence
interval based on the vector of IM

 RF_modelk, k=1,2,3



Robust Fragility Assessment

- Robust Fragility (RF) is defined as the expected value for a prescribed fragility model considering the joint probability distribution for the fragility model parameters θ_k . The RF herein can be expressed as:

$$P(D \geq D_j | IM, \mathbf{D}, M_k) = \int_{\Theta_k} P(D \geq D_j | IM, \theta_k) p(\theta_k | \mathbf{D}, M_k) d\theta_k = \mathbb{E}_{\theta_k | \mathbf{D}, M_k} [P(D \geq D_j | IM, \theta_k)]$$

$$\sigma_{\theta_k | \mathbf{D}, M_k}^2 [P(D \geq D_j | IM, \theta_k)] = \mathbb{E}_{\theta_k | \mathbf{D}, M_k} [P(D \geq D_j | IM, \theta_k)^2] - (\mathbb{E}_{\theta_k | \mathbf{D}, M_k} [P(D \geq D_j | IM, \theta_k)])^2$$

$$\cong \frac{1}{N_d} \sum_{j=1}^{N_d} P(D \geq D_j | IM, \theta_{k,j})^2 = P(D \geq D_j | IM, \mathbf{D}, M_k)^2 \quad (\text{Eq.16})$$

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RobustFragility_DS.m

Hierarchical Fragility Modelling
using Bayesian Inference for
the fragility model parameters

$$\{\theta_{k,1}, \theta_{k,2}, \dots, \theta_{k,N_d}\}$$

$$\theta = [\{\alpha_{0,j}, \alpha_{1,j}\}, j = 0:N_D - 1]$$

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 Fragility Curve and its confidence
interval based on the vector of IM

 RF_modelk, k=1,2,3

Using Monte Carlo Simulation for Fragility Assessment

- The RF integral can be solved numerically by employing Monte Carlo simulation with N_d generated samples from the vector θ_k as follows:

$$P(D \geq D_j | IM, \mathbf{D}, \mathbb{M}_k) \approx \frac{1}{N_d} \sum_{l=1}^{N_d} P(D \geq D_j | IM, \theta_{k,l})$$



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RobustFragility_DS.m

Hierarchical Fragility Modelling
using Bayesian Inference for
the fragility model parameters

$$\{\theta_{k,1}, \theta_{k,2}, \dots, \theta_{k,N_d}\}$$

$$\theta = [\{\alpha_{0,j}, \alpha_{1,j}\}, j = 0:N_D - 1]$$

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interval based on the vector of IM

 RF_modelk, k=1,2,3



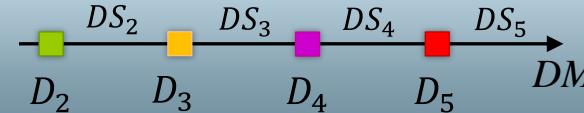
Using Monte Carlo Simulation for Fragility Assessment

- The integral equation for standard deviation of the fragility can be solved numerically by employing Monte Carlo simulation with N_d generated samples from the vector θ_k as follows:

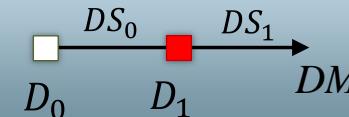
$$\sigma_{\theta_k | \mathbf{D}, \mathbb{M}_k}^2 \left[P(D \geq D_j | \mathbf{IM}, \theta_k) \right] \approx \frac{1}{N_d} \sum_{i=1}^{N_d} P(D \geq D_j | \mathbf{IM}, \theta_{k,i})^2 - P(D \geq D_j | \mathbf{IM}, \mathbf{D}, \mathbb{M}_k)^2$$

04  TutorialHierarchical Fragility Assessment using
Bayesian Inference

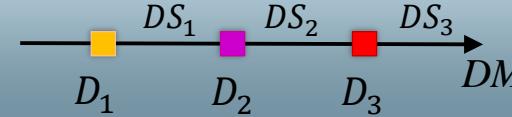
Building class 2 (Timber residential) of South Pacific 2009 Tsunami



Mixed Building type (Masonry and Wood) of Dichato, Maule, 2010 Chile Tsunami



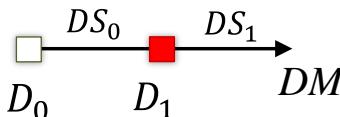
Building class 3 (Non engineered light timber) of Sulawesi-Palu 2018 Tsunami



Paulik, R., Gusman, A., Williams, J. H. et al. (2019). Tsunami hazard and built environment damage observations from Palu city after the September 28 2018 Sulawesi earthquake and tsunami. Pure Appl. Geophys. 176, 3305-3321.



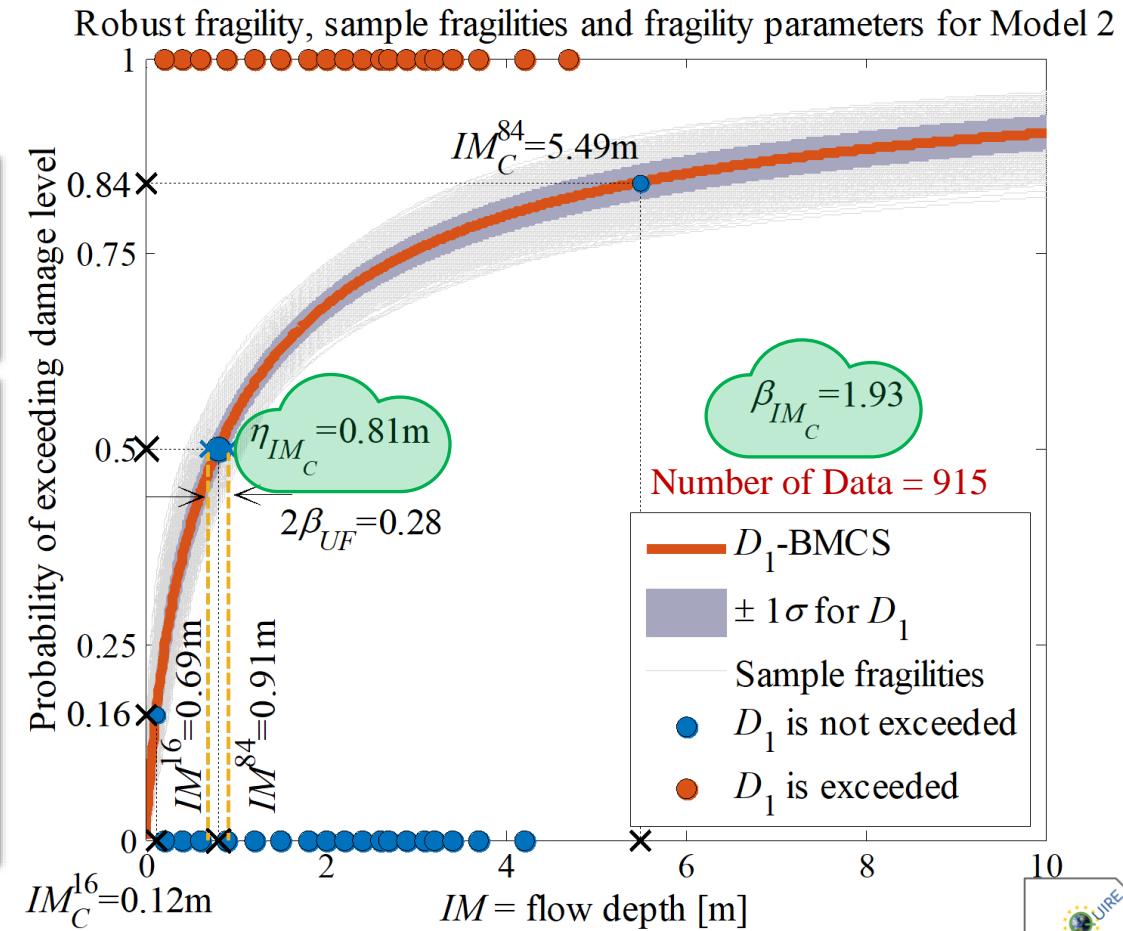
European Tsunami Risk Service (ETRIS)

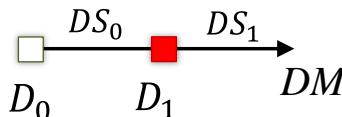


The median intensity, η_{IM_C} , for a given damage level, is calculated as the IM corresponding to 50% probability on the fragility curve.

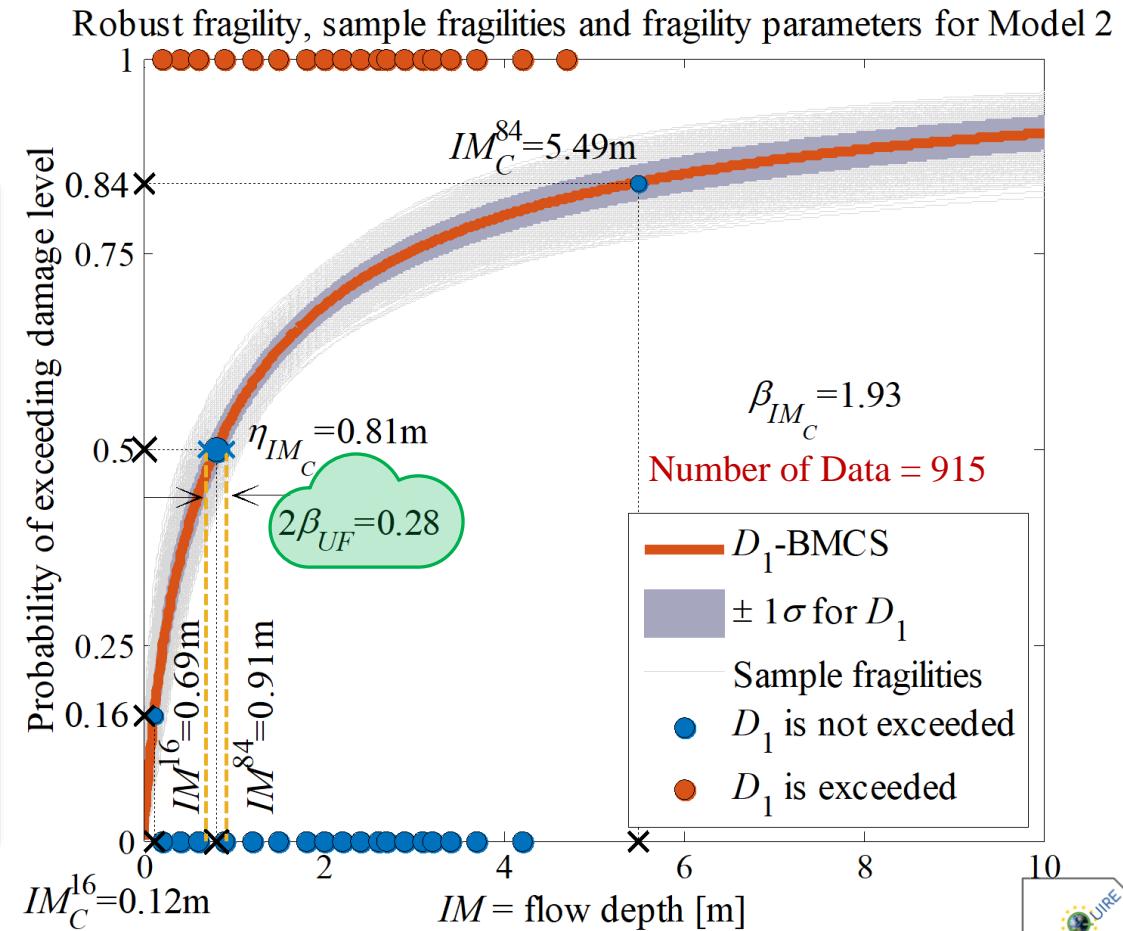
The logarithmic standard deviation (dispersion) of the equivalent lognormal fragility curve at the onset of damage threshold, β_{IM_C} , is estimated as half of the logarithmic distance between the IMs corresponding to the probabilities of 16% (IM_C^{16}) and the 84% (IM_C^{84}) on the fragility curve; thus, the dispersion can be estimated as

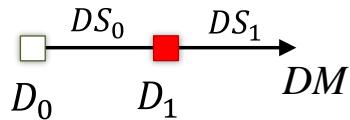
$$\beta_{IM_C} = 0.50 \times \ln(IM_C^{84}/IM_C^{16}).$$



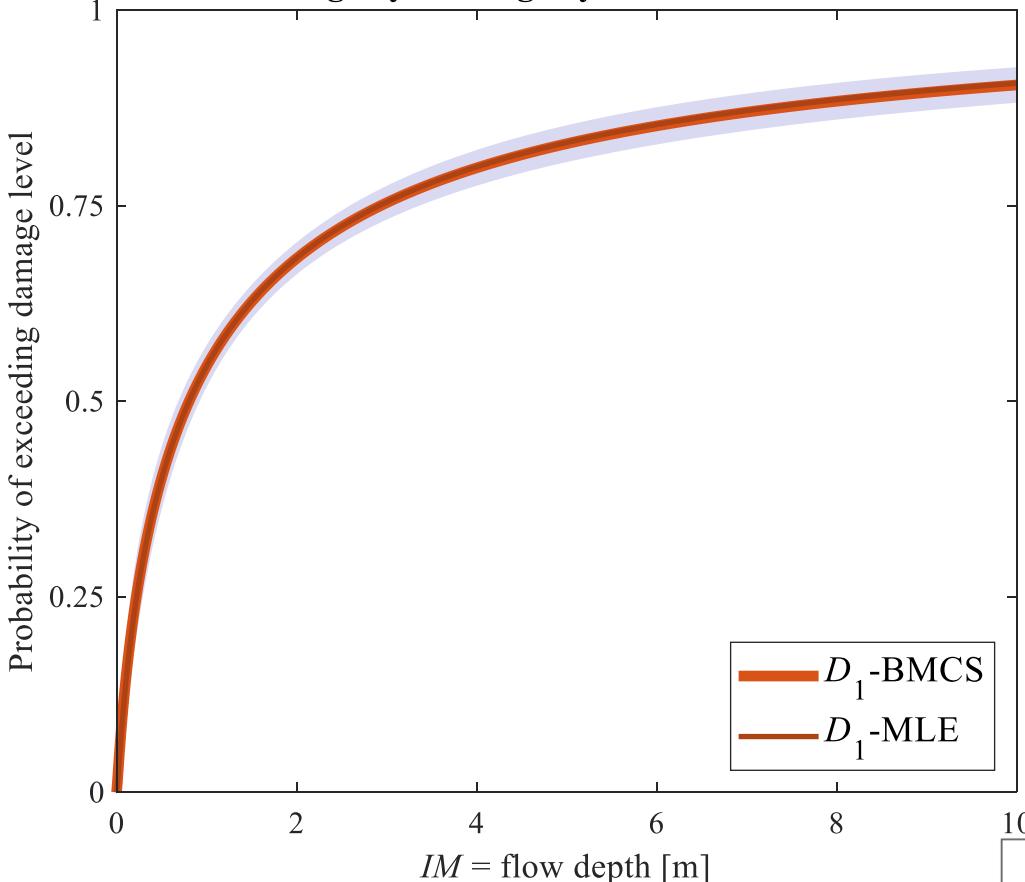


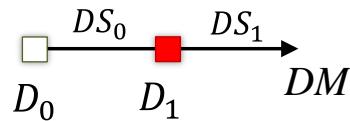
The overall effect of epistemic uncertainties (due to the uncertainty in the fragility model parameters and reflecting the effect of limited sample size) on the median of the empirical fragility curve is considered through (logarithmic) intensity-based standard deviation denoted as β_{UF} . It can be estimated as half of the (natural) logarithmic distance (along the IM axis) between the median intensities (i.e., 50% probability) of the RF's derived with 16% (denoted as IM^{84}) and 84% (IM^{16}) confidence levels, respectively:
 $\beta_{UF} = 0.50 \times \ln(IM^{84}/IM^{16})$.





Robust fragility vs. fragility assessment for Model 2





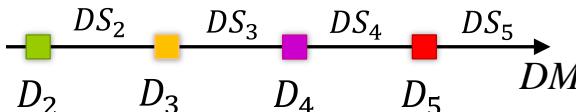
Jupyter Notebooks for Fragility Visualisation
<https://github.com/eurotsunamirisk/VisualizeFragility>



European Tsunami Risk Service (ETRIS)

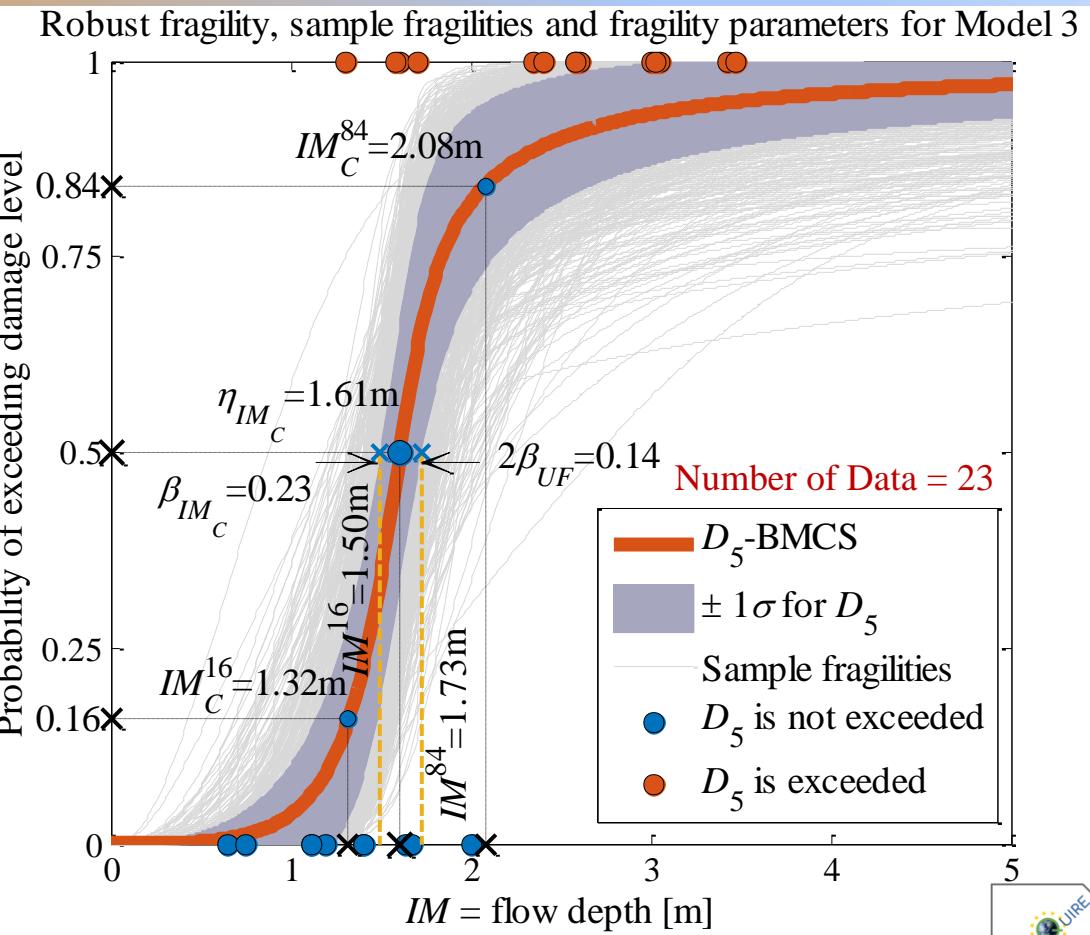
ETRIS - Geo-INQUIRE online training course, Monday and Tuesday, 06 and 07 November 2023

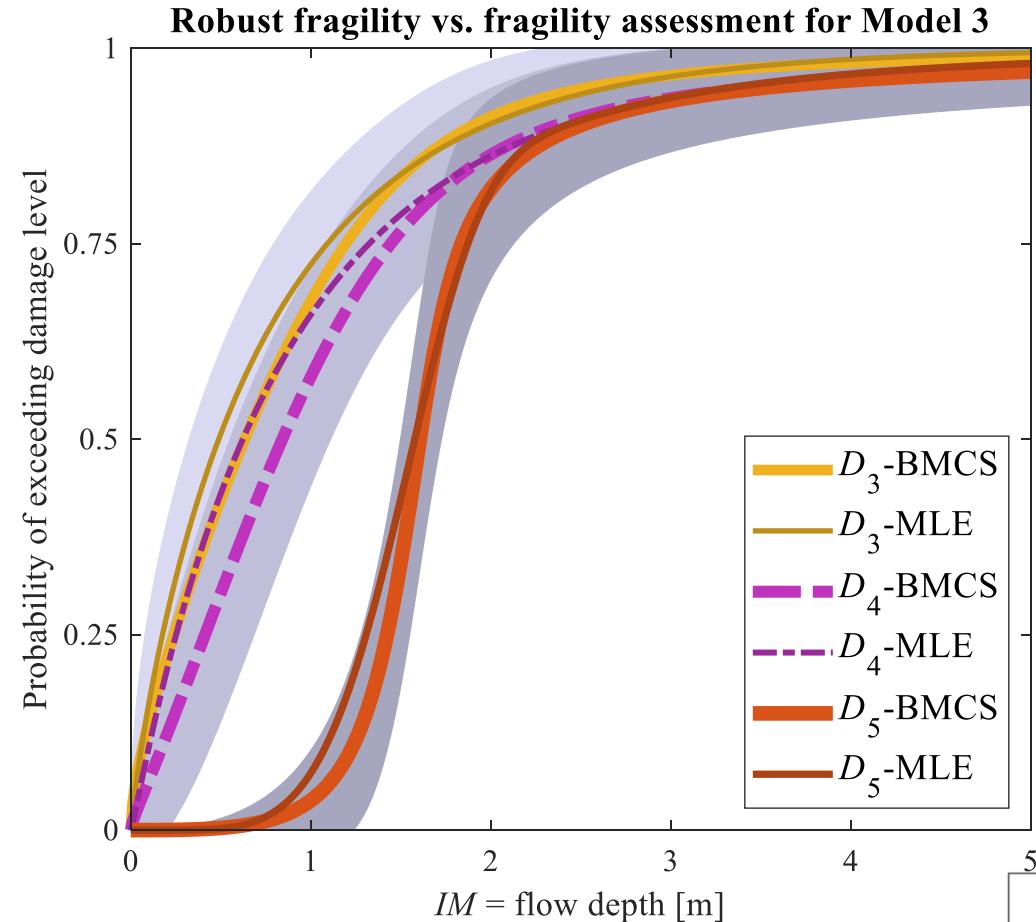
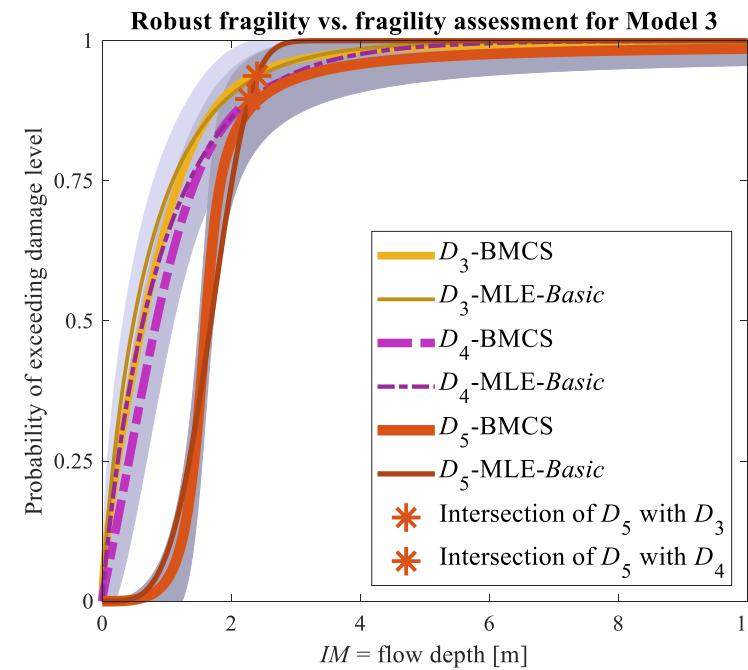
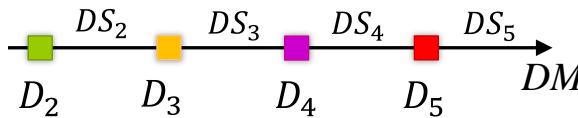


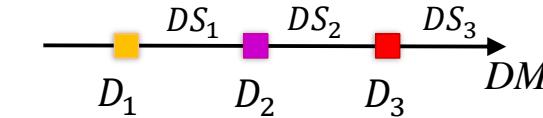


The Issue of rejected samples

Some samples $\theta_{k,l}$ may lead to fragility curves with unrealistic configurations as follows: (1) having negative slope as the IM increases; (2) Having high exceedance probability at very low IM values. To this end, those samples should be rejected. This case is more often when limited number of observed damages exists for a specific class of building.





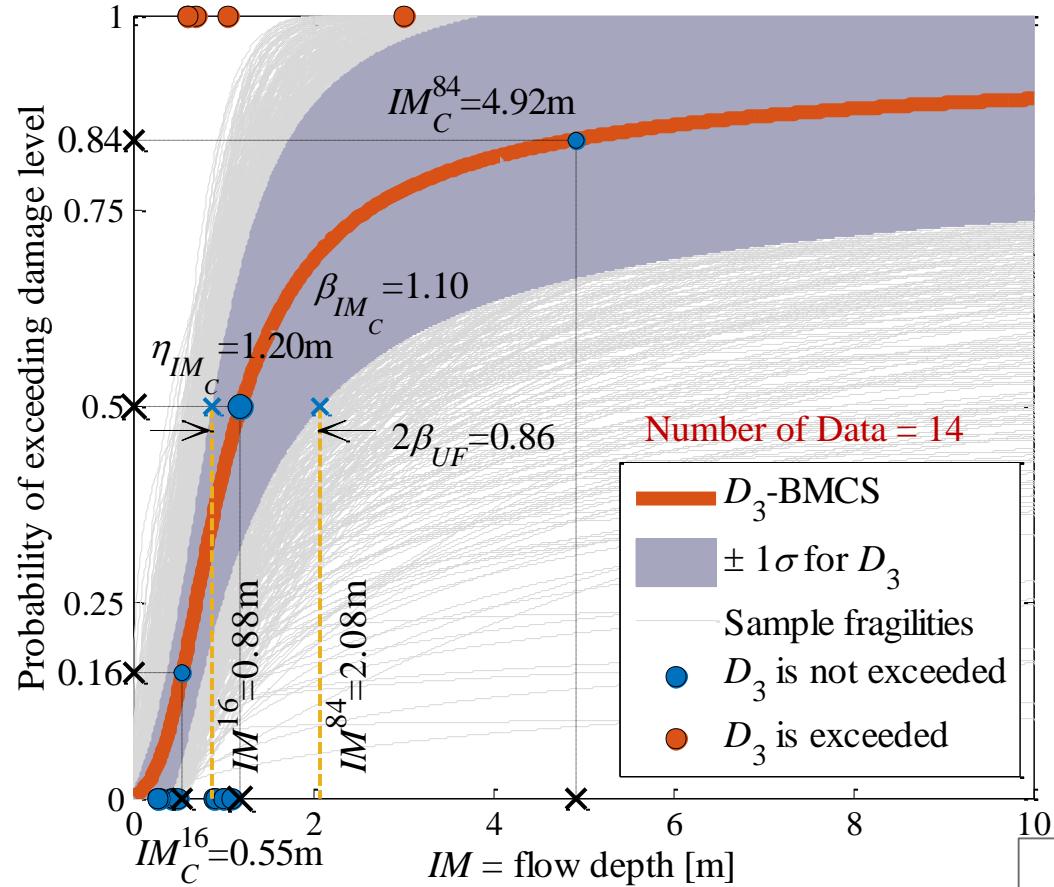


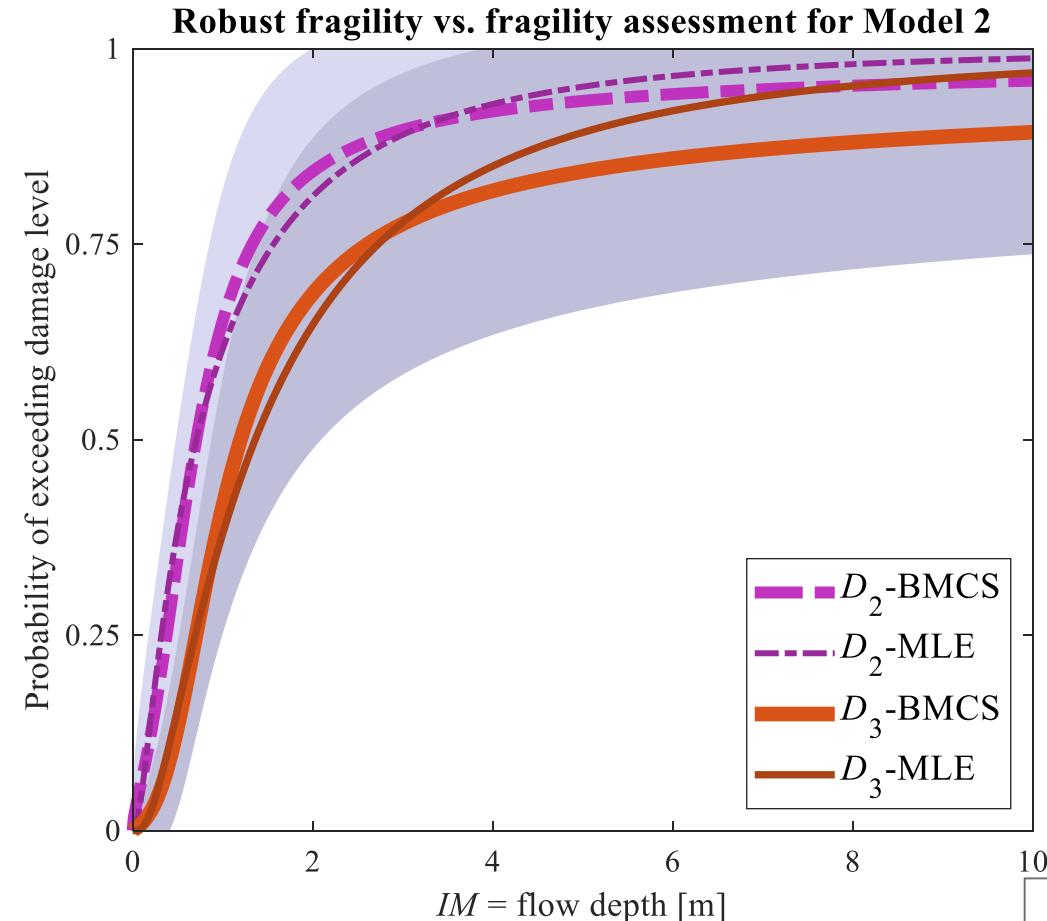
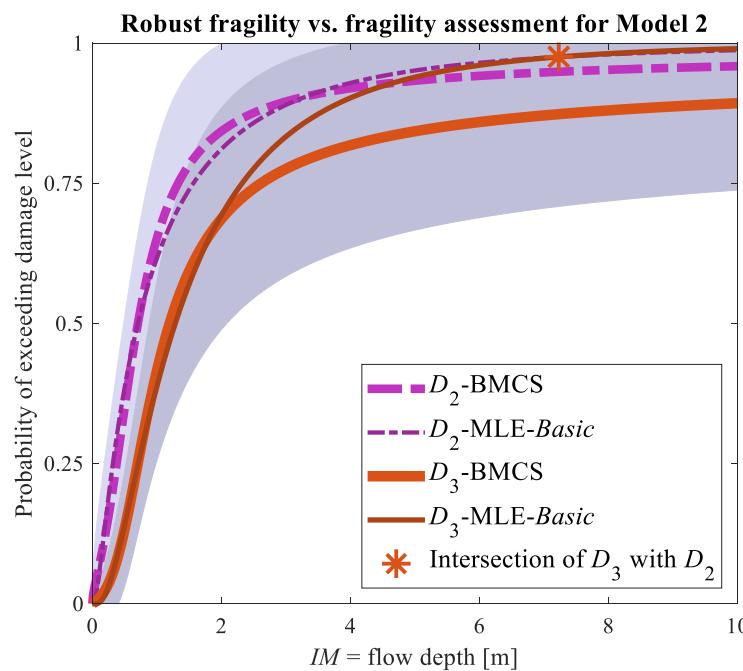
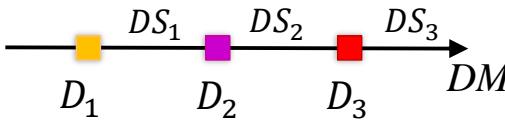
RF_model12

1x1 struct with 18 fields

Field	Value
fragility	1001x2 double
sfragility	1001x2 double
sample_fragility	1x1241 cell
sample_fragility_DSj	1x2 cell
rejected_samples	1x496 double
sample_theta	4x1241 double
RFp	1001x2 double
RFm	1001x2 double
RF84	1001x2 double
RF16	1001x2 double
etalMc	[0.7062, 1.1982]
IMc16	[0.2546, 0.5475]
IMc84	[1.9800, 4.9190]
etalMc_RF84	[0.4847, 0.8809]
etalMc_RF16	[1.0361, 2.0832]
betaMc	[1.0256, 1.0977]
betaUF	[0.3798, 0.4304]
sample_PDS_IM	1x1241 cell

Robust fragility, sample fragilities and fragility parameters for Model 2







Bayesian model class selection (BMCS) for identifying the best link model to use in the generalized linear regression scheme

calculate_logE.m

Nat. Hazards Earth Syst. Sci., 23, 909–931, 2023
<https://doi.org/10.5194/nhess-23-909-2023>
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Natural Hazards and Earth System Sciences
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Empirical tsunami fragility modelling for hierarchical damage levels

Fatemeh Jalayer^{1,2}, Hossein Ebrahimi², Konstantinos Trevlopoulos², and Brendon Bradley³
¹Institute for Risk and Disaster Reduction, University College London, Gower Street, London WC1E 6BT, UK
²Department of Structures for Engineering and Architecture, University of Naples Federico II, Naples 80125, Italy
³Department of Civil and Natural Resources Engineering, University of Canterbury, Private Bag 4800, Christchurch 8140, New Zealand

Posterior probability of each model class, $P(M_k | D)$, the log evidence, $\ln[p(D|M_k)]$, and the two terms

P_M, log_evidence,
 meanLogLikelihood, meanLogratioP



Bayesian Model Class Selection

- Given a set of N_M candidate model classes $\{M_k, k = 1:N_M\}$, and in the presence of the data D , the posterior probability of the k^{th} model class, denoted as $P(M_k | D)$ can be written as follows:

$$P(M_k | D) = \frac{p(D|M_k)P(M_k)}{\sum_{k=1}^{N_M} p(D|M_k)P(M_k)}$$



Bayesian model class selection (BMCS) for identifying the best link model to use in the generalized linear regression scheme

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Posterior probability of each model class, $P(M_k|\mathbf{D})$, the log evidence, $\ln[p(\mathbf{D}|M_k)]$, and the two terms

P_M, log_evidence,
 meanlogLikelihood, meanlogratioP



The (log) evidence

- that logarithm of the evidence (called *log-evidence*) $\ln[p(\mathbf{D}|M_k)]$ can be written as:

$$\ln[p(\mathbf{D}|M_k)] = \underbrace{\int_{\Omega_{\theta_k}} \ln[p(\mathbf{D}|\theta_k, M_k)] p(\theta_k|\mathbf{D}, M_k) d\theta_k}_{\text{log_evidence}} - \underbrace{\int_{\Omega_{\theta_k}} \ln \left[\frac{p(\theta_k|\mathbf{D}, M_k)}{p(\theta_k|M_k)} \right] p(\theta_k|\mathbf{D}, M_k) d\theta_k}_{\text{meanLogLikelihood} - \text{meanLogRatio}}$$

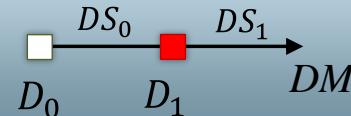
“Term 1” denotes the posterior mean of the log-likelihood, which is a measure of the average data fit to model M_k . “Term 2” is the relative entropy between the prior $p(\theta_k|M_k)$ and the posterior $p(\theta_k|\mathbf{D}, M_k)$ of θ_k given model M_k , which is a measure of the distance between the two PDFs.



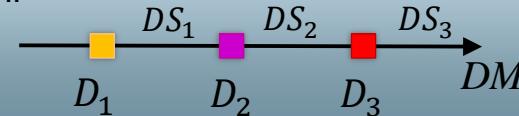
05 Tutorial

Bayesian model class selection (BMCS)

Mixed Building type (Masonry and Wood) of Dichato, Maule, 2010 Chile Tsunami



Building class 3 (Non engineered light timber) of Sulawesi-Palu 2018 Tsunami





- The posterior probability of Model Class 1 is 0.323
- The posterior probability of Model Class 2 is 0.342
- The posterior probability of Model Class 3 is 0.335

Model Class	Term 1: Average Data Fit	Term 2: Information Gain	Log-Evidence	Posterior Probability of the model
M_1	-545.208	5.4913	-550.700	0.3228
M_2	-545.085	5.5575	-550.642	0.3419
M_3	-544.257	6.405	-550.662	0.3353



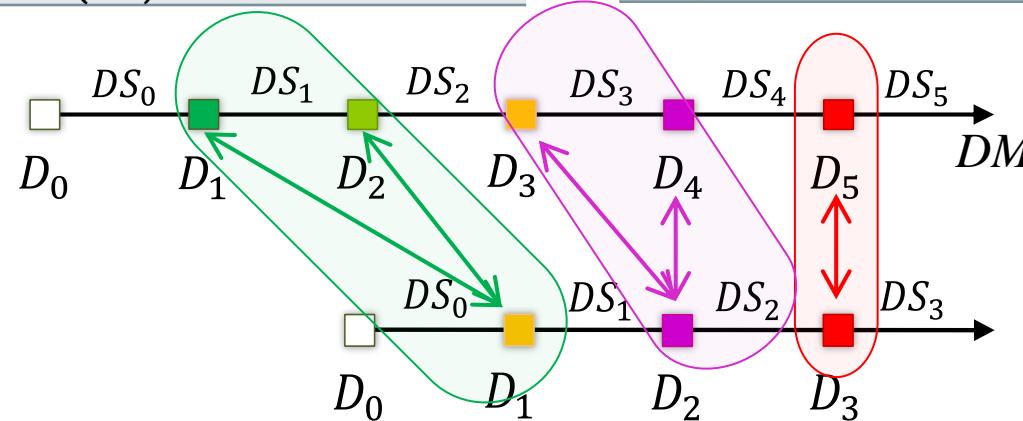
- The posterior probability of Model Class 1 is 0.210
- The posterior probability of Model Class 2 is 0.570
- The posterior probability of Model Class 3 is 0.220

Model Class	Term 1: Average Data Fit	Term 2: Information Gain	Log-Evidence	Posterior Probability of the model
M_1	-15.8034	4.2741	-20.0775	0.2101
M_2	-15.1575	3.9226	-19.0802	0.5697
M_3	-14.6294	5.4015	-20.0309	0.2202



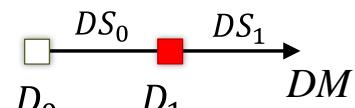
Damage Level		Damage level description	
D_0	None	no damage	
D_1	Light	non-structural damage	
D_2	Minor	significant non-structural damage, minor structural damage	
D_3	Moderate	significant structural and non-structural damage	
D_4	Severe	irreparable structural damage, will require demolition	
D_5	Collapse	complete structural collapse	
		South Pacific 2009	Sulawesi 2018
		Reese et al. (2011)	Paulik et al. 2019

Reese, S., Bradley, B. A., Bind, J., Smart, G., Power, W., & Sturman, J. (2011). Empirical building fragilities from observed damage in the 2009 South Pacific tsunami. *Earth-Science Reviews*, 107(1-2), 156-173.

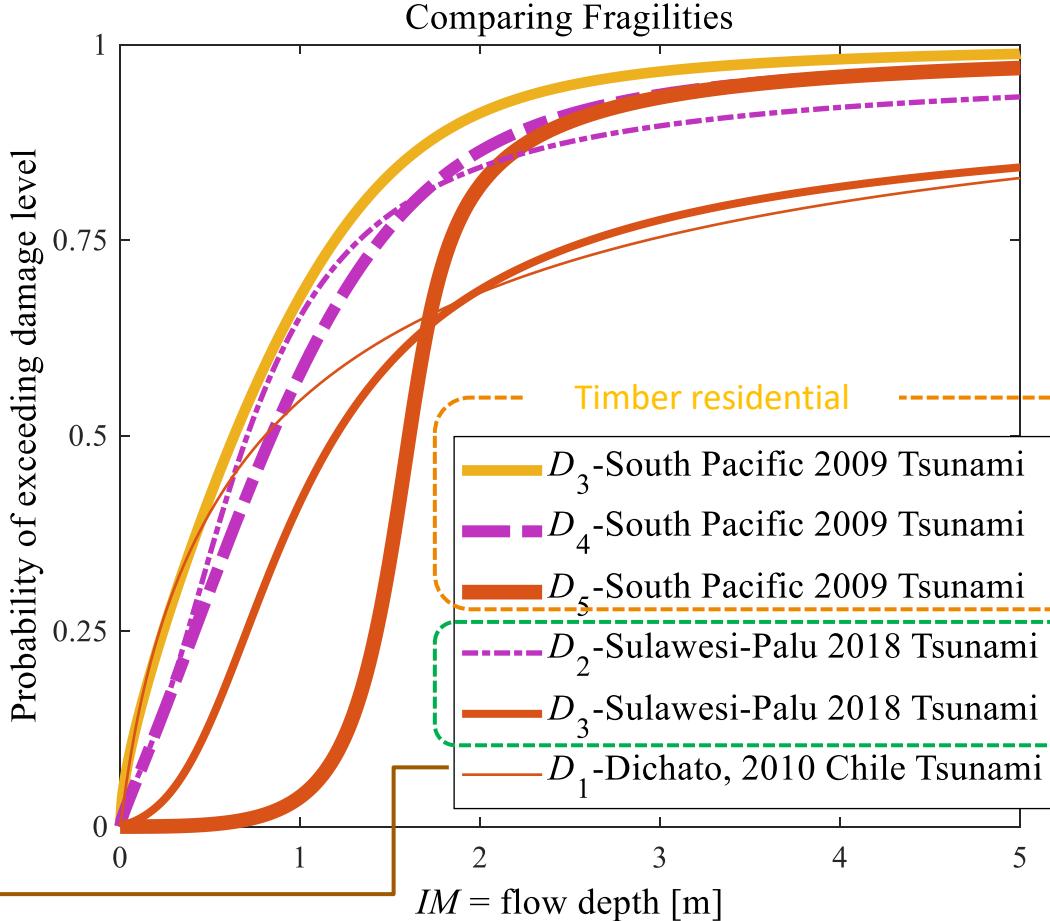


Paulik, R., Gusman, A., Williams, J. H., Pratama, G. M., Lin, S. L., Prawirabhakti, A., ... & Suwarni, N. W. I. (2019). Tsunami hazard and built environment damage observations from Palu City after the September 28 2018 Sulawesi earthquake and tsunami. *Pure and Applied Geophysics*, 176(8), 3305-3321.

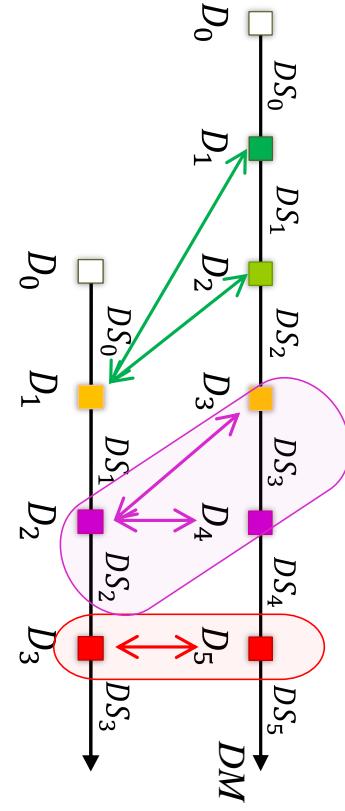


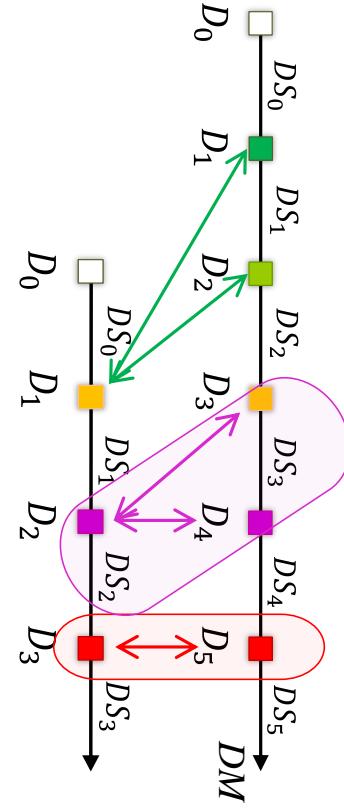
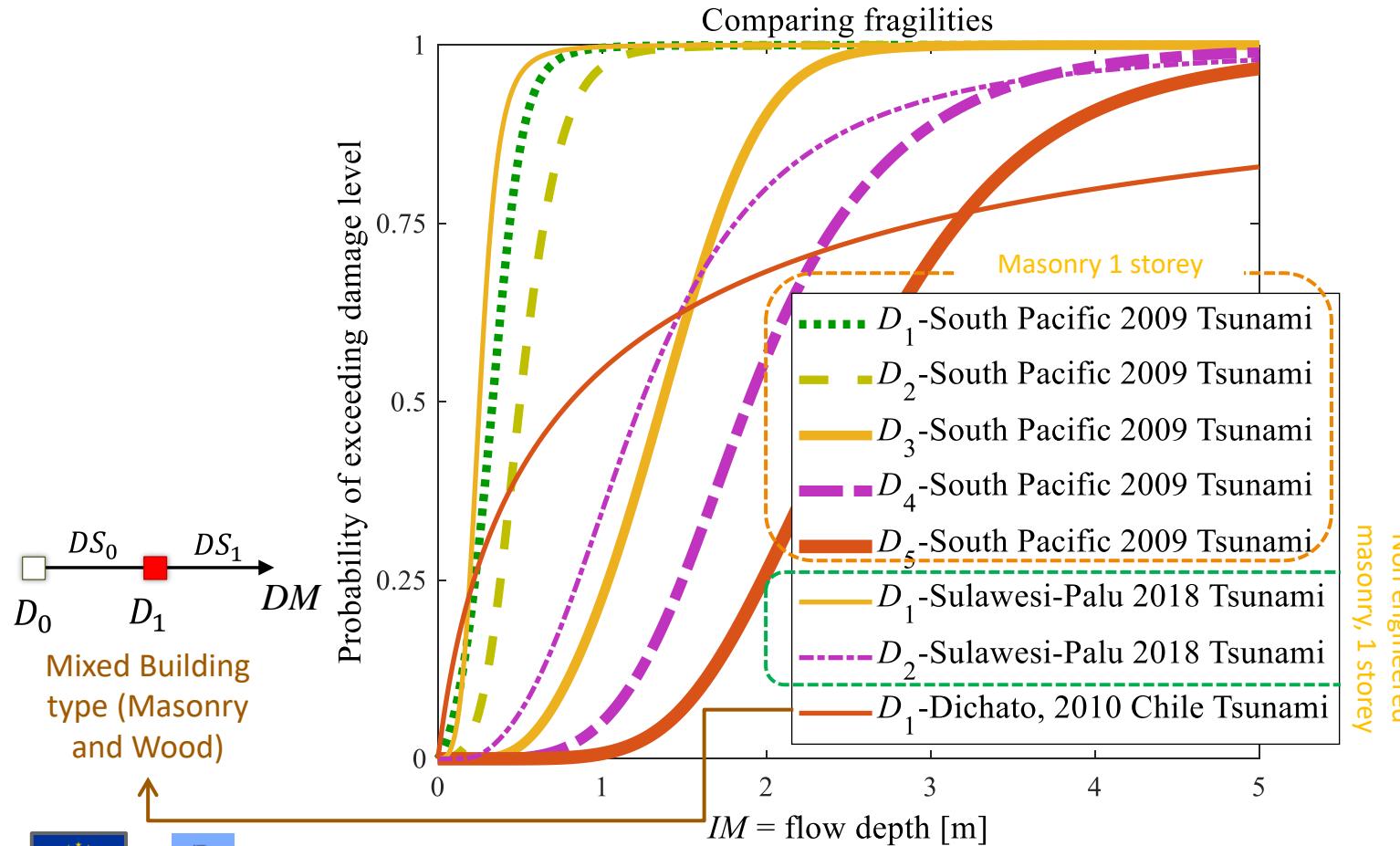


Mixed Building
type (Masonry
and Wood)



Non engineered
light timber





Vulnerability curves: propagating epistemic uncertainties in fragility



`calculate_vulnerability.m`

Vector of
fragility model
parameters

Sample
fragility curve

$$G(DV > dv | im) = \sum_{i=1}^{N_{DS}} G(DV > dv | DS_i) P(DS_i | im, \theta)$$

$P(DS_i | im, \theta)$
(Fragility Function)

DM (Damage Measure)
e.g., damage states

$G_{DV|DS}(dv | DS_i)$
(Consequence Function)

DV (Decision Variable)
e.g., fatalities, loss (loss ratio)

Sources of Uncertainty:
fragility model parameters
and consequence function

Vulnerability Curve with Epistemic Uncertainties



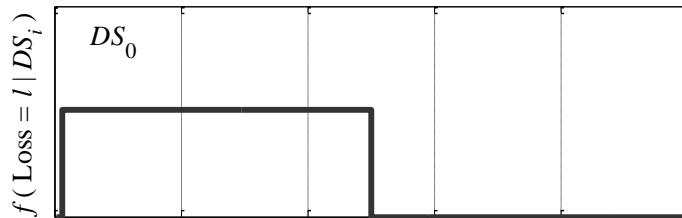
Median and logarithmic standard deviation of loss
ratio given IM



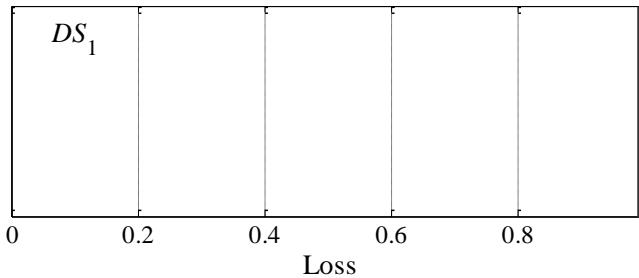
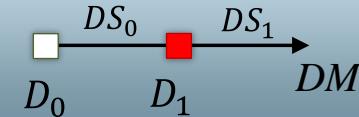
`Loss_modelk k=1,2,3`

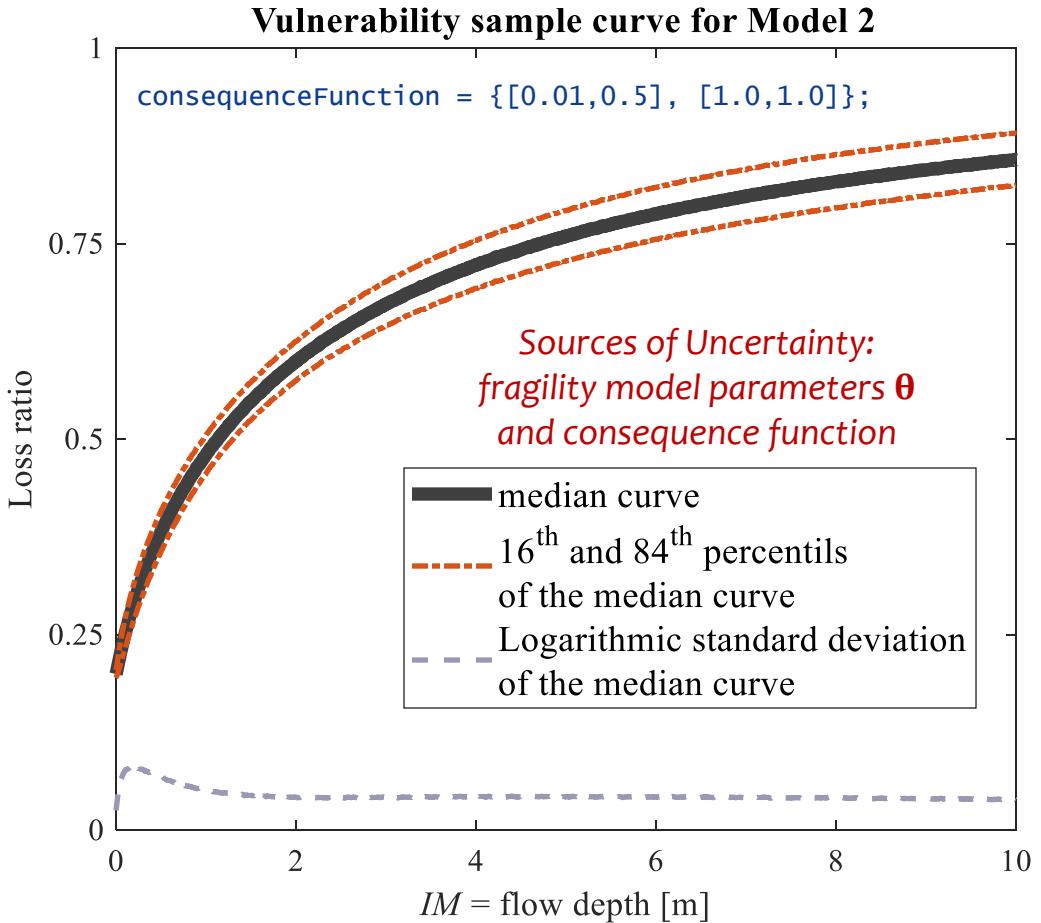
06  Tutorial

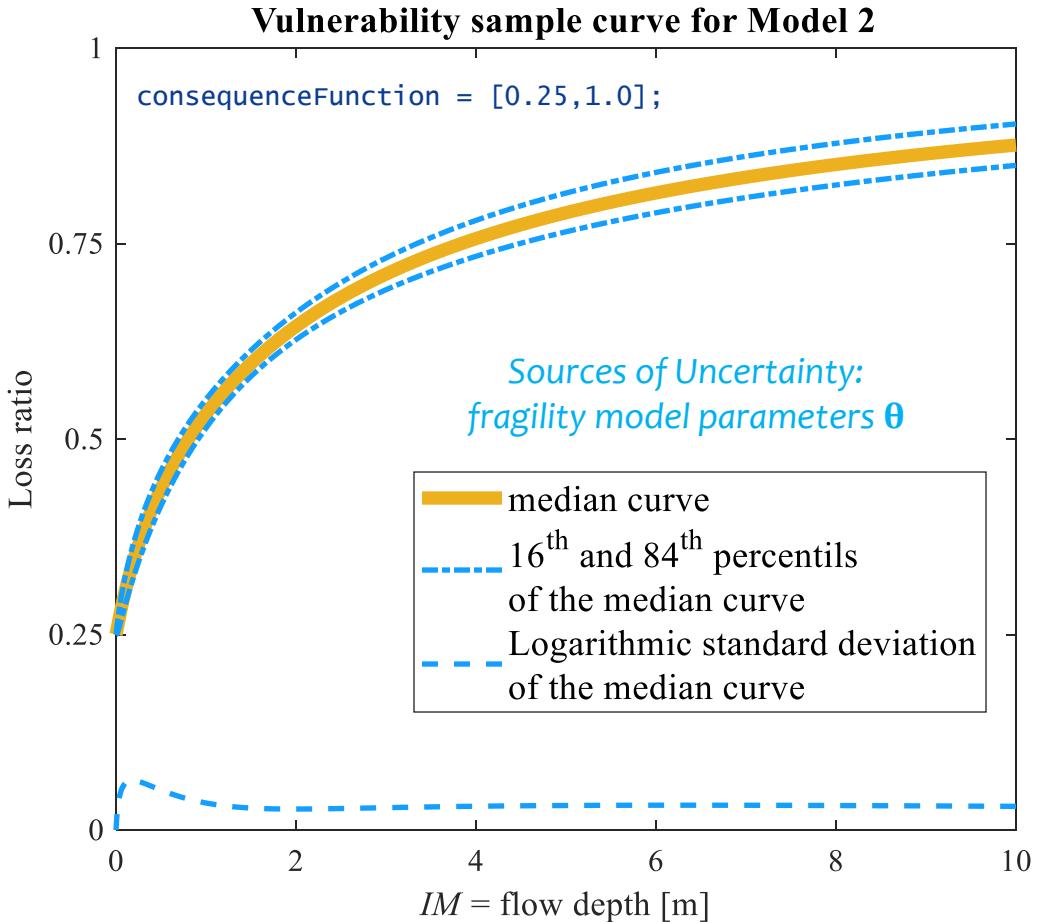
Vulnerability curves

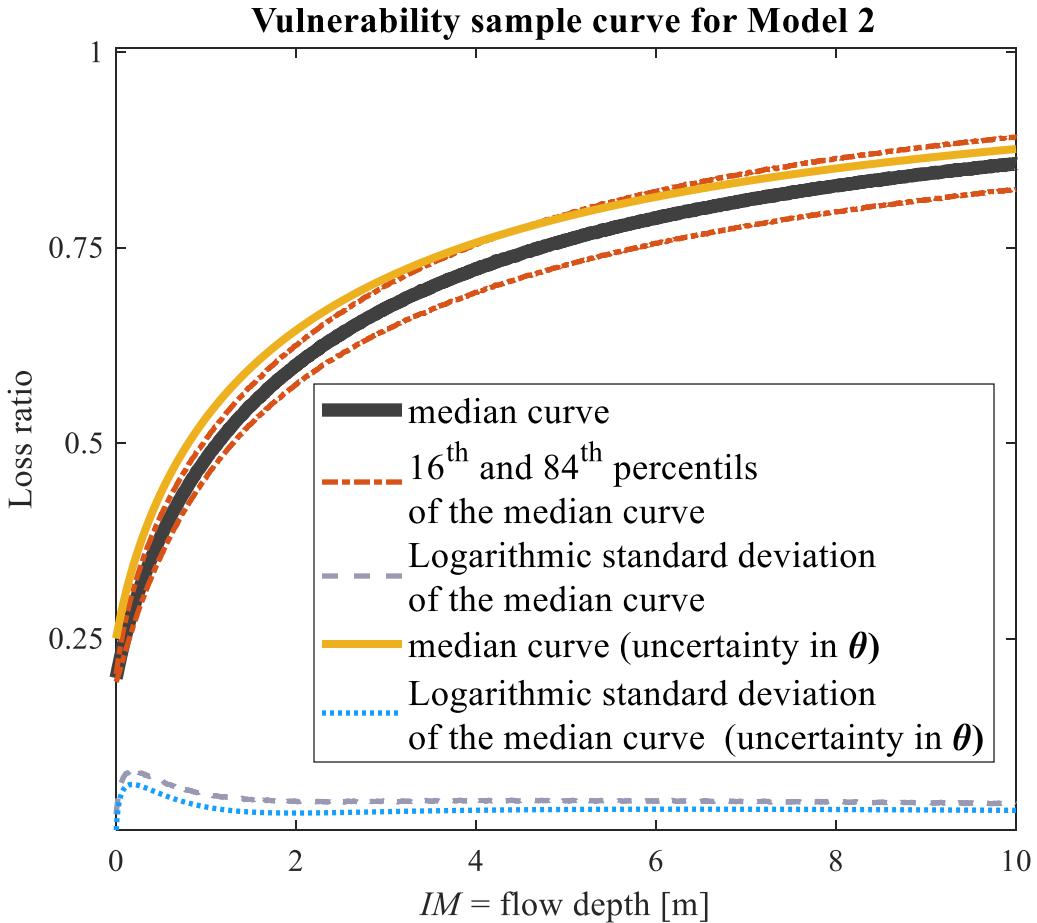


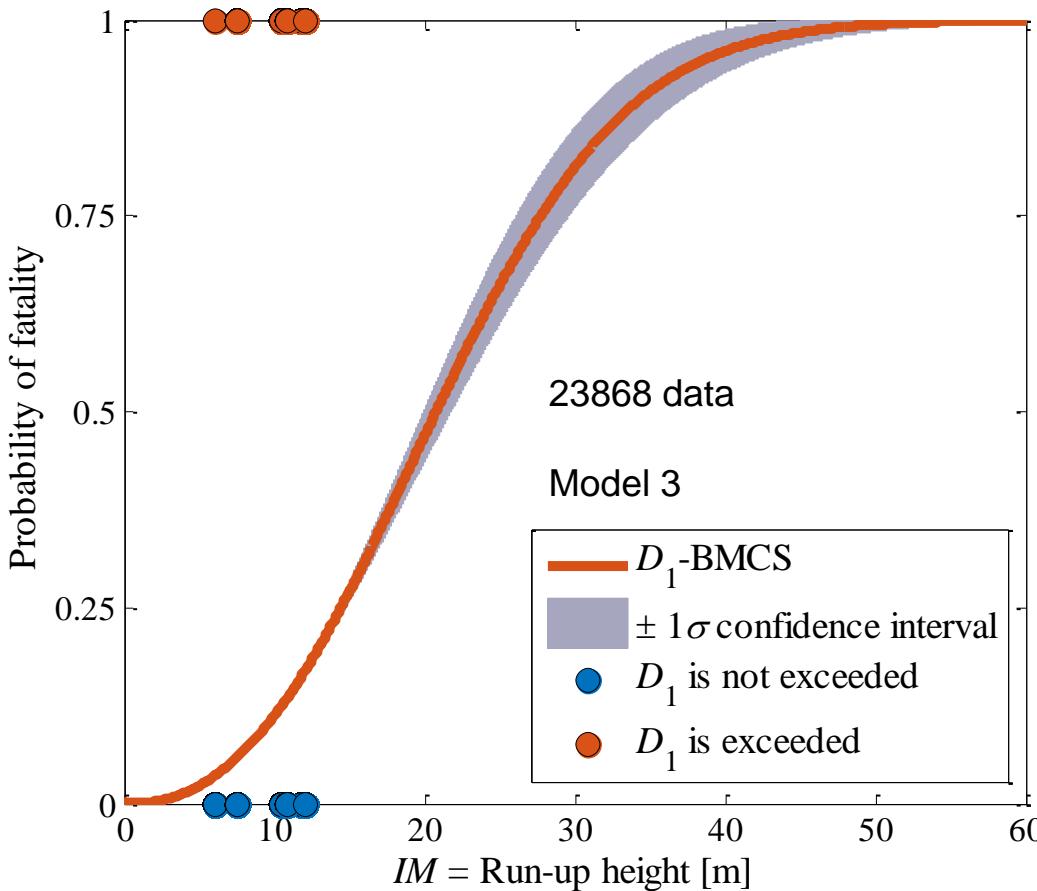
Mixed Building type (Masonry and Wood) of Dichato, Maule,
2010 Chile Tsunami



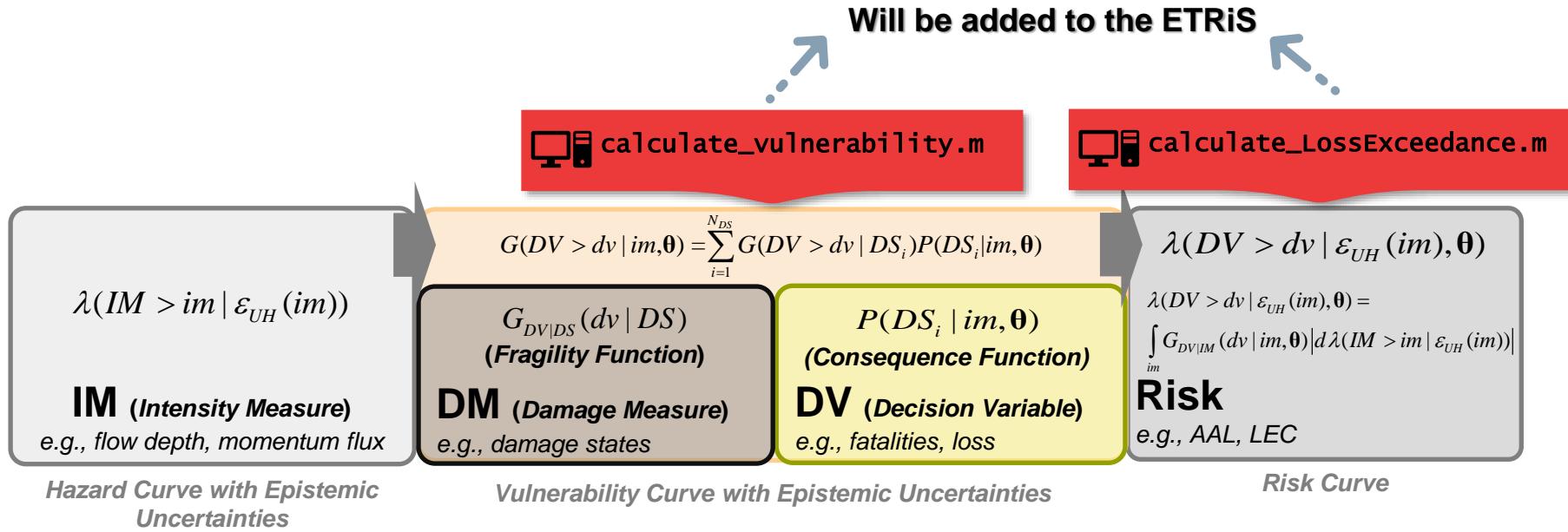








Santos, A., & Koshimura, S. (2015).
The historical review of the 1755
Lisbon Tsunami. *J. Geodesy
Geomat. Eng.*, 1, 38-52



Behrens, J., Løvholt, F., Jalayer, F., Lorito, S., Salgado-Gálvez, M.A., Sørensen, M., Abadie, S., Aguirre-Ayerbe, I., Aniel-Quiroga, I., Babeyko, A. and Baiguera, M., 2021. Probabilistic tsunami hazard and risk analysis: A review of research gaps. *Frontiers in Earth Science*, 9, p.628772.



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Geo-INQUIRE is a joint effort of 51 institutions



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