

# BVP Paper

Evan H. Anders and Benjamin P. Brown

*Dept. Astrophysical & Planetary Sciences, University of Colorado – Boulder, Boulder, CO 80309, USA and  
Laboratory for Atmospheric and Space Physics, Boulder, CO 80303, USA*

Jeffrey Oishi

*Bates*

WOW this is a really long sentence check out this abstract I'll just keep writing words to make this at least one line long so we know what the formatting looks like, ok?

## I. INTRODUCTION

In numerical studies of convection, the chosen boundary conditions at the upper and lower plates determines key quantities of the dynamics of the evolved state. Studies of incompressible, Boussinesq, Rayleigh-Bénard convection (RBC) often employ fixed temperature (Dirichlet) or fixed heat flux (Neumann) boundary conditions at both plates. Dirichlet conditions represent plates of infinite conductivity, whereas Neumann condition model plates of finite conductivity. In both cases, choosing symmetric boundary conditions maintains overall system symmetry, and despite evolving towards quite different thermal structures, both types of conditions transport heat in the same manner [1].

Studies of convection in stratified systems which aim to model convection in astrophysical systems, such as the outer envelopes of low-to-moderate mass stars like the Sun, often employ a mixture of these two types of boundary conditions [2, 3]. The flux at the lower boundary is fixed, modeling the constant energy generation of the stellar core, while the outer boundary condition is held at a fixed temperature, modeling the surface of a star which must output the energy generated internally. This set of boundary conditions is also being studied more recently in Boussinesq convection [4], and is displaying interesting characteristics such as internal layers which are stable to convection.

While this setup is a useful model for understanding natural systems, simulations which employ this setup often suffer from a long convective transient as the thermodynamic structure of the atmosphere relaxes to the adiabatic profile specified by the fixed temperature upper boundary condition. This long evolution occurs on the “Kelvin-Helmholtz,” or thermal diffusion timescale of the atmosphere,  $t_{KH} \approx L_z^2/\chi$ , where  $L_z$  is the domain depth and  $\chi$  is the thermal diffusivity. Interesting convection happens as high values of the Rayleigh number, which scales like  $\chi^{-1/2}$ , such that in the astrophysically interesting regime of high-Ra, highly stratified convection, evolving a simulation for a KH time becomes numerically intractable. As the Rayleigh number increases, the KH time increases while the average timestep required to resolve the more turbulent flows decreases. The net result is that under standard initial conditions of hydrostatic- and thermal- equilibrium, the desired convective solution cannot be obtained and the dynamics of convection there cannot be studied.

Knowledge of Mixing Length theory and the nature of evolved convection has been used in some previous studies (e.g., [5]) to choose initial conditions which are closer to the correct evolved adiabat than the hydrostatic polytropic states. However, these assumptions work best in convective regions which are bounded by stable layers. In simple atmospheres where boundary layers form to meet boundary conditions at the upper and lower edge of the atmosphere, we cannot know *a priori* what the extent or shape of the boundary layer will be, as that must be chosen by the convective dynamics, and specification of the proper boundary layer is essential for placing the atmosphere along the proper adiabat.

Here we present a method for using simple boundary value problems, along with information about the evolved flow fields, to fast-forward the slow thermal evolution of convecting simulations. We present this method in the context of RBC, and then demonstrate that applying it to stratified, compressible convection is simple. These methods allow us to study the convective flows driven by nearly the evolved thermal profile while only requiring initial value problems to run for long enough to resolve the fast dynamical timescales of convection.

## II. INCOMPRESSIBLE, BOUSSINESQ RAYLEIGH-BÉNARD CONVECTION

In general, the method for fast-forwarding the atmospheric structure to the correct adiabat is simple and involves only a few steps. At the start of convective simulations, a large transient occurs while the hydrostatic state gives way to the convective state. After the peak of this transient, we begin to average the mean vertical profile of the convective flux and the conductive flux through the domain. Once those flux profiles are converged, we solve a simple boundary value problem using the information that those fluxes provide to determine what the evolved thermal structure of the

atmosphere can be. The stratification of the initial value problems is then adjusted to match the output of the BVP, and we run convection for dynamical timescales to let the flows adjust to the new, updated thermal structure. We then measure quantities of the dynamics, and compare them to the dynamics of simulations which underwent a long thermal rundown, to determine if our simple BVPs effectively get our convective solution to the correct state.

### A. Governing Equations, Nondimensionalization, and Domain setup

In our first set of experiments, we adopt the Oberbeck-Boussinesq approximation. Here, the fluid has constant kinematic viscosity ( $\nu$ ), thermal diffusivity ( $\kappa$ ), and coefficient of thermal expansion ( $\alpha$ ). We non-dimensionalize length by the layer height ( $L_z$ ), temperature by the (constant) initial temperature gradient across the layer ( $\nabla T_0$ ), and time by the freefall timescale ( $L_z/v_{\text{ff}}$ , with  $v_{\text{ff}} = \sqrt{\alpha g L_z^2 \nabla T_0}$ , where  $g$  is uniform gravitational acceleration in the  $-\hat{z}$  direction). The dimensionless Boussinesq equations governing the velocity  $\mathbf{u} = u\hat{x} + v\hat{y} + w\hat{z}$ , temperature  $T = T_0 + T_1$ , and reduced pressure  $\varpi$  are [6]

$$\nabla \cdot \mathbf{u} = 0, \quad (1)$$

$$\frac{\partial \mathbf{u}}{\partial t} + \mathbf{u} \cdot \nabla \mathbf{u} = -\nabla \varpi + T_1 \hat{z} + \frac{\text{Pr}}{\text{Ra}} \nabla^2 \mathbf{u}, \quad (2)$$

$$\frac{\partial T_1}{\partial t} + \mathbf{u} \cdot \nabla (T_0 + T_1) = \frac{1}{\text{Pr Ra}} \nabla^2 T_1, \quad (3)$$

where the dimensionless control parameters are the Rayleigh and Prandtl numbers,

$$\text{Ra} = \frac{g \alpha L^4 \left( \frac{dT}{dz} \right)_0}{\nu \chi} = \frac{(L v_{\text{ff}})^2}{\nu \chi}, \quad \text{Pr} = \frac{\nu}{\chi}. \quad (4)$$

The dimensionless vertical extent of the domain is  $z = [-1/2, 1/2]$ , and at the boundaries we impose no-slip, impenetrable boundary conditions such that  $w = u = v = 0$  at  $z = \pm 1/2$ . At the lower boundary, we employ a fixed flux condition such that  $\partial T_1 / \partial z = 0$  at  $z = -1/2$ , and we impose a fixed temperature condition  $T_1 = 0$  at  $z = 1/2$ . Both horizontal directions are periodic and have equal aspect ratio,  $\gamma = 4$ , such that the horizontal coordinates  $x, y = [0, \Gamma]$ .

### B. The Boundary Value Problem

The Boussinesq BVP is simply the time-stationary, horizontally- and time- averaged equations of hydrostatic balance and energy conservation,

$$\frac{\partial}{\partial z} \langle \varpi \rangle = \langle T_1 \rangle \hat{z}, \quad (5)$$

$$\frac{\partial}{\partial z} \langle w T_1 \rangle = \frac{1}{\text{Pr Ra}} \frac{\partial^2}{\partial z^2} \langle T_1 \rangle, \quad (6)$$

where  $\langle A \rangle$  represents a time- and horizontally averaged profile of the quantity  $A$ . These equations arise from taking time- and horizontal- averages of Eqns (??-??) and neglecting terms that vanish due to symmetry in the evolved flows. Convective flows are perturbations around a thermal profile defined by these equations in the proper evolved state.

In Boussinesq RBC, the thermal structure of the atmosphere is fully determined by the specification of the convective flux,  $F_{\text{conv}} = \langle w T_1 \rangle$ . If this profile is known, then  $T_1$  and  $\varpi$  can be found under the proper specifications of boundary conditions. Under the choice of mixed thermal boundary conditions, the initial atmosphere contains more thermal energy ( $\propto T$ ) than the evolved adiabatic solution. As the atmosphere adjusts to be nearly isothermal in the interior, it must evolve towards the (cold) temperature value specified at the upper boundary. The evolution of the atmosphere results in an asymmetric flux profile during the slow thermal evolution of the atmosphere. Furthermore, under our nondimensionalization, the convective flux (and the flux at the upper boundary layer) are  $\mathcal{O}(1)$  during the convective transient, whereas the flux entering the atmosphere at the lower boundary is  $\mathcal{O}(\text{Ra}^{-1/2})$ , so the asymmetry of the fluxes becomes increasingly pronounced as  $\text{Ra}$  is increased into the turbulent realm.

In order to find the evolved temperature profile of the atmosphere using the Boussinesq BVP equations, the evolved profile of the convective flux must be properly specified. In order to construct this profile, we acknowledge that the

evolved solution will in flux equilibrium, carrying the amount of the flux entering through the bottom. Thus, the steady-state profile of the convective flux can be approximated as

$$F_{\text{conv, steady}} = F_{\text{bot}} \frac{\langle wT_1 \rangle}{\langle wT_1 - \kappa \partial_z(T_0 + T_1) \rangle} = F_{\text{bot}} \frac{\langle F_{\text{conv, IVP}} \rangle}{\langle F_{\text{tot, IVP}} \rangle}. \quad (7)$$

Or, put simply, the steady state convective flux is retrieved by properly removing the asymmetry from the flux profile.

In our Boussinesq BVPs, we solve Eqns. (5-6), substituting  $\langle wT_1 \rangle = F_{\text{conv, steady}}$  as defined in eqn. (7) to retrieve the proper vertical profile of  $T_1$  and  $\varpi$ . We then update the mean horizontal value of  $T_1$  and  $\varpi$  in a corresponding IVP, and continue to timestep forward with the newly adjusted atmosphere.

In essence, solving the BVP is equivalent to saying that even though the magnitude of flux through the system is not initially correct, the system appropriately picks out the ratios

$$f_{\text{conv}} = \frac{F_{\text{conv}}}{F_{\text{tot}}} \quad f_{\text{cond}} = \frac{F_{\text{cond}}}{F_{\text{tot}}}. \quad (8)$$

in the convective, transient state, but the total amount of flux is too large until the system reaches the proper isotherm.

### C. Numerics

We utilize the Dedalus<sup>1</sup> pseudospectral framework [7] to time-evolve (1)-(3) using an implicit-explicit (IMEX), third-order, four-step Runge-Kutta timestepping scheme RK443 [8]. The temperature field is decomposed as  $T = T_0(z) + T_1(x, y, z, t)$  and the velocity is  $\mathbf{u} = w\hat{\mathbf{z}} + u\hat{\mathbf{x}} + v\hat{\mathbf{y}}$ . In our 2D runs,  $v = 0$ . Variables are time-evolved on a dealiased Chebyshev (vertical) and Fourier (horizontal, periodic) domain in which the physical grid dimensions are 3/2 the size of the coefficient grid. Domain sizes range from 32x128 coefficients at the lowest values of Ra to 1024x4096 coefficients at  $\text{Ra} > 10^9$  in 2D.

As initial conditions, we fill  $T_1$  with random white noise whose magnitude is  $10^{-6}(\text{Ra Pr})^{-1/2}$ . This ensures that the initial perturbations are much smaller than the evolved convective temperature perturbations, even at large Ra. We filter this noise spectrum in coefficient space, such that only the lower 25% of the coefficients have power.

In 2D, there are often multiple steady state solutions (e.g., 2-roll and 3-roll solutions) which have slightly different flow properties (heat transport, etc.). Even though the initial perturbations are very small, they shape the convective transient and thus determine the nature of the steady state convection, at least in the laminar regime. In order to ensure that our results are not biased by differences in flow structure, we ran the simulations using distinct random temperature perturbations so as to compare statistics in comparable flow fields. In 3D, rolls are nonstationary over convective timescales, and so these effects need not be considered there.

### D. Results

We use the standard definition of the Nusselt number,

$$\text{Nu} = \frac{\langle wT - P\nabla T \rangle}{\langle -P\nabla T \rangle} = 1 + \frac{\langle wT \rangle}{-P\Delta T}, \quad (9)$$

where  $\Delta T = T(z = 1/2) - T(z = -1/2)$  is the evolved temperature difference between the top and bottom plates. This form of the Nusselt number is valid even when the system is not yet in flux equilibrium, and reduces to the standard fixed flux definition of  $\text{Nu} = [1 - \langle wT \rangle / P]^{-1}$  [1].

Here we talk about how the solutions are different, or similar. This includes:

1. Showing that the flow fields look similar
2. Showing how the temperature / flux profiles look similar/different
3. showing how Nu and Re scale with Ra in BVP / IVP.

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<sup>1</sup> <http://dedalus-project.org/>

4. showing how the PDFs of  $w$ ,  $wT$ , and  $T$  change.

Then we need to make some comments about whether this is good or bad

Then we need to mention how the same thing can be done in stratified, just there you don't assume symmetrical boundary layers.

### III. DISCUSSION & CONCLUSIONS

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#### Appendix A: Table of Boussinesq Runs

#### Appendix B: Table of stratified runs

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