# 1 Alternative hydrodynamic stellar structure equations EXPLAINED

$$\partial_r \overline{m} = -\overline{\rho} \, \overline{m} \, \overline{g}_r / \Gamma_1 \overline{P} + 4\pi r^2 \overline{\rho} \tag{1}$$

$$\partial_r \overline{P} = -\overline{\rho} \, \overline{g}_r \tag{2}$$

$$\partial_r \widetilde{L} = -4\pi r^2 \widetilde{u}_r \overline{\rho} \ \overline{g}_r / \Gamma_1 + \widetilde{\epsilon}_t \partial_r 4\pi r^2 \overline{\rho} \widetilde{u}_r \tag{3}$$

$$\partial_r \overline{T} = -(\Gamma_3 - 1) \,\overline{\rho} \,\overline{T} \,\overline{g}_r / \Gamma_1 \overline{P} \tag{4}$$

$$\partial_t \widetilde{X}_i = \widetilde{X}_i^{nuc} - (1/\overline{\rho}) \nabla_r f_i - \widetilde{u}_r \partial_r \widetilde{X}_i \tag{5}$$

Equations (1)-(4) can be derived by four assumptions: (i) adiabatic convection  $\Gamma_1 = \partial \ln P/\partial \ln \rho|_{ad}$ , (ii) hydrostatic equilibrium  $\partial_r = -\rho g_r$ , (iii)  $\epsilon_{nuc} << \varepsilon_i$ , (iv)  $\varepsilon_K << \varepsilon_i \sim \varepsilon_t$ .

### 1.1 Continuity equation

The continuity equation can be derived from first principles for adiabatic convection in hydrostatic equilibrium. We start from the definition of  $\Gamma_1 = \partial \ln P/\partial \ln \rho|_{ad}$ . I will avoid the <sub>ad</sub> suffix for clarity reasons and at some point assume hydrostatic equilibrium  $\partial_r P = -\rho g_r$ .

$$\Gamma_1 = \frac{\partial \ln P}{\partial \ln \rho} \tag{6}$$

$$\Gamma_1 = \frac{\rho}{P} \frac{\partial_r P}{\partial_r \rho} \tag{7}$$

$$\Gamma_1 P \partial_r \rho = \rho \partial_r P \tag{8}$$

$$\Gamma_1 P \partial_r \rho = \rho (-\rho g_r) \tag{9}$$

$$\partial_r \rho = -\frac{\rho \rho g_r}{\Gamma_1 P} \quad \backslash V \text{ (volume)} = 4\pi r^3 / 3$$
 (10)

$$V\partial_r \rho = -\frac{V\rho \ \rho \ g_r}{\Gamma_1 P} \tag{11}$$

$$\partial_r V \rho - \rho \partial_r V = -\frac{V \rho \ \rho \ g_r}{\Gamma_1 P} \tag{12}$$

$$\partial_r m - \rho 4\pi r^2 = -\frac{m \rho g_r}{\Gamma_1 P} \tag{13}$$

$$\partial_r m = -\frac{\rho \, m \, g_r}{\Gamma_1 P} + 4\pi r^2 \rho \tag{14}$$

$$\partial_r m = -\rho \ m \ g_r / \Gamma_1 P + 4\pi r^2 \rho \tag{15}$$

let's transform it to more familiar form (Kippenhahn & Weigert, page 4, Eq.1.6)

$$\partial_r \rho V = + V \partial_r \rho + \rho \partial_r V \tag{16}$$

$$\partial_r \rho V = + V \partial_r \rho + 4\pi r^2 \rho \tag{17}$$

$$-\rho \ m \ g_r/\Gamma_1 P + 4\pi r^2 \rho = + V \partial_r \rho + 4\pi r^2 \rho \quad (\partial_r \rho = -\rho \ \rho \ g_r/P \ \Gamma_1) \text{ can be derived from } \Gamma_1 \text{ and } \partial_r P = -\rho g_r$$
 (18)

$$\partial_r M = +4\pi r^2 \rho \tag{19}$$

## 1.2 Temperature equation

The temperature equation can be derived from first principles for adiabatic convection in hydrostatic equilibrium. We start from the definition of  $\Gamma_1 = \partial \ln P/\partial \ln \rho|_{ad}$ . I will avoid the <sub>ad</sub> suffix for clarity reasons and at some point assume hydrostatic equilibrium  $\partial_r P = -\rho g_r$ .

$$\Gamma_1 = \frac{\partial \ln P}{\partial \ln \rho} \tag{20}$$

$$\Gamma_1 = \frac{\rho}{P} \frac{\partial_r P}{\partial_r \rho} \quad \backslash \partial_r lnT \tag{21}$$

$$\partial_r lnT \ \Gamma_1 = \frac{\rho}{P} \frac{\partial_r P}{\partial_r \rho} \partial_r lnT \tag{22}$$

$$P \partial_r lnT \Gamma_1 = \rho \frac{\partial_r P}{\partial_r \rho} \partial_r lnT$$
 (23)

$$P \partial_r lnT \Gamma_1 = \frac{\partial_r P}{\partial_r ln\rho} \partial_r lnT \tag{24}$$

$$P \partial_r lnT \Gamma_1 = \frac{-\rho g_r}{\partial_r ln\rho} \partial_r lnT \tag{25}$$

$$\frac{P \partial_r T \Gamma_1}{T} = -\frac{\rho g_r}{\partial_r l n \rho} \partial_r l n T \tag{26}$$

$$-\frac{P \partial_r T \Gamma_1}{\rho g_r T} = \frac{\partial_r lnT}{\partial_r ln\rho} \tag{27}$$

$$-\frac{P \partial_r T \Gamma_1}{\rho q_r T} = \Gamma_3 - 1 \tag{28}$$

$$\partial_r T = -\frac{(\Gamma_3 - 1)\rho g_r T}{P\Gamma_1} \tag{29}$$

$$\partial_r T = -(\Gamma_3 - 1) \rho T g_r / \Gamma_1 P \tag{30}$$

let's transform it to more familiar form (Kippenhahn & Weigert, page 55, Eq.7.32)

$$\frac{\partial T}{\partial r} = -\frac{T}{P} \frac{\Gamma_3 - 1}{\Gamma_1} \rho \ g_r \tag{31}$$

$$\frac{\partial T}{\partial r} = +\frac{T}{P} \frac{\Gamma_3 - 1}{\Gamma_1} \frac{Gm}{r^2} \rho \quad \cdot \frac{1}{4\pi r^2 \rho} \tag{32}$$

$$\frac{\partial T}{\partial m} = +\frac{T}{P} \frac{Gm}{4\pi r^4} \frac{\Gamma_3 - 1}{\Gamma_1} \tag{33}$$

$$\frac{\partial T}{\partial m} = +\frac{T}{P} \frac{Gm}{4\pi r^4} \nabla_{ad} \tag{34}$$

#### 1.3 Luminosity equation

The luminosity equation can be derived from first principles for adiabatic convection in hydrostatic equilibrium. We start from the definition of  $\Gamma_1 = \partial \ln P/\partial \ln \rho|_{ad}$ . I will avoid the <sub>ad</sub> suffix for clarity reasons and at some point assume hydrostatic equilibrium  $\partial_r P = -\rho g_r$ , nuclear energy production and kinetic energy being negligible compared to internal energy i.e.  $\epsilon_{nuc} \ll \epsilon_i$  and  $\epsilon_K \ll \epsilon_i$ .

$$\Gamma_1 = \frac{\partial \ln P}{\partial \ln \rho} \tag{35}$$

$$\Gamma_1 = \frac{\rho}{P} \frac{\partial_r P}{\partial_r \rho} \tag{36}$$

$$\Gamma_1 = \frac{\rho}{P} \frac{-\rho g_r}{\partial_r \rho} = -\frac{\rho^2}{P} \frac{g_r}{\partial_r \rho} \tag{37}$$

$$\Gamma_1 = -\frac{g_r}{P\partial_r \rho/\rho^2} \tag{38}$$

$$dq = du + Pdv$$
  $dq = \epsilon_{nuc} \ll du = d\epsilon_i$   $v = 1/\rho$  1st thermodynamic law, e.g. Kippenhahn and Weigert, 1994, p.19 (39)

$$d\varepsilon_i = -Pdv = -Pd(1/\rho) = Pd\rho/\rho^2 \tag{40}$$

$$\Gamma_1 = -\frac{g_r}{\partial_r \varepsilon_i} \tag{41}$$

$$\partial_r \varepsilon_i = -\frac{g_r}{\Gamma_1} \quad \varepsilon_K \ll \varepsilon_i \text{ and } \varepsilon_i \sim \varepsilon_t$$
 (42)

$$\partial_r \varepsilon_t = -\frac{g_r}{\Gamma_1} \quad \backslash .4\pi r^2 \rho u_r \tag{43}$$

$$4\pi r^2 \rho u_r \partial_r \varepsilon_t = -\frac{4\pi r^2 \rho u_r g_r}{\Gamma_1} \tag{44}$$

$$\partial_r 4\pi r^2 \rho u_r \varepsilon_t - \varepsilon_t \partial_r 4\pi r^2 \rho u_r = -\frac{4\pi r^2 \rho u_r g_r}{\Gamma_1}$$

$$\partial_r L - \varepsilon_t \partial_r 4\pi r^2 \rho u_r = -\frac{4\pi r^2 \rho u_r g_r}{\Gamma_1}$$

$$(45)$$

$$\partial_r L - \varepsilon_t \partial_r 4\pi r^2 \rho u_r = -\frac{4\pi r^2 \rho u_r g_r}{\Gamma_1} \tag{46}$$

$$\partial_r L = -\frac{4\pi r^2 \rho u_r g_r}{\Gamma_1} + \varepsilon_t \partial_r 4\pi r^2 \rho u_r \tag{47}$$

$$\partial_r L = -4\pi r^2 u_r \rho g_r / \Gamma_1 + \varepsilon_t \partial_r 4\pi r^2 \rho u_r \tag{48}$$

#### Table 1: Definitions:

 $\rho$  density

$$m = \rho V = \rho \frac{4}{3} \pi r^3$$
 mass

T temperature

P pressure

 $u_r, u_\theta, u_\phi$  velocity components

 $\mathbf{u} = u(u_r, u_\theta, u_\phi)$  velocity

 $j_z = r \sin \theta \ u_\phi$  specific angular momentum

 $d = \nabla \cdot \mathbf{u}$  dilatation

 $\epsilon_I$  specific internal energy

h specific enthalpy

 $k = (1/2)\widetilde{u_i''u_i''}$  turbulent kinetic energy

 $\epsilon_k$  specific kinetic energy

 $\epsilon_t$  specific total energy

s specific entropy

 $v = 1/\rho$  specific volume

 $X_{\alpha}$  mass fraction of isotope  $\alpha$ 

 $\dot{X}_{\alpha}^{\mathrm nuc}$  rate of change of  $X_{\alpha}$ 

 $A_{\alpha}$  number of nucleons in isotope  $\alpha$ 

 $Z_{\alpha}$  charge of isotope  $\alpha$ 

A mean number of nucleons per isotope

Z mean charge per isotope

 $f_P = \overline{P'u'_r}$  acoustic flux

 $g_r$  radial gravitational acceleration

$$M = \int \rho(r)dV = \int \rho(r)4\pi r^2 dr$$
 integrated mass

 $S = \rho \epsilon_{\text{nuc}}(q)$  nuclear energy production (cooling function)

 $\tau_{ij} = 2\mu S_{ij}$  viscous stress tensor ( $\mu$  kinematic viscosity)

 $S_{ij} = (1/2)(\partial_i u_j + \partial_j u_i)$  strain rate

 $\widetilde{R}_{ij} = \overline{\rho} \widetilde{u_i''} u_i''$  Reynolds stress tensor

 $F_T = \chi \partial_r T$  heat flux

 $\Gamma_1 = (d \ln P/d \ln \rho)|_s$ 

 $\Gamma_2/(\Gamma_2-1)=(d\ ln\ P/d\ ln\ T)|_s$ 

 $\Gamma_3 - 1 = (d \ln T/d \ln \rho)|_s$ 

 $\widetilde{k}^r = (1/2)\widetilde{u_r''}u_r'' = (1/2)\widetilde{R}_{rr}/\overline{\rho}$  radial turbulent kinetic energy

 $\widetilde{k}^{\theta} = (1/2)\widetilde{u_{\theta}''u_{\theta}''} = (1/2)\widetilde{R}_{\theta\theta}/\overline{\rho}$  angular turbulent kinetic energy

 $\widetilde{k}^\phi=(1/2)\widetilde{u''_\phi u''_\phi}=(1/2)\widetilde{R}_{\phi\phi}/\overline{\rho}$  angular turbulent kinetic energy

 $\widetilde{k}^h = \widetilde{k}^\theta + \widetilde{k}^\phi$  horizontal turbulent kinetic energy

 $f_k = (1/2)\overline{\rho}u_i^{\prime\prime}\overline{u_i^{\prime\prime}}u_r^{\prime\prime}$  turbulent kinetic energy flux

 $f_k^r = (1/2)\overline{\rho}u_r^{\prime\prime}\overline{u_r^{\prime\prime}}u_r^{\prime\prime}$  radial turbulent kinetic energy flux

 $f_k^\theta = (1/2) \overline{\rho} u_\theta'' u_\theta'' u_r''$ angular turbulent kinetic energy flux

 $f_k^{\phi} = (1/2) \overline{\rho} u_{\phi}^{\prime\prime} \overline{u_{\phi}^{\prime\prime}} u_r^{\prime\prime}$  angular turbulent kinetic energy flux

 $f_k^h = f_k^\theta + f_k^\phi$  horizontal turbulent kinetic energy flux

 $W_p = \overline{P'd''}$  turbulent pressure dilatation

 $W_b = \overline{\rho} \overline{u_r''} \widetilde{g}_r$  buoyancy

 $f_T = -\overline{\chi \partial_r T}$  heat flux ( $\chi$  thermal conductivity)

Table 2: Definitions (continued):

$$\begin{split} f_I &= \overline{\rho_L^{\prime\prime}u_l^{\prime\prime}} & \text{ internal energy flux} & f_\alpha &= \overline{\rho X_\alpha^{\prime\prime}u_l^{\prime\prime}} X_\alpha \text{ flux} \\ f_s &= \overline{\rho s^{\prime\prime\prime}u_l^{\prime\prime}} & \text{ entropy flux} & f_{jz} &= \overline{\rho j_z^{\prime\prime\prime}u_l^{\prime\prime}} & \text{ angular momentum flux} \\ f_T &= \overline{u_r^{\prime\prime}T^{\prime\prime}} & \text{ turbulent heat flux} & f_A &= \overline{\rho A^{\prime\prime\prime}u_l^{\prime\prime}} & \text{ A (mean number of nucleons per isotope) flux} \\ f_h &= \overline{\rho h^{\prime\prime\prime}u_l^{\prime\prime}} & \text{ enthalpy flux} & f_Z &= \overline{\rho Z^{\prime\prime\prime}u_l^{\prime\prime}} & \text{ A (mean number of nucleons per isotope) flux} \\ f_{\tau} &= \overline{\rho h^{\prime\prime\prime}u_l^{\prime\prime}} & \text{ enthalpy flux} & f_Z &= \overline{\rho Z^{\prime\prime\prime}u_l^{\prime\prime}} & \text{ A (mean number of nucleons per isotope) flux} \\ f_{\tau} &= \overline{\rho h^{\prime\prime\prime}u_l^{\prime\prime}} & \text{ enthalpy flux} & f_Z &= \overline{\rho Z^{\prime\prime\prime}u_l^{\prime\prime}} & \text{ A (mean number of nucleons per isotope) flux} \\ f_{\tau} &= \overline{\rho h^{\prime\prime\prime}u_l^{\prime\prime}} & \text{ viscous flux} & f_Z &= \overline{\rho Z^{\prime\prime\prime}u_l^{\prime\prime}} & \text{ A (mean number of nucleons per isotope) flux} \\ f_{\tau} &= \overline{\rho h^{\prime\prime\prime}u_l^{\prime\prime}} & \text{ viscous flux} & f_Z &= \overline{\rho Z^{\prime\prime\prime}u_l^{\prime\prime}} & \text{ A (mean number of nucleons per isotope) flux} \\ f_{\tau} &= \overline{\rho h^{\prime\prime\prime}u_l^{\prime\prime}} & \text{ viscous flux} & f_Z &= \overline{\rho Z^{\prime\prime\prime}u_l^{\prime\prime}} & \text{ A (mean number of nucleons per isotope) flux} \\ f_{\tau} &= \overline{\rho h^{\prime\prime\prime}u_l^{\prime\prime}} & \text{ viscous flux} & f_Z &= \overline{\rho Z^{\prime\prime\prime}u_l^{\prime\prime}} & \text{ Numerical effect} \\ f_{\tau} &= \overline{\rho h^{\prime\prime\prime}u_l^{\prime\prime}} & \text{ viscous flux} & f_Z &= \overline{\rho Z^{\prime\prime\prime}u_l^{\prime\prime}} & \text{ viscous flux} & f_Z &= \overline{\rho Z^{\prime\prime\prime}u_l^{\prime\prime}} & \text{ numerical effect} \\ f_{\tau}^{\prime\prime} &= \overline{\rho h^{\prime\prime\prime}u_l^{\prime\prime\prime}u_l^{\prime\prime}} & \text{ radial flux of } f_I & f_I &= \overline{\rho h^{\prime\prime\prime}u_l^{\prime\prime\prime}u_l^{\prime\prime}} & \text{ radial flux of } f_I & f_I &= \overline{\rho h^{\prime\prime\prime}u_l^{\prime\prime}u_l^{\prime\prime}} & \text{ radial flux of } f_I & f_I &= \overline{\rho h^{\prime\prime\prime}u_l^{\prime\prime\prime}u_l^{\prime\prime}} & \text{ radial flux of } f_I & f_I &= \overline{\rho h^{\prime\prime\prime}u_l^{\prime\prime\prime}u_l^{\prime\prime}} & \text{ radial flux of } f_I & f_I &= \overline{\rho h^{\prime\prime\prime}u_l^{\prime\prime\prime}u_l^{\prime\prime}} & \text{ radial flux of } f_I & f_I &= \overline{\rho h^{\prime\prime\prime}u_l^{\prime\prime\prime}u_l^{\prime\prime\prime}} & \text{ radial flux of } f_I & f_I &= \overline{\rho h^{\prime\prime\prime}u_l^{\prime\prime\prime}u_l^{\prime\prime\prime}} & \text{ radial flux of } f_I & f_I &= \overline{\rho h^{\prime\prime\prime}u_l^{\prime\prime\prime}u_l^{\prime\prime\prime}} & \text{ radial flux of } f_I & f_I &= \overline{\rho h^{\prime\prime\prime}u_l^{\prime\prime\prime}u_l^{\prime\prime\prime}} & f_I &= \overline{\rho h$$

#### Table 3: Definitions (continued):

$$\begin{array}{lll} \mathcal{G}_k^\theta = -(1/2)\overline{G_{R\theta}^\theta} - \overline{u_\theta''G_\phi^M} & \mathcal{N}_b \text{ numerical effect} \\ \mathcal{G}_k^\phi = -(1/2)\overline{G_{Q\phi}^R} - u_\phi''G_\phi^M & \mathcal{N}_{fI} = -\nabla_r(\overline{e_I''r_{fr}'}) + \overline{u_r''\tau_{ij}\partial_i u_j} - \varepsilon_I \text{ numerical effect} \\ \mathcal{G}_k^h = +\mathcal{G}_k^\theta + \mathcal{G}_k^\phi & \mathcal{N}_{fh} = -\nabla_r(\overline{e_I''r_{fr}'}) + \overline{u_r''\tau_{ij}\partial_i u_j} - \overline{u_r''\nabla_i u_i\tau_{ji}} - \varepsilon_h \text{ numerical effect} \\ \mathcal{G}_a = +\overline{\rho'vG_r^M} & \mathcal{N}_{fs} = -\nabla_r(\overline{s''r_{fr}'}) + \overline{u_r''\tau_{ij}\partial_i u_j} / T - \varepsilon_s \text{ numerical effect} \\ \mathcal{G}_I = -\overline{G_r^I} - \overline{\epsilon_I''G_r^M} & \mathcal{N}_{fs} = -\nabla_r(\overline{s''r_{fr}'}) - \varepsilon_A \text{ numerical effect} \\ \mathcal{G}_A = -\overline{G_r^\alpha} - \overline{X_\alpha''G_r^M} & \mathcal{N}_{fs} = -\nabla_r(\overline{Z''r_{fr}'}) - \varepsilon_A \text{ numerical effect} \\ \mathcal{G}_A = -\overline{G_r^\alpha} - \overline{A''G_r^M} & \mathcal{N}_{fs} = -\nabla_r(\overline{Z''r_{fr}'}) - \varepsilon_A \text{ numerical effect} \\ \mathcal{G}_A = -\overline{G_r^\alpha} - \overline{A''G_r^M} & \mathcal{N}_{fs} = -\nabla_r(\overline{a''r_{fr}'}) - \varepsilon_A \text{ numerical effect} \\ \mathcal{G}_B = -\overline{G_r^\alpha} - \overline{A''G_r^M} & \mathcal{N}_{fs} = -\nabla_r(\overline{a''r_{fr}'}) - \varepsilon_A \text{ numerical effect} \\ \mathcal{G}_B = -\overline{G_r^\alpha} - \overline{A''G_r^M} & \mathcal{N}_{fs} = -\nabla_r(\overline{a''r_{fr}'}) - \varepsilon_A \text{ numerical effect} \\ \mathcal{G}_B = -\overline{G_r^\alpha} - \overline{A''G_r^M} & \mathcal{N}_{fs} = -\nabla_r(\overline{a''r_{fr}'}) - \varepsilon_B \text{ numerical effect} \\ \mathcal{G}_B = -\overline{G_r^\alpha} - \overline{A''G_r^M} & \mathcal{N}_{fs} = -\nabla_r(\overline{a''r_{fr}'}) - \varepsilon_B \text{ numerical effect} \\ \mathcal{G}_B = -\overline{G_r^\alpha} - \overline{A''G_r^M} & \mathcal{N}_{fs} = -\nabla_r(\overline{a''r_{fr}'}) - \varepsilon_B \text{ numerical effect} \\ \mathcal{G}_B = -\overline{G_r^\alpha} - \overline{A''G_r^M} & \mathcal{N}_{fs} = -\nabla_r(\overline{a''r_{fr}'}) - \varepsilon_B \text{ numerical effect} \\ \mathcal{G}_B = -\overline{G_r^\alpha} - \overline{A''G_r^M} & \mathcal{N}_{fs} = +\overline{A''r_{fs}'} - \overline{a''r_{fs}'} - \overline{a''r_{fs}'} - \overline{a''r_{fs}'} - \overline{a''r_{fs}'} - \overline{a''r_{fs}'} \\ \mathcal{G}_B = -\overline{G_r^\alpha} - \overline{A''G_r^M} & \mathcal{N}_{fs} = +2(\Gamma_3 - 1)\overline{P'\tau_{ij}\partial_i u_j} \text{ numerical effect} \\ \mathcal{N}_{\sigma_B} = +2\overline{A''r_{fs}'} - 2\varepsilon_F^\alpha \text{ numerical effect} \\ \mathcal{N}_{\sigma_B} = +2\overline{A''r_{fs}'} - 2\varepsilon_F^\alpha \text{ numerical effect} \\ \mathcal{N}_{\sigma_B} = +2\overline{A''r_{fs}'} - 2\varepsilon_F^\alpha \text{ numerical effect} \\ \mathcal{N}_{\sigma_B} = +2\overline{A''r_{fs}'} - 2\varepsilon_F^\alpha \text{ numerical effect} \\ \mathcal{N}_{\sigma_B} = +2\overline{A''r_{fs}'} - 2\varepsilon_F^\alpha \text{ numerical effect} \\ \mathcal{N}_{\sigma_B} = -2\overline{A''r_{fs}'} - 2\varepsilon_F^\alpha \text{ numerical effect}$$

Table 4: Definitions (continued):

$$\begin{split} \varepsilon_k^r &= \overline{\tau_{rr}'} \partial_r u_l''' + \overline{\tau_{r\theta}'} (1/r) \partial_\theta u_l'' + \overline{\tau_{r\phi}'} (1/r \sin \theta) \partial_\phi u_l'' \\ \varepsilon_k^\theta &= \overline{\tau_{\theta}'} \partial_r u_\theta''' + \overline{\tau_{\theta\theta}'} (1/r) \partial_\theta u_\theta'' + \overline{\tau_{\theta\phi}'} (1/r \sin \theta) \partial_\phi u_\theta'' \\ \varepsilon_k^\phi &= \overline{\tau_{\theta}'} \partial_r u_\theta'' + \overline{\tau_{\theta\theta}'} (1/r) \partial_\theta u_\theta'' + \overline{\tau_{\theta\phi}'} (1/r \sin \theta) \partial_\phi u_\theta'' \\ \varepsilon_k^\phi &= \overline{\tau_{\theta}'} \partial_r u_\theta'' + \overline{\tau_{\theta\theta}'} (1/r) \partial_\theta u_\phi'' + \overline{\tau_{\phi\phi}'} (1/r \sin \theta) \partial_\phi u_\phi'' \\ \varepsilon_k^\phi &= \varepsilon_k^\phi + \varepsilon_k^\phi \\ \varepsilon_k^\phi &= \varepsilon_k^\theta + \varepsilon_k^\phi \\ \varepsilon_k^\phi &= \varepsilon_k^\theta + \varepsilon_k^\phi \\ \varepsilon_k^\phi &= \overline{\rho'} v \nabla_r \overline{\tau_{rr}'} \\ \varepsilon_k &= \varepsilon_l^\theta + \varepsilon_k^\phi \\ \varepsilon_k &= \overline{\varepsilon_r'} \nabla_r \varepsilon_l'' + \overline{\tau_{r\theta}'} (1/r) \partial_\theta \varepsilon_l'' + \overline{\tau_{r\phi}'} (1/r \sin \theta) \partial_\phi \varepsilon_l'' \\ \varepsilon_k &= \overline{\tau_{rr}'} \partial_r \varepsilon_l'' + \overline{\tau_{r\theta}'} (1/r) \partial_\theta \varepsilon_l'' + \overline{\tau_{r\phi}'} (1/r \sin \theta) \partial_\phi \varepsilon_l'' \\ \varepsilon_k &= \overline{\tau_{rr}'} \partial_r \overline{\lambda_l''} + \overline{\tau_{r\theta}'} (1/r) \partial_\theta X_\alpha'' + \overline{\tau_{r\phi}'} (1/r \sin \theta) \partial_\phi X_\alpha'' \\ \varepsilon_k &= \overline{\tau_{rr}'} \partial_r \overline{\lambda_l''} + \overline{\tau_{r\theta}'} (1/r) \partial_\theta X_\alpha'' + \overline{\tau_{r\phi}'} (1/r \sin \theta) \partial_\phi X_\alpha'' \\ \varepsilon_k &= \overline{\tau_{rr}'} \partial_r \overline{\lambda_l''} + \overline{\tau_{r\theta}'} (1/r) \partial_\theta Z_l'' + \overline{\tau_{r\phi}'} (1/r \sin \theta) \partial_\phi Z_l'' \\ \varepsilon_k &= \overline{\tau_{rr}'} \partial_r \overline{\lambda_l''} + \overline{\tau_{r\theta}'} (1/r) \partial_\theta Z_l'' + \overline{\tau_{r\phi}'} (1/r \sin \theta) \partial_\phi Z_l'' \\ \varepsilon_k &= \overline{\tau_{rr}'} \partial_r \overline{\lambda_l''} + \overline{\tau_{r\theta}'} (1/r) \partial_\theta Z_l'' + \overline{\tau_{r\phi}'} (1/r \sin \theta) \partial_\phi Z_l'' \\ \varepsilon_k &= \overline{\tau_{rr}'} \partial_r \overline{\lambda_l''} + \overline{\tau_{r\theta}'} (1/r) \partial_\theta Z_l'' + \overline{\tau_{r\phi}'} (1/r \sin \theta) \partial_\phi Z_l'' \\ \varepsilon_k &= \overline{\tau_{rr}'} \partial_r \overline{\lambda_l''} + \overline{\tau_{r\theta}'} (1/r) \partial_\theta Z_l'' + \overline{\tau_{r\phi}'} (1/r \sin \theta) \partial_\phi Z_l'' \\ \varepsilon_k &= \overline{\tau_{rr}'} \partial_r \overline{\lambda_l''} + \overline{\tau_{r\theta}'} (1/r) \partial_\theta Z_l'' + \overline{\tau_{r\phi}'} (1/r \sin \theta) \partial_\phi Z_l'' \\ \varepsilon_k &= \overline{\tau_{rr}'} \partial_r \overline{\lambda_l''} + \overline{\tau_{r\theta}'} (1/r) \partial_\theta Z_l'' + \overline{\tau_{r\phi}'} (1/r \sin \theta) \partial_\phi Z_l'' \\ \varepsilon_k &= \overline{\tau_{rr}'} \partial_r \overline{\lambda_l''} + \overline{\tau_{r\theta}'} (1/r) \partial_\theta Z_l'' + \overline{\tau_{r\phi}'} (1/r \sin \theta) \partial_\phi Z_l'' \\ \varepsilon_k &= \overline{\tau_{rr}'} \partial_r \overline{\lambda_l''} + \overline{\tau_{r\theta}'} (1/r) \partial_\theta Z_l'' + \overline{\tau_{r\phi}'} (1/r \sin \theta) \partial_\phi Z_l'' \\ \varepsilon_k &= \overline{\tau_{rr}'} \partial_r \overline{\lambda_l''} + \overline{\tau_{r\theta}'} (1/r) \partial_\theta Z_l'' + \overline{\tau_{r\phi}'} (1/r \sin \theta) \partial_\phi Z_l'' \\ \varepsilon_k &= \overline{\tau_{rr}'} \partial_r \overline{\lambda_l''} + \overline{\tau_{r\theta}'} (1/r) \partial_\theta Z_l'' + \overline{\tau_{r\phi}'} (1/r \sin \theta) \partial_\phi Z_l'' \\ \varepsilon_k &= \overline{\tau_{rr}'} \partial_r \overline{\lambda_l''} + \overline{\tau_{r\theta}'} (1/r) \partial_\theta Z_l'' + \overline{\tau_{r\phi}'} (1/r \sin \theta) \partial_\phi Z_l'' \\ \varepsilon_k &= \overline{\tau_{rr}'} \partial_r \overline{$$

$$\nabla(.) = \nabla_r(.) + \nabla_{\theta}(.) + \nabla_{\phi}(.) = \frac{1}{r^2} \partial_r(r^2.) + \frac{1}{r \sin \theta} \partial_{\theta}(\sin \theta.) + \frac{1}{r \sin \theta} \partial_{\phi}(.)$$