

# 1 Hydrodynamic stellar structure equations (non-local and time-dependent)

Below is a set of hydrodynamic stellar structure equations derived from RANS (viscosity explicitly neglected), where red terms are the ones used in classical approach:

$$\partial_r \bar{m} = 4\pi r^2 \bar{\rho} + (4\pi r^3/3 \tilde{u}_r) [-\nabla_r f_\rho + (f_\rho/\bar{\rho}) \partial_r \bar{\rho} - \bar{\rho} \bar{d} - \partial_t \bar{\rho}] \quad (1)$$

$$\partial_r \bar{P} = \bar{\rho} \tilde{g} - \bar{\rho} \partial_t \tilde{u}_r - \nabla_r \tilde{R}_{rr} - \bar{G}_r^M - \bar{\rho} \tilde{u}_r \partial_r \tilde{u}_r \quad (2)$$

$$\partial_r \tilde{L} = 4\pi r^2 \bar{\rho} \tilde{\epsilon}_{nuc} + 4\pi r^2 [-\nabla_r (f_i + f_{th} + f_K + f_p) - \bar{P} \bar{d} - \tilde{R}_{ir} \partial_r \tilde{u}_i + W_b + \bar{\rho} \tilde{D}_t \tilde{u}_i \tilde{u}_i / 2 - \bar{\rho} \partial_t \tilde{\epsilon}_t] + \tilde{\epsilon}_t \partial_r 4\pi r^2 \bar{\rho} \tilde{u}_r \quad (3)$$

$$\partial_r \bar{T} = (1/\bar{u}_r) [-\nabla_r f_T + (1 - \Gamma_3) \bar{T} \bar{d} + (2 - \Gamma_3) \bar{T}' \bar{d}' + \epsilon_{nuc}/c_v + \nabla \cdot f_{th}/(\rho c_v) - \partial_t T] \quad (4)$$

$$\partial_t \tilde{X}_i = \tilde{X}_i^{nuc} - (1/\bar{\rho}) \nabla_r f_i - \tilde{u}_r \partial_r \tilde{X}_i \quad (5)$$

## 1.1 Continuity Equation

### Derivation

Using full 3D hydrodynamic continuity equation, we derive its mean field counterpart in the following way:

$$\begin{aligned} \partial_t \rho + \nabla \rho \mathbf{u} &= 0 \\ \partial_t \bar{\rho} + \bar{u}_r \partial_r \bar{\rho} &= -\nabla_r \overline{\rho' u'_r} - \bar{\rho} \bar{d} \\ \partial_t \bar{\rho} + \overline{u''}_r \partial_r \bar{\rho} + \tilde{u}_r \partial_r \bar{\rho} &= -\nabla_r \overline{\rho' u'_r} - \bar{\rho} \bar{d} \\ \partial_t \bar{\rho} + \tilde{u}_r \partial_r \bar{\rho} &= -\nabla_r \overline{\rho' u'_r} + (\overline{\rho' u'_r}/\bar{\rho}) \partial_r \bar{\rho} - \bar{\rho} \bar{d} \\ \partial_t \bar{\rho} + \tilde{u}_r \partial_r \bar{\rho} &= -\nabla_r f_\rho + (f_\rho/\bar{\rho}) \partial_r \bar{\rho} - \bar{\rho} \bar{d} \\ \tilde{D}_t \bar{\rho} &= -\nabla_r f_\rho + (f_\rho/\bar{\rho}) \partial_r \bar{\rho} - \bar{\rho} \bar{d} \end{aligned}$$

For the derivation, we used the following identities:  $\overline{\rho u_r} = \overline{\rho' u'_r} + \overline{\rho u_r}$  and  $\overline{u''}_r = \bar{u}_r - \tilde{u}_r$  and  $\overline{\rho u''}_r = -f_\rho$  and  $f_\rho = \overline{\rho' u'_r}$  (turbulent mass flux)

From there, let us now express gradient of mean density  $\partial_r \bar{\rho}$ . We get:

$$\partial_r \bar{\rho} = -(1/\tilde{u}_r) (\nabla_r f_\rho + (f_\rho/\bar{\rho}) \partial_r \bar{\rho} - \bar{\rho} \bar{d} - \partial_t \bar{\rho}) \quad (6)$$

We want to derive hydrodynamic continuity equation into the form familiar from its classical form. Therefore, let us now find relation between  $\partial_r \bar{\rho}$  and  $\partial_r \bar{m}$  using total differentials of  $\rho$  and  $m$ . We know, that  $\rho = \rho(r, t)$  and  $m = m(r, t)$  and:

$$\begin{aligned} d\rho &= \partial_r \rho \, dr + \partial_t \rho \, dt \\ dm &= \partial_r m \, dr + \partial_t m \, dt \end{aligned}$$

Let us now transform the  $d\rho$  equation to  $dm$  equation by multiplying it by volume  $V = 4\pi r^3/3$  and few algebraic modifications:

$$\begin{aligned} V d\rho &= V \partial_r \rho \, dr + V \partial_t \rho \, dt \\ dm - \rho dV &= V \partial_r \rho \, dr + V \partial_t \rho \, dt \\ dm - 4\pi r^2 \rho dr &= V \partial_r \rho \, dr + V \partial_t \rho \, dt \\ dm &= 4\pi r^2 \rho dr + V \partial_r \rho \, dr + V \partial_t \rho \, dt \\ dm &= (4\pi r^2 \rho + V \partial_r \rho) dr + V \partial_t \rho \, dt \end{aligned}$$

By comparing this result to  $dm = \partial_r m \, dr + \partial_t m \, dt$  we get:

$$(4\pi r^2 \rho + V \partial_r \rho) dr + V \partial_t \rho \, dt = \partial_r m \, dr + \partial_t m \, dt$$

and

$$\partial_r m = V \partial_r \rho + 4\pi r^2 \rho \tag{7}$$

By space-time averaging and using equation 6 we get the desired form of the continuity equation for stellar evolution.

$$\partial_r \bar{m} = 4\pi r^2 \bar{\rho} + (4\pi r^3/3 \tilde{u}_r) \left( -\nabla_r f_\rho + (f_\rho/\bar{\rho}) \partial_r \bar{\rho} - \bar{\rho} \bar{d} - \partial_t \bar{\rho} \right) \tag{8}$$

Term description:

$$\partial_r \bar{m} = \underbrace{4\pi r^2 \bar{\rho}}_{\text{density distribution}} + (4\pi r^3/3 \tilde{u}_r) \left( \underbrace{-\nabla_r f_\rho}_{\text{transport of turbulent density field}} + \underbrace{(f_\rho/\bar{\rho}) \partial_r \bar{\rho}}_{\text{down-gradient density source/sink term}} - \underbrace{\bar{\rho} \bar{d}}_{\text{compressibility effects}} - \underbrace{\partial_t \bar{\rho}}_{\text{time-dependence}} \right) \tag{9}$$

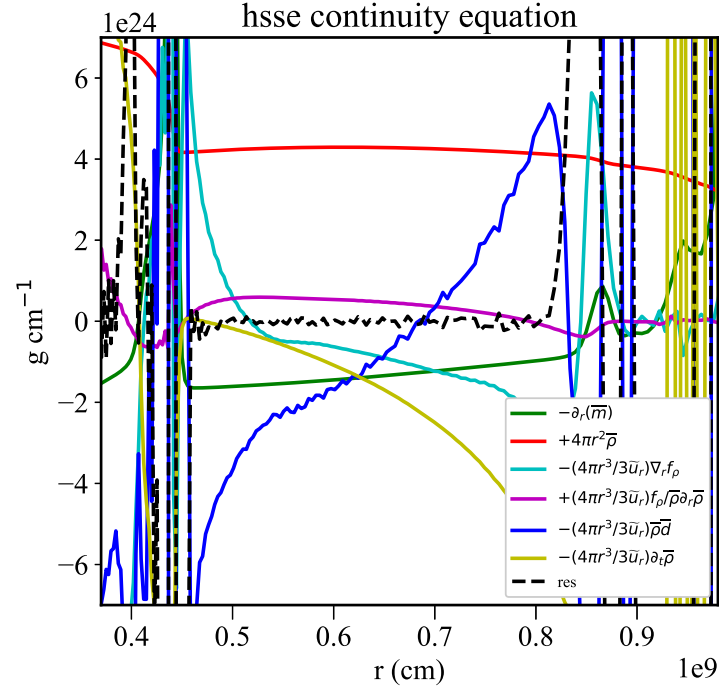


Figure 1: Hydrodynamic stellar structure continuity equation.

## 1.2 Momentum Equation

### Derivation

We start from the RANS equation for X momentum and modify it into form familiar from classical stellar evolution theory.

$$\bar{\rho}\tilde{D}_t\tilde{u}_r = -\nabla_r\tilde{R}_{rr} - \overline{G_r^M} - \partial_r\bar{P} + \bar{\rho}\tilde{g}_r \quad (10)$$

$$\bar{\rho}\partial_t\tilde{u}_r + \bar{\rho}\tilde{u}_r\partial_r\tilde{u}_r = -\nabla_r\tilde{R}_{rr} - \overline{G_r^M} - \partial_r\bar{P} + \bar{\rho}\tilde{g}_r \quad (11)$$

$$\partial_r\bar{P} = \bar{\rho}\tilde{g}_r - \bar{\rho}\partial_t\tilde{u}_r - \nabla_r\tilde{R}_{rr} - \overline{G_r^M} - \bar{\rho}\tilde{u}_r\partial_r\tilde{u}_r \quad (12)$$

Term description:

$$\partial_r \bar{P} = \underbrace{\widetilde{\rho g_r}}_{\text{gravity}} - \underbrace{\widetilde{\rho \partial_t \tilde{u}_r}}_{\text{acceleration due to expansion}} - \underbrace{\nabla_r \tilde{R}_{rr}}_{\text{transport of turbulent velocity field}} - \underbrace{\overline{G_r^M}}_{\text{centrifugal forces}} - \underbrace{\widetilde{\rho \tilde{u}_r \partial_r \tilde{u}_r}}_{\text{advection due to expansion}} \quad (13)$$

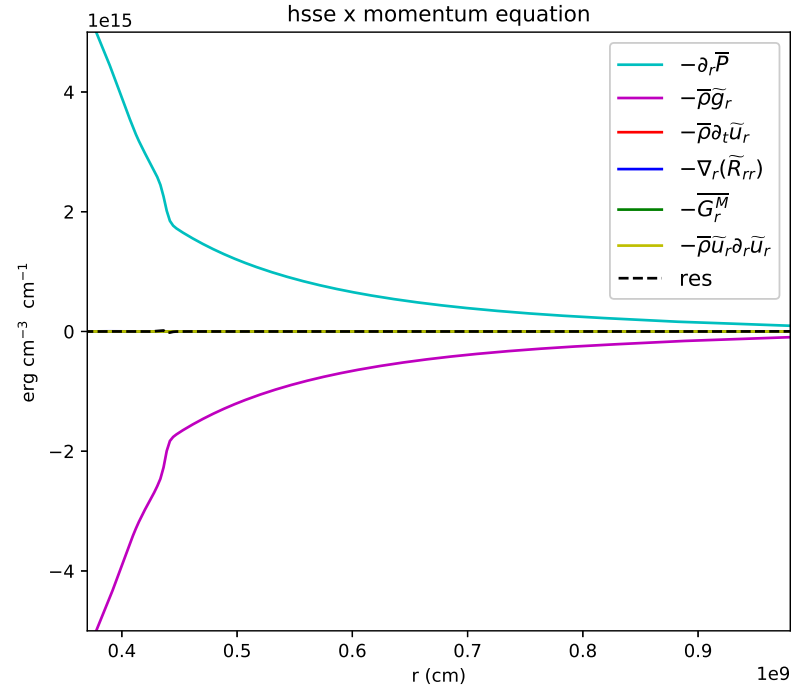


Figure 2: Hydrodynamic stellar structure momentum equation.

### 1.3 Luminosity Equation

$$\bar{\rho}\tilde{D}_t\tilde{\epsilon}_t = -\nabla_r(f_i + f_{th} + f_K + f_p) - \bar{P}\bar{d} - \tilde{R}_{ir}\partial_r\tilde{u}_r + W_b + \bar{\rho}\tilde{\epsilon}_{nuc} + \bar{\rho}\tilde{D}_t\tilde{u}_i\tilde{u}_i/2 \quad (14)$$

$$\bar{\rho}\partial_t\tilde{\epsilon}_t + \bar{\rho}\tilde{u}_r\partial_r\tilde{\epsilon}_t = -\nabla_r(f_i + f_{th} + f_K + f_p) - \bar{P}\bar{d} - \tilde{R}_{ir}\partial_r\tilde{u}_r + W_b + \bar{\rho}\tilde{\epsilon}_{nuc} + \bar{\rho}\tilde{D}_t\tilde{u}_i\tilde{u}_i/2 \quad (15)$$

$$4\pi r^2\bar{\rho}\partial_t\tilde{\epsilon}_t + 4\pi r^2\bar{\rho}\tilde{u}_r\partial_r\tilde{\epsilon}_t = 4\pi r^2 \left[ -\nabla_r(f_i + f_{th} + f_K + f_p) - \bar{P}\bar{d} - \tilde{R}_{ir}\partial_r\tilde{u}_r + W_b + \bar{\rho}\tilde{\epsilon}_{nuc} + \bar{\rho}\tilde{D}_t\tilde{u}_i\tilde{u}_i/2 \right] \quad (16)$$

$$4\pi r^2\bar{\rho}\partial_t\tilde{\epsilon}_t + \underbrace{\partial_r 4\pi r^2\bar{\rho}\tilde{u}_r\tilde{\epsilon}_t}_{\partial_r\tilde{L}} - \tilde{\epsilon}_t\partial_r 4\pi r^2\bar{\rho}\tilde{u}_r = 4\pi r^2 \left[ -\nabla_r(f_i + f_{th} + f_K + f_p) - \bar{P}\bar{d} - \tilde{R}_{ir}\partial_r\tilde{u}_r + W_b + \bar{\rho}\tilde{\epsilon}_{nuc} + \bar{\rho}\tilde{D}_t\tilde{u}_i\tilde{u}_i/2 \right] \quad (17)$$

$$\partial_r\tilde{L} = 4\pi r^2 \left[ -\nabla_r(f_i + f_{th} + f_K + f_p) - \bar{P}\bar{d} - \tilde{R}_{ir}\partial_r\tilde{u}_r + W_b + \bar{\rho}\tilde{\epsilon}_{nuc} + \bar{\rho}\tilde{D}_t\tilde{u}_i\tilde{u}_i/2 - \bar{\rho}\partial_t\tilde{\epsilon}_t \right] + \tilde{\epsilon}_t\partial_r 4\pi r^2\bar{\rho}\tilde{u}_r \quad (18)$$

Or

$$\partial_r\tilde{L} = 4\pi r^2\bar{\rho}\tilde{\epsilon}_{nuc} + 4\pi r^2 \left[ -\nabla_r(f_i + f_{th} + f_K + f_p) - \bar{P}\bar{d} - \tilde{R}_{ir}\partial_r\tilde{u}_r + W_b + \bar{\rho}\tilde{D}_t\tilde{u}_i\tilde{u}_i/2 - \bar{\rho}\partial_t\tilde{\epsilon}_t \right] + \tilde{\epsilon}_t\partial_r 4\pi r^2\bar{\rho}\tilde{u}_r \quad (19)$$

Some term description:

$$\begin{aligned} \partial_r\tilde{L} = & \underbrace{4\pi r^2\bar{\rho}\tilde{\epsilon}_{nuc}}_{\text{nuclear}} + 4\pi r^2 \left[ \underbrace{-\nabla_r(f_i + f_K + f_p + f_{th})}_{\text{transport of internal energy, kinetic energy, pressure and heat due to conduction and radiation}} - \right. \\ & \underbrace{\bar{P}\bar{d}}_{\text{compressibility}} - \underbrace{\tilde{R}_{ir}\partial_r\tilde{u}_r}_{\text{down-gradient source/sink term}} + \underbrace{W_b}_{\text{buoyancy work}} + \underbrace{\bar{\rho}\tilde{D}_t\tilde{u}_i\tilde{u}_i/2 - \bar{\rho}\partial_t\tilde{\epsilon}_t}_{\text{time-dependence}} \left. \right] + \tilde{\epsilon}_t\partial_r 4\pi r^2\bar{\rho}\tilde{u}_r \end{aligned} \quad (20)$$

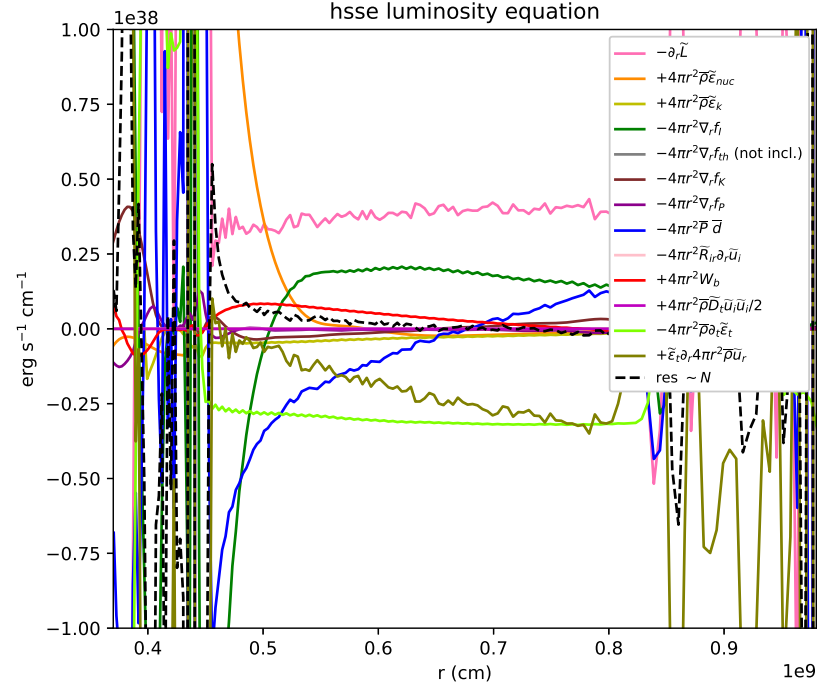


Figure 3: Hydrodynamic stellar structure luminosity equation.

## 1.4 Temperature Equation

### Derivation

We start from the RANS equation for temperature evolution. At the end, there will be no resemblance to the temperature equation of the classical stellar evolution theory.

$$\begin{aligned}
\overline{D_t T} &= -\nabla_r f_T + (1 - \Gamma_3) \overline{T} \overline{d} + (2 - \Gamma_3) \overline{T'} \overline{d'} + \overline{(\nabla \cdot f_{th}) / \rho c_v} + \overline{\epsilon_{nuc} / c_v} \\
\partial_t \overline{T} + \overline{u_r} \partial_r \overline{T} &= -\nabla_r f_T + (1 - \Gamma_3) \overline{T} \overline{d} + (2 - \Gamma_3) \overline{T'} \overline{d'} + \overline{(\nabla \cdot f_{th}) / \rho c_v} + \overline{\epsilon_{nuc} / c_v} \\
\overline{u_r} \partial_r \overline{T} &= -\nabla_r f_T + (1 - \Gamma_3) \overline{T} \overline{d} + (2 - \Gamma_3) \overline{T'} \overline{d'} + \overline{(\nabla \cdot f_{th}) / \rho c_v} + \overline{\epsilon_{nuc} / c_v} - \partial_t \overline{T}
\end{aligned}$$

$$\partial_r \bar{T} = - (1/\bar{u}_r) \left( \nabla_r f_T + (1 - \Gamma_3) \bar{T} \bar{d} + (2 - \Gamma_3) \bar{T}' \bar{d}' + \overline{(\nabla \cdot f_{th})/\rho c_v} + \overline{\epsilon_{nuc}/c_v} - \partial_t \bar{T} \right)$$

Term description:

$$\partial_r \bar{T} = - (1/\bar{u}_r) \left( \underbrace{\nabla_r f_T}_{\text{transport of turbulent temperature field}} + \underbrace{(1 - \Gamma_3) \bar{T} \bar{d} + (2 - \Gamma_3) \bar{T}' \bar{d}'}_{\text{compressibility effects}} + \underbrace{\overline{(\nabla \cdot f_{th})/\rho c_v}}_{\text{source/sink term due to thermal transport}} + \underbrace{\overline{\epsilon_{nuc}/c_v}}_{\text{source/sink due to nuclear burning}} - \underbrace{\partial_t \bar{T}}_{\text{time-dependence}} \right) \quad (21)$$

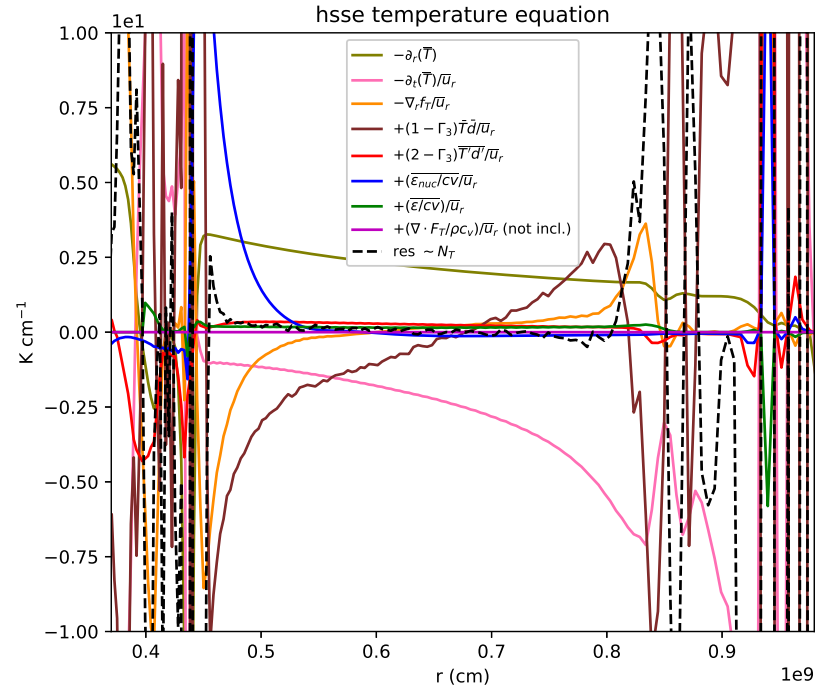


Figure 4: Hydrodynamic stellar structure temperature equation.

## 1.5 Composition Equation

### Derivation

We start from the RANS equation for composition and modify it into form familiar from classical stellar evolution theory.

$$\begin{aligned}
\bar{\rho} \tilde{D}_t \tilde{X}_\alpha &= -\nabla_r f_\alpha + \bar{\rho} \widetilde{\dot{X}_\alpha^{nuc}} \\
\bar{\rho} \partial_t \tilde{X}_\alpha + \bar{\rho} \tilde{u}_r \partial_r \tilde{X}_\alpha &= -\nabla_r f_\alpha + \bar{\rho} \widetilde{\dot{X}_\alpha^{nuc}} \\
\bar{\rho} \partial_t \tilde{X}_\alpha &= -\nabla_r f_\alpha + \bar{\rho} \widetilde{\dot{X}_\alpha^{nuc}} - \bar{\rho} \tilde{u}_r \partial_r \tilde{X}_\alpha \\
\partial_t \tilde{X}_\alpha &= \tilde{X}_\alpha^{nuc} - (1/\bar{\rho}) \nabla_r f_\alpha - \tilde{u}_r \partial_r \tilde{X}_\alpha
\end{aligned}$$

Term description:

$$\partial_t \tilde{X}_\alpha = \underbrace{\tilde{X}_\alpha^{nuc}}_{\text{nuclear burning}} - \underbrace{(1/\bar{\rho}) \nabla_r f_\alpha}_{\text{transport of turbulent composition field}} - \underbrace{\tilde{u}_r \partial_r \tilde{X}_\alpha}_{\text{advection due to expansion}} \quad (22)$$



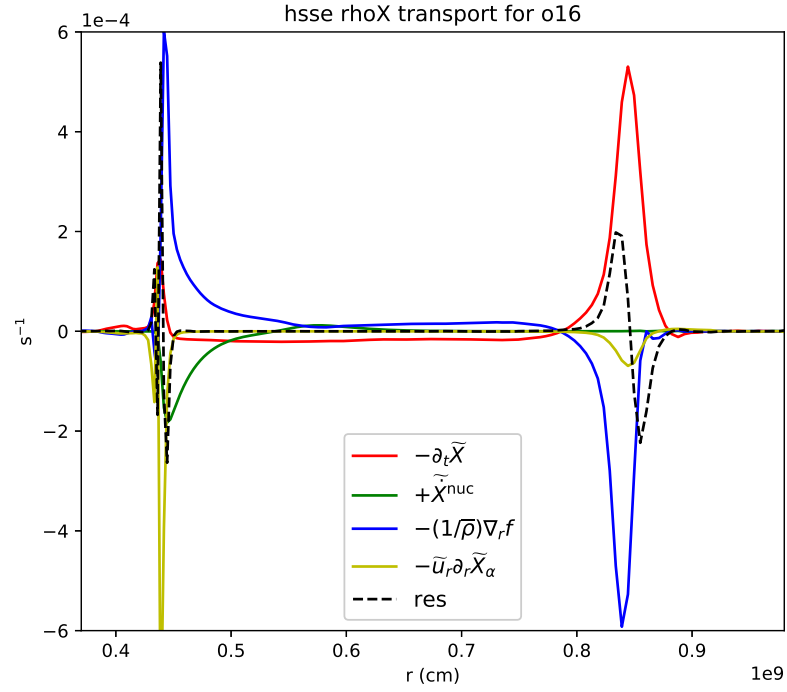


Figure 5: Hydrodynamic stellar structure composition transport equation.

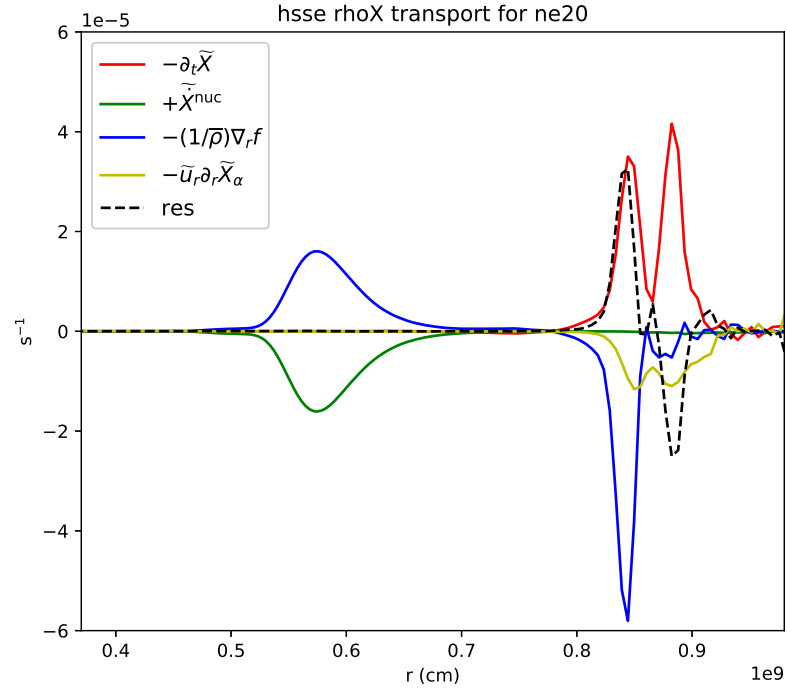


Figure 6: Hydrodynamic stellar structure composition transport equation.

Table 1: Definitions:

$\rho$ density	$g_r$ radial gravitational acceleration
$m = \rho V = \rho \frac{4}{3} \pi r^3$ mass	$M = \int \rho(r) dV = \int \rho(r) 4\pi r^2 dr$ integrated mass
$T$ temperature	$\mathcal{S} = \rho \epsilon_{\text{nuc}}(q)$ nuclear energy production (cooling function)
$P$ pressure	$\tau_{ij} = 2\mu S_{ij}$ viscous stress tensor ( $\mu$ kinematic viscosity)
$u_r, u_\theta, u_\phi$ velocity components	$S_{ij} = (1/2)(\partial_i u_j + \partial_j u_i)$ strain rate
$\mathbf{u} = u(u_r, u_\theta, u_\phi)$ velocity	$\tilde{R}_{ij} = \overline{\rho u_i'' u_j''}$ Reynolds stress tensor
$j_z = r \sin \theta u_\phi$ specific angular momentum	$F_T = \chi \partial_r T$ heat flux
$d = \nabla \cdot \mathbf{u}$ dilatation	$\Gamma_1 = (d \ln P / d \ln \rho) _s$
$\epsilon_I$ specific internal energy	$\Gamma_2 / (\Gamma_2 - 1) = (d \ln P / d \ln T) _s$
$h$ specific enthalpy	$\Gamma_3 - 1 = (d \ln T / d \ln \rho) _s$
$k = (1/2) \overline{u_i'' u_i''}$ turbulent kinetic energy	$\tilde{k}^r = (1/2) \overline{u_r'' u_r''} = (1/2) \tilde{R}_{rr} / \bar{\rho}$ radial turbulent kinetic energy
$\epsilon_k$ specific kinetic energy	$\tilde{k}^\theta = (1/2) \overline{u_\theta'' u_\theta''} = (1/2) \tilde{R}_{\theta\theta} / \bar{\rho}$ angular turbulent kinetic energy
$\epsilon_t$ specific total energy	$\tilde{k}^\phi = (1/2) \overline{u_\phi'' u_\phi''} = (1/2) \tilde{R}_{\phi\phi} / \bar{\rho}$ angular turbulent kinetic energy
$s$ specific entropy	$\tilde{k}^h = \tilde{k}^\theta + \tilde{k}^\phi$ horizontal turbulent kinetic energy
$v = 1/\rho$ specific volume	$f_k = (1/2) \overline{\rho u_i'' u_i''}$ turbulent kinetic energy flux
$X_\alpha$ mass fraction of isotope $\alpha$	$f_k^r = (1/2) \overline{\rho u_r'' u_r''}$ radial turbulent kinetic energy flux
$\dot{X}_\alpha^{\text{nuc}}$ rate of change of $X_\alpha$	$f_k^\theta = (1/2) \overline{\rho u_\theta'' u_\theta''}$ angular turbulent kinetic energy flux
$A_\alpha$ number of nucleons in isotope $\alpha$	$f_k^\phi = (1/2) \overline{\rho u_\phi'' u_\phi''}$ angular turbulent kinetic energy flux
$Z_\alpha$ charge of isotope $\alpha$	$f_k^h = f_k^\theta + f_k^\phi$ horizontal turbulent kinetic energy flux
$A$ mean number of nucleons per isotope	$W_p = \overline{P' d''}$ turbulent pressure dilatation
$Z$ mean charge per isotope	$W_b = \overline{\rho u_r'' g_r}$ buoyancy
$f_P = \overline{P' u_r'}$ acoustic flux	$f_T = -\overline{\chi \partial_r T}$ heat flux ( $\chi$ thermal conductivity)

Table 2: Definitions (continued):

$f_I = \overline{\rho \epsilon_I'' u_r''}$ internal energy flux	$f_\alpha = \overline{\rho X_\alpha'' u_r''}$ $X_\alpha$ flux
$f_s = \overline{\rho s'' u_r''}$ entropy flux	$f_{jz} = \overline{\rho j_z'' u_r''}$ angular momentum flux
$f_T = \overline{u_r' T'}$ turbulent heat flux	$f_A = \overline{\rho A'' u_r''}$ $A$ (mean number of nucleons per isotope) flux
$f_h = \overline{\rho h'' u_r''}$ enthalpy flux	$f_Z = \overline{\rho Z'' u_r''}$ $Z$ (mean charge per isotope) flux
$b = \overline{v' \rho'}$ density-specific volume covariance	$\mathcal{N}_\rho, \mathcal{N}_{ur}, \mathcal{N}_{u\theta}, \mathcal{N}_{u\phi}, \mathcal{N}_{jz}, \mathcal{N}_\alpha, \mathcal{N}_A, \mathcal{N}_Z$ numerical effect
$f_\tau = f_\tau^r + f_\tau^\theta + f_\tau^\phi$ viscous flux	$\mathcal{N}_{\epsilon I} = -\nabla_r f_\tau + \varepsilon_k$ numerical effect
$f_\tau^r = -\overline{\tau_{rr}' u_r'}$ viscous flux	$\mathcal{N}_{\epsilon k} = -\varepsilon_k$ numerical effect
$f_\tau^\theta = -\overline{\tau_{\theta r}' u_\theta'}$ viscous flux	$\mathcal{N}_{\epsilon t} = -\nabla_r f_\tau$ numerical effect
$f_\tau^\phi = -\overline{\tau_{\phi r}' u_\phi'}$ viscous flux	$\mathcal{N}_s = \overline{-\varepsilon_k / T}$ numerical effect
$f_\tau^h = f_\tau^\theta + f_\tau^\phi$ viscous flux	$\mathcal{N}_h = -\nabla_r f_\tau + (\Gamma_3 - 1)\varepsilon_k$ numerical effect
$f_I^r = \overline{\rho \epsilon_I'' u_r'' u_r''}$ radial flux of $f_I$	$\mathcal{N}_P = +(\Gamma_3 - 1)\varepsilon_k$ numerical effect
$f_s^r = \overline{\rho s'' u_r'' u_r''}$ radial flux of $f_s$	$\mathcal{N}_T = +(\tau_{ij} \partial_j u_i) / (c_v \rho)$ numerical effect
$f_h^r = \overline{\rho h'' u_r'' u_r''}$ radial flux of $f_h$	$\mathcal{N}_{Rrr} = -2\nabla_r f_\tau^r - 2\varepsilon_k^r$ numerical effect
$f_T^r = \overline{T' u_r' u_r'}$ radial flux of $f_T$	$\mathcal{N}_{R\theta\theta} = -2\nabla_r f_\tau^\theta - 2\varepsilon_k^\theta$ numerical effect
$f_{jz}^r = \overline{\rho j_z'' u_r'' u_r''}$ radial flux of $f_{jz}$	$\mathcal{N}_{R\phi\phi} = -2\nabla_r f_\tau^\phi - 2\varepsilon_k^\phi$ numerical effect
$f_\alpha^r = \overline{\rho X_\alpha'' u_r'' u_r''}$ radial flux of $f_\alpha$	$\mathcal{N}_k = -\nabla_r f_\tau - \varepsilon_k$ numerical effect
$f_A^r = \overline{\rho A'' u_r'' u_r''}$ radial flux of $f_A$	$\mathcal{N}_{kr} = -\nabla_r f_\tau^r - \varepsilon_k^r$ numerical effect
$f_Z^r = \overline{\rho Z'' u_r'' u_r''}$ radial flux of $f_Z$	$\mathcal{N}_{kh} = -\nabla_r f_\tau^h - \varepsilon_k^h$ numerical effect
$\mathcal{G}_k^r = -(1/2)\overline{G_{rr}^R} - \overline{u_r'' G_r^M}$	$\mathcal{N}_a = -\varepsilon_a$ numerical effect

Table 3: Definitions (continued):

$\mathcal{G}_k^\theta = -(1/2)\overline{G_{\theta\theta}^R} - \overline{u_\theta'' G_\theta^M}$	$\mathcal{N}_b$ numerical effect
$\mathcal{G}_k^\phi = -(1/2)\overline{G_{\phi\phi}^R} - \overline{u_\phi'' G_\phi^M}$	$\mathcal{N}_{fI} = -\nabla_r(\overline{\epsilon_I'' \tau_{rr}'}) + \overline{u_r'' \tau_{ij} \partial_i u_j} - \varepsilon_I$ numerical effect
$\mathcal{G}_k^h = +\mathcal{G}_k^\theta + \mathcal{G}_k^\phi$	$\mathcal{N}_{fh} = -\nabla_r(\overline{h'' \tau_{rr}'}) + \overline{u_r'' (\Gamma_3 - 1) \tau_{ij} \partial_i u_j} - \overline{u_r'' \nabla_i u_i \tau_{ji}} - \varepsilon_h$ numerical effect
$\mathcal{G}_a = +\overline{\rho' v G_r^M}$	$\mathcal{N}_{fs} = -\nabla_r(\overline{s'' \tau_{rr}'}) + \overline{u_r'' \tau_{ij} \partial_i u_j / T} - \varepsilon_s$ numerical effect
$\mathcal{G}_I = -\overline{G_r^I} - \overline{\epsilon_I'' G_r^M}$	$\mathcal{N}_{fA} = -\nabla_r(\overline{A'' \tau_{rr}'}) - \varepsilon_A$ numerical effect
$\mathcal{G}_\alpha = -\overline{G_r^\alpha} - \overline{X_\alpha'' G_r^M}$	$\mathcal{N}_{fZ} = -\nabla_r(\overline{Z'' \tau_{rr}'}) - \varepsilon_Z$ numerical effect
$\mathcal{G}_A = -\overline{G_r^A} - \overline{A'' G_r^M}$	$\mathcal{N}_{f\alpha} = -\nabla_r(\overline{\alpha'' \tau_{rr}'}) - \varepsilon_\alpha$ numerical effect
$\mathcal{G}_Z = -\overline{G_r^Z} - \overline{Z'' G_r^M}$	$\mathcal{N}_{fjz} = -\nabla_r(\overline{j_z'' \tau_{rr}'}) - \varepsilon_{jz}$ numerical effect
$\mathcal{G}_h = -\overline{G_r^h} - \overline{h'' G_r^M}$	$\mathcal{N}_{fT} = +\overline{T' \partial_i \tau_{ri} / \rho} + \overline{u_r' \tau_{ij} \partial_i u_j / \rho c_v}$ numerical effect
$\mathcal{G}_T = -\overline{G_r^T} - \overline{T' G_r^M}$	
$\mathcal{G}_s = -\overline{G_r^s} - \overline{s'' G_r^M}$	
$\mathcal{G}_{jz} = -\overline{G_r^{jz}} - \overline{j_z'' G_r^M}$	
$\sigma_\rho = \overline{\rho' \rho'}$	$\mathcal{N}_{\sigma_\rho}$ numerical effect
$\sigma_P = \overline{P' P'}$	$\mathcal{N}_{\sigma_P} = +2(\Gamma_3 - 1) \overline{P' \tau_{ij} \partial_i u_j}$ numerical effect
$\sigma_T = \overline{T' T'}$	$\mathcal{N}_{\sigma_T} = +2 \overline{T' \tau_{ij} \partial_i u_j / \rho c_v}$ numerical effect
$\sigma_{ur} = \overline{u_r'' u_r''}$	$\mathcal{N}_{\sigma_{ur}} = +2 \nabla_r f_\tau^r - 2 \varepsilon_k^r$ numerical effect
$\sigma_s = \overline{s'' s''}$	$\mathcal{N}_{\sigma_s} = +2 \overline{s'' \tau_{ij} \partial_j u_i / T}$ numerical effect
$\sigma_\alpha = \overline{X_\alpha'' X_\alpha''}$	$\mathcal{N}_{\sigma_\alpha}$ numerical effect    numerical effect
$\sigma_{\epsilon I} = \overline{\epsilon_I'' \epsilon_I''}$	$\mathcal{N}_{\sigma_{\epsilon I}} = +2 \overline{\epsilon_I'' \tau_{ij} \partial_j u_i}$ numerical effect

Table 4: Definitions (continued):

$$\begin{aligned}
 \varepsilon_k^r &= \overline{\tau'_{rr} \partial_r u_r''} + \overline{\tau'_{r\theta} (1/r) \partial_\theta u_r''} + \overline{\tau'_{r\phi} (1/r \sin \theta) \partial_\phi u_r''} \\
 \varepsilon_k^\theta &= \overline{\tau'_{\theta r} \partial_r u_\theta''} + \overline{\tau'_{\theta\theta} (1/r) \partial_\theta u_\theta''} + \overline{\tau'_{\theta\phi} (1/r \sin \theta) \partial_\phi u_\theta''} \\
 \varepsilon_k^\phi &= \overline{\tau'_{\phi r} \partial_r u_\phi''} + \overline{\tau'_{\phi\theta} (1/r) \partial_\theta u_\phi''} + \overline{\tau'_{\phi\phi} (1/r \sin \theta) \partial_\phi u_\phi''} \\
 \varepsilon_k &= \varepsilon_k^r + \varepsilon_k^\theta + \varepsilon_k^\phi \\
 \varepsilon_k^h &= \varepsilon_k^\theta + \varepsilon_k^\phi \\
 \varepsilon_a &= \overline{\rho' v \nabla_r \tau'_{rr}} \\
 \varepsilon_I &= \overline{\tau'_{rr} \partial_r \epsilon_I''} + \overline{\tau'_{r\theta} (1/r) \partial_\theta \epsilon_I''} + \overline{\tau'_{r\phi} (1/r \sin \theta) \partial_\phi \epsilon_I''} \\
 \varepsilon_s &= \overline{\tau'_{rr} \partial_r s''} + \overline{\tau'_{r\theta} (1/r) \partial_\theta s''} + \overline{\tau'_{r\phi} (1/r \sin \theta) \partial_\phi s''} \\
 \varepsilon_\alpha &= \overline{\tau'_{rr} \partial_r X_\alpha''} + \overline{\tau'_{r\theta} (1/r) \partial_\theta X_\alpha''} + \overline{\tau'_{r\phi} (1/r \sin \theta) \partial_\phi X_\alpha''} \\
 \varepsilon_A &= \overline{\tau'_{rr} \partial_r A''} + \overline{\tau'_{r\theta} (1/r) \partial_\theta A''} + \overline{\tau'_{r\phi} (1/r \sin \theta) \partial_\phi A''} \\
 \varepsilon_Z &= \overline{\tau'_{rr} \partial_r Z''} + \overline{\tau'_{r\theta} (1/r) \partial_\theta Z''} + \overline{\tau'_{r\phi} (1/r \sin \theta) \partial_\phi Z''} \\
 \varepsilon_h &= \overline{\tau'_{rr} \partial_r h''} + \overline{\tau'_{r\theta} (1/r) \partial_\theta h''} + \overline{\tau'_{r\phi} (1/r \sin \theta) \partial_\phi h''} \\
 \varepsilon_{jz} &= \overline{\tau'_{rr} \partial_r j_z''} + \overline{\tau'_{r\theta} (1/r) \partial_\theta j_z''} + \overline{\tau'_{r\phi} (1/r \sin \theta) \partial_\phi j_z''} \\
 G_r^M &= -\overline{\rho u_\theta u_\theta / r} - \overline{\rho u_\phi u_\phi / r} \\
 G_\theta^M &= +\overline{\rho u_\theta u_r / r} - \overline{\rho u_\phi u_\phi / (r \tan \theta)} \\
 G_\phi^M &= +\overline{\rho u_\phi u_r / r} + \overline{\rho u_\phi u_\theta / (r \tan \theta)} \\
 G_{rr}^R &= -\overline{\rho u_\theta'' u_\theta'' u_r'' / r} - \overline{\rho u_\theta'' u_r'' u_\theta'' / r} - \overline{\rho u_\phi'' u_\phi'' u_r'' / r} - \overline{\rho u_\phi'' u_r'' u_\phi'' / r} \\
 G_{\theta\theta}^R &= +\overline{\rho u_\theta'' u_r'' u_\theta'' / r} + \overline{\rho u_\theta'' u_\theta'' u_r'' / r} - \overline{\rho u_\phi'' u_\phi'' u_\theta'' / (r \tan \theta)} - \overline{u_\phi'' u_\theta'' u_\phi'' / (r \tan \theta)} \\
 G_{\phi\phi}^R &= +\overline{\rho u_\phi'' u_r'' r_\phi / r} + \overline{\rho u_\phi'' u_\theta'' u_\phi'' / (r \tan \theta)} + \overline{\rho u_\phi'' u_\phi'' u_r'' / r} + \overline{\rho u_\phi'' u_\phi'' u_\theta'' / (r \tan \theta)} \\
 G_r^I &= -\overline{\rho \epsilon_I'' u_\theta'' u_\theta'' / r} - \overline{\rho \epsilon_I'' u_\phi'' u_\phi'' / r} \\
 G_r^s &= -\overline{\rho s'' u_\theta'' u_\theta'' / r} - \overline{\rho s'' u_\phi'' u_\phi'' / r} \\
 G_r^\alpha &= -\overline{\rho X_\alpha'' u_\theta'' u_\theta'' / r} - \overline{\rho X_\alpha'' u_\phi'' u_\phi'' / r} \\
 G_r^A &= -\overline{\rho A'' u_\theta'' u_\theta'' / r} - \overline{\rho A'' u_\phi'' u_\phi'' / r} \\
 G_r^Z &= -\overline{\rho Z'' u_\theta'' u_\theta'' / r} - \overline{\rho Z'' u_\phi'' u_\phi'' / r} \\
 G_r^h &= -\overline{\rho h'' u_\theta'' u_\theta'' / r} - \overline{\rho h'' u_\phi'' u_\phi'' / r} \\
 G_r^T &= -\overline{\rho T' u_\theta' u_\theta' / r} - \overline{\rho T' u_\phi' u_\phi' / r} \\
 G_r^{jz} &= -\overline{\rho j_z'' u_\theta'' u_\theta'' / r} - \overline{\rho j_z'' u_\phi'' u_\phi'' / r}
 \end{aligned}$$

$$\nabla(\cdot) = \nabla_r(\cdot) + \nabla_\theta(\cdot) + \nabla_\phi(\cdot) = \frac{1}{r^2} \partial_r(r^2 \cdot) + \frac{1}{r \sin \theta} \partial_\theta(\sin \theta \cdot) + \frac{1}{r \sin \theta} \partial_\phi(\cdot)$$