| Company Name | LoremIpsum | Project Title | Fossee |
|-----------------|--------------|---------------|------------|
| Group/Team Name | LoremIpsum | Subtitle | |
| Designer | LoremIpsum | Job Number | 123 |
| Date | 29 /04 /2020 | Client | LoremIpsum |

1 Input Parameters

| Module | | | Fin Plate | | |
|-------------------------------|---|--------------------|--|---|--|
| MainMe | MainModule | | | Shear Connection | |
| Connectivity | | | Co | olumn flange-Beam web | |
| Shear(l | (N)* | | | 1.0 | |
| | Su | pporting Sect | ion | | |
| | Supportin | ng Section | | HB 200 | |
| | Mate | Material * | | E 250 (Fe 410 W)A | |
| т т | Ultimate strer | ngth, fu (MPa) | | 410 | |
| | Yield Streng | th , fy (MPa) | | 230 | |
| $(B-t)$ α | Mass | 37.3 | Iz(cm4) | 36000000.0 | |
| 4 | Area(cm2) - | 4750.0 | Iy(cm4) | 9670000.0 | |
| ZZ D | A | | | | |
| | D(mm) | 200.0 | rz(cm) | 87.10000000000001 | |
| R ₁ | B(mm) | 200.0 | ry(cm) | 45.09999999999994 | |
| В | t(mm) | 6.1 | Zz(cm3) | 361000.0 | |
| · · | T(mm) | 9 | Zy(cm3) | 96700.0 | |
| | FlangeSlope | 94 | Zpz(cm3) | 361000.0 | |
| | R1(mm) | 9.0 | Zpy(cm3) | 96700.0 | |
| | R2(mm) | 4.5 | | | |
| | | pported Secti | on | | |
| | | d Section | | JB 225 | |
| , | | erial * | | E 250 (Fe 410 W)A | |
| T | Ultimate strength, fu (MPa) | | 410 | | |
| | | th , fy (MPa) | | 230 | |
| $(B-t)$ α | Mass | 12.8 | Iz(cm4) | 13100000.0 | |
| 4 | Area(cm2) - | 1630.0 | Iy(cm4) | 405000.0 | |
| ZZ D | A | 227.0 | | | |
| -R. | D(mm) | 225.0 | rz(cm) | 89.7 | |
| -R ₂ | B(mm) | 80.0 | ry(cm) | 15.8 | |
| В | t(mm) | 3.7 | Zz(cm3) | 116000.0 | |
| | | | | | |
| ¥ | T(mm) | 5.0 | Zy(cm3) | 10100.0 | |
| | FlangeSlope | 91.5 | Zpz(cm3) | 116000.0 | |
| | FlangeSlope R1(mm) | 91.5 6.5 | , , | | |
| | FlangeSlope | 91.5 6.5 1.5 | Zpz(cm3) | 116000.0 | |
| Ť | FlangeSlope R1(mm) R2(mm) | 91.5 6.5 | Zpz(cm3) Zpy(cm3) | 116000.0 10100.0 | |
|) Diameter | FlangeSlope R1(mm) R2(mm) | 91.5 6.5 1.5 | Zpz(cm3) Zpy(cm3) [12.0, | 116000.0 10100.0 16.0, 20.0, 24.0, 30.0, 36.0] | |
| Diameter Grade | FlangeSlope R1(mm) R2(mm) (mm)* | 91.5 6.5 1.5 | Zpz(cm3) Zpy(cm3) [12.0, | 116000.0 10100.0 16.0, 20.0, 24.0, 30.0, 36.0] 8, 5.6, 5.8, 6.8, 8.8, 9.8, 10.9, 12.9] | |
| Diameter Grade Type | FlangeSlope R1(mm) R2(mm) (mm)* | 91.5 6.5 1.5 | Zpz(cm3) Zpy(cm3) [12.0, | 116000.0 10100.0 16.0, 20.0, 24.0, 30.0, 36.0] 8, 5.6, 5.8, 6.8, 8.8, 9.8, 10.9, 12.9] Bearing Bolt | |
| Diameter Grade Type Bolt hole | FlangeSlope R1(mm) R2(mm) (mm)* e * e * e type | 91.5 6.5 1.5 | Zpz(cm3) Zpy(cm3) [12.0, | 116000.0 10100.0 16.0, 20.0, 24.0, 30.0, 36.0] 8, 5.6, 5.8, 6.8, 8.8, 9.8, 10.9, 12.9] Bearing Bolt Standard | |
| Diameter Grade Type | FlangeSlope R1(mm) R2(mm) (mm)* e * e type r (µ_f) | 91.5 6.5 1.5 | Zpz(cm3) Zpy(cm3) [12.0, [3.6, 4.6, 4.8] | 116000.0 10100.0 16.0, 20.0, 24.0, 30.0, 36.0] 8, 5.6, 5.8, 6.8, 8.8, 9.8, 10.9, 12.9] Bearing Bolt | |

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| Gap between beam and support (mm) | 10.0 |
|--|-----------|
| Are the members exposed to corrosive influences | False |
| Weld Details | |
| Weld Type | Fillet |
| Type of weld fabrication | Shop Weld |
| Material grade overwrite (MPa) Fu | 410.0 |

2 Design Checks

2.1 Bolt Design Checks

| Check | Required | Provided | Remarks |
|------------------------|--|--|---------|
| Shear Capacity (kN) | | $V_{dsb} = \frac{f_{ub} n_n A_{nb}}{\sqrt{3} \gamma_{mb}}$ $= \frac{410 * 1 * 84.3}{\sqrt{3} * 1.25}$ $= 11.68$ | |
| Bearing Capacity (kN) | | $V_{dpb} = \frac{2.5 \ k_b \ d \ t \ f_u}{\gamma_{mb}}$ $= \frac{2.5 \ * 0.52 * 12.0 * 3.7 * 410}{1.25}$ $= 11.68$ | |
| Capacity (KN) | | $V_{db} = min (V_{dsb}, V_{dpb})$ $= min (11.68, 11.68)$ $= 11.68$ | |
| No of Bolts | $R_{u} = \sqrt{V_{u}^{2} + A_{u}^{2}}$ $n_{trial} = R_{u}/V_{bolt}$ $R_{u} = \frac{\sqrt{1.0^{2} + 1.0^{2}}}{11.68}$ $= 1$ | 2 | |
| No of Columns | | 1 | |
| No of Rows | | 2 | |
| Min. Pitch (mm) | $p/g_{min} = 2.5 d$ =2.5 * 12.0 = 30.0 | 0.0 | N/A |
| Max. Pitch (mm) | $p/g_{max} = \min(32 \ t, \ 300 \ mm)$ = $\min(32 * \ 3.7, \ 300 \ mm)$ = 300 | 0.0 | N/A |
| Min. Gauge (mm) | $p/g_{min} = 2.5 d$ = $2.5 * 12.0 = 30.0$ | 85 | Pass |
| Max. Gauge (mm) | $p/g_{max} = \min(32 \ t, \ 300 \ mm)$ = $\min(32 * \ 3.7, \ 300 \ mm)$ = 300 | 85 | Pass |
| Min. End Distance (mm) | $e/e'_{min} = [1.5 \text{ or } 1.7] * d_0$ = 1.7 * 13.0 = 22.1 | 25 | Pass |

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| Check | Required | Provided | Remarks |
|-------------------------|--|----------|---------|
| Max. End Distance (mm) | $e/e'_{max} = 12 \ t \ \varepsilon$ $\varepsilon = \sqrt{\frac{250}{f_y}}$ $e/e'_{max} = 12 \ *4.0 * \sqrt{\frac{250}{230}}$ $= 49.92$ | 25 | Pass |
| Min. Edge Distance (mm) | $e/e'_{min} = [1.5 \text{ or } 1.7] * d_0$ = 1.7 * 13.0 = 22.1 | 25 | Pass |
| Max. Edge Distance (mm) | $e/e'_{max} = 12 \ t \ \varepsilon$ $\varepsilon = \sqrt{\frac{250}{f_y}}$ $e/e'_{max} = 12 \ *4.0 * \sqrt{\frac{250}{230}}$ $= 49.92$ | 25 | Pass |
| Capacity (KN) | 1039.86 | 11680.95 | Pass |

2.2 Plate Design Checks

| Check | Required | Provided | Remarks |
|---|---|---|---------|
| Min. Plate Height (mm) | $0.6 * d_b = 0.6 * 225.0 = 135.0$ | 135 | Pass |
| Max. Plate Height (mm) | $d_b - 2(t_{bf} + r_{b1} + gap)$ $= 225.0 - 2 * (5.0 + 6.5 + 10)$ $= 202.0$ | 135 | Pass |
| Min. Plate Length (mm) | $2 * e_{min} + (n \ c - 1) * p_{min})$ $= 2 * 22.1 + (1 - 1) * 30.0$ $= 54.2$ | 60.0 | Pass |
| Min.Plate Thickness (mm) | $t_w = 3.7$ | 4.0 | Pass |
| Shear yielding Capacity (V_dy) (kN) | | $V_{dg} = \frac{A_v * f_y}{\sqrt{3} * \gamma_{mo}}$ $= \frac{135 * 4.0 * 230}{\sqrt{3} * 1.1}$ $= 39.11$ | |
| Shear Rupture Capacity (V_dn) (kN) | | $V_{dn} = \frac{0.75 * A_{vn} * f_u}{\sqrt{3} * \gamma_{mo}}$ $= 1 * (135 - (2 * 13.0)) * 4.0 * 410$ $= 134.07$ | |
| Block Shear Capacity in Shear (V_db) (kN) | | 79.79 | |
| Shear Capacity (V_d) (kN) | 1.0 | $V_d = Min(V_{dy}, V_{dn}, V_{db})$ $= Min(39.11, 134.07, 79.79)$ $= 39.11$ | Pass |

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| Check | Required | Provided | Remarks |
|--|----------|--|---------|
| Tension Yielding Capacity (kN) | | $T_{dg} = \frac{l * t * f_y}{\gamma_{mo}}$ $= \frac{60.0 * 4.0 * 230}{\sqrt{3} * 1.1}$ $= 50.18$ | |
| Tension Rupture Capacity(kN) | | $T_{dn} = \frac{0.9 * A_n * f_u}{\gamma_{m1}}$ $= \frac{0.9 * (60.0 - 2 * 13.0) * 4.0 * 410}{1.25}$ $= 55.5$ | |
| Block Shear Capacity in Tension (T_db) (kN) | | 79.79 | |
| Tension Capacity (kN) | 1.0 | $T_d = Min(T_{dg}, T_{dn}, T_{db})$ $= Min(50.18, 55.5, 79.79)$ $= 50.18$ | Pass |
| Moment Capacity (kNm) | 0.04 | 3.05 | Pass |
| Interaction Ratio | ≤ 1 | $\frac{0.04}{3.05} + \frac{1.0}{50.18} = 0.03$ | Pass |

2.3 Weld Checks

| Check | Required | Provided | Remarks |
|-----------------------|--|---|---------|
| Min Weld Size (mm) | $Thickness of Thicker part \\ = Max(9,9) = 9 \\ IS800: 2007 \ cl.10.5.2.3 \ Table 21, \\ t_{w_{min}} = 3$ | 3 | Pass |
| Max Weld Size (mm) | Thickness of Thinner part $= Min(9,9) = 4.0$ $t_{w_{max}} = 4.0$ | 3 | Pass |
| Weld Strength (kN/mm) | $R_{w} = \sqrt{(T_{wh} + A_{wh})^{2} + (T_{wv} + V_{wv})^{2}}$ $T_{wh} = \frac{M * y_{max}}{Ipw} = \frac{35000.0 * 64.5}{357781.5}$ $T_{wv} = \frac{M * x_{max}}{Ipw} = \frac{35000.0 * 0.0}{357781.5}$ $V_{wv} = \frac{V}{l_{w}} = \frac{1000.0}{258}$ $A_{wh} = \frac{A}{l_{w}} = \frac{1000.0}{258}$ $R_{w} = \sqrt{(6.31 + 3.88)^{2} + (0.0 + 3.88)^{2}}$ $= 10.9$ | $f_w = \frac{t_t * f_u}{\sqrt{3} * \gamma_{mw}}$ $= \frac{3 * 410}{\sqrt{3}} * 1.25$ $= 568.11$ | Pass |

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3 3D View



Figure 1: 3D View