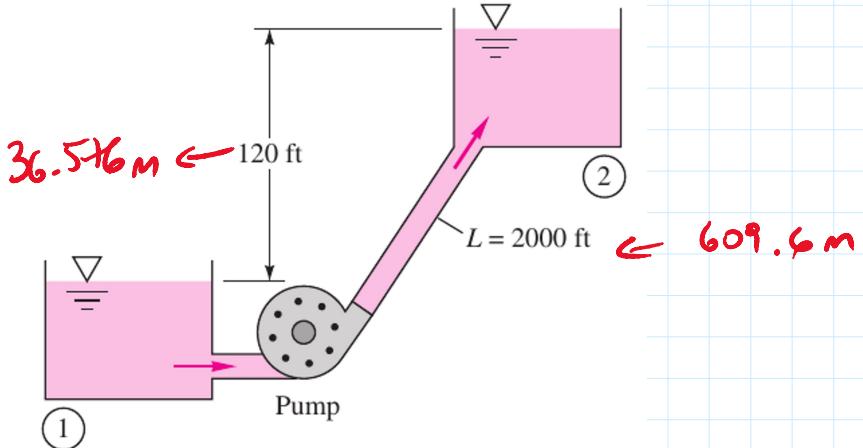


$$Q = 3 \text{ ft}^3/\text{s} = 0.0849 \text{ m}^3/\text{s}$$



$$20^\circ\text{C} \rightarrow \rho = 10^3 \text{ kg/m}^3$$

$$\mu = 0.001 \text{ Pa}\cdot\text{s}$$

Argua a 20°C

Eq. Energia

~~$$\frac{P_1}{\gamma} + \frac{V_1^2}{2g} + z_1 = \frac{P_2}{\gamma} + \frac{V_2^2}{2g} + z_2 + h_f - h_{\text{bomba}}$$~~

$$0 = z_2 - z_1 + h_f - h_{\text{bomba}}$$

Pendidos ou cargas maiores?

Eq Darcy

$$h_f = f \cdot \frac{L}{D} \cdot \frac{V^2}{2g}$$

TUBOS diam 6 in

$$D_i = 156 \text{ mm} = 0.156 \text{ m}$$

$$\epsilon = 2.4 \times 10^{-4} \text{ m}$$

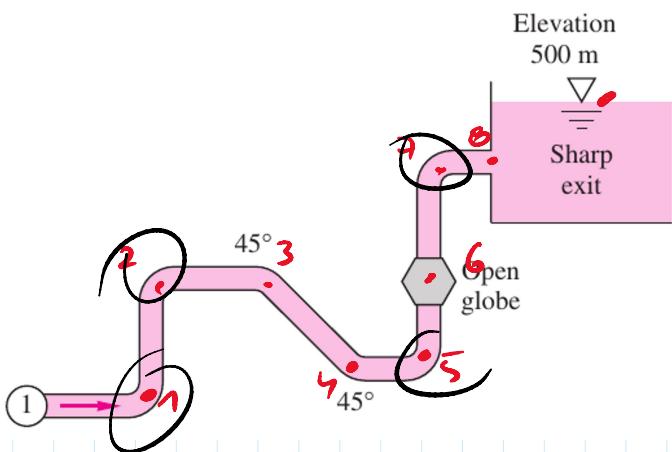
$$h_{\text{Damm}} = 210 \text{ m}$$

$$\begin{aligned}\dot{W} &= Q \cdot T \cdot h_{\text{Damm}} \\ &= 0.0849 \frac{\text{m}^3}{\text{s}} \cdot 9.81 \cdot 10^3 \frac{\text{Pa}}{\text{m}} \cdot 210 \text{ m} \\ &= 177902 \text{ W}\end{aligned}$$

$$\eta = \frac{\dot{W}_{\text{Damm}}}{\dot{W}_{\text{in}}} \rightarrow \dot{W}_{\text{in}} = \frac{\dot{W}_{\text{Damm}}}{\eta} = \frac{177902}{0.85} = 233 \text{ kW}$$

Problema 2

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F.P. Ensayo

Agua @ 20°C

$$\rho = 10^3 \text{ kg/m}^3$$

$$\mu = 10^{-3} \text{ Pa}\cdot\text{s}$$

$$Q = 0.005 \text{ m}^3/\text{s}$$

$$D = 5 \times 10^{-2} \text{ m}$$

$$\epsilon = 2.4 \times 10^{-4} \text{ m}$$

CASE I

$$\frac{P_1}{\gamma} + \frac{V_1^2}{2g} + z_1 = \frac{P_2}{\gamma} + \frac{V_2^2}{2g} + z_2 + h_f + h_L, \text{ m}$$

Pérdidas mayores:

$$h_f = f \frac{L}{D} \frac{V^2}{2g}$$

Pérdidas menores

Elementos

1, 2, 5, + 6 son 90° rectos largos

$$k = 20 \text{ ft} = k_1, k_2, k_5, k_7$$

3, 4 con dobl 45°

$$k = 16 \text{ ft} = k_3 = k_4$$

6 válvula globo cerrada

$$\frac{k_6}{D} = 340 \rightarrow k_6 = 340 \cdot ft$$

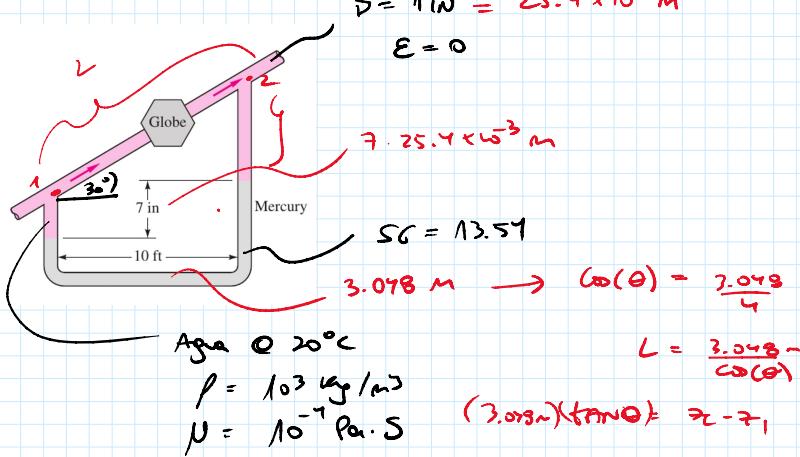
8 Salida

$$k_B = 1$$

$$h_{l,m} = \frac{v^2}{2g} \left(\sum_i k_i \right)$$

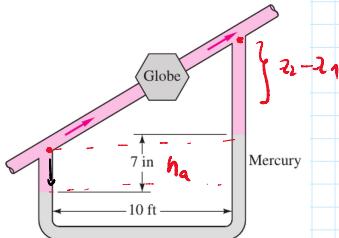
$$p_1 = \left(z_2 + h_l + h_{l,m} - \frac{v_1^2}{2g} - z_1 \right) r$$

$$p_1 = 3365 \text{ Pa}$$



Eq. Energia

~~$$P_1 + z_1 + \frac{V^2}{2g} = P_2 + z_2 + \frac{V^2}{2g} + h_f + h_m \Rightarrow 0 = \frac{P_2 - P_1}{\gamma} + (z_2 - z_1) + h_f + h_m$$~~



$$P_1 + h_a \cdot \gamma_w - h_a \cdot \gamma_{SG} - (z_2 - z_1) \cdot \gamma_w - P_2 = 0$$

$$P_1 - P_2 = - (h_a \cdot \gamma_w - h_a \cdot \gamma_{SG} - (z_2 - z_1) \cdot \gamma_w)$$

$$\frac{P_1 - P_2}{\gamma_w} = - (h_a - h_a \cdot SG_{\text{Ag}} - (z_2 - z_1)) \Rightarrow \frac{P_2 - P_1}{\gamma_w} = h_a - h_a \cdot SG_{\text{Ag}} - (z_2 - z_1) \quad (1)$$

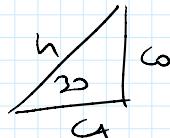
Parámetros del agua mayores

Ecuación del agua:

$$h_f = f \cdot \frac{L}{D} \cdot \frac{V^2}{2g}$$

Parámetros en el agua menores

$$K_1 = 160$$



$$\tan \theta = \frac{ca}{h}$$

$$h = \frac{ca}{\tan \theta} \rightarrow 0$$

$$\tan \theta = \frac{ca}{h}$$

$$ca = \tan \theta \cdot h$$

Resolviendo (1)

$$J = 1.65 \text{ m/s}$$

$$Q = 8.4 \times 10^{-4} \text{ m}^3/\text{s}$$

Ojo:

Si consideramos $K_1 = 160 \text{ ft}$ (de textos)

$$f_T = f(\varepsilon/D, R_f \rightarrow \infty)$$

función de Coloumb:

$$f^{-0.5} = -2 \log \left(\frac{\varepsilon/D}{3.7} + \frac{2.51}{R_f f^{-0.5}} \right)$$

En este caso
 $\varepsilon = 0$
 con $R_f \rightarrow \infty$
 este término tiende a 0

$$f(\varepsilon/D, R_f \rightarrow \infty)^{-0.5} = -2 \log(x) \quad x \rightarrow 0$$

$\Rightarrow f^{-0.5}$ tiende a $-\infty$
 $\Rightarrow f_T$ tiende a ∞

en otros palabras, si consideramos parámetros leídos, $f_T \approx 0 \Rightarrow K \approx 0$

sin embargo esta puede no ser la situación



la ecuación de Coloumb es una función empírica
 y no cubre el 100% de los casos

en este ejemplo si consideramos $K_1 = 0$:

$$V = 56.2 \text{ m/s}$$

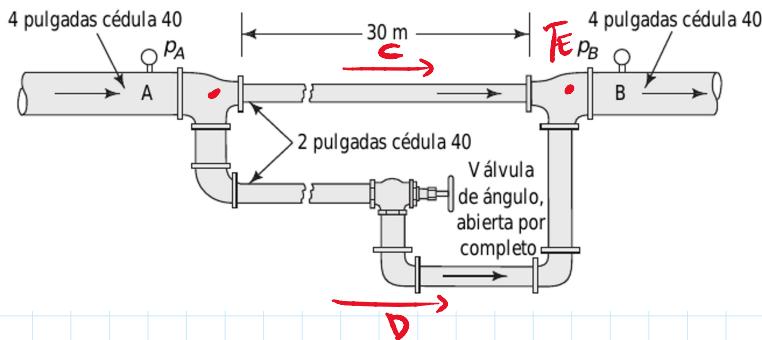


34 veces el valor si consideramos $K = 16$

\Rightarrow los períodos de larga moménto no pueden ser optimizados

Problema 4

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$$Q = 850 \text{ L/min}$$

$$= 850 \left[\frac{10^{-3} \text{ m}^3}{\text{L}} \right] \left[\frac{1 \text{ min}}{60 \text{ s}} \right]$$

$$= 0.1417 \text{ m}^3/\text{s}$$

TUBOS:

$$4 \text{ in } \rightarrow D_A = D_B = 102.3 \text{ mm}$$

$$2 \text{ in } \rightarrow D_C = D_D = 52.5 \text{ mm}$$

Arena comunes:

$$\epsilon = 4.6 \times 10^{-5}$$

Flujos volumétricos:

$$Q_A = Q_C + Q_D = Q_B$$

$$Q_A = \frac{\pi D_C^2}{4} V_C + \frac{\pi D_D^2}{4} V_D \xrightarrow{D_C = D_D} Q_A = \frac{\pi D^2}{4} (V_C + V_D)$$

Paso abierto (ruta c)

E.P. Energía

$$\frac{P_A}{\gamma} + \frac{z_A}{\gamma} - \frac{V_A^2}{2g} = \frac{P_B}{\gamma} + \frac{z_B}{\gamma} + \frac{V_B^2}{2g} \rightarrow (h_f + h_m)_C$$

$$0 = \frac{P_B - P_A}{\gamma} + (h_f + h_m)_C$$

Péndulos de Césped Mayors

$$h_f = f_c \cdot \frac{L_c}{D_c} \cdot \frac{V_c^2}{2g}$$

\downarrow
E/D conocido

\ddot{E}/D conocido
 V_C desconocido

Pendulos de conga móviles:

Elementos

1: T_E peso efectivo

$$k_{1C} = 20 \text{ ft}_A$$

2: T_C pesos efectivos

$$k_{2C} = 20 \text{ ft}_C$$

$$h_m = \frac{V_A^2}{2g} k_{1C} + \frac{V_C^2}{2g} k_{2C}$$

Peso por el normal (ruta D)

E.p. Energia

$$\cancel{\frac{P_A}{T}} + \cancel{z_A - \frac{V_A^2}{2g}} = \cancel{\frac{P_B}{T}} + \cancel{z_B} + \cancel{\frac{V_B^2}{2g}} \rightarrow (h_0 + h_m)_D$$

$$0 = \frac{P_B - P_A}{T} + (h_0 + h_m)_D$$

Pendulos rígidos

$$h_0 = f_D \frac{L_D}{g_D} \frac{V_D^2}{2g_D}$$

Lo E/D crece

Re descendente

Pendulos móviles

Elementos

1: T_E , peso por E' normal

$$K_{1D} = 60 \text{ ft}_r$$

2. corde estenderas P_0'

$$K_{2D} = 30 \text{ ft}_r$$

3. valvula de Angus 100% abierta

$$K_{3D} = 150 \text{ ft}_r$$

4. corde estenderas P_0''

$$K_{4D} = 30 \text{ ft}_r$$

5: corde estenderas P_0'''

$$K_{5D} = 30 \text{ ft}_r$$

6: T_C , P_{025} per st' around

$$K_{6D} = 60 \text{ ft}_P$$

$$hlm_{n,D} = \frac{V_A^2}{2g} K_{1D} + \frac{V_D^2}{2g} \left(\sum_{i=2}^6 K_{iD} \right)$$

Para obtener V_C y V_D :

$$Q_A = \frac{\pi D^2}{4} (V_C + V_D) \quad (1)$$

$$(h_1 + hlm)_C = (hl + hlm)_D \quad (2)$$

$$\left. \begin{array}{l} 0 = Q_A - \frac{\pi D^2}{4} (V_C + V_D) \\ 0 = (h_1 + hlm)_C - (hl + hlm)_D \end{array} \right\}$$

Sistema de ecuaciones no lineales (1) + (2)

$$Q_C = 8.63 \times 10^{-3} \text{ m}^3/\text{s}$$

$$Q_D = 5.48 \times 10^{-3} \text{ m}^3/\text{s}$$

$$V_C = 4.01 \text{ m/s}$$

$$V_D = 2.53 \text{ m/s}$$

$$\left. \begin{array}{l} Q_C + Q_D = Q_A \\ \end{array} \right\} \quad //$$

Para obtener $P_A - P_D$:

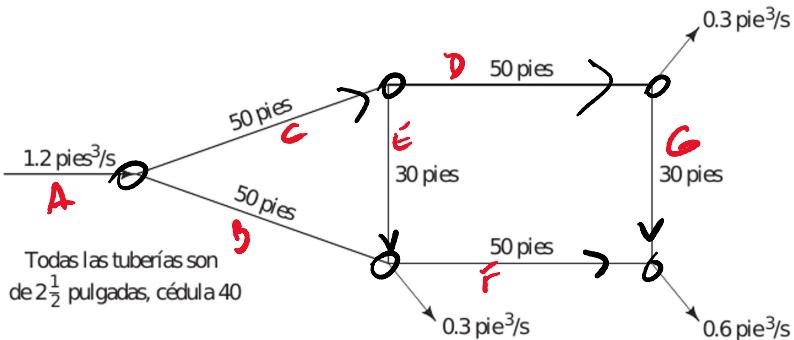
$$P_A - P_B = \gamma (h_L + h_m)_C$$

$$P_A - P_B = 99.6 \text{ kPa}$$

Problema 5

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Ve+vd-vchl

Flujos:

$$Q_A = Q_B + Q_C \quad (1)$$

$$Q_B + Q_E = Q_F + 0.3 \text{ ft}^3/\text{s} \quad (2)$$

$$Q_G + Q_F = 0.6 \text{ ft}^3/\text{s} \quad (3)$$

$$Q_B = 0.3 + Q_G \quad (4)$$

$$Q_C = Q_E + Q_D \quad (5)$$

v

Principios de carga

$$h_{P_0} = h_{L_C} + h_{L_E} \quad (6)$$

Resolvemos el sistema de ecuaciones no lineales

1 - 6 :

$$V_B = 5.58 \text{ m/s}$$

$$V_C = 5.42 \text{ m/s}$$

$$V_D = 3.77 \text{ m/s}$$

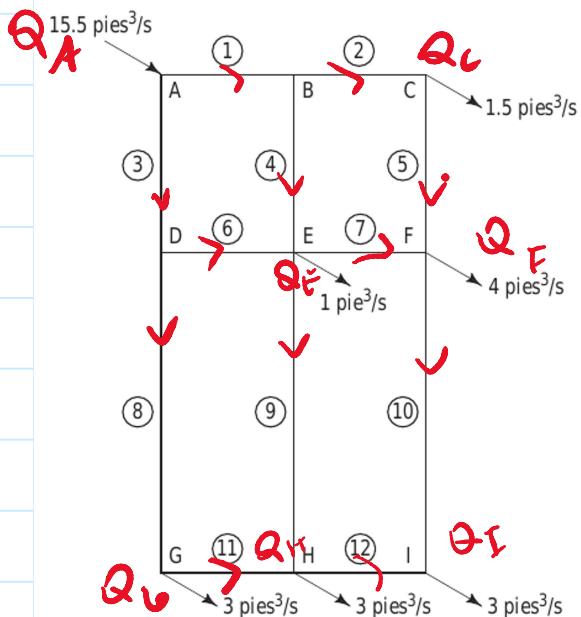
$$V_E = 1.60 \text{ m/s}$$

$$V_F = 4.51 \text{ m/s}$$

$$V_G = 0.99 \text{ m/s}$$

Problema 6

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Datos de las tuberías
Todas las tuberías son cédula 40

Tubo númer.	Longitud (pies)	Tamaño (pulg)
1	1500	16
2	1500	16
3	2000	18
4	2000	12
5	2000	16
6	1500	16
7	1500	12
8	4000	14
9	4000	12
10	4000	8
11	1500	12
12	1500	8

10) Resuelto
Flujos volumétricos:

Nodos

A

$$0 = Q_A - \Theta_1 - \Theta_3$$

B

$$0 = \Theta_1 - \Theta_4 - \Theta_2$$

C

$$0 = Q_2 - Q_C - Q_5$$

D

$$0 = Q_3 - Q_6 - Q_8$$

E

$$0 = \Theta_6 + Q_4 - \Theta_E - \Theta_9 - \Theta_F$$

F

$$0 = \Theta_7 + \Theta_5 - Q_F - Q_{10}$$

G

$$0 = Q_B - Q_G - Q_{11}$$

H

$$0 = Q_{11} + Q_9 - \Theta_H - Q_{12}$$

I

$$0 = \Theta_{12} + \Theta_{10} - Q_I$$

Predicadores de Carga:

de A a E:

$$O = h\ell_3 + h\ell_6 - (h\ell_1 + h\ell_4)$$

2º Irregular