FDM Demo: 2, 4, 6,and 8thOrder FDM

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1 Problem Statement

Consider a constant-area cylinder undergoing heat diffusion. The ends of the rod have constant temperatures. Energy balance on a differential element of the cylinder gives

$$u''(x) = -\alpha^2 u(x) + u_a \tag{1}$$

where u(x) represents the temperature of the cylinder as a function of x. Equation 1 is a homogeneous differential equation whose exact solution can be found as a boundary value problem. Assume the solution takes the form

$$u(x) = C \sinh(\alpha x) + D \cosh(\alpha x). \tag{2}$$

The boundary conditions for each case will be used to solve for the constants C and D. Equation 2 represents the general solution for the equation.

2 Analytical Solutions

2.1 Case 1

In case 1, we consider the ambient temperature to be 0° Celsius. The temperature at the left end of the cylinder is 0° as well. The temperature at the right end of the cylinder is 100° .

$$u(0) = 0 (3)$$

$$u(L) = 100 \tag{4}$$

To solve for C and D employing boundary conditions from equations 3 and 4:

$$0 = C \sinh (\alpha \cdot 0) + D \cosh (\alpha \cdot 0) + 0$$

$$D = 0$$

$$100 = C \sinh (\alpha \cdot L) + D \cosh (\alpha \cdot L) + 0$$

$$100 = C \sinh (\alpha L)$$

$$C = \frac{100}{\sinh (\alpha L)}$$

Therefore, for Case 1,

$$u(x) = \frac{100}{\sinh(\alpha L)}\sinh(\alpha x) \tag{5}$$

2.2 Case 2

For the second case, the right end is still 100° C. The left end is insulated, so that no heat is lost from that end. The atmospheric temperature is still considered as 0° C. Therefore, the boundary conditions are

$$u(L) = 100 \tag{6}$$

$$u'(0) = 0. (7)$$

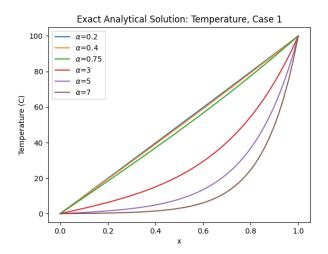


Figure 1: Exact Analytical Solution, Case 1

To solve for C and D we need the derivative of u(x).

$$u'(x) = \alpha C \cosh(\alpha x) + \alpha D \sinh(\alpha x)$$

Then,

$$u'(0) = 0 = \alpha C \cosh(\alpha \cdot 0) + \alpha D \sinh(\alpha \cdot 0)$$

$$0 = \alpha C$$

$$C = 0$$

$$u(L) = 100 = C \sinh(\alpha \cdot L) + D \cosh(\alpha \cdot L)$$

$$100 = D \cosh(\alpha L)$$

$$D = \frac{100}{\cosh(\alpha L)}$$

Therefore, for Case 2,

$$u(x) = \frac{100}{\cosh(\alpha L)}\cosh(\alpha x). \tag{8}$$

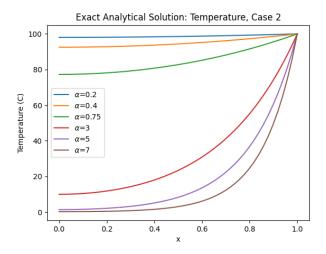


Figure 2: Exact Analytical Solution, Case 2

3 FDM: 2nd Order Scheme

3.1 Case 1

To begin, take the grid from [0, L] and divide into n amount of segments. Let $x_i = i\Delta x$ and i = 1, 2, ..., n. Using the differential equation for the temperature, equation 1, at each nodal position (x_i) , I use the Taylor series:

$$u(x_i \pm \Delta x) = u(x_i) \pm u'(x_i) \Delta x \pm u''(x_i) \frac{\Delta x^2}{2} + \dots$$
$$u(x_i + \Delta x) - 2u(x_i) + u(x_i - \Delta x) = u''(x_i) \Delta x^2$$

Now I can approximate u and its second derivative used in equation 1:

$$-u(x_{i-1}) + (2 + \alpha^2 \Delta x^2)u(x_i) - u(x_{i+1}) = 0 \text{ for } i = 1, \dots, n-1.$$
(9)

In Equation 9, $\kappa = 2 + \alpha^2 \Delta x^2$, and U_i represents the i^{th} approximate temperature:

$$-U_{i-1} + \kappa U_i - U_{i+1} = 0 \tag{10}$$

where $U_i \approx u(x_i)$. By solving Equation 10, I can approximate the solution for Equation 1 with measurable precision. The general solution is given with

$$\begin{bmatrix} \kappa & -1 & 0 & \dots & 0 & 0 \\ -1 & \kappa & -1 & \dots & 0 & 0 \\ 0 & -1 & \kappa & \dots & 0 & 0 \\ \vdots & \vdots & \vdots & \kappa & -1 & 0 \\ 0 & 0 & 0 & -1 & \kappa & -1 \\ 0 & 0 & 0 & 0 & -1 & \kappa \end{bmatrix} \begin{bmatrix} U_0 \\ U_1 \\ \vdots \\ \vdots \\ U_{n-2} \\ U_{n-1} \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ \vdots \\ \vdots \\ 0 \\ -100 \end{bmatrix}$$

$$(11)$$

3.2 Case 2

Case 2 is formulated in a similar way to Case 1, with the exception that boundary conditions 6 and 7 are used. Therefore, I will skip to solving Equation 10 for these new BCs.

$$i = 0: U_{-1} - (2 + \alpha^2 dx^2)U_0 + U_1 = 0$$

$$i = 1: U_0 - (2 + \alpha^2 dx^2)U_1 + U_2 = 0$$

$$i = 2: U_1 - (2 + \alpha^2 dx^2)U_2 + U_3 = 0$$

$$i = 3: U_2 - (2 + \alpha^2 dx^2)U_3 + U_4 = 0$$

$$i = 4: U_3 - (2 + \alpha^2 dx^2)U_4 + U_5 = 0$$

$$U'_0 = 0$$

$$U_5 = 100.$$

With these, we'll look at the first point, i = 0.

$$U_{-1} - \alpha^2 dx U_0 + U_1 = 0$$

There are two unknowns for this equation, U_{-1} and U_0 . However, I have one more equation I can use:

$$U_i' = \frac{U_{i+1} - U_{i-1}}{2dx}$$

and this can be solved for U_{-1} like so:

$$U_{-1} = U_1 - 2dxU_0'.$$

The boundary conditions state that $U'_0 = 0$, and the equation for i = 0 was given, so that

$$U_{-1} - (2 + \alpha^2 dx^2) U_0 + U_1 = 0$$

$$U_1 - 2dx U_0' - (2 + \alpha^2 dx^2) U_0$$

$$2U_1 - (2 + \alpha^2 dx^2) U_0 = 0$$

$$U_1 - \frac{\kappa}{2} U_0 = 0.$$

This goes right back into Equation 12 for Case 1 like so:

$$\begin{bmatrix} \frac{\kappa}{2} & -1 & 0 & \dots & 0 & 0 \\ -1 & \kappa & -1 & \dots & 0 & 0 \\ 0 & -1 & \kappa & \dots & 0 & 0 \\ \vdots & \vdots & \vdots & \kappa & -1 & 0 \\ 0 & 0 & 0 & -1 & \kappa & -1 \\ 0 & 0 & 0 & 0 & -1 & \kappa \end{bmatrix} \begin{bmatrix} U_0 \\ U_1 \\ \vdots \\ \vdots \\ U_{n-2} \\ U_{n-1} \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ \vdots \\ \vdots \\ 0 \\ 100 \end{bmatrix}$$

$$(12)$$

3.3 Approximation of Heat Loss

To approximate the heat loss at the end of the rod,

$$\dot{Q} = -kaU'(L) \tag{13}$$

where $U^{\prime}(L)$ is found once again through a Taylor series expansion as:

$$U'(L) = \frac{\left(1 + \frac{dx^2\alpha^2}{2}\right)U_n - U_{n-1}}{dx}$$
 (14)

3.4 Results

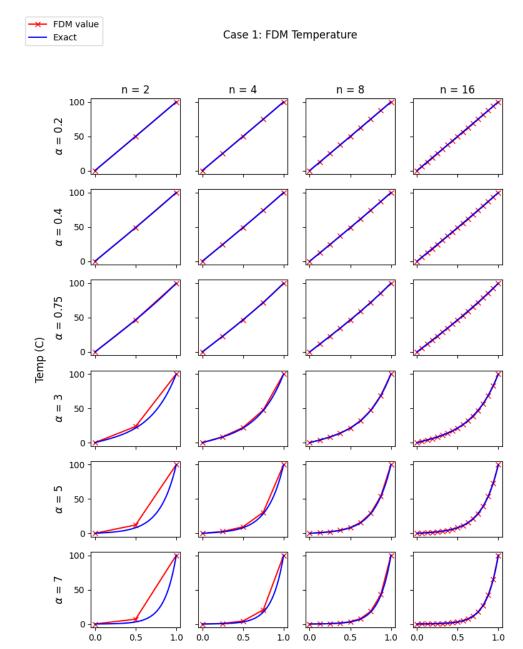


Figure 3: 2nd Order: Case 1

FDM value
Exact

Case 2: FDM Temperature

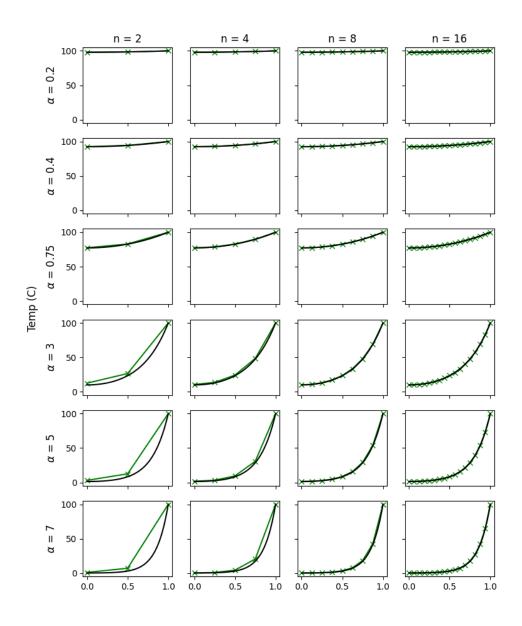


Figure 4: 2nd Order: Case 2

4 FDM: 4th Order Scheme

4.1 Case 1

I can further extend the results from the 2nd order scheme to a 4th order scheme, to make the calculations more accurate. To construct the fourth order FDM, the process is identical to the second order, taking the Taylor series to the 4th order:

$$u(x_i + \Delta x) = u(x_i) + u'(x_i)\Delta x + u''(x_i)\frac{\Delta x^2}{2} + u'''(x_i)\frac{\Delta x^3}{6} + u''''(x_i)\frac{\Delta x^4}{24}$$
$$u(x_i - \Delta x) = u(x_i) - u'(x_i)\Delta x + u''(x_i)\frac{\Delta x^2}{2} - u'''(x_i)\frac{\Delta x^3}{6} + u''''(x_i)\frac{\Delta x^4}{24}$$

Therefore, to add these two equations together to get $u(x_i - \Delta x) + u(x_i + \Delta x)$:

$$u(x_i - \Delta x) + u(x_i + \Delta x) = 2u(x_i) + u''(x_i)\Delta x^2 + u''''(x_i)\frac{\Delta x^4}{12}$$
(15)

Next, I want to substitute these terms into the original differential equation, equation 1.

$$u_{i-1} + u_{i+1} - 2u_i = u_i'' \Delta x^2 + u_i''' \frac{\Delta x^4}{12}$$

$$\frac{u_{i-1} + u_{i+1} - 2u_i}{\Delta x^2} = u_i'' + u_i''' \frac{\Delta x^2}{12}$$

$$\text{since } u_i'''' = \alpha^2 u_i''$$

$$\frac{u_{i-1} + u_{i+1} - 2u_i}{\Delta x^2} = u_i'' + u_i'' \alpha^2 \frac{\Delta x^2}{12} = u_i'' (1 + \alpha^2 \frac{\Delta x^2}{12})$$

For brevity $\beta = \alpha^2 \frac{\Delta x^2}{12}$ and the second derivative can be solved for as

$$u_i'' = \frac{u_{i-1} + u_{i+1} - 2u_i}{\Delta x^2} \frac{1}{1+\beta}$$
 (16)

Using the mathematical approximation

$$1 - \epsilon \approx \frac{1}{1 + \epsilon} \tag{17}$$

$$u_i'' = (1 - \beta) \frac{u_{i-1} + u_{i+1} - 2u_i}{\Delta x^2}$$
(18)

If I put this term back into equation 1,

$$-(1-\beta)\frac{u_{i-1} + u_{i+1} - 2u_i}{\Delta x^2} + \alpha^2 u_i = 0$$

or,

$$-(1-\beta)u_{i-1} - (2+10\beta)u_i - (1-\beta)u_{i+1} = 0$$
(19)

4.2 Case 2

4.3 Approximation of Heat Loss

To approximate the heat loss at the end of the rod,

$$\dot{Q} = -kaU'(L) \tag{20}$$

where U'(L) is found once again through a Taylor series expansion as:

$$U'(L) = \frac{\left(1 + \frac{dx^2\alpha^2}{2} + \frac{dx^4\alpha^4}{24}\right)U_n - U_{n-1}}{dx + \frac{dx^3\alpha^s}{6}}$$
(21)

4.4 Results

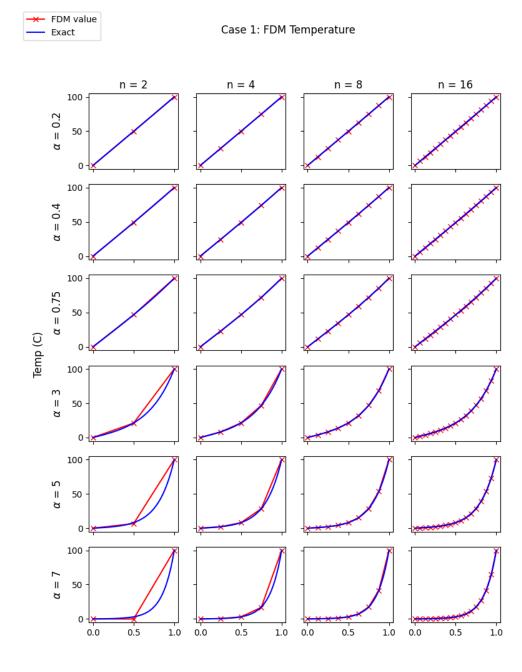


Figure 5: 4th Order: Case 1

FDM value
Exact

Case 2: FDM Temperature

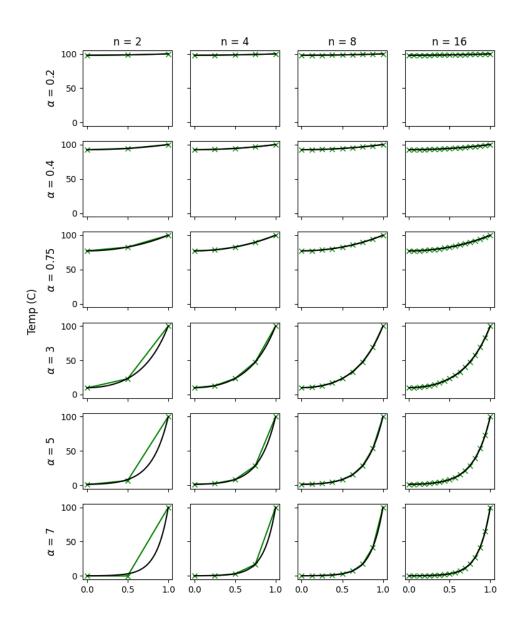


Figure 6: 4th Order: Case 2

5 FDM: 6th Order Scheme

The sixth order scheme is constructed in a similar manner to the fourth order. The only difference will be that the Taylor series is taken out to the sixth term.

$$-U_{i-1} + \kappa U_i - U_{i+1} = 0$$

where

$$\kappa = 2 + \alpha^2 dx^2 + \frac{\alpha^4 dx^4}{12} + \frac{\alpha^6 dx^6}{360}.$$
 (22)

5.1 Approximation of Heat Loss

To approximate the heat loss at the end of the rod,

$$\dot{Q} = -kaU'(L) \tag{23}$$

where U'(L) is found once again through a Taylor series expansion as:

$$U'(L) = \frac{\left(1 + \frac{dx^2\alpha^2}{2} + \frac{dx^4\alpha^4}{24} + \frac{dx^6\alpha^6}{720}\right)U_n - U_{n-1}}{dx + \frac{dx^3\alpha^2}{6} + \frac{dx^5\alpha^4}{120}}$$
(24)

5.2 Results

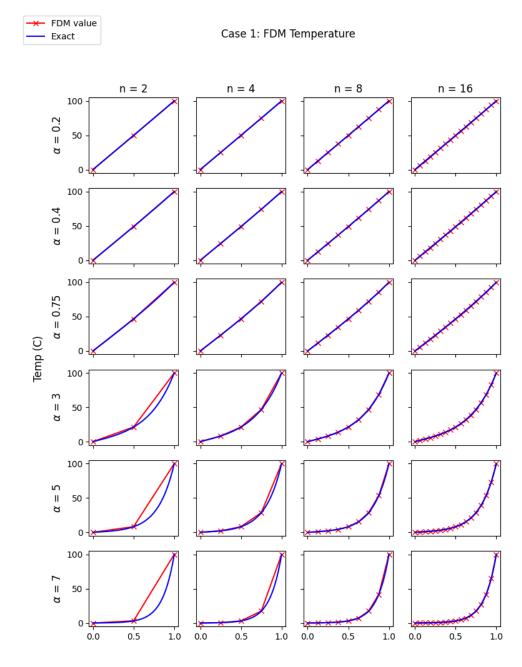


Figure 7: 6th Order: Case 1

FDM value
Exact

Case 2: FDM Temperature

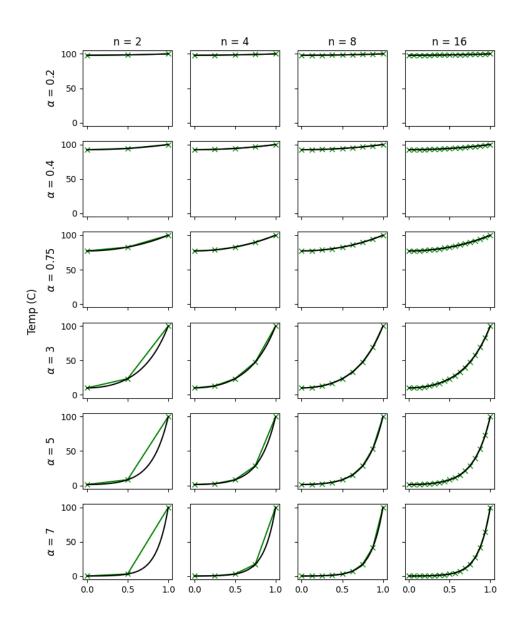


Figure 8: 6th Order: Case 2

6 FDM: 8th Order Scheme

$$-U_{i-1} + \kappa U_i - U_{i+1} = 0$$

where

$$\kappa = 2 + \alpha^2 dx^2 + \frac{\alpha^4 dx^4}{12} + \frac{\alpha^6 dx^6}{360} + \frac{\alpha^8 dx^8}{20160}.$$
 (25)

6.1 Approximation of Heat Loss

To approximate the heat loss at the end of the rod,

$$\dot{Q} = -kaU'(L) \tag{26}$$

where U'(L) is found once again through a Taylor series expansion as:

$$U'(L) = \frac{\left(1 + \frac{dx^2\alpha^2}{2} + \frac{dx^4\alpha^4}{24} + \frac{dx^6\alpha^6}{720} + \frac{dx^8\alpha^8}{40320}\right)U_n - U_{n-1}}{dx + \frac{dx^3\alpha^2}{6} + \frac{dx^5\alpha^4}{120} + \frac{dx^7\alpha^6}{5040}}$$
(27)

6.2 Results

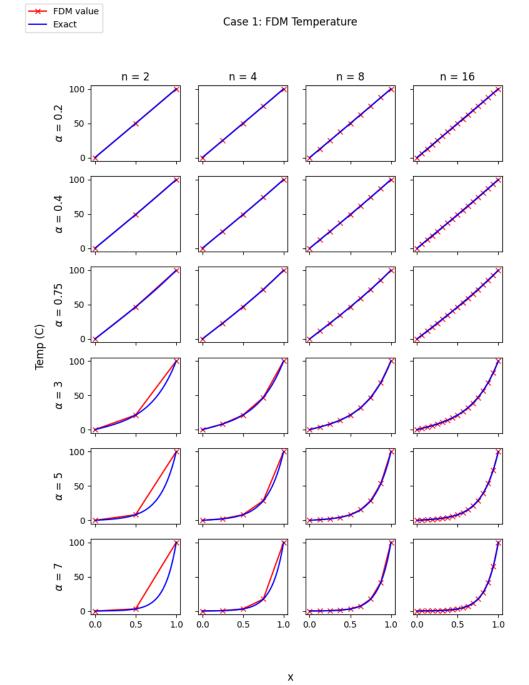


Figure 9: 8th Order: Case 1

→ FDM value — Exact

Case 2: FDM Temperature

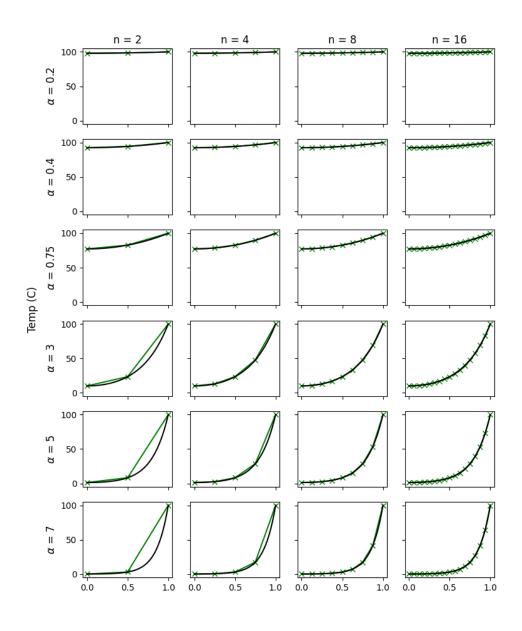


Figure 10: 8th Order: Case 2

7 Rate of Convergence

The rate of convergence can be found in a similar way to Assignment 1, but instead of the exact temperature, we compare to an extrapolated value given by:

$$Q_{extr} = \frac{Q_{dx/2}^2 - Q_{dx} * Q_{dx/4}}{2Q_{dx/2} - Q_{dx} - Q_{dx/4}}$$
(28)

where the values of Q are given for different mesh sizes dx, $\frac{dx}{2}$, and $\frac{dx}{4}$. The rate of convergence is then found in a similar manner to the previous assignment.

$$Q_{extr} - Q_{\Delta x} \approx C (\Delta x)^{\beta}$$

 $Q_{extr} - Q_{\Delta x/2} \approx C \left(\frac{\Delta x}{2}\right)^{\beta}$

If I divide the first equation by the second,

$$\begin{split} \frac{Q_{extr} - Q_{\Delta x}}{Q_{extr} - Q_{\Delta x/2}} &\approx 2^{\beta} \\ \beta &\approx \frac{\log \frac{Q_{extr} - Q_{\Delta x}}{Q_{extr} - Q_{\Delta x/2}}}{\log 2} \end{split}$$

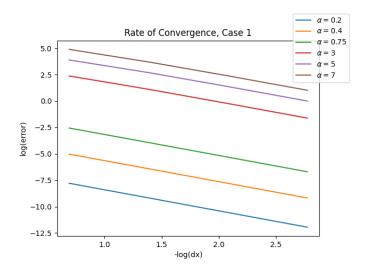


Figure 11: Rate of Convergence, 2nd Order, Case 1

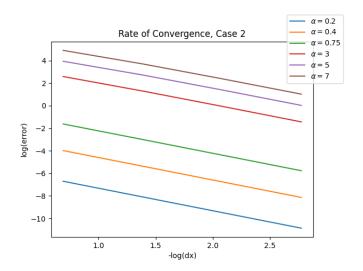


Figure 12: Rate of Convergence, 2nd Order, Case 2

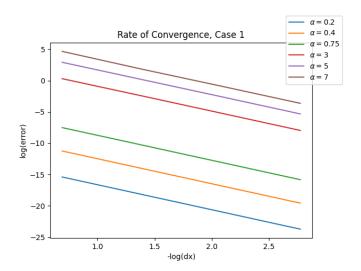


Figure 13: Rate of Convergence, 4th Order, Case 1 $\,$

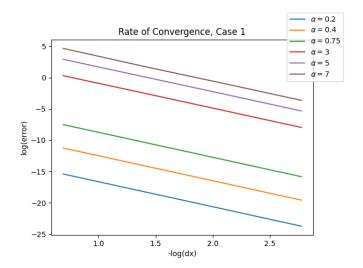


Figure 14: Rate of Convergence, 4th Order, Case 2

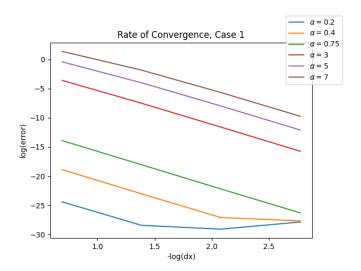


Figure 15: Rate of Convergence, 6th Order, Case 1 $\,$

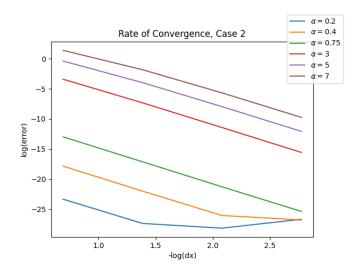


Figure 16: Rate of Convergence, 6th Order, Case 2

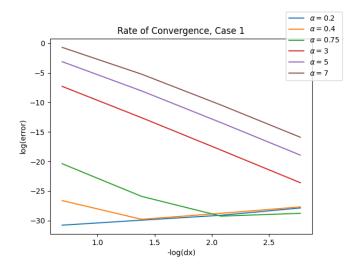


Figure 17: Rate of Convergence, 8th Order, Case 1 $\,$

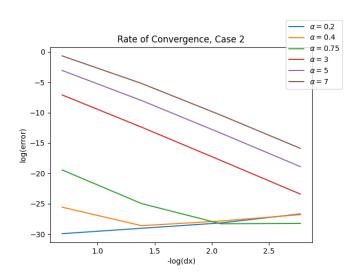


Figure 18: Rate of Convergence, 8th Order, Case 2

8 Conclusion

The rates of convergence look as expected for all except 6th and 8th order case 2. I have been unable to find the reason for these convergences, although they only occur when alpha is small. Not included in this report is The values for U'(L), but they should be included in HW 3.

A Tables

A.1 2nd Order

A.1.1 $\alpha = 0.2$

		n = 2	
		Case 1	
X	$T_{-}exact$	$T_{-}FDM$	Error
0	0	0	nan
0.5	49.751	49.7512	0.000414732
1	100	100	0
		Case 2	
X	T_{exact}	$T_{-}FDM$	Error
0	98.0328	98.0344	0.00164263
0.5	98.5234	98.5246	0.00122789
1	100	100	0
		n = 4	
		Case 1	
X	$T_{-}exact$	$T_{-}FDM$	Error
0	0	0	nan
0.25	24.8445	24.8445	0.000129798
0.5	49.751	49.7511	0.000103786
0.75	74.782	74.7821	6.04917e-05
1	100	100	0
		Case 2	
X	$T_{-}exact$	$T_{-}FDM$	Error
0	98.0328	98.0332	0.000411063
0.25	98.1554	98.1557	0.000385052
0.5	98.5234	98.5237	0.000307276
0.75	99.1377	99.1379	0.000178507
1	100	100	0
		n = 8	
		Case 1	

X	T_exact	T_FDM	Error
0	0	0	nan
0.125	12.4183	12.4184	3.40846 e - 05
0.25	24.8445	24.8445	3.24575 e-05
0.375	37.2861	37.2861	2.97465e-05
0.5	49.751	49.7511	2.5953 e-05
0.625	62.2471	62.2471	2.1079e-05
0.75	74.782	74.782	1.51267e-05
0.875	87.3637	87.3637	8.09922e-06
1	100	100	0
		Case 2	
X	$T_{-}exact$	$T_{-}FDM$	Error
0	98.0328	98.0329	0.000102791
0.125	98.0634	98.0635	0.000101164
0.25	98.1554	98.1555	9.62867e-05
0.375	98.3086	98.3087	8.81713e-05
0.5	98.5234	98.5234	7.68381e-05
0.625	98.7997	98.7997	6.2315 e-05
0.75	99.1377	99.1378	4.46377e-05
0.875	99.5378	99.5378	2.38494e-05
1	100	100	0
		n = 16	
		Case 1	
X	T_exact	T_FDM	Error
0	0	0	nan
0.0625	6.20869	6.20869	8.62341e-06
0.125	12.4183	12.4183	8.52169e-06
0.1875	18.6299	18.6299	8.35218e-06
0.25	24.8445	24.8445	8.11488e-06
0.3125	31.0628	31.0629	7.80984e-06
0.375	37.2861	37.2861	7.4371e-06
0.4375	43.5152	43.5152	6.99669e-06
0.5	49.751	49.751	6.48867e-06
0.5625	55.9947	55.9947	5.91311e-06
0.625	62.2471	62.2471	5.27007e-06
0.6875	68.5092	68.5092	4.55964 e-06
0.75	74.782	74.782	3.78191e-06
0.8125	81.0665	81.0665	2.93697e-06
0.875	87.3637	87.3637	2.02493e-06
0.9375	93.6745	93.6745	1.0459 e-06
1	100	100	0
<u> </u>		Case 2	

X	T_exact	T_FDM	Error
0	98.0328	98.0328	2.56994e-05
0.0625	98.0405	98.0405	2.55977e-05
0.125	98.0634	98.0635	2.52926 e - 05
0.1875	98.1017	98.1018	2.47843e-05
0.25	98.1554	98.1554	2.40732e-05
0.3125	98.2243	98.2244	2.31596e-05
0.375	98.3086	98.3087	2.20442e-05
0.4375	98.4083	98.4083	2.07276e-05
0.5	98.5234	98.5234	1.92107e-05
0.5625	98.6538	98.6538	1.74944e-05
0.625	98.7997	98.7997	1.55797e-05
0.6875	98.961	98.961	1.34679e-05
0.75	99.1377	99.1377	1.11601e-05
0.8125	99.33	99.33	8.6579 e-06
0.875	99.5378	99.5378	5.96271 e-06
0.9375	99.7611	99.7611	3.07617e-06
1	100	100	0

A.1.2 $\alpha = 0.4$

			n=2	
			Case 1	
	X	T_{exact}	T_{FDM}	Error
	0	0	0	nan
0.	.5	49.0164	49.0196	0.00654467
	1	100	100	0
			Case 2	
	\mathbf{X}	$T_{-}exact$	$T_{-}FDM$	Error
	0	92.5007	92.5241	0.0252009
C	0.5	94.3569	94.3745	0.0186551
	1	100	100	0
			n = 4	
			Case 1	
	X	$T_{-}exact$	$T_{-}FDM$	Error
	0	0	0	nan
0.2	25	24.3862	24.3867	0.00205737
0.	.5	49.0164	49.0172	0.00164263
0.7	' 5	74.1372	74.1379	0.000955048
	1	100	100	0
			Case 2	
	\mathbf{x}	$T_{-}exact$	$T_{-}FDM$	Error
-	0	92.5007	92.5066	0.00632438
0.	25	92.9636	92.9691	0.00590963
0	0.5	94.3569	94.3614	0.00468168
0.	75	96.6946	96.6972	0.00268762
	1	100	100	0

		n = 8	
	T_exact	Case 1	Ennon
x	1_exact 0	T_FDM 0	Error
0.125	12.1779	12.1779	nan 0.000540861
0.125 0.25	24.3862	24.3863	0.00051485
$0.25 \\ 0.375$	36.6555	24.3803 36.6556	0.00031485 0.000471555
$0.575 \\ 0.5$	49.0164	49.0166	0.000411063
0.625	61.4999	61.5001	0.000411003 0.000333493
0.025 0.75	74.1372	74.1374	0.000333493
$0.75 \\ 0.875$	86.9599	86.96	0.000238999
0.873	100	100	0.000127703
		$\frac{100}{\text{Case 2}}$	
X	T_exact	T_{FDM}	Error
0	92.5007	92.5022	0.00158261
0.125	92.6164	92.6178	0.0015566
0.25	92.9636	92.965	0.00147883
0.375	93.5433	93.5446	0.00135005
0.5	94.3569	94.358	0.00117155
0.625	95.4065	95.4074	0.000945008
0.75	96.6946	96.6952	0.000672552
0.875	98.2245	98.2248	0.000356637
1	100	100	0
	1	n = 16	
		Case 1	
X	T_exact	T_FDM	Error
0	0	0	nan
0.0625	6.08703	6.08704	0.000136876
0.125	12.1779	12.1779	0.000135249
0.1875	18.2763	18.2763	0.000132538
0.25	24.3862	24.3862	0.000128744
0.3125	30.5113	30.5113	0.00012387
0.375	36.6555	36.6555	0.000117918
0.4375	42.8225	42.8226	0.00011089
0.5	49.0164	49.0165	0.000102791
0.5625	55.2409	55.2409	9.36242e-05
0.625	61.4999	61.5	8.3394e-05
0.6875	67.7974	67.7974	7.21056e-05
0.75	74.1372	74.1372	5.97645e-05
0.8125	80.5234	80.5234	4.63766e-05
0.075	00.0500	00 0500	
0.875	86.9599	86.9599	3.19486e-05
0.9375	93.4507	93.4508	1.64872 e-05
	93.4507 100		

X	$T_{-}exact$	$T_{-}FDM$	Error
0	92.5007	92.5011	0.000395748
0.0625	92.5297	92.53	0.000394121
0.125	92.6164	92.6168	0.000389244
0.1875	92.761	92.7614	0.000381129
0.25	92.9636	92.964	0.000369795
0.3125	93.2243	93.2247	0.000355272
0.375	93.5433	93.5436	0.000337595
0.4375	93.9208	93.9211	0.000316806
0.5	94.3569	94.3572	0.000292957
0.5625	94.8521	94.8523	0.000266103
0.625	95.4065	95.4067	0.000236309
0.6875	96.0205	96.0207	0.000203643
0.75	96.6946	96.6948	0.000168179
0.8125	97.4291	97.4292	0.000129997
0.875	98.2245	98.2246	8.91807e-05
0.9375	99.0813	99.0813	4.58181e-05
1	100	100	0

A.1.3 $\alpha = 0.75$

		n = 2	
		Case 1	
X	$T_{-}exact$	T_{FDM}	Error
0	0	0	nan
0.5	46.6792	46.7153	0.0773463
1	100	100	0
		Case 2	
X	$T_{-}exact$	$T_{-}FDM$	Error
0	77.239	77.4511	0.27461
0.5	82.7338	82.8969	0.197111
1	100	100	0
		n = 4	
		Case 1	
X	$T_{-}exact$	$T_{-}FDM$	Error
0	0	0	nan
0.25	22.9353	22.9409	0.0246644
0.5	46.6792	46.6884	0.0195966
0.75	72.0691	72.0772	0.0113036
1	100	100	0
		Case 2	
X	$T_{-}exact$	$T_{-}FDM$	Error
0	77.239	77.2926	0.0694934
0.25	78.6007	78.6513	0.0644233
0.5	82.7338	82.775	0.049887
0.75	89.784	89.8089	0.0276546
1	100	100	0

		n = 8 Case 1	
X	T_exact	$\frac{\text{Dase I}}{\text{T_FDM}}$	Error
0	0	0	nan
0.125	11.4174	11.4182	0.00650747
0.25	22.9353	22.9367	0.0061869
0.375	34.6548	34.6568	0.0056551
0.5	46.6792	46.6815	0.00491573
0.625	59.1142	59.1165	0.00397379
0.75	72.0691	72.0711	0.00283551
0.875	85.6578	85.6591	0.00150817
1	100	100	0
		Case 2	
X	$T_{-}exact$	T_FDM	Error
0	77.239	77.2524	0.0174269
0.125	77.5786	77.5919	0.0171063
0.25	78.6007	78.6134	0.0161556
0.375	80.314	80.3258	0.014607
0.5	82.7338	82.7441	0.0125106
0.625	85.8812	85.8897	0.00992966
0.75	89.784	89.7903	0.00693542
0.875	94.4765	94.4799	0.00360161
1	100	100	0
1	1	n = 16	0
	r (n = 16 Case 1	-
X	T_exact	n = 16 Case 1 T_FDM	Error
x 0	T_exact 0	$\begin{array}{c} n = 16 \\ \underline{\text{Case 1}} \\ \underline{\text{T-FDM}} \\ 0 \end{array}$	Error
x 0 0.0625	T_exact 0 5.70245	T_FDM 0 5.70254	Error nan 0.00164834
x 0 0.0625 0.125	T_exact 0 5.70245 11.4174	n = 16 Case 1 T.FDM 0 5.70254 11.4176	Error nan 0.00164834 0.00162824
x 0 0.0625 0.125 0.1875	T_exact 0 5.70245 11.4174 17.1575	n = 16 Case 1 T_FDM 0 5.70254 11.4176 17.1578	Error nan 0.00164834 0.00162824 0.00159479
x 0 0.0625 0.125 0.1875 0.25	T_exact 0 5.70245 11.4174 17.1575 22.9353	n = 16 Case 1 T_FDM 0 5.70254 11.4176 17.1578 22.9356	Error nan 0.00164834 0.00162824 0.00159479 0.00154803
x 0 0.0625 0.125 0.1875 0.25 0.3125	T_exact 0 5.70245 11.4174 17.1575 22.9353 28.7635	n = 16 Case 1 T_FDM 0 5.70254 11.4176 17.1578 22.9356 28.7639	Error nan 0.00164834 0.00162824 0.00159479 0.00154803 0.00148806
x 0 0.0625 0.125 0.1875 0.25 0.3125 0.375	T_exact 0 5.70245 11.4174 17.1575 22.9353 28.7635 34.6548	n = 16 Case 1 T_FDM 0 5.70254 11.4176 17.1578 22.9356 28.7639 34.6553	Error nan 0.00164834 0.00162824 0.00159479 0.00154803 0.00148806 0.00141497
x 0 0.0625 0.125 0.1875 0.25 0.3125 0.375 0.4375	T_exact 0 5.70245 11.4174 17.1575 22.9353 28.7635 34.6548 40.6224	n = 16 Case 1 T.FDM 0 5.70254 11.4176 17.1578 22.9356 28.7639 34.6553 40.6229	Error nan 0.00164834 0.00162824 0.00159479 0.00154803 0.00148806 0.00141497 0.00132889
x 0 0.0625 0.125 0.1875 0.25 0.3125 0.375 0.4375 0.5	T_exact 0 5.70245 11.4174 17.1575 22.9353 28.7635 34.6548 40.6224 46.6792	n = 16 Case 1 T.FDM 0 5.70254 11.4176 17.1578 22.9356 28.7639 34.6553 40.6229 46.6798	Error nan 0.00164834 0.00162824 0.00159479 0.00154803 0.00148806 0.00141497 0.00132889 0.00122997
x 0 0.0625 0.125 0.1875 0.25 0.3125 0.375 0.4375 0.5 0.5625	T_exact 0 5.70245 11.4174 17.1575 22.9353 28.7635 34.6548 40.6224 46.6792 52.8386	n = 16 Case 1 T.FDM 0 5.70254 11.4176 17.1578 22.9356 28.7639 34.6553 40.6229 46.6798 52.8392	Error nan 0.00164834 0.00162824 0.00159479 0.00154803 0.00144806 0.00141497 0.00132889 0.00122997 0.00111838
x 0 0.0625 0.125 0.1875 0.25 0.3125 0.375 0.4375 0.5 0.5625 0.625	T_exact 0 5.70245 11.4174 17.1575 22.9353 28.7635 34.6548 40.6224 46.6792 52.8386 59.1142	$\begin{array}{l} n = 16 \\ \hline \text{Case 1} \\ \hline \text{T.FDM} \\ \hline 0 \\ 5.70254 \\ 11.4176 \\ 17.1578 \\ 22.9356 \\ 28.7639 \\ 34.6553 \\ 40.6229 \\ 46.6798 \\ 52.8392 \\ 59.1148 \\ \end{array}$	Error nan 0.00164834 0.00162824 0.00159479 0.00154803 0.00148806 0.00141497 0.00132889 0.00122997 0.00111838 0.000994293
x 0 0.0625 0.125 0.1875 0.25 0.3125 0.375 0.4375 0.5625 0.625 0.625	T_exact 0 5.70245 11.4174 17.1575 22.9353 28.7635 34.6548 40.6224 46.6792 52.8386 59.1142 65.5196	n = 16 Case 1 T_FDM 0 5.70254 11.4176 17.1578 22.9356 28.7639 34.6553 40.6229 46.6798 52.8392 59.1148 65.5202	Error nan 0.00164834 0.00162824 0.00159479 0.00154803 0.00148806 0.00141497 0.00132889 0.00122997 0.00111838 0.000994293 0.00085792
x 0 0.0625 0.125 0.1875 0.25 0.3125 0.375 0.4375 0.5 0.5625 0.625 0.6875 0.75	T_exact 0 5.70245 11.4174 17.1575 22.9353 28.7635 34.6548 40.6224 46.6792 52.8386 59.1142 65.5196 72.0691	$\begin{array}{l} n = 16 \\ \hline \text{Case 1} \\ \hline \text{T.FDM} \\ \hline 0 \\ 5.70254 \\ 11.4176 \\ 17.1578 \\ 22.9356 \\ 28.7639 \\ 34.6553 \\ 40.6229 \\ 46.6798 \\ 52.8392 \\ 59.1148 \\ 65.5202 \\ 72.0696 \end{array}$	Error nan 0.00164834 0.00162824 0.00159479 0.00154803 0.00148806 0.00141497 0.00132889 0.00122997 0.00111838 0.000994293 0.00085792 0.000709482
x 0 0.0625 0.125 0.1875 0.25 0.3125 0.375 0.4375 0.5 0.5625 0.6625 0.6875 0.75 0.8125	T_exact 0 5.70245 11.4174 17.1575 22.9353 28.7635 34.6548 40.6224 46.6792 52.8386 59.1142 65.5196 72.0691 78.7769	$\begin{array}{l} n = 16 \\ \hline \text{Case 1} \\ \hline \text{T.FDM} \\ \hline 0 \\ 5.70254 \\ 11.4176 \\ 17.1578 \\ 22.9356 \\ 28.7639 \\ 34.6553 \\ 40.6229 \\ 46.6798 \\ 52.8392 \\ 59.1148 \\ 65.5202 \\ 72.0696 \\ 78.7773 \\ \end{array}$	Error nan 0.00164834 0.00162824 0.00159479 0.00154803 0.00141497 0.00132889 0.00122997 0.00111838 0.000994293 0.00085792 0.0007709482 0.000549214
x 0 0.0625 0.125 0.1875 0.25 0.3125 0.375 0.4375 0.5 0.5625 0.625 0.6875 0.75 0.8125 0.875	T_exact 0 5.70245 11.4174 17.1575 22.9353 28.7635 34.6548 40.6224 46.6792 52.8386 59.1142 65.5196 72.0691 78.7769 85.6578	$\begin{array}{l} n = 16 \\ \hline \text{Case 1} \\ \hline \text{T.FDM} \\ \hline 0 \\ 5.70254 \\ 11.4176 \\ 17.1578 \\ 22.9356 \\ 28.7639 \\ 34.6553 \\ 40.6229 \\ 46.6798 \\ 52.8392 \\ 59.1148 \\ 65.5202 \\ 72.0696 \\ 78.7773 \\ 85.6582 \\ \end{array}$	Error nan 0.00164834 0.00162824 0.00159479 0.00154803 0.00141497 0.00132889 0.00122997 0.00111838 0.000994293 0.00085792 0.000709482 0.000549214 0.000377366
x 0 0.0625 0.125 0.1875 0.25 0.3125 0.375 0.4375 0.5 0.5625 0.625 0.6875 0.75 0.8125 0.875 0.9375	T_exact 0 5.70245 11.4174 17.1575 22.9353 28.7635 34.6548 40.6224 46.6792 52.8386 59.1142 65.5196 72.0691 78.7769 85.6578 92.727	$\begin{array}{l} n = 16 \\ \hline \text{Case 1} \\ \hline \text{T.FDM} \\ \hline 0 \\ 5.70254 \\ 11.4176 \\ 17.1578 \\ 22.9356 \\ 28.7639 \\ 34.6553 \\ 40.6229 \\ 46.6798 \\ 52.8392 \\ 59.1148 \\ 65.5202 \\ 72.0696 \\ 78.7773 \\ 85.6582 \\ 92.7272 \\ \end{array}$	Error nan 0.00164834 0.00162824 0.00159479 0.00154803 0.00144896 0.00141497 0.00132889 0.00122997 0.00111838 0.000994293 0.00085792 0.000709482 0.000549214 0.000377366 0.000194203
x 0 0.0625 0.125 0.1875 0.25 0.3125 0.375 0.4375 0.5 0.5625 0.625 0.6875 0.75 0.8125 0.875	T_exact 0 5.70245 11.4174 17.1575 22.9353 28.7635 34.6548 40.6224 46.6792 52.8386 59.1142 65.5196 72.0691 78.7769 85.6578 92.727 100	$\begin{array}{l} n = 16 \\ \hline \text{Case 1} \\ \hline \text{T.FDM} \\ \hline 0 \\ 5.70254 \\ 11.4176 \\ 17.1578 \\ 22.9356 \\ 28.7639 \\ 34.6553 \\ 40.6229 \\ 46.6798 \\ 52.8392 \\ 59.1148 \\ 65.5202 \\ 72.0696 \\ 78.7773 \\ 85.6582 \\ \end{array}$	Error nan 0.00164834 0.00162824 0.00159479 0.00154803 0.00141497 0.00132889 0.00122997 0.00111838 0.000994293 0.00085792 0.000709482 0.000549214 0.000377366

X	T_exact	T_FDM	Error
0	77.239	77.2423	0.0043601
0.0625	77.3238	77.3272	0.00434
0.125	77.5786	77.582	0.00427989
0.1875	78.0039	78.0072	0.00418028
0.25	78.6007	78.6038	0.00404203
0.3125	79.3701	79.3732	0.00386632
0.375	80.314	80.317	0.00365459
0.4375	81.4344	81.4372	0.00340854
0.5	82.7338	82.7364	0.00313009
0.5625	84.215	84.2173	0.00282129
0.625	85.8812	85.8833	0.00248436
0.6875	87.7362	87.7381	0.00212157
0.75	89.784	89.7856	0.00173522
0.8125	92.0292	92.0304	0.00132764
0.875	94.4765	94.4774	0.000901116
0.9375	97.1315	97.132	0.000457858
1	100	100	0

A.1.4 $\alpha = 3$

			n=2	
			Case 1	
X		$T_{\text{-exact}}$	T_FDM	Error
0		0	0	nan
0.5		21.2548	23.5294	10.7016
1		100	100	1.42109e-14
			Case 2	
	Х	T_exact	T_FDM	Error
	0	9.93279	12.4514	25.3561
0.	.5	23.366	26.4591	13.2378
	1	100	100	0
			n = 4	
			Case 1	
X		T_{-exact}	$T_{-}FDM$	Error
0		0	0	nan
0.25		0 8.20849	0 8.54597	nan 4.11135
_		•	~	
0.25		8.20849	8.54597	4.11135
$0.25 \\ 0.5$		8.20849 21.2548	8.54597 21.8991	4.11135 3.03111
0.25 0.5 0.75		8.20849 21.2548 46.828 100	8.54597 21.8991 47.5704 100 Case 2	4.11135 3.03111 1.58535 1.42109e-14
0.25 0.5 0.75		8.20849 21.2548 46.828 100	8.54597 21.8991 47.5704 100	4.11135 3.03111 1.58535 1.42109e-14
0.25 0.5 0.75		8.20849 21.2548 46.828 100	8.54597 21.8991 47.5704 100 Case 2 T_FDM	4.11135 3.03111 1.58535 1.42109e-14
0.25 0.5 0.75	x 0	8.20849 21.2548 46.828 100	8.54597 21.8991 47.5704 100 Case 2 T_FDM 10.6089	4.11135 3.03111 1.58535 1.42109e-14 Error 6.80699
0.25 0.5 0.75 1 ———————————————————————————————————	x 0	8.20849 21.2548 46.828 100 T_exact 9.93279	8.54597 21.8991 47.5704 100 Case 2 T_FDM 10.6089 13.5927	4.11135 3.03111 1.58535 1.42109e-14 Error 6.80699 5.69879
0.25 0.5 0.75 1 ———————————————————————————————————	x 0 25 0.5	8.20849 21.2548 46.828 100 T_exact 9.93279 12.8598	8.54597 21.8991 47.5704 100 Case 2 T_FDM 10.6089 13.5927 24.2223	4.11135 3.03111 1.58535 1.42109e-14 Error 6.80699 5.69879 3.66479

n = 8					
	T	Case 1	T7		
X	T_exact	T_FDM	Error		
0	0	0	nan		
0.125	3.83166	3.87536	1.14054		
0.25	8.20849	8.2957	1.06237		
0.375	13.7532	13.8826	0.940723		
0.5	21.2548	21.4218	0.785602		
0.625	31.7805	31.9734	0.606869		
0.75	46.828	47.0212	0.412696		
0.875	68.5382	68.6815	0.20907		
1	100	100 Case 2	1.42109e-14		
X	T_exact	$\frac{\text{Jase } z}{\text{T_FDM}}$	Error		
0	9.93279	10.1053	1.73677		
0.125	10.6394	10.1055	1.65814		
0.125	12.8598	13.0473	1.45816		
0.25 0.375	16.9099	17.1136	1.20458		
0.575	23.366	23.5865	0.943758		
0.625	33.1466	33.3763	0.69288		
0.025 0.75	47.6433	47.8595	0.09288 0.453852		
$0.75 \\ 0.875$	68.9188	69.0731	0.433832 0.223914		
0.873	100	100	0.223914		
	100 n				
		Case 1			
X	T_exact	T_FDM	Error		
0	0	0	nan		
0.0625	1.88264	1.88815	0.292617		
0.125	3.83166	3.84268	0.287536		
0.1875	5.91578	5.9323	0.279221		
0.25	8.20849	8.23048	0.267887		
0.3125	10.7906	10.818	0.253808		
0.375	13.7532	13.7859	0.237294		
0.4375	17.2008	17.2384	0.21867		
0.5	21.2548	21.2969	0.198256		
0.5625	26.0583	26.1042	0.176353		
0.625	31.7805	31.8292	0.153234		
0.6875	38.6233	38.6732	0.129139		
0.75	46.828	46.8768	0.10427		
0.8125	56.6838	56.7284	0.078797		
0.875	68.5382	68.5744	0.052858		
0.9375	82.8092	82.8312	0.0265633		
1	100	100	1.42109e-14		

	X	T_{-} exact	T_FDM	Error
	0	9.93279	9.97615	0.4365
	0.0625	10.1079	10.1515	0.431411
	0.125	10.6394	10.6838	0.416822
	0.1875	11.5461	11.5916	0.394508
	0.25	12.8598	12.907	0.366752
	0.3125	14.627	14.6761	0.335743
	0.375	16.9099	16.9612	0.303211
Case 2	0.4375	19.7891	19.8426	0.270328
Case 2	0.5	23.366	23.4216	0.237773
	0.5625	27.7668	27.8239	0.205873
	0.625	33.1466	33.2045	0.174731
	0.6875	39.6951	39.7524	0.144321
	0.75	47.6433	47.6979	0.11456
	0.8125	57.2714	57.3202	0.0853443
	0.875	68.9188	68.9577	0.0565714
	0.9375	82.9962	83.0195	0.0281491
	1	100	100	0

A.1.5 $\alpha = 5$

n = 2					
Case 1					
x	$T_{-}exact$	$T_{-}FDM$	Error		
0	0	0	nan		
0.5	8.15356	12.1212	48.6616		
1	100	100	0		
	C	lase 2			
X	T _exact	$T_{-}FDM$	Error		
0	1.34753	3.02744	124.666		
0.5	8.26343	12.4882	51.1257		
1	100	100	0		
	_	1 = 4			
		lase 1			
X	$T_{-}exact$	T_FDM	Error		
0	0	0	nan		
0.25	2.15883	2.62549	21.6165		
0.5	8.15356	9.35331	14.7144		
0.75	28.6359	30.6957	7.19282		
1	100	100	0		
Case 2					
X	$T_{-}exact$	$T_{-}FDM$	Error		
0	1.34753	1.78085	32.1565		
0.25	2.5447	3.17213	24.6562		
0.5	8.26343	9.51987	15.2048		
0.75	28.665	30.7424	7.24715		
1	100	100	0		

n = 8 Case 1					
x	T_exact	$\frac{\text{ase 1}}{\text{T}\text{-FDM}}$	Error		
$\frac{\lambda}{0}$	0	0	nan		
0.125	0.898199	0.954044	6.21746		
0.125	2.15883	2.28076	5.64815		
0.25	4.29056	4.4984	4.84417		
0.5	8.15356	8.47323	3.92057		
0.625	15.3066	15.7579	2.94855		
0.75	28.6359	29.198	1.96289		
0.875	53.5201	54.0436	0.978188		
1	100	100	0.010100		
		ase 2			
X	T_exact	T_FDM	Error		
0	1.34753	1.45683	8.11132		
0.125	1.6194	1.74137	7.53186		
0.25	2.5447	2.70613	6.34346		
0.375	4.49682	4.72797	5.14025		
0.5	8.26343	8.59667	4.03265		
0.625	15.3644	15.8234	2.98768		
0.75	28.665	29.2313	1.97532		
0.875	53.5322	54.0575	0.981321		
1	100	100	0		
		= 16 ase 1			
X	T_exact	T_FDM	Error		
		0			
0	0		nan		
0.0625	0.428029	0.434917	$\frac{\text{nan}}{1.60917}$		
-		_			
0.0625	0.428029	0.434917	1.60917		
$0.0625 \\ 0.125$	0.428029 0.898199	0.434917 0.912305	$\begin{array}{c} 1.60917 \\ 1.57056 \end{array}$		
0.0625 0.125 0.1875 0.25	0.428029 0.898199 1.4568 2.15883	$0.434917 \\ 0.912305 \\ 1.47879$	1.60917 1.57056 1.50929		
0.0625 0.125 0.1875	0.428029 0.898199 1.4568	0.434917 0.912305 1.47879 2.18968	1.60917 1.57056 1.50929 1.42918		
0.0625 0.125 0.1875 0.25 0.3125	0.428029 0.898199 1.4568 2.15883 3.0734	0.434917 0.912305 1.47879 2.18968 3.11441	1.60917 1.57056 1.50929 1.42918 1.3344		
0.0625 0.125 0.1875 0.25 0.3125 0.375	0.428029 0.898199 1.4568 2.15883 3.0734 4.29056	0.434917 0.912305 1.47879 2.18968 3.11441 4.34328	1.60917 1.57056 1.50929 1.42918 1.3344 1.22884		
0.0625 0.125 0.1875 0.25 0.3125 0.375 0.4375	0.428029 0.898199 1.4568 2.15883 3.0734 4.29056 5.93014	0.434917 0.912305 1.47879 2.18968 3.11441 4.34328 5.9963	1.60917 1.57056 1.50929 1.42918 1.3344 1.22884 1.11573		
0.0625 0.125 0.1875 0.25 0.3125 0.375 0.4375 0.5	0.428029 0.898199 1.4568 2.15883 3.0734 4.29056 5.93014 8.15356	0.434917 0.912305 1.47879 2.18968 3.11441 4.34328 5.9963 8.2349	1.60917 1.57056 1.50929 1.42918 1.3344 1.22884 1.11573 0.997575		
0.0625 0.125 0.1875 0.25 0.3125 0.375 0.4375 0.5 0.5625	0.428029 0.898199 1.4568 2.15883 3.0734 4.29056 5.93014 8.15356 11.1797	0.434917 0.912305 1.47879 2.18968 3.11441 4.34328 5.9963 8.2349 11.2777	1.60917 1.57056 1.50929 1.42918 1.3344 1.22884 1.11573 0.997575 0.876171		
0.0625 0.125 0.1875 0.25 0.3125 0.375 0.4375 0.5 0.5625 0.625	0.428029 0.898199 1.4568 2.15883 3.0734 4.29056 5.93014 8.15356 11.1797 15.3066	0.434917 0.912305 1.47879 2.18968 3.11441 4.34328 5.9963 8.2349 11.2777 15.4218	1.60917 1.57056 1.50929 1.42918 1.3344 1.22884 1.11573 0.997575 0.876171 0.752755		
0.0625 0.125 0.1875 0.25 0.3125 0.375 0.4375 0.5 0.5625 0.625 0.6875	0.428029 0.898199 1.4568 2.15883 3.0734 4.29056 5.93014 8.15356 11.1797 15.3066 20.9404	0.434917 0.912305 1.47879 2.18968 3.11441 4.34328 5.9963 8.2349 11.2777 15.4218 21.072	1.60917 1.57056 1.50929 1.42918 1.3344 1.22884 1.11573 0.997575 0.876171 0.752755 0.628147		
0.0625 0.125 0.1875 0.25 0.3125 0.375 0.4375 0.5 0.5625 0.625 0.6875 0.75	0.428029 0.898199 1.4568 2.15883 3.0734 4.29056 5.93014 8.15356 11.1797 15.3066 20.9404 28.6359	0.434917 0.912305 1.47879 2.18968 3.11441 4.34328 5.9963 8.2349 11.2777 15.4218 21.072 28.7799	1.60917 1.57056 1.50929 1.42918 1.3344 1.22884 1.11573 0.997575 0.876171 0.752755 0.628147 0.502869		
0.0625 0.125 0.1875 0.25 0.3125 0.375 0.4375 0.5 0.5625 0.625 0.6875 0.75 0.8125	0.428029 0.898199 1.4568 2.15883 3.0734 4.29056 5.93014 8.15356 11.1797 15.3066 20.9404 28.6359 39.1507	0.434917 0.912305 1.47879 2.18968 3.11441 4.34328 5.9963 8.2349 11.2777 15.4218 21.072 28.7799 39.2984	1.60917 1.57056 1.50929 1.42918 1.3344 1.22884 1.11573 0.997575 0.876171 0.752755 0.628147 0.502869 0.377251		
0.0625 0.125 0.1875 0.25 0.3125 0.375 0.4375 0.5 0.5625 0.625 0.6875 0.75 0.8125 0.875	0.428029 0.898199 1.4568 2.15883 3.0734 4.29056 5.93014 8.15356 11.1797 15.3066 20.9404 28.6359 39.1507 53.5201 73.1587	0.434917 0.912305 1.47879 2.18968 3.11441 4.34328 5.9963 8.2349 11.2777 15.4218 21.072 28.7799 39.2984 53.6547	1.60917 1.57056 1.50929 1.42918 1.3344 1.22884 1.11573 0.997575 0.876171 0.752755 0.628147 0.502869 0.377251 0.251493		

X	$T_{-}exact$	$T_{-}FDM$	Error
0	1.34753	1.37492	2.03267
0.0625	1.41386	1.44205	1.9939
0.125	1.6194	1.65001	1.89064
0.1875	1.98437	2.01911	1.75077
0.25	2.5447	2.58538	1.5985
0.3125	3.35558	3.40413	1.44702
0.375	4.49682	4.55532	1.30094
0.4375	6.08079	6.15136	1.1606
0.5	8.26343	8.34812	1.02487
0.5625	11.2596	11.3601	0.892458
0.625	15.3644	15.4815	0.76229
0.6875	20.9818	21.1148	0.633606
0.75	28.665	28.81	0.505901
0.8125	39.1704	39.3188	0.378852
0.875	53.5322	53.6672	0.252258
0.9375	73.1644	73.2566	0.125999
1	100	100	0

A.1.6 $\alpha = 7$

Case 1					
X	$T_{-}exact$	$T_{-}FDM$	Error		
0	0	0	nan		
0.5	3.01699	7.01754	132.601		
1	100	100	0		
	С	lase 2			
x	$T_{-}exact$	$T_{-}FDM$	Error		
0	0.182376	0.994716	445.419		
0.5	3.02249	7.08735	134.487		
1	100	100	0		
	n	1 = 4			
		lase 1			
X	$T_{-}exact$	$T_{-}FDM$	Error		
0	0	0	nan		
0.25	0.508906	0.835971	64.2683		
0.5	3.01699	4.2321	40.2759		
0.75	17.3769	20.5891	18.485		
1	100	100	0		
Case 2					
X	$T_{-}exact$	$T_{-}FDM$	Error		
0	0.182376	0.359502	97.121		
0.25	0.540598	0.909989	68.3303		
0.5	3.02249	4.24732	40.5239		
0.75	17.3779	20.5921	18.496		
1	100	100	0		
n = 8					

Case 1				
X	$T_{-}exact$	T_FDM	Error	
0	0	0	nan	
0.125	0.180736	0.214032	18.422	
0.25	0.508906	0.591931	16.3144	
0.375	1.25221	1.42303	13.6414	
0.5	3.01699	3.34363	10.8268	
0.625	7.24283	7.8242	8.0268	
0.75	17.3769	18.2952	5.28429	
0.875	41.686	42.7734	2.60845	
1	100	100	0	
		ase 2		
X	$T_{-}exact$	$T_{-}FDM$	Error	
0	0.182376	0.224098	22.877	
0.125	0.256762	0.309886	20.6901	
0.25	0.540598	0.63293	17.0798	
0.375	1.26542	1.44056	13.8407	
0.5	3.02249	3.35112	10.873	
0.625	7.24512	7.82739	8.03677	
0.75	17.3779	18.2965	5.2863	
0.875	41.6864	42.7739	2.60879	
1	100	100	0	
		= 16		
	Cε T_exact	ase 1 T_FDM	Ennon	
0 0	1_exact 0	0	Error	
0.0625	0.0823596	0.086265	nan 4.74189	
0.0025 0.125	0.0823330 0.180736	0.080203 0.189042	4.59524	
0.125 0.1875	0.130730 0.314263	0.103042 0.328002	4.37198	
0.1675 0.25	0.514205 0.508906	0.529744	4.09465	
0.3125	0.802521	0.832882	3.78323	
0.375	1.25221	1.29544	3.4523	
0.4375	1.94543	2.00595	3.11119	
0.4915	3.01699	3.10042	2.76532	
0.5625	4.67529	4.78832	2.41764	
0.625	7.24283	7.39274	2.06969	
0.6875	11.219	11.4122	1.72221	
0.75	17.3769	17.616	1.3756	
0.8125	26.9143	27.1916	1.03001	
0.875	41.686	41.9718	0.685524	
0.9375	64.5648	64.7857	0.342184	
1	100	100	0.012101	
	100	100	0	

Case 2

X	T_exact	T_FDM	Error
0	0.182376	0.192622	5.61791
0.0625	0.20011	0.211056	5.47003
0.125	0.256762	0.269889	5.11243
0.1875	0.363348	0.380379	4.68726
0.25	0.540598	0.563676	4.26912
0.3125	0.822982	0.854865	3.87407
0.375	1.26542	1.30968	3.49773
0.4375	1.95395	2.01518	3.13327
0.5	3.02249	3.10639	2.77583
0.5625	4.67884	4.79218	2.42256
0.625	7.24512	7.39523	2.07195
0.6875	11.2204	11.4138	1.72324
0.75	17.3779	17.617	1.37605
0.8125	26.9149	27.1922	1.0302
0.875	41.6864	41.9722	0.685601
0.9375	64.5649	64.7859	0.342208
1	100	100	0

A.2 4th Order

A.2.1 $\alpha = 0.2$

		n = 2	
		Case 1	
X	$T_{-}exact$	$T_{-}FDM$	Error
0	0	0	nan
0.5	49.751	49.751	2.07559e-07
1	100	100	0
		Case 2	
X	T _exact	$T_{-}FDM$	Error
0	98.0328	98.0328	8.22072e-07
0.5	98.5234	98.5234	6.14512 e-07
1	100	100	0
		n = 4	
		Case 1	
X	$T_{-}exact$	$T_{-}FDM$	Error
0	0	0	nan
0.25	24.8445	24.8445	1.62285 e-08
0.5	49.751	49.751	1.29763e-08
0.75	74.782	74.782	7.56323e-09
1	100	100	0
		Case 2	

X	$T_{-}exact$	$T_{-}FDM$	Error
0	98.0328	98.0328	5.13948e-08
0.25	98.1554	98.1554	4.81426e-08
0.5	98.5234	98.5234	3.84184e-08
0.75	99.1377	99.1377	2.23185e-08
1	100	100	0
		n = 8	
		Case 1	
X	$T_{-}exact$	$T_{-}FDM$	Error
0	0	0	nan
0.125	12.4183	12.4183	1.06495e-09
0.25	24.8445	24.8445	1.0141e-09
0.375	37.2861	37.2861	9.29405e-10
0.5	49.751	49.751	8.10873e-10
0.625	62.2471	62.2471	6.5857e-10
0.75	74.782	74.782	4.72606e-10
0.875	87.3637	87.3637	2.53039e-10
1	100	100	0
		Case 2	
X	$T_{-}exact$	$T_{-}FDM$	Error
0	98.0328	98.0328	3.21188e-09
0.125	98.0634	98.0634	3.16106e-09
0.25	98.1554	98.1554	3.00866e-09
0.375	98.3086	98.3086	2.75509e-09
0.5	98.5234	98.5234	2.40095e-09
0.625	98.7997	98.7997	1.94717e-09
0.75	99.1377	99.1377	1.3948e-09
0.875	99.5378	99.5378	7.45209e-10
1	100	100	0
		n = 16	

 ${\it Case}\ 1$

X	T_exact	T_FDM	Error
0	0	0	nan
0.0625	6.20869	6.20869	6.66918e-11
0.125	12.4183	12.4183	6.59142e-11
0.1875	18.6299	18.6299	6.46088e-11
0.25	24.8445	24.8445	6.27476e-11
0.3125	31.0628	31.0628	6.03997e-11
0.375	37.2861	37.2861	5.75316e-11
0.4375	43.5152	43.5152	5.41294e-11
0.5	49.751	49.751	5.02011e-11
0.5625	55.9947	55.9947	4.57328e-11
0.625	62.2471	62.2471	4.07625e-11
0.6875	68.5092	68.5092	3.52838e-11
0.75	74.782	74.782	2.92647e-11
0.8125	81.0665	81.0665	2.27012e-11
0.875	87.3637	87.3637	1.56645 e-11
0.9375	93.6745	93.6745	8.07068e-12
1	100	100	0
		Case 2	
X	T_exact	T_FDM	Error
0	98.0328	98.0328	1.98566e-10
0.0625	98.0405	98.0405	1.97797e-10
0.125	98.0634	98.0634	1.95432e-10
0.1875	98.1017	98.1017	1.91503e-10
0.25	98.1554	98.1554	1.86041e-10
0.3125	98.2243	98.2243	1.78995e-10
0.375	98.3086	98.3086	1.70385e-10
0.4375	98.4083	98.4083	1.60205e-10
0.5	98.5234	98.5234	1.48479e-10
0.5625	98.6538	98.6538	1.35232e-10
0.625	98.7997	98.7997	1.20433e-10
0.6875	98.961	98.961	1.0411e-10
0.75	99.1377	99.1377	8.62504 e-11
0.8125	99.33	99.33	6.68982 e-11
0.875	99.5378	99.5378	4.60714e-11
0.9375	99.7611	99.7611	2.3789e-11
1	100	100	0

A.2.2 $\alpha = 0.4$

		n=2	
		Case 1	
X	$T_{-}exact$	$T_{-}FDM$	Error
0	0	0	nan
0.5	49.0164	49.0164	1.31377e-05
1	100	100	0
		Case 2	

X	T_exact	T_FDM	Error
0	92.5007	92.5007	5.05802e-05
0.5	94.3569	94.3569	3.74425 e-05
1	100	100	0
		n = 4	-
		Case 1	
X	T_exact	T_{FDM}	Error
0	0	0	nan
0.25	24.3862	24.3862	1.02963e-06
0.5	49.0164	49.0164	8.22072 e-07
0.75	74.1372	74.1372	4.77966e-07
1	100	100	0
		Case 2	
X	$T_{-}exact$	T_FDM	Error
0	92.5007	92.5007	3.16499e-06
0.25	92.9636	92.9636	2.95743e-06
0.5	94.3569	94.3569	2.34292e-06
0.75	96.6946	96.6946	1.345 e-06
1	100	100	0
		n = 8	
		Case 1	
X	$T_{-}exact$	T_FDM	Error
0	0	0	nan
0.125	12.1779	12.1779	6.76233e-08
0.25	24.3862	24.3862	6.43711e-08
0.375	36.6555	36.6555	5.8958e-08
0.5	49.0164	49.0164	5.13948e-08
0.625	61.4999	61.4999	4.16963e-08
0.75	74.1372	74.1372	2.98818e-08
0.875	86.9599	86.9599	1.5974e-08
1	100	100	0
		Case 2	
X	T_exact	T_FDM	Error
0	92.5007	92.5007	1.9787e-07
0.125	92.6164	92.6164	1.94618e-07
0.25	92.9636	92.9636	1.84894e-07
0.375	93.5433	93.5433	1.68794 e - 07
0.5	94.3569	94.3569	1.46476e-07
0.625	95.4065	95.4065	1.18152e-07
0.75	96.6946	96.6946	8.40877e-08
0.875	98.2245	98.2245	4.45895e-08
1	100	100	0
		n = 16	
		Cago 1	

Case 1

X	T_exact	T_FDM	Error
0	0	0	nan
0.0625	6.08703	6.08703	4.27668e-09
0.125	12.1779	12.1779	4.22583e-09
0.1875	18.2763	18.2763	4.14113e-09
0.25	24.3862	24.3862	4.0226e-09
0.3125	30.5113	30.5113	3.87029e-09
0.375	36.6555	36.6555	3.68433e-09
0.4375	42.8225	42.8225	3.46476e-09
0.5	49.0164	49.0164	3.21172e-09
0.5625	55.2409	55.2409	2.92531e-09
0.625	61.4999	61.4999	2.60566e-09
0.6875	67.7974	67.7974	2.25297e-09
0.75	74.1372	74.1372	1.8674e-09
0.8125	80.5234	80.5234	1.44907e-09
0.875	86.9599	86.9599	9.98258e-10
0.9375	93.4507	93.4507	5.1516e-10
1	100	100	0
		Case 2	
X	T_exact	T_FDM	Error
0	92.5007	92.5007	1.23656e-08
0.0625	92.5297	92.5297	1.23148e-08
0.125	92.6164	92.6164	1.21624e-08
0.1875	92.761	92.761	1.19088e-08
0.25	92.9636	92.9636	1.15547e-08
0.3125	93.2243	93.2243	1.11009e-08
0.375	93.5433	93.5433	1.05485e-08
0.4375	93.9208	93.9208	9.89893e-09
0.5	94.3569	94.3569	9.15372e-09
0.5625	94.8521	94.8521	8.31464e-09
0.625	95.4065	95.4065	7.38366e-09
0.6875	96.0205	96.0205	6.36296e-09
0.75	96.6946	96.6946	5.25487e-09
0.8125	97.4291	97.4291	4.06184e-09
0.875	98.2245	98.2245	2.78653e-09
0.9375	99.0813	99.0813	1.43162e-09
1	100	100	0

A.2.3 $\alpha = 0.75$

n = 2Case 1

		Case 1	
X	$T_{-}exact$	$T_{-}FDM$	Error
0	0	0	nan
0.5	46.6792	46.679	0.000550658
1	100	100	0
		Case 2	

X	T_exact	$T_{-}FDM$	Error
0	77.239	77.2375	0.00195194
0.5	82.7338	82.7326	0.00140129
1	100	100	0
		n = 4	
		Case 1	
X	T_exact	T_FDM	Error
0	0	0	nan
0.25	22.9353	22.9353	4.34904 e - 05
0.5	46.6792	46.6792	3.4555e-05
0.75	72.0691	72.069	1.99322e-05
1	100	100	0
		Case 2	
X	T_exact	$T_{-}FDM$	Error
0	77.239	77.2389	0.00012249
0.25	78.6007	78.6006	0.000113554
0.5	82.7338	82.7337	8.79347e-05
0.75	89.784	89.784	4.87484e-05
1	100	100	0
		n = 8	
		Case 1	
X	T_exact	T_FDM	Error
0	0	0	nan
0.125	11.4174	11.4174	2.86195e-06
0.25	22.9353	22.9353	2.72097e-06
0.375	34.6548	34.6548	2.48709e-06
0.5	46.6792	46.6792	2.16192e-06
0.625	59.1142	59.1142	1.74767e-06
0.75	72.0691	72.0691	1.24706e-06
0.875	85.6578	85.6578	6.63297e-07
1	100	100	0
		Case 2	
X	T_exact	T_FDM	Error
0	77.239	77.239	7.66354e-06
0.125	77.5786	77.5786	7.52256e-06
0.25	78.6007	78.6007	7.1045e-06
0.375	80.314	80.314	6.42351e-06
0.5	82.7338	82.7338	5.50162e-06
0.625	85.8812	85.8812	4.36666e-06
0.75	89.784	89.784	3.04994e-06
0.875	94.4765	94.4765	1.58386e-06
1	100	100	0
		n = 16	
		Case 1	

X	T_exact	T_FDM	Error	
0	0	0	nan	
0.0625	5.70245	5.70245	1.81126e-07	
0.125	11.4174	11.4174	1.78918e-07	
0.1875	17.1575	17.1575	1.75242 e-07	
0.25	22.9353	22.9353	1.70104e-07	
0.3125	28.7635	28.7635	1.63514 e-07	
0.375	34.6548	34.6548	1.55483e-07	
0.4375	40.6224	40.6224	1.46025 e-07	
0.5	46.6792	46.6792	1.35155e-07	
0.5625	52.8386	52.8386	1.22893e-07	
0.625	59.1142	59.1142	1.09257e-07	
0.6875	65.5196	65.5196	9.42722e-08	
0.75	72.0691	72.0691	7.79612e-08	
0.8125	78.7769	78.7769	6.03502 e-08	
0.875	85.6578	85.6578	4.14668e-08	
0.9375	92.727	92.727	2.134e-08	
1	100	100	0	
Case 2				
X	$T_{-}exact$	T_{FDM}	Error	
0	T_exact 77.239	T_FDM 77.239	4.79095e-07	
0 0.0625	T_exact 77.239 77.3238	T_FDM 77.239 77.3238	4.79095e-07 4.76886e-07	
$0 \\ 0.0625 \\ 0.125$	T_exact 77.239 77.3238 77.5786	T_FDM 77.239 77.3238 77.5786	4.79095e-07 4.76886e-07 4.70281e-07	
0 0.0625 0.125 0.1875	T_exact 77.239 77.3238 77.5786 78.0039	T_FDM 77.239 77.3238 77.5786 78.0039	4.79095e-07 4.76886e-07 4.70281e-07 4.59336e-07	
0 0.0625 0.125 0.1875 0.25	T_exact 77.239 77.3238 77.5786 78.0039 78.6007	T_FDM 77.239 77.3238 77.5786 78.0039 78.6007	4.79095e-07 4.76886e-07 4.70281e-07 4.59336e-07 4.44145e-07	
0 0.0625 0.125 0.1875 0.25 0.3125	T_exact 77.239 77.3238 77.5786 78.0039 78.6007 79.3701	T_FDM 77.239 77.3238 77.5786 78.0039 78.6007 79.3701	4.79095e-07 4.76886e-07 4.70281e-07 4.59336e-07 4.44145e-07 4.24838e-07	
0 0.0625 0.125 0.1875 0.25 0.3125 0.375	T_exact 77.239 77.3238 77.5786 78.0039 78.6007 79.3701 80.314	T_FDM 77.239 77.3238 77.5786 78.0039 78.6007 79.3701 80.314	4.79095e-07 4.76886e-07 4.70281e-07 4.59336e-07 4.44145e-07 4.24838e-07 4.01573e-07	
0 0.0625 0.125 0.1875 0.25 0.3125 0.375 0.4375	T_exact 77.239 77.3238 77.5786 78.0039 78.6007 79.3701 80.314 81.4344	T_FDM 77.239 77.3238 77.5786 78.0039 78.6007 79.3701 80.314 81.4344	4.79095e-07 4.76886e-07 4.70281e-07 4.59336e-07 4.44145e-07 4.24838e-07 4.01573e-07 3.74537e-07	
0 0.0625 0.125 0.1875 0.25 0.3125 0.375 0.4375 0.5	T_exact 77.239 77.3238 77.5786 78.0039 78.6007 79.3701 80.314 81.4344 82.7338	T_FDM 77.239 77.3238 77.5786 78.0039 78.6007 79.3701 80.314 81.4344 82.7338	4.79095e-07 4.76886e-07 4.70281e-07 4.59336e-07 4.44145e-07 4.24838e-07 4.01573e-07 3.74537e-07 3.4394e-07	
0 0.0625 0.125 0.1875 0.25 0.3125 0.375 0.4375 0.5 0.5625	T_exact 77.239 77.3238 77.5786 78.0039 78.6007 79.3701 80.314 81.4344 82.7338 84.215	T_FDM 77.239 77.3238 77.5786 78.0039 78.6007 79.3701 80.314 81.4344 82.7338 84.215	4.79095e-07 4.76886e-07 4.70281e-07 4.59336e-07 4.44145e-07 4.24838e-07 4.01573e-07 3.74537e-07 3.4394e-07 3.10009e-07	
0 0.0625 0.125 0.1875 0.25 0.3125 0.375 0.4375 0.5 0.5625 0.625	T_exact 77.239 77.3238 77.5786 78.0039 78.6007 79.3701 80.314 81.4344 82.7338 84.215 85.8812	T_FDM 77.239 77.3238 77.5786 78.0039 78.6007 79.3701 80.314 81.4344 82.7338 84.215 85.8812	4.79095e-07 4.76886e-07 4.70281e-07 4.59336e-07 4.44145e-07 4.24838e-07 4.01573e-07 3.74537e-07 3.4394e-07 3.10009e-07 2.72987e-07	
0 0.0625 0.125 0.1875 0.25 0.3125 0.375 0.4375 0.5 0.5625 0.625 0.6875	T_exact 77.239 77.3238 77.5786 78.0039 78.6007 79.3701 80.314 81.4344 82.7338 84.215 85.8812 87.7362	T_FDM 77.239 77.3238 77.5786 78.0039 78.6007 79.3701 80.314 81.4344 82.7338 84.215 85.8812 87.7362	4.79095e-07 4.76886e-07 4.70281e-07 4.59336e-07 4.44145e-07 4.24838e-07 4.01573e-07 3.74537e-07 3.4394e-07 3.10009e-07 2.72987e-07 2.33122e-07	
0 0.0625 0.125 0.1875 0.25 0.3125 0.375 0.4375 0.5 0.5625 0.625 0.6875 0.75	T_exact 77.239 77.3238 77.5786 78.0039 78.6007 79.3701 80.314 81.4344 82.7338 84.215 85.8812 87.7362 89.784	T_FDM 77.239 77.3238 77.5786 78.0039 78.6007 79.3701 80.314 81.4344 82.7338 84.215 85.8812 87.7362 89.784	4.79095e-07 4.76886e-07 4.70281e-07 4.59336e-07 4.44145e-07 4.24838e-07 4.01573e-07 3.74537e-07 3.4394e-07 3.10009e-07 2.72987e-07 2.33122e-07 1.9067e-07	
0 0.0625 0.125 0.1875 0.25 0.3125 0.375 0.4375 0.5 0.5625 0.6625 0.6875 0.75 0.8125	T_exact 77.239 77.3238 77.5786 78.0039 78.6007 79.3701 80.314 81.4344 82.7338 84.215 85.8812 87.7362 89.784 92.0292	T_FDM 77.239 77.3238 77.5786 78.0039 78.6007 79.3701 80.314 81.4344 82.7338 84.215 85.8812 87.7362 89.784 92.0292	4.79095e-07 4.76886e-07 4.70281e-07 4.59336e-07 4.44145e-07 4.24838e-07 4.01573e-07 3.74537e-07 3.10009e-07 2.72987e-07 2.33122e-07 1.9067e-07 1.45885e-07	
0 0.0625 0.125 0.1875 0.25 0.3125 0.375 0.4375 0.5 0.5625 0.625 0.6875 0.75 0.8125 0.875	T_exact 77.239 77.3238 77.5786 78.0039 78.6007 79.3701 80.314 81.4344 82.7338 84.215 85.8812 87.7362 89.784 92.0292 94.4765	T_FDM 77.239 77.3238 77.5786 78.0039 78.6007 79.3701 80.314 81.4344 82.7338 84.215 85.8812 87.7362 89.784 92.0292 94.4765	4.79095e-07 4.76886e-07 4.70281e-07 4.59336e-07 4.44145e-07 4.24838e-07 4.01573e-07 3.74537e-07 3.10009e-07 2.72987e-07 2.33122e-07 1.9067e-07 1.45885e-07 9.90168e-08	
0 0.0625 0.125 0.1875 0.25 0.3125 0.375 0.4375 0.5 0.5625 0.6625 0.6875 0.75 0.8125	T_exact 77.239 77.3238 77.5786 78.0039 78.6007 79.3701 80.314 81.4344 82.7338 84.215 85.8812 87.7362 89.784 92.0292	T_FDM 77.239 77.3238 77.5786 78.0039 78.6007 79.3701 80.314 81.4344 82.7338 84.215 85.8812 87.7362 89.784 92.0292	4.79095e-07 4.76886e-07 4.70281e-07 4.59336e-07 4.44145e-07 4.24838e-07 4.01573e-07 3.74537e-07 3.10009e-07 2.72987e-07 2.33122e-07 1.9067e-07 1.45885e-07	

A.2.4 $\alpha = 3$

		n=2			
		Case 1			
X	$T_{-}exact$	$T_{-}FDM$	Error		
0	0	0	nan		
0.5	21.2548	20.9677	1.35056		
1	100	100	1.42109e-14		
	Case 2				

X	$T_{-}exact$	T_FDM	Error
0	9.93279	9.64062	2.94154
0.5	23.366	22.9892	1.61275
1	100	100	0
		n = 4	
	(T)	Case 1	
X	T_exact	T_FDM	Error
0	0	0	nan
0.25	8.20849	8.19877	0.118462
0.5	21.2548	21.2362	0.0877048
0.75	46.828	46.8064	0.0461534
1	100	100	1.42109e-14
	T_exact	Case 2 T_FDM	Error
X			
0	9.93279	9.91365	0.192715
0.25	12.8598	12.839	0.16198
0.5	23.366	23.3414	0.105102
0.75	47.6433	47.6192	0.0506849
1	100	100	0
		n = 8	
X	T_exact	$\frac{\text{Case 1}}{\text{T-FDM}}$	Error
0	0	0	
0.125	3.83166	3.83135	nan 0.0080657
0.125 0.25	8.20849	8.20788	0.0080037 0.00751509
0.25 0.375	13.7532	13.7523	0.00751509
0.575	21.2548	21.2536	0.00005700 0.00556326
0.625	31.7805	31.7791	0.00430073
0.75	46.828	46.8266	0.00292711
0.875	68.5382	68.5371	0.0014842
1	100	100	1.42109e-14
X	T_exact	$\frac{\text{Case 2}}{\text{T_FDM}}$	Error
0	9.93279	9.93158	0.0122312
0.125	9.95279	9.95158 10.6382	0.0122312 0.0116806
0.125 0.25		10.0382 12.8585	0.0116806 0.0102795
	12.8598		
0.375	16.9099	16.9085	0.00850086
0.5	23.366	23.3644	0.00666833
0.625	33.1466	33.145	0.00490192
0.75	47.6433	47.6418	0.00321492
0.875	68.9188	68.9177	0.00158808
1	100	100	0
]	n = 16	

Case 1

X	T_exact	T_FDM	Error
0	0	0	nan
0.0625	1.88264	1.88263	0.000515098
0.125	3.83166	3.83164	0.000506162
0.1875	5.91578	5.91576	0.00049154
0.25	8.20849	8.20846	0.000471607
0.3125	10.7906	10.7906	0.000446846
0.375	13.7532	13.7532	0.000417799
0.4375	17.2008	17.2007	0.000385035
0.5	21.2548	21.2547	0.000349118
0.5625	26.0583	26.0582	0.000310576
0.625	31.7805	31.7804	0.000269888
0.6875	38.6233	38.6232	0.000227472
0.75	46.828	46.8279	0.000183687
0.8125	56.6838	56.6837	0.000138828
0.875	68.5382	68.5381	9.31383e-05
0.9375	82.8092	82.8091	4.68113e-05
1	100	100	1.42109e-14
		Case 2	
X	T_exact	T_FDM	Error
0	9.93279	9.93272	0.000767589
0.0625	10.1079	10.1078	0.000758654
0.125	10.6394	10.6393	0.000733034
0.1875	11.5461	11.546	0.000693848
0.25	12.8598	12.8597	0.0006451
0.3125	14.627	14.6269	0.000590631
0.375	16.9099	16.9098	0.000533478
0.4375	19.7891	19.789	0.000475693
0.5	23.366	23.3659	0.000418472
0.5625	27.7668	27.7667	0.000362388
0.625	33.1466	33.1465	0.000307618
0.6875	39.6951	39.695	0.000254121
0.75	47.6433	47.6432	0.00020175
0.8125	57.2714	57.2713	0.000150322
0.875	68.9188	68.9187	9.9658e-05
0.9375	82.9962	82.9961	4.95958e-05
1	100	100	0

A.2.5 $\alpha = 5$

	n=2						
	(Case 1					
X	$T_{-}exact$	T_{FDM}	Error				
0	0	0	nan				
0.5	8.15356	6.6474	18.4725				
1	100	100	0				
	Case 2						

Case 1

x T_exact T_		T_FDM	Error
	0 0 0		nan
0.0625	0.428029	0.427995	0.00785374
0.125	0.898199	0.89813	0.00766651
0.1875	1.4568	1.45669	0.00736928
0.25	2.15883	2.15868	0.00698049
0.3125	3.0734	3.0732	0.00652024
0.375	4.29056	4.2903	0.00600723
0.4375	5.93014	5.92981	0.0054571
0.5	8.15356	8.15316	0.00488186
0.5625	11.1797	11.1793	0.0042902
0.625	15.3066	15.306	0.00368806
0.6875	20.9404	20.9398	0.00307941
0.75	28.6359	28.6352	0.00246676
0.8125	39.1507	39.15	0.0018517
0.875	53.5201	53.5194	0.0012352
0.9375	73.1587	73.1582	0.000617849
1	100	100	0
		Case 2	
X	T_exact	T_FDM	Error
0	1.34753	1.34739	0.00989504
0.0625	1.41386	1.41373	0.00970782
0.125	1.6194	1.61925	0.00920903
0.1875	1.98437	1.9842	0.00853303
0.25	2.5447	2.54451	0.00779647
0.3125	3.35558	3.35534	0.00706296
0.375	4.49682	4.49653	0.0063547
0.4375	6.08079	6.08044	0.00567333
0.5	8.26343	8.26302	0.00501342
0.5625	11.2596	11.2592	0.0043687
0.625	15.3644	15.3638	0.00373402
0.6875	20.9818	20.9812	0.00310573
0.75	28.665	28.6643	0.00248138
0.8125	39.1704	39.1696	0.00185942
0.875	53.5322	53.5315	0.00123889
0.9375	73.1644	73.164	0.0006192
1	100	100	0

A.2.6 $\alpha = 7$

n = 2Case 1

	Case 1						
X	$T_{\text{-}exact}$	T_FDM	Error				
0	0	0	nan				
0.5	3.01699	-0.170648	105.656				
1	100	100	0				
Case 2							

X	T_exact	T_FDM	Error
0	0.182376	0.000582421	99.6806
0.5	3.02249	-0.170649	105.646
1	100	100	0
		n = 4	
		Case 1	
X	T_exact	$T_{-}FDM$	Error
0		0	nan
0.25		0.462777	9.0644
0.5			6.24951
0.75	17.3769	16.8243	3.18006
1			0
		Case 2	
X			Error
0			12.1279
0.25			9.40781
0.5			6.27021
0.75			3.18097
1	. 100		0
		n = 8 Case 1	
X			Error
			nan
0.125	0.180736	0.179502	0.682755
0.25	0.508906	0.505802	0.609911
0.375	1.25221	1.24575	0.515978
0.5	3.01699	3.00447	0.41486
0.625	7.24283	7.22026	0.311709
0.75	17.3769	17.3408	0.20799
0.875	41.686	41.6427	0.10406
1	100	100	0
		Case 2	
X			Error
(0.829496
0.125			0.756759
0.25			0.634875
0.375			0.522478
0.5			0.416363
0.625			0.312034
0.75			0.208055
0.875			0.104071
1			0
	:	n = 16	

Case 1

x	T_exact	T_FDM	Error
0	0	0	nan
0.0625	0.0823596	0.0823225	0.0449748
0.125	0.180736	0.180658	0.043611
0.1875	0.314263	0.314132	0.0415324
0.25	0.508906	0.508708	0.038946
0.3125	0.802521	0.802232	0.0360353
0.375	1.25221	1.2518	0.0329342
0.4375	1.94543	1.94485	0.0297283
0.5	3.01699	3.01619	0.0264676
0.5625	4.67529	4.6742	0.0231792
0.625	7.24283	7.24139	0.0198772
0.6875	11.219	11.2171	0.0165686
0.75	17.3769	17.3746	0.0132567
0.8125	26.9143	26.9117	0.0099434
0.875	41.686	41.6833	0.00662929
0.9375	64.5648	64.5626	0.00331477
1	100	100	0
		Case 2	
X	T_exact	T_FDM	Error
0	0.182376	0.18228	0.0530248
0.0625	0.20011	0.200007	0.0516611
0.125	0.256762	0.256638	0.0483602
0.1875	0.363348	0.363186	0.0444275
0.25	0.540598	0.540378	0.0405481
0.3125	0.822982	0.822678	0.0368694
0.375	1.26542	1.265	0.0333513
0.4375	1.95395	1.95337	0.0299311
0.5	3.02249	3.02169	0.0265641
0.5625	4.67884	4.67775	0.0232244
0.625	7.24512	7.24368	0.019898
0.6875	11.2204	11.2186	0.016578
0.75	17.3779	17.3756	0.0132609
0.8125	26.9149	26.9122	0.0099452
0.875	41.6864	41.6836	0.00663
0.9375	64.5649	64.5628	0.00331499
1	100	100	0

A.3 6th Order

A.3.1
$$\alpha = 0.2$$

 $\begin{array}{l} n=2 \\ Case \ 1 \end{array}$

	X	$T_{-}exact$	$T_{-}FDM$	Error
	0	0	0	nan
	0.5	49.751	49.751	2.47221e-11
	1	100	100	0
			Case 2	
	X	$T_{\text{-}}$ exact	$T_{-}FDM$	Error
	0	98.0328	98.0328	9.78771e-11
	0.5	98.5234	98.5234	7.31721e-11
	1	100	100	0
			n = 4	
			Case 1	
	X	$T_{-}exact$	$T_{-}FDM$	Error
	0	0	0	nan
	0.25	24.8445	24.8445	5.57693e-13
	0.5	49.751	49.751	4.42741e-13
	0.75	74.782	74.782	2.47039e-13
	1	100	100	0
-			Case 2	
	X	T_exact	T_FDM	Error
	0	98.0328	98.0328	1.72503e-12
	0.25	98.1554	98.1554	1.60705e-12
	0.5	98.5234	98.5234	1.29815e-12
	0.75	99.1377	99.1377	7.45392e-13
	1	100	100	0
-			n = 8	
			Case 1	
_	X	T_exact	T_FDM	Error
_	0	0	0	nan
	0.125	12.4183	12.4183	3.0039e-13
	0.25	24.8445	24.8445	3.00296e-13
	0.375	37.2861	37.2861	2.66791e-13
	0.5	49.751	49.751	2.28511e-13
	0.625	62.2471	62.2471	1.94053e-13
	0.75	74.782	74.782	1.33021e-13
	0.875	87.3637	87.3637	8.13316e-14
	1	100	100	0.13310e-14
_	1	100		0
_	X	T_exact	Case 2 T_FDM	Error
_	0	98.0328	98.0328	8.11777e-13
	0.125	98.0634	98.0634	7.82541e-13
	0.125 0.25	98.1554	98.0034	7.82541e-15 7.38374e-13
	0.375	98.3086	98.3086	6.64946e-13
	0.5	98.5234	98.5234	5.91377e-13
	0.625	98.7997	98.7997	4.74656e-13
	0.75	99.1377	99.1377	3.58361e-13
	0.875	99.5378	99.5378	1.99876e-13
_	1	100	100	0

n = 16						
	T arrant	$\frac{\text{Case 1}}{\text{T_FDM}}$	Eman			
X	T_exact		Error			
0 0005	0	0	nan			
0.0625	6.20869	6.20869	1.07291e-12			
0.125	12.4183	12.4183	1.05852e-12			
0.1875	18.6299	18.6299	1.02978e-12			
0.25	24.8445	24.8445	1.01529e-12			
0.3125	31.0628	31.0628	9.7216e-13			
0.375	37.2861	37.2861	9.14712e-13			
0.4375	43.5152	43.5152	8.49088e-13			
0.5	49.751	49.751	7.85508e-13			
0.5625	55.9947	55.9947	7.233e-13			
0.625	62.2471	62.2471	6.39233e-13			
0.6875	68.5092	68.5092	5.60061e-13			
0.75	74.782	74.782	4.75076e-13			
0.8125	81.0665	81.0665	4.03187e-13			
0.875	87.3637	87.3637	2.76527e-13			
0.9375	93.6745	93.6745	1.66875e-13			
1	100	100	0			
		Case 2 T FDM	Eman			
x 0	T_exact 98.0328	98.0328	Error 3.53703e-12			
0.0625	98.0328	98.0405	3.50776e-12			
0.00_0	98.0403	00.0-00				
0.125		98.0634	3.46347e-12			
0.1875	98.1017	98.1017	3.40417e-12			
0.25	98.1554	98.1554	3.27201e-12			
0.3125	98.2243	98.2243	3.12503e-12			
0.375	98.3086	98.3086	2.9778e-12			
0.4375	98.4083	98.4083	2.8015e-12			
0.5	98.5234	98.5234	2.59629e-12			
0.5625	98.6538	98.6538	2.33357e-12			
0.625	98.7997	98.7997	2.08561e-12			
0.6875	98.961	98.961	1.78065e-12			
0.75	99.1377	99.1377	1.47645e-12			
0.8125	99.33	99.33	1.14454e-12			
0.875	99.5378	99.5378	7.99503e-13			
0.9375	99.7611	99.7611	3.98857e-13			
1	100	100	0			

A.3.2
$$\alpha = 0.4$$

 $n = 2$
Case 1

	_	X	T_e	xact	T_I	FDM		Error	_
	_	0		0		0		nan	_
	0.		49.0	0164	49.	0164	6.3	22706e-09	
		1		100		100		0	
					Cas				_
		X	T_e:	xact	T_{-}	FDM		Error	
		0	92.5	5007	92.	5007	2.	39743e-08	
	0.	5	94.3	3569	94.	3569	1.	77472e-08	
		1		100		100		0	_
					n =				
			т.		Cas			F	_
		X	1_6	exact	_ L _	$\frac{\text{FDM}}{\Omega}$		Erro	_
	0.6	0	0.4	0	0.4	0		nar	
	0.5			3862		.3862		.22565e-10	
		1.5		0164		.0164		78481e-11	
	0.		14.	1372	74	.1372		.68532e-11	
		1		100	Cas	100		(<u> </u>
		x	Τ ε	exact		FDM		Erroi	_
		0		5007		$\frac{15007}{15007}$	3.	76823e-10	
	0.5			9636		.9636		52124e-10	
		.5		3569		.3569		78955e-10	
	0.			6946		.6946		60149e-10	
		1		100		100		(
					n =	= 8			_
					Cas	e 1			_
		X	T_{-}	exact		FDM	[Erro	r
		0		0		()	na	n
	0.1	25		.1779		2.1779		.23178e-1	2
		25	24	.3862	24	1.3862	2 2	.12701e-1	2
	0.3	75	36	.6555	36	6.6555	5 1	.93844e-1	2
	(0.5		.0164		9.0164		.68154e-1	2
	0.6	25	61	.4999		1.4999		.37487e-1	2
	0.	75	74	.1372		1.1372		.58416e-1	3
	0.8	75	86	.9599	86	3.9599) 5	.22939e-1	3
		1		100		100)		0
	_		X	T_ex	act	T_F	'DM	I	Error
	_		0	92.5	007	92.5	5007	6.62144	4e-12
		0.1	125	92.6	164	92.6	6164	6.50576	6e-12
		0	.25	92.9	636	92.9	9636	6.19102	2e-12
Case	. 2	0.3	375	93.5	433	93.5	5433	5.63613	Be-12
Case	5 4		0.5	94.3	569	94.3	3569	4.87968	8e-12
		0.6	325	95.4	065	95.4	4065	3.94719	9e-12
		0	.75	96.6	946	96.6	6946	2.79236	6e-12
		0.8	375	98.2	245	98.2	2245	1.47571	le-12
			1		100		100		0
	-				n =	16		<u>-</u>	

	Case 1						
X	$T_{-}exact$	$T_{-}FDM$	Error				
0	0	0	nan				
0.0625	6.08703	6.08703	1.24026e-12				
0.125	12.1779	12.1779	1.22529e-12				
0.1875	18.2763	18.2763	1.20521e-12				
0.25	24.3862	24.3862	1.16548e-12				
0.3125	30.5113	30.5113	1.12946e-12				
0.375	36.6555	36.6555	1.06614e-12				
0.4375	42.8225	42.8225	1.02875e-12				
0.5	49.0164	49.0164	9.42241e-13				
0.5625	55.2409	55.2409	8.74658e-13				
0.625	61.4999	61.4999	7.85642e-13				
0.6875	67.7974	67.7974	6.70745 e-13				
0.75	74.1372	74.1372	5.36713e-13				
0.8125	80.5234	80.5234	4.41203e-13				
0.875	86.9599	86.9599	2.94153e-13				
0.9375	93.4507	93.4507	1.52068e-13				
1	100	100	0				
		Case 2					
X	$T_{-}exact$	$T_{-}FDM$	Error				
0	92.5007	92.5007	3.10332e-12				
0.0625	92.5297	92.5297	3.07163e-12				
0.125	92.6164	92.6164	3.03807e-12				
0.1875	92.761	92.761	2.97205e-12				
0.25	92.9636	92.9636	2.88914e-12				
0.3125	93.2243	93.2243	2.77436e-12				
0.375	93.5433	93.5433	2.65855e-12				
0.4375	93.9208	93.9208	2.49656e-12				
0.5	94.3569	94.3569	2.30429e-12				
0.5625	94.8521	94.8521	2.11248e-12				
0.625	95.4065	95.4065	1.89167e-12				
0.6875	96.0205	96.0205	1.62798e-12				
0.75	96.6946	96.6946	1.3227e-12				
0.8125	97.4291	97.4291	1.03559e-12				
0.875	98.2245	98.2245	6.94451e-13				
0.9375	99.0813	99.0813	3.58566e-13				
1	100	100	0				

A.3.3 $\alpha = 0.75$

 $\begin{array}{c|cccc} & n=2 \\ & Case \ 1 \\ \hline x & T_exact & T_FDM & Error \\ \hline 0 & 0 & 0 & nan \\ 0.5 & 46.6792 & 46.6792 & 9.06905e-07 \\ 1 & 100 & 100 & 0 \\ \end{array}$

		Case 2	
X	$T_{\text{-}}$ exact	$T_{-}FDM$	Error
0	77.239	77.239	3.21478e-06
0.5	82.7338	82.7338	2.30787e-06
1	100	100	0
		n = 4	
		Case 1	
X	$T_{-}exact$	T_FDM	Error
0	0	0	nan
0.25	22.9353	22.9353	1.81279e-08
0.5	46.6792	46.6792	1.44033e-08
0.75	72.0691	72.0691	8.30824e-09
1	100	100	0
		Case 2	
X	T_exact	T_FDM	Error
0	77.239	77.239	5.10567e-08
0.25	78.6007	78.6007	4.73321e-08
0.5	82.7338	82.7338	3.66533e-08
0.75	89.784	89.784	2.03195e-08
1	100	100	0
		n = 8	
		Case 1	
X	$T_{-}exact$	T_FDM	Error
0	0	0	nan
0.125	11.4174	11.4174	2.99046e-10
0.25	22.9353	22.9353	2.84338e-10
0.375	34.6548	34.6548	2.59881e-10
0.5	46.6792	46.6792	2.25892e-10
0.625	59.1142	59.1142	1.82593e-10
0.75	72.0691	72.0691	1.30299e-10
0.875	85.6578	85.6578	6.92975 e-11
1	100	100	0
		Case 2	
X	T_exact	T_FDM	Error
0	77.239	77.239	8.00852e-10
0.125	77.5786	77.5786	7.86135e-10
0.25	78.6007	78.6007	7.42411e-10
0.375	80.314	80.314	6.71279e-10
0.5	82.7338	82.7338	5.74935e-10
0.625	85.8812	85.8812	4.5632 e-10
0.75	89.784	89.784	3.18741e-10
0.875	94.4765	94.4765	1.65549 e-10
1	100	100	0
		n = 16	
		Case 1	

X	T_exact	T_FDM	Error
0	0	0	nan
0.0625	5.70245	5.70245	5.03085e-12
0.125	11.4174	11.4174	4.94754e-12
0.1875	17.1575	17.1575	4.86602 e-12
0.25	22.9353	22.9353	4.7245e-12
0.3125	28.7635	28.7635	4.533e-12
0.375	34.6548	34.6548	4.30572e-12
0.4375	40.6224	40.6224	4.04051e-12
0.5	46.6792	46.6792	3.74457e-12
0.5625	52.8386	52.8386	3.41564e-12
0.625	59.1142	59.1142	3.04102e-12
0.6875	65.5196	65.5196	2.62443e-12
0.75	72.0691	72.0691	2.16902e-12
0.8125	78.7769	78.7769	1.65962 e-12
0.875	85.6578	85.6578	1.14473e-12
0.9375	92.727	92.727	5.67043e-13
1	100	100	0
		Case 2	
X	$T_{\text{-exact}}$	T_FDM	Error
0	77.239	77.239	1.33941e-11
0.0625	77.3238	77.3238	1.33243e-11
0.125	77.5786	77.5786	1.31706e-11
0.1875	78.0039	78.0039	1.2862e-11
0.25	78.6007	78.6007	1.24208e-11
0.3125	79.3701	79.3701	1.18886e-11
0.375	80.314	80.314	1.12358e-11
0.4375	81.4344	81.4344	1.0453e-11
0.5	82.7338	82.7338	9.58455e-12
0.5625	84.215	84.215	8.63975e-12
0.625	85.8812	85.8812	7.57857e-12
0.6875	87.7362	87.7362	6.4789e-12
0.75	89.784	89.784	5.28649e-12
0.8125	92.0292	92.0292	4.04572e-12
0.875	94.4765	94.4765	2.75263e-12
0.9375	97.1315	97.1315	1.40453e-12
1	100	100	0

A.3.4 $\alpha = 3$

n = 2Case 1 T_exact Error T_FDM 0 0 0 nan 0.5 21.254821.26070.0277156100 100 1.42109e-141 Case 2

x	T_exact	T_FDM	Error
0	9.93279	9.93885	0.0609488
0.5	23.366	23.3738	0.0009488 0.033224
0.5			
1	100	$\frac{100}{n=4}$	0
		Case 1	
X	T_exact	T_FDM	Error
0	0	0	nan
0.25	8.20849	8.20856	0.000743033
0.5	21.2548	21.2549	0.000550047
0.75	46.828	46.8281	0.000289403
1	100	100	1.42109e-14
		Case 2	
X	$T_{-}exact$	T_FDM	Error
0	9.93279	9.93291	0.00120937
0.25	12.8598	12.86	0.00101638
0.5	23.366	23.3662	0.000659318
0.75	47.6433	47.6435	0.000317863
1	100	100	0
		n = 8	
		Case 1	
X	T-exact	$T_{-}FDM$	Error
0	0	0	nan
0.125	3.83166	3.83166	1.32844e-05
0.25	8.20849	8.2085	1.23775e-05
0.375	13.7532	13.7532	1.09653e-05
0.5	21.2548	21.2548	9.16274e-06
0.625	31.7805	31.7805	7.0833e-06
0.75	46.828	46.828	4.82092e-06
0.875	68.5382	68.5382	2.44445e-06
1	100	100	1.42109e-14
	TD /	Case 2	
X	T_exact	T_FDM	Error
0	9.93279	9.93279	2.01457e-05
0.125	10.6394	10.6394	1.92388e-05
0.25	12.8598	12.8598	1.69309e-05
0.375	16.9099	16.9099	1.40013e-05
0.5	23.366	23.366	1.0983e-05
0.625	33.1466	33.1466	8.07356e-06
0.75	47.6433	47.6433	5.295e-06
0.875	68.9188	68.9188	2.61556e-06
1	100	100	0
		n = 16	
		Case 1	

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X	T_exact	T_FDM	Error
0	0	0	nan
0.0625	1.88264	1.88264	2.14706e-07
0.125	3.83166	3.83166	2.10981e-07
0.1875	5.91578	5.91578	2.04886e-07
0.25	8.20849	8.20849	1.96578e-07
0.3125	10.7906	10.7906	1.86257e-07
0.375	13.7532	13.7532	1.74149e-07
0.4375	17.2008	17.2008	1.60493e-07
0.5	21.2548	21.2548	1.45521 e-07
0.5625	26.0583	26.0583	1.29456e-07
0.625	31.7805	31.7805	1.12496e-07
0.6875	38.6233	38.6233	9.48161e-08
0.75	46.828	46.828	7.65652 e-08
0.8125	56.6838	56.6838	5.7867e-08
0.875	68.5382	68.5382	3.88223 e-08
0.9375	82.8092	82.8092	1.95121e-08
1	100	100	1.42109e-14
		7.22	
		Case 2	
X	$T_{-}exact$	T_FDM	Error
0	T_exact 9.93279	T_FDM 9.93279	3.19951e-07
0 0.0625	T_exact 9.93279 10.1079	T_FDM 9.93279 10.1079	3.19951e-07 3.16227e-07
$0 \\ 0.0625 \\ 0.125$	T_exact 9.93279 10.1079 10.6394	T_FDM 9.93279 10.1079 10.6394	3.19951e-07 3.16227e-07 3.05548e-07
0 0.0625 0.125 0.1875	T_exact 9.93279 10.1079 10.6394 11.5461	T_FDM 9.93279 10.1079 10.6394 11.5461	3.19951e-07 3.16227e-07 3.05548e-07 2.89214e-07
0 0.0625 0.125 0.1875 0.25	7_exact 9.93279 10.1079 10.6394 11.5461 12.8598	7.FDM 9.93279 10.1079 10.6394 11.5461 12.8598	3.19951e-07 3.16227e-07 3.05548e-07 2.89214e-07 2.68895e-07
0 0.0625 0.125 0.1875 0.25 0.3125	T_exact 9.93279 10.1079 10.6394 11.5461 12.8598 14.627	T.FDM 9.93279 10.1079 10.6394 11.5461 12.8598 14.627	3.19951e-07 3.16227e-07 3.05548e-07 2.89214e-07 2.68895e-07 2.4619e-07
0 0.0625 0.125 0.1875 0.25 0.3125 0.375	T_exact 9.93279 10.1079 10.6394 11.5461 12.8598 14.627 16.9099	T.FDM 9.93279 10.1079 10.6394 11.5461 12.8598 14.627 16.9099	3.19951e-07 3.16227e-07 3.05548e-07 2.89214e-07 2.68895e-07 2.4619e-07 2.22367e-07
0 0.0625 0.125 0.1875 0.25 0.3125 0.375 0.4375	T.exact 9.93279 10.1079 10.6394 11.5461 12.8598 14.627 16.9099 19.7891	7.FDM 9.93279 10.1079 10.6394 11.5461 12.8598 14.627 16.9099 19.7891	3.19951e-07 3.16227e-07 3.05548e-07 2.89214e-07 2.68895e-07 2.4619e-07 2.22367e-07 1.98281e-07
0 0.0625 0.125 0.1875 0.25 0.3125 0.375 0.4375 0.5	T.exact 9.93279 10.1079 10.6394 11.5461 12.8598 14.627 16.9099 19.7891 23.366	T.FDM 9.93279 10.1079 10.6394 11.5461 12.8598 14.627 16.9099 19.7891 23.366	3.19951e-07 3.16227e-07 3.05548e-07 2.89214e-07 2.68895e-07 2.4619e-07 2.22367e-07 1.98281e-07 1.7443e-07
0 0.0625 0.125 0.1875 0.25 0.3125 0.375 0.4375 0.5 0.5625	T_exact 9.93279 10.1079 10.6394 11.5461 12.8598 14.627 16.9099 19.7891 23.366 27.7668	T.FDM 9.93279 10.1079 10.6394 11.5461 12.8598 14.627 16.9099 19.7891 23.366 27.7668	3.19951e-07 3.16227e-07 3.05548e-07 2.89214e-07 2.68895e-07 2.4619e-07 1.98281e-07 1.7443e-07 1.51053e-07
0 0.0625 0.125 0.1875 0.25 0.3125 0.375 0.4375 0.5 0.5625	T_exact 9.93279 10.1079 10.6394 11.5461 12.8598 14.627 16.9099 19.7891 23.366 27.7668 33.1466	T.FDM 9.93279 10.1079 10.6394 11.5461 12.8598 14.627 16.9099 19.7891 23.366 27.7668 33.1466	3.19951e-07 3.16227e-07 3.05548e-07 2.89214e-07 2.68895e-07 2.4619e-07 2.22367e-07 1.98281e-07 1.7443e-07 1.51053e-07 1.28223e-07
0 0.0625 0.125 0.1875 0.25 0.3125 0.375 0.4375 0.5 0.5625 0.625 0.6875	T-exact 9.93279 10.1079 10.6394 11.5461 12.8598 14.627 16.9099 19.7891 23.366 27.7668 33.1466 39.6951	7.FDM 9.93279 10.1079 10.6394 11.5461 12.8598 14.627 16.9099 19.7891 23.366 27.7668 33.1466 39.6951	3.19951e-07 3.16227e-07 3.05548e-07 2.89214e-07 2.68895e-07 2.4619e-07 2.22367e-07 1.98281e-07 1.7443e-07 1.51053e-07 1.28223e-07 1.05924e-07
0 0.0625 0.125 0.1875 0.25 0.3125 0.375 0.4375 0.5 0.5625 0.625 0.6875 0.75	T-exact 9.93279 10.1079 10.6394 11.5461 12.8598 14.627 16.9099 19.7891 23.366 27.7668 33.1466 39.6951 47.6433	7.FDM 9.93279 10.1079 10.6394 11.5461 12.8598 14.627 16.9099 19.7891 23.366 27.7668 33.1466 39.6951 47.6433	3.19951e-07 3.16227e-07 3.05548e-07 2.89214e-07 2.68895e-07 2.4619e-07 2.22367e-07 1.98281e-07 1.7443e-07 1.51053e-07 1.28223e-07 1.05924e-07 8.40943e-08
0 0.0625 0.125 0.1875 0.25 0.3125 0.375 0.4375 0.5 0.5625 0.625 0.6875 0.75	T_exact 9.93279 10.1079 10.6394 11.5461 12.8598 14.627 16.9099 19.7891 23.366 27.7668 33.1466 39.6951 47.6433 57.2714	T.FDM 9.93279 10.1079 10.6394 11.5461 12.8598 14.627 16.9099 19.7891 23.366 27.7668 33.1466 39.6951 47.6433 57.2714	3.19951e-07 3.16227e-07 3.05548e-07 2.89214e-07 2.68895e-07 2.4619e-07 2.22367e-07 1.98281e-07 1.7443e-07 1.51053e-07 1.28223e-07 1.05924e-07 8.40943e-08 6.2658e-08
0 0.0625 0.125 0.1875 0.25 0.3125 0.375 0.4375 0.5 0.5625 0.625 0.6875 0.75 0.8125 0.875	T_exact 9.93279 10.1079 10.6394 11.5461 12.8598 14.627 16.9099 19.7891 23.366 27.7668 33.1466 39.6951 47.6433 57.2714 68.9188	T.FDM 9.93279 10.1079 10.6394 11.5461 12.8598 14.627 16.9099 19.7891 23.366 27.7668 33.1466 39.6951 47.6433 57.2714 68.9188	3.19951e-07 3.16227e-07 3.05548e-07 2.89214e-07 2.68895e-07 2.4619e-07 2.22367e-07 1.98281e-07 1.7443e-07 1.51053e-07 1.28223e-07 1.05924e-07 8.40943e-08 6.2658e-08 4.15399e-08
0 0.0625 0.125 0.1875 0.25 0.3125 0.375 0.4375 0.5 0.5625 0.625 0.6875 0.75	T_exact 9.93279 10.1079 10.6394 11.5461 12.8598 14.627 16.9099 19.7891 23.366 27.7668 33.1466 39.6951 47.6433 57.2714	T.FDM 9.93279 10.1079 10.6394 11.5461 12.8598 14.627 16.9099 19.7891 23.366 27.7668 33.1466 39.6951 47.6433 57.2714	3.19951e-07 3.16227e-07 3.05548e-07 2.89214e-07 2.68895e-07 2.4619e-07 2.22367e-07 1.98281e-07 1.7443e-07 1.51053e-07 1.28223e-07 1.05924e-07 8.40943e-08 6.2658e-08

A.3.5 $\alpha = 5$

		T_exact	T_FDM	Error
	$\frac{\lambda}{0}$	1.34753	1.3658	1.35571
	0.5	8.26343	8.32001	0.684646
	1	100	100	0.004040
		100	n=4	
			Case 1	
	X	T_exact	T_FDM	Error
	0	0	0	nan
(0.25	2.15883	2.1594	0.0264998
	0.5	8.15356	8.15507	0.018532
(0.75	28.6359	28.6386	0.00936355
	1	100	100	0
			Case 2	
_	X	T_exact	$T_{-}FDM$	Error
	0	1.34753	1.34803	0.0375672
(0.25	2.5447	2.54546	0.0295985
	0.5	8.26343	8.26501	0.0190316
(0.75	28.665	28.6677	0.00941907
	1	100	100	0
			n = 8	_
			Case 1	
	X	T_exact	T_FDM	Error
	0	0	0	nan
	125	0.898199	0.898204	0.000539309
	.25	2.15883	2.15884	0.000491048
	375	4.29056	4.29058	0.000422582
	0.5	8.15356	8.15359	0.000343415
	625	15.3066	15.3066	0.000259436
	.75	28.6359	28.636	0.000173522
0.8	875	53.5201	53.5201	8.68886e-05
	1	100	100	0
_		T	Case 2	
	X	T_exact	T_FDM	Error
0	105	1.34753	1.34754	0.000696087
	.125	1.6194	1.61941	0.000647826
	0.25	2.5447	2.54472	0.000548453
U.	.375	4.49682	4.49684	0.000447027
0	0.5	8.26343	8.26346	0.00035267
	.625	15.3644	15.3644	0.000262669
	0.75	28.665	28.6651	0.000174551
U.	.875	53.5322	53.5322	8.71483e-05
	1	100	100	0
			n = 16 Case 1	

X	T_exact	T_FDM	Error
0	0	0	nan
0.0625	0.428029	0.428029	9.02795 e-06
0.125	0.898199	0.898199	8.81273 e-06
0.1875	1.4568	1.4568	8.47104 e-06
0.25	2.15883	2.15883	8.02412 e-06
0.3125	3.0734	3.0734	7.49504e-06
0.375	4.29056	4.29056	6.90532 e-06
0.4375	5.93014	5.93014	6.27293 e-06
0.5	8.15356	8.15356	5.61168e-06
0.5625	11.1797	11.1797	4.93155e-06
0.625	15.3066	15.3066	4.23939e-06
0.6875	20.9404	20.9404	3.53974e-06
0.75	28.6359	28.6359	2.8355e-06
0.8125	39.1507	39.1507	2.12849e-06
0.875	53.5201	53.5201	1.41983e-06
0.9375	73.1587	73.1587	7.102e-07
1	100	100	0
		Case 2	
X	T_exact	T_FDM	Error
0	1.34753	1.34753	1.13746e-05
0.0625	1.41386	1.41386	1.11594e-05
0.125	1.6194	1.6194	1.0586e-05
0.1875	1.98437	1.98437	9.80887e-06
0.25	2.5447	2.5447	8.96215e-06
0.3125	3.35558	3.35558	8.11894e-06
0.375	4.49682	4.49682	7.30477e-06
0.4375	6.08079	6.08079	6.5215e-06
0.5	8.26343	8.26343	5.76291e-06
0.5625	11.2596	11.2596	5.02179e-06
0.625	15.3644	15.3644	4.29222e-06
0.6875	20.9818	20.9818	3.57e-06
0.75	28.665	28.665	2.85231e-06
0.8125	39.1704	39.1704	2.13737e-06
0.875	53.5322	53.5322	1.42407e-06
0.9375	73.1644	73.1644	7.11753e-07
1	100	100	0

A.3.6 $\alpha = 7$

X	T_exact	T_FDM	Error
0	0.182376	0.197403	8.23948
0.5	3.02249	3.14478	4.04601
1	100	100	0
		n = 4	
	T_exact	$\frac{\text{Case 1}}{\text{T-FDM}}$	Error
$\frac{\mathbf{x}}{0}$	1_exact 0	0	
0.25	_	0.510118	$ \begin{array}{r} \text{nan} \\ 0.238063 \end{array} $
$0.25 \\ 0.5$	$0.508906 \\ 3.01699$	3.02187	0.258005
$0.5 \\ 0.75$	3.01099 17.3769	$\frac{3.02187}{17.391}$	0.101718 0.0809614
0.75	100	100	0.0009014
		Case 2	
x	T_exact	T_FDM	Error
${0}$	0.182376	0.182968	$\frac{0.32429}{0.32429}$
0.25	0.540598	0.162908 0.541938	0.24788
0.25	3.02249	3.0274	0.162309
0.75	17.3779	17.3919	0.0809871
0.75	100	100	0.0003071
		$\frac{100}{n=8}$	
		Case 1	
X	T_exact	T ₋ FDM	Error
0	0	0	nan
0.125	0.180736	0.180747	0.00570646
0.25	0.508906	0.508932	0.00509593
0.375	1.25221	1.25226	0.00430916
0.5	3.01699	3.01709	0.00346295
0.625	7.24283	7.24302	0.00260058
0.75	17.3769	17.3772	0.00173434
0.875	41.686	41.6864	0.000867259
1	100	100	0
		Case 2	
X	$T_{-}exact$	$T_{-}FDM$	Error
0	0.182376	0.182389	0.00693864
0.125	0.256762	0.256778	0.00632811
0.25	0.540598	0.540626	0.00530563
0.375	1.26542	1.26547	0.00436376
0.5	3.02249	3.02259	0.00347558
0.625	7.24512	7.24531	0.0026033
0.75	17.3779	17.3782	0.00173489
0.875	41.6864	41.6867	0.000867352
1	100	100	0
	1	n = 16	
		O 1	

Case 1

X	T_exact	T_FDM	Error
0	0	0	nan
0.0625	0.0823596	0.0823597	0.000100247
0.125	0.180736	0.180737	9.72069e-05
0.1875	0.314263	0.314263	9.2573 e-05
0.25	0.508906	0.508907	8.68071e-05
0.3125	0.802521	0.802522	8.03182e-05
0.375	1.25221	1.25221	7.34051e-05
0.4375	1.94543	1.94543	6.62587 e-05
0.5	3.01699	3.01699	5.89903e-05
0.5625	4.67529	4.67529	5.16604 e - 05
0.625	7.24283	7.24284	4.43003e-05
0.6875	11.219	11.219	3.69257e-05
0.75	17.3769	17.3769	2.95443e-05
0.8125	26.9143	26.9144	2.21597e-05
0.875	41.686	41.686	1.47737e-05
0.9375	64.5648	64.5648	7.387e-06
1	100	100	0
		Case 2	
X	T_{-} exact	T_{FDM}	Error
0	0.182376	0.182376	0.000118196
0.0625	0.20011	0.200111	0.000115155
0.125	0.256762	0.256762	0.000107796
0.1875	0.363348	0.363348	9.9028e-05
0.25	0.540598	0.540598	9.03791e-05
0.3125	0.822982	0.822983	8.21779e-05
0.375	1.26542	1.26542	7.43351e-05
0.4375	1.95395	1.95395	6.67108e-05
0.5	3.02249	3.02249	5.92055e-05
0.5625	4.67884	4.67884	5.17611e-05
0.625	7.24512	7.24512	4.43467e-05
0.6875	11.2204	11.2204	3.69468e-05
0.75	17.3779	17.3779	2.95537e-05
0.8125	26.9149	26.9149	2.21638e-05
0.875	41.6864	41.6864	1.47753e-05
0.9375	64.5649	64.5649	7.3875e-06
1	100	100	0

A.4 8th Order

A.4.1
$$\alpha = 0.2$$

 $\begin{array}{l} n=2 \\ Case \ 1 \end{array}$

X	$T_{\text{-exact}}$	T_FDM	Error
0	0	0	nan
0.5	49.751	49.751	4.28459e-14
1	100	100	0
		Case 2	
X	$T_{\text{-}exact}$	$T_{-}FDM$	Error
0	98.0328	98.0328	1.30464e-13
0.5	98.5234	98.5234	1.00967e-13
1	100	100	0
		n = 4	
		Case 1	
X	T_exact	T_FDM	Error
0	0	0	nan
0.25	24.8445	24.8445	1.28698e-13
0.5	49.751	49.751	9.99738e-14
0.75	74.782	74.782	5.70091e-14
1	100	100	0
		Case 2	
X	T_exact	T_FDM	Error
0	98.0328	98.0328	3.18912e-13
0.25	98.1554	98.1554	2.89558e-13
0.5	98.5234	98.5234	2.45205e-13
0.75	99.1377	99.1377	1.2901e-13
1	100	100	0
-		n = 8	
		Case 1	
X	T_exact	T_FDM	Error
0	0	0	nan
0.125	12.4183	12.4183	3.0039e-13
0.25	24.8445	24.8445	3.00296e-13
0.375	37.2861	37.2861	2.66791e-13
0.5	49.751	49.751	2.28511e-13
0.625	62.2471	62.2471	1.94053e-13
0.75	74.782	74.782	1.33021e-13
0.875	87.3637	87.3637	8.13316e-14
1	100	100	0.100100 11
	100	Case 2	0
X	T_exact	T_FDM	Error
0	98.0328	98.0328	8.11777e-13
0.125	98.0634	98.0634	7.82541e-13
0.125	98.1554	98.1554	7.38374e-13
0.25 0.375	98.3086	98.3086	6.64946e-13
0.575	98.5234	98.5234	5.91377e-13
0.625	98.7997	98.7997	4.74656e-13
0.75	99.1377	99.1377	3.58361e-13
0.875	99.5378	99.5378	1.99876e-13
1	100	100	0

n = 16 Case 1				
X	T_exact	T_FDM	Error	
0	0	0	nan	
0.0625	6.20869	6.20869	1.07291e-12	
0.125	12.4183	12.4183	1.05852e-12	
0.1875	18.6299	18.6299	1.02978e-12	
0.25	24.8445	24.8445	1.01529e-12	
0.3125	31.0628	31.0628	9.7216e-13	
0.375	37.2861	37.2861	9.14712e-13	
0.4375	43.5152	43.5152	8.49088e-13	
0.5	49.751	49.751	7.85508e-13	
0.5625	55.9947	55.9947	7.233e-13	
0.625	62.2471	62.2471	6.39233e-13	
0.6875	68.5092	68.5092	5.60061e-13	
0.75	74.782	74.782	4.75076e-13	
0.8125	81.0665	81.0665	4.03187e-13	
0.875	87.3637	87.3637	2.76527e-13	
0.9375	93.6745	93.6745	1.66875e-13	
1	100	100	0	
		Case 2		
X	$T_{-}exact$	T_{FDM}	Error	
0	98.0328	98.0328	3.53703e-12	
0.0625	98.0405	98.0405	3.50776e-12	
0.125	98.0634	98.0634	3.46347e-12	
0.1875	98.1017	98.1017	3.40417e-12	
0.25	98.1554	98.1554	3.27201e-12	
0.3125	98.2243	98.2243	3.12503e-12	
0.375	98.3086	98.3086	2.9778e-12	
0.4375	98.4083	98.4083	2.8015e-12	
0.5	98.5234	98.5234	2.59629e-12	
0.5625	98.6538	98.6538	2.33357e-12	
0.625	98.7997	98.7997	2.08561e-12	
0.6875	98.961	98.961	1.78065e-12	
0.75	99.1377	99.1377	1.47645e-12	
0.8125	99.33	99.33	1.14454e-12	
0.875	99.5378	99.5378	7.99503e-13	
0.9375	99.7611	99.7611	3.98857e-13	
1	100	100	0	

A.4.2 $\alpha = 0.4$

 $\begin{array}{l} n=2 \\ Case \ 1 \end{array}$

X	$T_{-}exact$	$T_{-}FDM$	Error
0	0	0	nan
0.5	49.0164	49.0164	2.75424e-12
1	100	100	0
		Case 2	
X	T_exact	T_FDM	Error
0	92.5007	92.5007	1.06619e-11
0.5	94.3569	94.3569	7.89183e-12
1	100	100	0
		n = 4	
		Case 1	
X	$T_{-}exact$	$T_{-}FDM$	Error
0	0	0	nan
0.25	24.3862	24.3862	1.60254e-13
0.5	49.0164	49.0164	1.15968e-13
0.75	74.1372	74.1372	3.83366e-14
1	100	100	0
		Case 2	
X	T_exact	T_FDM	Error
0	92.5007	92.5007	5.06978e-13
0.25	92.9636	92.9636	4.89167e-13
0.5	94.3569	94.3569	3.76519e-13
0.75	96.6946	96.6946	2.2045e-13
1	100	100	0
	100	n = 8	
		Case 1	
X	T_exact	T_FDM	Error
	0	0	nan
0.125	12.1779	12.1779	4.23016e-13
0.25	24.3862	24.3862	4.0792e-13
0.375	36.6555	36.6555	3.68303e-13
0.5	49.0164	49.0164	3.18912e-13
0.625	61.4999	61.4999	2.65732e-13
	74.1372	74.1372	
0.75	86.9599		1.53347e-13
0.875	00.000	86.9599	9.80511e-14
1	100	100	0
	Torroct	Case 2	Eman
X	T_exact	T_FDM	Error 1.13686e-12
0.105	92.5007	92.5007	
0.125	92.6164	92.6164	1.1201e-12
0.25	92.9636	92.9636	1.07005e-12
0.375	93.5433	93.5433	9.57079e-13
0.5	94.3569	94.3569	8.1328e-13
0.625	95.4065	95.4065	6.70278e-13
0.75	96.6946	96.6946	4.84989e-13
0.875	98.2245	98.2245	2.60419e-13
1	100	100	0

n = 16				
x	T_exact	$\frac{\text{Case 1}}{\text{T_FDM}}$	Error	
0	0	0	nan	
0.0625	6.08703	6.08703	1.24026e-12	
0.125	12.1779	12.1779	1.22529e-12	
0.1875	18.2763	18.2763	1.20521e-12	
0.25	24.3862	24.3862	1.16548e-12	
0.3125	30.5113	30.5113	1.12946e-12	
0.375	36.6555	36.6555	1.06614e-12	
0.4375	42.8225	42.8225	1.02875e-12	
0.5	49.0164	49.0164	9.42241e-13	
0.5625	55.2409	55.2409	8.74658e-13	
0.625	61.4999	61.4999	7.85642e-13	
0.6875	67.7974	67.7974	6.70745e-13	
0.75	74.1372	74.1372	5.36713e-13	
0.8125	80.5234	80.5234	4.41203e-13	
0.875	86.9599	86.9599	2.94153e-13	
0.9375	93.4507	93.4507	1.52068e-13	
1	100	100	0	
	(Case 2		
X	$T_{-}exact$	T_FDM	Error	
0	92.5007	92.5007	3.10332e-12	
0.0625	92.5297	92.5297	3.07163e-12	
0.125	92.6164	92.6164	3.03807e-12	
0.1875	92.761	92.761	2.97205e-12	
0.25	92.9636	92.9636	2.88914e-12	
0.3125	93.2243	93.2243	2.77436e-12	
0.375	93.5433	93.5433	2.65855e-12	
0.4375	93.9208	93.9208	2.49656e-12	
0.5	94.3569	94.3569	2.30429e-12	
0.5625	94.8521	94.8521	2.11248e-12	
0.625	95.4065	95.4065	1.89167e-12	
0.6875	96.0205	96.0205	1.62798e-12	
0.75	96.6946	96.6946	1.3227e-12	
0.8125	97.4291	97.4291	1.03559e-12	
0.875	98.2245	98.2245	6.94451e-13	
0.9375	99.0813	99.0813	3.58566e-13	
1	100	100	0	

$$\mathbf{A.4.3} \quad \alpha = 0.75$$

$$\mathbf{n} = 2$$

$$\mathbf{Case} \ 1$$

x	T_exact	T_FDM	Error
0	0	0	nan
0.5	46.6792	46.6792	1.41633e-09
1	100	100	0
	100	Case 2	
X	T_exact	T_FDM	Error
0	77.239	77.239	5.02062e-09
0.5	82.7338	82.7338	3.60427e-09
0.5	100	100	0
	100	n=4	
x	T_exact	Case 1 T_FDM	Error
0	0		
-	~	00.0050	nan
0.25	22.9353	22.9353	7.07901e-12
0.5	46.6792	46.6792	5.61685e-12
0.75	72.0691	72.0691	3.25353e-12
1	100	100	0
		Case 2	
X	T_exact	T_FDM	Error
0	77.239	77.239	1.99256e-11
0.25	78.6007	78.6007	1.84595e-11
0.5	82.7338	82.7338	1.43081e-11
0.75	89.784	89.784	7.92974e-12
1	100	100	0
		n = 8	
		Case 1	
X	T_exact	$T_{-}FDM$	Error
0	0	0	nan
0.125	11.4174	11.4174	2.80049e-13
0.25	22.9353	22.9353	2.47843e-13
0.375	34.6548	34.6548	2.46041e-13
0.5	46.6792	46.6792	1.97884e-13
0.625	59.1142	59.1142	1.44238e-13
0.025	72.0691	72.0691	9.85919e-14
0.75			6.6361e-14
0.0.0	85.6578	85.6578	0.000=0==
1	100	100	0
	T	Case 2	E
X	T_exact	T_FDM	Error
0	77.239	77.239	7.35942e-13
0.125	77.5786	77.5786	7.14402e-13
0.25	78.6007	78.6007	6.87033e-13
0.375	80.314	80.314	6.016e-13
0.5	82.7338	82.7338	5.15298e-13
0.625	85.8812	85.8812	4.13678e-13
0.75	89.784	89.784	2.84901e-13
0.875	94.4765	94.4765	1.35375e-13
	_		
1	100	100	0

n = 16					
X	T_exact	$\frac{\text{Case 1}}{\text{T}_{-}\text{FDM}}$	Error		
	0	0	nan		
0.0625	5.70245	5.70245	4.20536e-13		
0.125	11.4174	11.4174	4.35632e-13		
0.1875	17.1575	17.1575	4.1413e-13		
0.25	22.9353	22.9353	4.02745 e-13		
0.3125	28.7635	28.7635	4.07599e-13		
0.375	34.6548	34.6548	3.89565e-13		
0.4375	40.6224	40.6224	3.49828e-13		
0.5	46.6792	46.6792	3.19658e-13		
0.5625	52.8386	52.8386	2.82396e-13		
0.625	59.1142	59.1142	2.64436e-13		
0.6875	65.5196	65.5196	2.38584e-13		
0.75	72.0691	72.0691	1.97184e-13		
0.8125	78.7769	78.7769	1.62354e-13		
0.875	85.6578	85.6578	9.95415e-14		
0.9375	92.727	92.727	6.13019e-14		
1	100	100	0		
		Case 2			
X	$T_{-}exact$	T_{FDM}	Error		
0	77.239	77.239	7.17544e-13		
0.0625	77.3238	77.3238	7.16756e-13		
0.125	77.5786	77.5786	6.96084 e-13		
0.1875	78.0039	78.0039	6.92289e-13		
0.25	78.6007	78.6007	6.87033e-13		
0.3125	79.3701	79.3701	6.44563e-13		
0.375	80.314	80.314	6.19294e-13		
0.4375	81.4344	81.4344	5.93323e-13		
0.5	82.7338	82.7338	5.49651e-13		
0.5625	84.215	84.215	5.06235e-13		
0.625	85.8812	85.8812	4.46772e-13		
0.6875	87.7362	87.7362	3.72537e-13		
0.75	89.784	89.784	3.00729e-13		
0.8125	92.0292	92.0292	2.16184e-13		
0.875	94.4765	94.4765	1.35375e-13		
0.9375	97.1315	97.1315	5.85221e-14		
1	100	100	0		

A.4.4 $\alpha = 3$

 $\begin{array}{l} n=2 \\ Case \ 1 \end{array}$

X	$T_{-}exact$	$T_{-}FDM$	Error
0	0	0	nan
0.5	21.2548	21.2549	0.00068718
1	100	100	1.42109e-14
	_	Case 2	
X	$T_{\text{-}exact}$	T_FDM	Error
0	9.93279	9.93294	0.00151088
0.5	23.366	23.3662	0.000823694
1	100	100	0
		n = 4	
	TT 1	Case 1	
X	T_exact	T_FDM	Error
0	0	0	nan
0.25	8.20849	8.2085	4.63469e-06
0.5	21.2548	21.2548	3.43094e-06
0.75	46.828	46.828	1.80517e-06
1	100	100	1.42109e-14
	T_exact	Case 2 T_FDM	Error
X		9.93279	
0	9.93279		7.54345e-06 6.33969e-06
0.25	12.8598	12.8598	0.000000000
0.5	23.366	23.366	4.11251e-06
0.75	47.6433	47.6433	1.98268e-06
1	100	100	0
		n = 8	
X	T_exact	Case 1 T_FDM	Error
0	0	0	nan
0.125	3.83166	3.83166	2.07466e-08
0.125	8.20849	8.20849	1.93303e-08
0.375	13.7532	13.7532	1.71247e-08
0.5	21.2548	21.2548	1.43097e-08
0.625	31.7805	31.7805	1.10622e-08
0.75	46.828	46.828	7.52894e-09
0.875	68.5382	68.5382	3.81754e-09
1	100	100	1.42109e-14
1	100	Case 2	1.421030-14
X	T_exact	T_FDM	Error
0	9.93279	9.93279	3.1462e-08
0.125	10.6394	10.6394	3.00457e-08
0.25	12.8598	12.8598	2.64415e-08
0.375	16.9099	16.9099	2.18663e-08
0.5	23.366	23.366	1.71524e-08
0.625	33.1466	33.1466	1.26087e-08
0.025	47.6433	47.6433	8.26933e-09
0.875	68.9188	68.9188	4.08479e-09
0.075	100	100	4.004796-09
	100	100	U

n = 16 Case 1					
X	T_exact	T_FDM	Error		
0	0	0	nan		
0.0625	1.88264	1.88264	8.37397e-11		
0.125	3.83166	3.83166	8.22773e-11		
0.1875	5.91578	5.91578	7.99179e-11		
0.25	8.20849	8.20849	7.66722e-11		
0.3125	10.7906	10.7906	7.26469e-11		
0.375	13.7532	13.7532	6.79377e-11		
0.4375	17.2008	17.2008	6.26034 e-11		
0.5	21.2548	21.2548	5.67804 e-11		
0.5625	26.0583	26.0583	5.04994e-11		
0.625	31.7805	31.7805	4.38996e-11		
0.6875	38.6233	38.6233	3.69958e-11		
0.75	46.828	46.828	2.98614e-11		
0.8125	56.6838	56.6838	2.25634e-11		
0.875	68.5382	68.5382	1.5136e-11		
0.9375	82.8092	82.8092	7.60231e-12		
1	100	100	1.42109e-14		
		Case 2			
X	T_exact	T_FDM	Error		
0	9.93279	9.93279	1.24668e-10		
0.0625	10.1079	10.1079	1.23211e-10		
0.125	10.6394	10.6394	1.19042e-10		
0.1875	11.5461	11.5461	1.12664e-10		
0.25	12.8598	12.8598	1.04732e-10		
0.3125	14.627	14.627	9.58919e-11		
0.375	16.9099	16.9099	8.66227e-11		
0.4375	19.7891	19.7891	7.72333e-11		
0.5	23.366	23.366	6.79495e-11		
0.5625	27.7668	27.7668	5.88307e-11		
0.625	33.1466	33.1466	4.99039e-11		
0.6875	39.6951	39.6951	4.12237e-11		
0.75	47.6433	47.6433	3.27358e-11		
0.8125	57.2714	57.2714	2.4379e-11		
0.875	68.9188	68.9188	1.61659e-11		
0.9375	82.9962	82.9962	8.03036e-12		
1	100	100	0		

A.4.5 $\alpha = 5$

n = 2Case 1

		- T	T DDM	
	X	T_exact	T_FDM	Error
	0	0	0	nan
	0.5	8.15356	8.15723	0.0449772
	1	100	100	0
			Case 2	
	X	$T_{-}exact$	T_FDM	Error
	0	1.34753	1.34876	0.0911882
	0.5	8.26343	8.26725	0.0461902
	1	100	100	0
			n = 4	
			Case 1	
	X	$T_{-}exact$	T_{FDM}	Error
	0	0	0	nan
(0.25	2.15883	2.15884	0.00045744
	0.5	8.15356	8.15359	0.000319911
(0.75	28.6359	28.636	0.000161646
	1	100	100	0
_			Case 2	
	X	T_exact	T_FDM	Error
	0	1.34753	1.34754	0.000648445
(0.25	2.5447	2.54472	0.000510916
	0.5	8.26343	8.26346	0.000328533
(0.75	28.665	28.6651	0.000162605
`	1	100	100	0
_			n = 8	
			Case 1	
	X	T_exact	T_FDM	Error
	0	0	0	nan
0.	125	0.898199	0.898199	2.33751e-06
(0.25	2.15883	2.15883	2.12834e-06
0.	375	4.29056	4.29056	1.83158e-06
	0.5	8.15356	8.15356	1.48845e-06
0	625	15.3066	15.3066	1.12447e-06
	0.75	28.6359	28.6359	7.52094e-07
	.875	53.5201	53.5201	3.76599e-07
0.	1	100	100	0.100330-01
	1	100	Case 2	0
_	X	T_exact	T_FDM	Error
_	0	1.34753	1.34753	3.01702e-06
C	0.125	1.6194	1.6194	2.80785e-06
C	0.25	2.5447	2.5447	2.37714e-06
C	0.25 0.375	4.49682	4.49682	1.93753e-06
U	0.5	4.49682 8.26343		1.93753e-06 1.52857e-06
0			8.26343	
U	0.625	$15.3644 \\ 28.665$	15.3644	1.13848e-06
		7× 665	28.665	7.56552e-07
_	0.75			
C	0.75	53.5322	53.5322	3.77725e-07

n = 16 Case 1					
x	T_exact	$\frac{\text{Jase I}}{\text{T_FDM}}$	Error		
	0	0	nan		
0.0625	0.428029	0.428029	9.79261e-09		
0.125	0.898199	0.898199	9.55917e-09		
0.1875	1.4568	1.4568	9.18853e-09		
0.25	2.15883	2.15883	8.70376e-09		
0.3125	3.0734	3.0734	8.12987e-09		
0.375	4.29056	4.29056	7.49022e-09		
0.4375	5.93014	5.93014	6.80426 e-09		
0.5	8.15356	8.15356	6.087e-09		
0.5625	11.1797	11.1797	5.34925 e-09		
0.625	15.3066	15.3066	4.59846e-09		
0.6875	20.9404	20.9404	3.83957e-09		
0.75	28.6359	28.6359	3.07567e-09		
0.8125	39.1507	39.1507	2.30878e-09		
0.875	53.5201	53.5201	1.54008e-09		
0.9375	73.1587	73.1587	7.70345e-10		
1	100	100	0		
-		Case 2			
X	T_exact	T_FDM	Error		
0	1.34753	1.34753	1.2338e-08		
0.0625	1.41386	1.41386	1.21046e-08		
0.125	1.6194	1.6194	1.14826e-08		
0.1875	1.98437	1.98437	1.06397e-08		
0.25	2.5447	2.5447	9.72122e-09		
0.3125	3.35558	3.35558	8.80659e-09		
0.375	4.49682	4.49682	7.92346e-09		
0.4375	6.08079	6.08079	7.07383e-09		
0.5	8.26343	8.26343	6.25102e-09		
0.5625	11.2596	11.2596	5.4471e-09		
0.625	15.3644	15.3644	4.65574e-09		
0.6875	20.9818	20.9818	3.87235e-09		
0.75	28.665	28.665	3.09389e-09		
0.8125	39.1704	39.1704	2.31839e-09		
0.875	53.5322	53.5322	1.54469e-09		
0.9375	73.1644	73.1644	7.72052e-10		
1	100	100	0		

$$\mathbf{A.4.6} \quad \alpha = 7$$
$$\mathbf{n} = 2$$
$$\mathbf{Case} \ 1$$

	x	T_exact	T_FDM	Error
	0	0	0	nan
	0.5	3.01699	3.03228	0.506833
	1	100	100	0
			Case 2	
_	X	T_exact	T_FDM	Error
-	0	0.182376	0.184233	1.01811
	0.5	3.02249	3.03786	0.508696
	1	100	100	0
-			n = 4	
_			Case 1	
	X	T_exact	T_FDM	Error
	0	0	0	nan
(0.25	0.508906	0.508947	0.00800042
	0.5	3.01699	3.01715	0.00543668
(0.75	17.3769	17.3774	0.00272283
	1	100	100	0
			Case 2	
_	X	T_exact	T_FDM	Error
	0	0.182376	0.182396	0.0108935
(0.25	0.540598	0.540643	0.00832966
	0.5	3.02249	3.02265	0.00545651
(0.75	17.3779	17.3783	0.00272369
	1	100	100	0
			n = 8 Case 1	
	X	T_exact	T ₋ FDM	Error
	0	0	0	nan
0.	.125	0.180736	0.180736	4.84114e-05
(0.25	0.508906	0.508906	4.3232e-05
	.375	1.25221	1.25221	3.65575 e - 05
_	0.5	3.01699	3.01699	2.93786e-05
0.	.625	7.24283	7.24284	2.20626e-05
	0.75	17.3769	17.3769	1.47138e-05
	.875	41.686	41.686	7.35766e-06
0.	1	100	100	0
		100	Case 2	<u> </u>
	X	T_exact	T_FDM	Error
	0	0.182376	0.182376	5.88644e-05
0.	.125	0.256762	0.256762	5.3685 e - 05
	0.25	0.540598	0.540598	4.5011e-05
	.375	1.26542	1.26542	3.70207e-05
-	0.5	3.02249	3.02249	2.94858e-05
0.	.625	7.24512	7.24512	2.20857e-05
	0.75	17.3779	17.3779	1.47185e-05
	.875	41.6864	41.6864	7.35845e-06
0.	1	100	100	0.000400
	т.	100	100	U

n = 16					
Case 1					
X	T_exact	T_FDM	Error		
0	0	0	nan		
0.0625	0.0823596	0.0823596	2.13055e-07		
0.125	0.180736	0.180736	2.06593e-07		
0.1875	0.314263	0.314263	1.96745e-07		
0.25	0.508906	0.508906	1.84491e-07		
0.3125	0.802521	0.802521	1.707e-07		
0.375	1.25221	1.25221	1.56007e-07		
0.4375	1.94543	1.94543	1.40819e-07		
0.5	3.01699	3.01699	1.25372e-07		
0.5625	4.67529	4.67529	1.09794e-07		
0.625	7.24283	7.24283	9.41512e-08		
0.6875	11.219	11.219	7.8478e-08		
0.75	17.3769	17.3769	6.27904 e-08		
0.8125	26.9143	26.9143	4.7096e-08		
0.875	41.686	41.686	3.13985e-08		
0.9375	64.5648	64.5648	1.56996e-08		
1	100	100	0		
		Case 2			
X	T_exact	T_FDM	Error		
0	0.182376	0.182376	2.51201e-07		
0.0625	0.20011	0.20011	2.4474e-07		
0.125	0.256762	0.256762	2.29098e-07		
0.1875	0.363348	0.363348	2.10464e-07		
0.25	0.540598	0.540598	1.92082e-07		
0.3125	0.822982	0.822982	1.74652e-07		
0.375	1.26542	1.26542	1.57984e-07		
0.4375	1.95395	1.95395	1.4178e-07		
0.5	3.02249	3.02249	1.25829e-07		
0.5625	4.67884	4.67884	1.10008e-07		
0.625	7.24512	7.24512	9.42499e-08		
0.6875	11.2204	11.2204	7.85229e-08		
0.75	17.3779	17.3779	6.28104 e-08		
0.8125	26.9149	26.9149	4.71046e-08		
0.875	41.6864	41.6864	3.14019e-08		
0.9375	64.5649	64.5649	1.57006e-08		
1	100	100	0		

Bibliography

 $[{\rm Hof}01]$ Joe D. Hoffman. "Numerical Methods for Engineers and Scientists". In: Marcel Decker, 2001. Chap. 8.