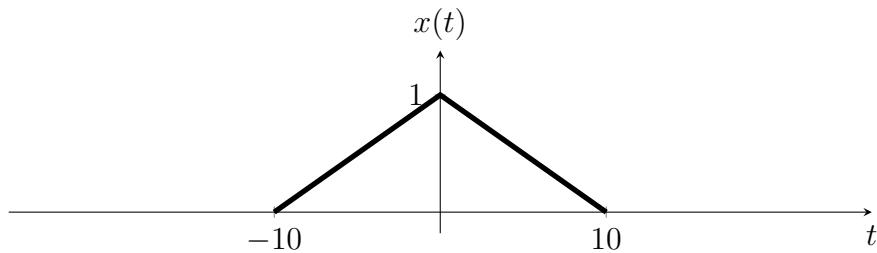


Score Table (for teacher use only)

Question:	1	2	3	4	5	Total
Points:	15	20	25	20	20	100
Score:						

This is an open-book exam. Please provide ALL DERIVATIONS and EXPLANATIONS with your answers. Simply writing down the final answer corresponds to 1 point. Any communication with others during the exam will be regarded as a cheating case.

1. (15 points) Consider a triangular signal  $x(t)$  shown below:



- (a) (5 points) Find the Fourier transform  $X(j\omega)$  of this signal.

Solution 1) Consider a signal  $g(t)$  of duration  $L = 10$ .

$$g(t) = \text{rect}(t/10)$$

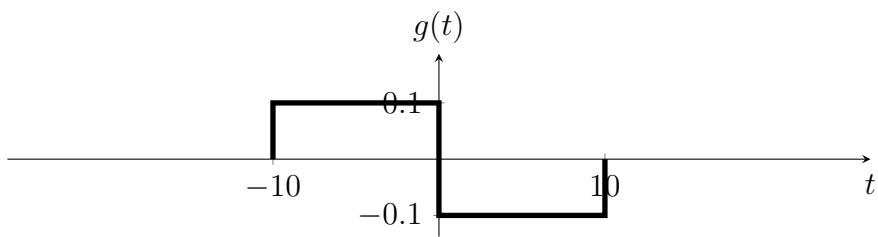
The given signal is obtained by the convolution:  $x(t) = (1/10)(g(t) * g(t))$ . From the FT of the rectangular signal

$$\text{rect}(t/L) \leftrightarrow L \text{sinc}(Lf) = 2 \frac{\sin(\omega L/2)}{\omega}$$

and the convolution-multiplication property of the FT,

$$X(j\omega) = \frac{1}{10} \left( 2 \frac{\sin(5\omega)}{\omega} \right)^2 = 2 \frac{\sin^2(5\omega)}{5\omega^2}$$

Solution 2) The given signal is obtained by integrating the following signal  $g(t)$ :



This signal consists of two delayed rectangular signals of duration  $L = 10$ :

$$g(t) = -\frac{1}{10}\text{rect}((t-5)/10) + \frac{1}{10}\text{rect}((t+5)/10)$$

From the FT of the rectangular signal

$$\text{rect}(t/L) \leftrightarrow L\text{sinc}(Lf) = 2\frac{\sin(\omega L/2)}{\omega}$$

and the time shifting property

$$x(t-\tau) \leftrightarrow X(j\omega)e^{-j\omega\tau},$$

the FT of  $g(t)$  is given by

$$\begin{aligned} G(j\omega) &= \frac{\sin(5\omega)}{5\omega} (e^{j5\omega} - e^{-j5\omega}) \\ &= \frac{\sin(5\omega)}{5\omega} \cdot 2j \sin(5\omega) \\ &= 2j \frac{\sin^2(5\omega)}{5\omega} \end{aligned}$$

The integral property of FT states that

$$\int_{-\infty}^t g(\tau)d\tau \longleftrightarrow \frac{1}{j\omega}G(j\omega) + \underbrace{\pi G(0)\delta(\omega)}_{\text{dc value}}$$

The signal  $g(t)$  has zero mean value, so the integration of  $g(t)$  corresponds to

$$x(t) = \int_{-\infty}^t g(\tau)d\tau \longleftrightarrow \frac{1}{j\omega}G(j\omega) = 2\frac{\sin^2(5\omega)}{5\omega^2} = X(j\omega)$$

(b) (5 points) The signal  $x(t)$  is now filtered by a filter

$$h(t) = \frac{1}{\pi} \frac{\sin(\frac{\pi}{5}t)}{t}$$

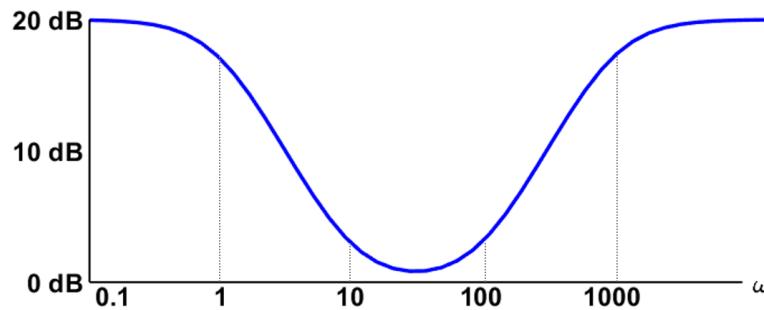
Determine the Nyquist rate  $\omega_s$  to sample the filtered signal  $y(t) = x(t) * h(t)$  without aliasing.

The original signal  $X(j\omega)$  has infinite bandwidth. This is filtered by the  $h(t) \leftrightarrow H(j\omega) = \text{rect}(\omega/(2\pi/5))$  of bandwidth  $2\pi/5$ . Therefore, the Nyquist rate is the filter's bandwidth  $\omega_s = 2\pi/5$ .

(c) (5 points) After the sampling at the Nyquist rate, the signal  $y(t)$  is converted to a discrete sequence  $y[n]$ . Determine the Fourier transform  $Y(e^{j\Omega})$  of the sampled sequence  $y[n]$ .

The conversion to a DT sequence accompanies the amplitude scaling by  $1/T$  ( $T = 2\pi/\omega_s = 5$ ) and frequency scale compression by  $(\Omega = \omega T)$ . As a result, the sampled sequence becomes  $Y(e^{j\Omega}) = 2\frac{\sin^2(\Omega)}{\Omega^2}$ .

2. (20 points) A stable LTI system's magnitude response  $|H(j\omega)|$  is shown as a Bode plot with its 4 break frequencies. **The frequency response is the rational function of  $j\omega$ , and its impulse response is a real-valued signal.**



- (a) (10 points) Derive its frequency response  $H(j\omega)$  such that its phase change is minimal. In other words, design a 'minimum phase' system that yields the given magnitude response.

From the magnitude response, the possible forms of  $H(j\omega)$  are given by

$$10 \frac{(j\omega \pm 10)(j\omega \pm 100)}{(j\omega \pm 1)(j\omega \pm 1000)}$$

Since the LTI system is stable, there are four possibilities (any solution among these four cases will be evaluated as a correct answer):

- (1) For right-sided signal

Poles should be on the left hand side

$$10 \frac{(j\omega \pm 10)(j\omega \pm 100)}{(j\omega + 1)(j\omega + 1000)}$$

To have the minimum phase, the phase drop at  $\omega = 1$  should be compensated by the phase change at  $\omega = 10$ . Likewise, the coefficient at  $\omega = 1000$  should have the same sign with that for  $\omega = 100$ .

$$\therefore H_1(j\omega) = 10 \frac{(j\omega + 10)(j\omega + 100)}{(j\omega + 1)(j\omega + 1000)}$$

- (2) For left-sided signal

Poles should be on the right half plane. The same signs for  $\omega = 1, 10$  and  $\omega = 100, 10000$  yields

$$\therefore H_2(j\omega) = 10 \frac{(j\omega - 10)(j\omega - 100)}{(j\omega - 1)(j\omega - 1000)}$$

- (3,4) For both-sided signal

There are two chances. Two denominator terms for  $\omega = 1$  and  $\omega = 1000$  should lie on the other side of half plane, respectively, so that the ROC is given by the strip. The minimum phase condition implies that the signs for  $\omega = 1, 10$  and  $\omega = 100, 10000$  should be the same. Accordingly, we have

$$\therefore H_3(j\omega) = 10 \frac{(j\omega - 10)(j\omega + 100)}{(j\omega - 1)(j\omega + 1000)} \text{ or } H_4(j\omega) = 10 \frac{(j\omega + 10)(j\omega - 100)}{(j\omega + 1)(j\omega - 1000)}.$$

- (b) (10 points) Find its impulse response  $h(t)$ .

Any solution among those shown below will be regarded as a correct answer.

To derive a left-sided or right-sided impulse response, we use the property

$$\begin{aligned}\frac{1}{j\omega + a} &\leftrightarrow e^{-at}u(t) \text{ for } a > 0 \text{ and right-sided signal} \\ &\leftrightarrow -e^{-at}u(-t) \text{ for } a < 0 \text{ and left-sided signal}\end{aligned}$$

(1) For right-sided signal

$$\begin{aligned}H_1(j\omega) &= 10 \frac{(j\omega)^2 + 110(j\omega) + 1000}{(j\omega)^2 + 1001(j\omega) + 1000} \\ &= 10 \left( 1 - 891 \frac{(j\omega)}{(j\omega + 1)(j\omega + 1000)} \right) \\ &= 10 \left( 1 + \frac{891}{999} \left[ \frac{1}{j\omega + 1} - \frac{1000}{j\omega + 1000} \right] \right) \\ \therefore h_1(t) &= 10 \left( \delta(t) + \frac{33}{37} [e^{-t} - 1000e^{-1000t}] u(t) \right)\end{aligned}$$

(2) For left-sided signal

$$\begin{aligned}H_2(j\omega) &= H_1(j\omega)^* \\ \therefore h_2(t) &= h_1(-t)^* \\ &= 10 \left( \delta(t) + \frac{33}{37} [e^t - 1000e^{1000t}] u(-t) \right)\end{aligned}$$

(3)

$$\begin{aligned}H_3(j\omega) &= 10 \frac{(j\omega + 10)(j\omega - 100)}{(j\omega + 1)(j\omega - 1000)} \\ &= 10 \frac{(j\omega)^2 - 90(j\omega) - 1000}{(j\omega)^2 - 999(j\omega) - 1000} \\ &= 10 \left( 1 + 909 \frac{(j\omega)}{(j\omega + 1)(j\omega - 1000)} \right) \\ &= 10 \left( 1 - \frac{909}{1001} \left[ \frac{1}{j\omega + 1} + \frac{1000}{j\omega - 1000} \right] \right) \\ \therefore h_3(t) &= 10 \left( \delta(t) + \frac{909}{1001} [e^{-t}u(t) - 1000e^{1000t}u(-t)] \right)\end{aligned}$$

(4)

$$\begin{aligned}H_4(j\omega) &= H_3(j\omega)^* \\ \therefore h_4(t) &= h_3(-t)^* \\ &= 10 \left( \delta(t) + \frac{909}{1001} [e^t u(-t) - 1000e^{-1000t} u(t)] \right)\end{aligned}$$

3. (25 points) Consider a CT filter  $h(t)$  given by

$$h(t) = \text{sgn}(t)e^{-a|t|}$$

where  $\text{sgn}(t) = 1$  for  $t > 0$  and  $\text{sgn}(t) = -1$  for  $t < 0$ . The parameter  $a$  is positive ( $a > 0$ ).

- (a) (10 points) Find the Fourier transform  $H(j\omega)$  of  $h(t)$ .

The signal can be rewritten as

$$h(t) = e^{-at}u(t) - e^{at}u(-t)$$

Using the following properties of FT,

$$\begin{aligned} e^{-at}u(t) &\leftrightarrow \frac{1}{j\omega + a} \\ x(-t) &\leftrightarrow X(-j\omega) \end{aligned}$$

The FT of  $h(t)$  is given by

$$\begin{aligned} H(j\omega) &= \frac{1}{j\omega + a} - \frac{1}{-j\omega + a} \\ &= \frac{-2j\omega}{\omega^2 + a^2} \end{aligned}$$

- (b) (10 points) Suppose that we want to design a system that has the maximum magnitude response at frequency  $\omega_0$ . Determine the system parameter  $a$  to have the maximum response at  $\omega = \omega_0$ .

The given magnitude response  $|H(j\omega)|$  decays out for both  $\omega \rightarrow 0, \infty$  and has the maximum value at the break frequency. To find the frequency of maximum magnitude, we can take the derivative of  $H(j\omega)$  with respect to  $\omega$ .

$$\begin{aligned} \frac{dH(j\omega)}{dt} &= \frac{-2j}{\omega^2 + a^2} - \frac{-4j\omega^2}{(\omega^2 + a^2)^2} \\ &= \frac{2j(\omega^2 - a^2)}{(\omega^2 + a^2)^2} \end{aligned}$$

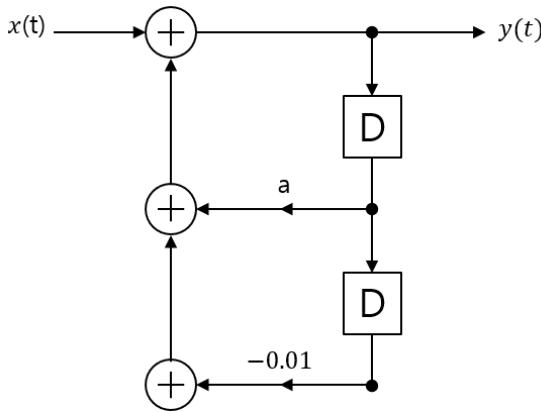
This derivative becomes zero at  $\omega = a$ . Therefore,  $a$  should be equal to  $\omega_0$  ( $a = \pm\omega_0$  is okay).

- (c) (5 points) Derive the Laplace transform of this system and determine the region of convergence (ROC).

$$\begin{aligned} H(s) &= \frac{1}{s+a} - \frac{1}{-s+a} \\ &= \frac{2s}{s^2 - a^2} \end{aligned}$$

Since the impulse response is both-sided, its ROC is given by the strip between two poles. (ROC:  $-a < \text{Re}\{s\} < a$ ).

4. (20 points) A continuous-time, causal LTI system's block diagram is shown below.



- (a) (10 points) Draw the pole-zero plot of this system for  $a = -0.1$  (mark the locations of poles and zeros, and specify the region of convergence).

The LCCDE of the given system can be written as

$$\begin{aligned} y(t) &= x(t) - 0.01 \frac{d^2 y(t)}{dt^2} + a \frac{dy(t)}{dt} \\ \frac{d^2 y(t)}{dt^2} - 100a \frac{dy(t)}{dt} + 100y(t) &= 100x(t) \end{aligned}$$

For  $a = -0.1$ , the system response is given by

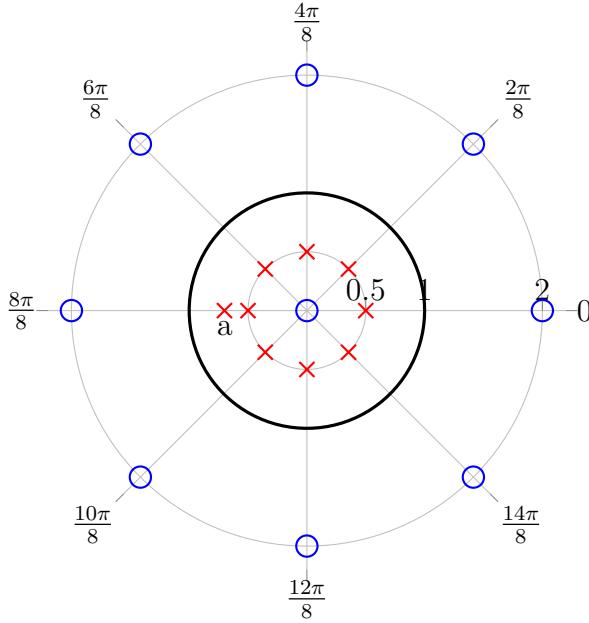
$$\begin{aligned} H(s) &= \frac{100}{s^2 + 10s + 100} \\ &= \frac{100}{(s + 5 + 5\sqrt{3}j)(s + 5 - 5\sqrt{3}j)} \end{aligned}$$

which has two poles at  $s = -5 \pm 5\sqrt{3}j$ . Since the system is causal, the ROC is the right half plane from  $\text{Re}\{s\} > -5$ .

- (b) (10 points) Find the value of  $a$  that makes this system critically damped.

From the LCCDE,  $\omega_n = 10$  and  $2\zeta\omega_n = -100a$ . Therefore, for critically damped system ( $\zeta = 1$ ),  $a = -0.2$ .

5. (20 points) A pole-zero plot of a causal DT LTI system is shown below. The real-valued parameter  $a$  satisfies  $-1 < a < 0$ .



- (a) (10 points) The system's frequency response  $H(e^{j\Omega})$  at zero frequency is given by  $H(e^{j0}) = 2$ . Plot the magnitude response  $|H(e^{j\Omega})|$  in dB scale for the frequency range  $-\pi \leq \Omega \leq \pi$ . Also mark the maximum and minimum values of the magnitude response.

The evenly spaced poles ( $p_n$ ) and zeros ( $z_n$ ) satisfy the reciprocal relation:  $p_n = 1/z_n^*$ . Therefore, evenly spaced poles and zeros exhibits all-pass characteristic with unknown gain factor.

On the other hand, the pole at  $a$  and the zero at 0 yield the first-order response with unknown gain. Therefore, the total response of the system can be written as

$$H(z) = G \cdot \frac{1}{1 - az^{-1}} \cdot H_{all}(z) \quad (1)$$

where  $G$  represents the unknown (complex-valued) gain of the system, and the all-pass response  $H_{all}(z)$  satisfies  $|H_{all}(z)| = 1$ . The standard form of the all-pass response with unit gain is given by

$$H_{all}(z) = \prod_n \frac{z^{-1} - p_n^*}{1 - p_n z^{-1}}$$

At the zero frequency,  $z = e^{j\Omega} = 1$ . In addition, the poles and zeros of the given all-pass system are also symmetric with respect to the real axis. Accordingly, for any pole  $p_n$ , there will be a complex-conjugated pole  $p_n^*$  (for the poles on the real axis, the complex conjugation equals to the original pole itself). This results in poles and zeros cancelled out at the zero frequency such that

$$H_{all}(e^{j0}) = \prod_n \frac{1 - p_n^*}{1 - p_n} = 1 \quad (2)$$

Using this result and from the zero frequency response, we can determine the unknown gain

$G.$

$$\begin{aligned} H(e^{j0}) &= G \cdot \frac{1}{1-a} \cdot H_{all}(e^{j0}) \\ &= G \cdot \frac{1}{1-a} = 2 \\ \therefore G &= 2(1-a) \end{aligned}$$

Consequently, the magnitude response can be written as

$$|H(e^{j\Omega})| = 2(1-a) \cdot \left| \frac{1}{1-ae^{-j\Omega}} \right| \quad (3)$$

For negative  $a$ , the response shows the high-pass characteristic, which has a minimum  $2(1-a)/(1-a) = 2$  at  $\Omega = 0$  and maximum  $2(1-a)/(1+a)$  at  $\Omega = \pi$ .

- (b) (10 points) Express the initial value of the impulse response  $h[0]$  in terms of  $a$ .

From the initial value theorem,  $h[0] = \lim_{z \rightarrow \infty} H(z)$ .

As  $z \rightarrow \infty$ , its inverse  $z^{-1} \rightarrow 0$ . Under this condition, the system response becomes

$$\begin{aligned} \lim_{z \rightarrow \infty} H(z) &= \lim_{z \rightarrow \infty} 2(1-a) \frac{1}{1-az^{-1}} \prod_n \frac{z^{-1}-p_n^*}{1-p_n z^{-1}} \\ &= 2(1-a) \prod_n (-p_n^*) \end{aligned}$$

Since  $p_n = \frac{e^{j2\pi n/8}}{2}$ ,  $\prod_{n=0}^7 (-p_n^*) = -\frac{1}{2^8} = -\frac{1}{256}$ .

$$\therefore h[0] = \frac{a-1}{128}$$