

## HW#2 Solution

**E3.2** A robot-arm drive system for one joint can be represented by the differential equation [8]

$$\frac{dv(t)}{dt} = -k_1 v(t) - k_2 y(t) + k_3 i(t),$$

where  $v(t)$  = velocity,  $y(t)$  = position, and  $i(t)$  is the control-motor current. Put the equations in state variable form and set up the matrix form for  $k_1 = k_2 = 1$ .

**(Ans)**

By the relation between velocity and position, we can get the below equation

$$\frac{dy}{dt} = v,$$

and the given statement

$$\frac{dv}{dt} = -k_1 v(t) - k_2 y(t) + k_3 i(t)$$

can be written in matrix form as

$$\frac{d}{dt} \begin{pmatrix} y \\ v \end{pmatrix} = \begin{bmatrix} 0 & 1 \\ -k_2 & -k_1 \end{bmatrix} \begin{pmatrix} y \\ v \end{pmatrix} + \begin{bmatrix} 0 \\ k_3 \end{bmatrix} i.$$

If we let  $u = i$ ,  $k_1 = k_2 = 1$ , for the state variable form,

$$\dot{\mathbf{x}} = \mathbf{Ax} + \mathbf{Bu}$$

we can get the coefficients as follows:

$$\mathbf{A} = \begin{bmatrix} 0 & 1 \\ -1 & -1 \end{bmatrix}, \quad \mathbf{B} = \begin{bmatrix} 0 \\ k_3 \end{bmatrix}, \quad \text{and } \mathbf{x} = \begin{pmatrix} y \\ v \end{pmatrix}.$$

**E3.4** Obtain a state variable matrix for a system with a differential equation

$$\frac{d^3y(t)}{dt^3} + 4\frac{d^2y(t)}{dt^2} + 6\frac{dy(t)}{dt} + 8y(t) = 20u(t).$$

**(Ans)**

If we define the state vector  $\mathbf{x}$  as

$$\mathbf{x} = [x_1 \ x_2 \ x_3]^T, \text{ where } x_1 = y(t), x_2 = y(t)', x_3 = y(t)'',$$

then we can get the differential equation as follows:

$$x_3' = -8x_1 - 6x_2 - 4x_3 + 20u(t).$$

Now, you can obtain the state variable matrix as follows:

$$\dot{\mathbf{x}} = \mathbf{Ax} + \mathbf{Bu}$$

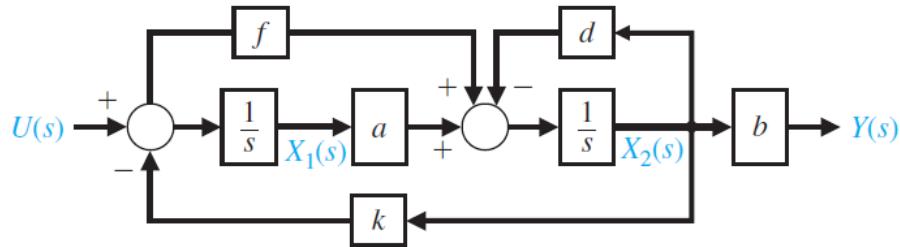
$$y = \mathbf{Cx}$$

where

$$\mathbf{A} = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -8 & -6 & -4 \end{bmatrix}, \quad \mathbf{B} = \begin{bmatrix} 0 \\ 0 \\ 20 \end{bmatrix}, \quad \mathbf{C} = [1 \ 0 \ 0].$$

**E3.5** A system is represented by a block diagram as shown in Figure E3.5. Write the state equations in the form

$$\begin{aligned}\dot{\mathbf{x}}(t) &= \mathbf{A}\mathbf{x}(t) + \mathbf{B}u(t) \\ y(t) &= \mathbf{C}\mathbf{x}(t) + \mathbf{D}u(t)\end{aligned}$$



**FIGURE E3.5** Block diagram.

**(Ans)**

From the block diagram we determine that the state equations are

$$\begin{aligned}\dot{x}_2 &= -(fk + d)x_2 + ax_1 + fu \\ \dot{x}_1 &= -kx_2 + u\end{aligned}$$

and the output equation is

$$y = bx_2.$$

Define a state vector  $\mathbf{x}$  like

$$\mathbf{x} = [x_1 \quad x_2]^T$$

then you can derive the state equations in a matrix form as follows:

$$\begin{aligned}\dot{\mathbf{x}} &= \mathbf{Ax} + \mathbf{Bu} \\ y &= \mathbf{Cx} + \mathbf{Du}\end{aligned}$$

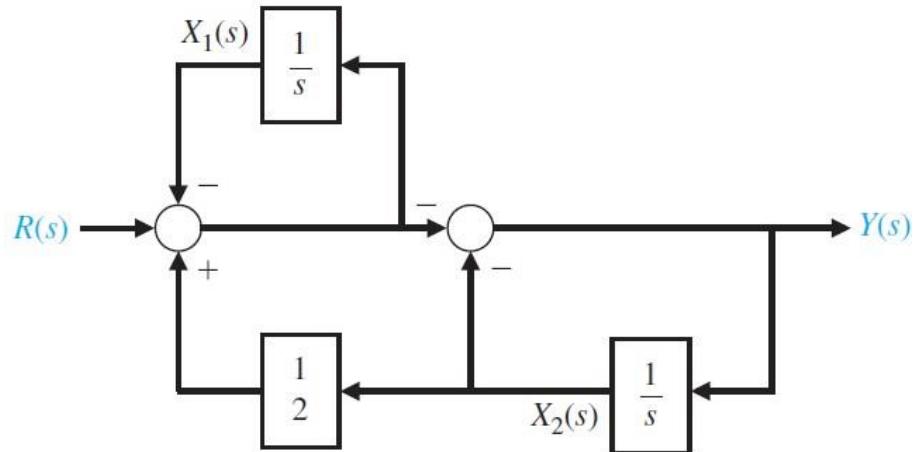
where

$$\mathbf{A} = \begin{bmatrix} 0 & -k \\ a & -(fk + d) \end{bmatrix}, \quad \mathbf{B} = \begin{bmatrix} 1 \\ f \end{bmatrix}, \quad \mathbf{C} = [0 \quad b], \quad \mathbf{D} = [0].$$

**E3.9** A multi-loop block diagram is shown in Figure E3.9.

The state variables are denoted by  $x_1(t)$  and  $x_2(t)$ .

(a) Determine a state variable representation of the closed-loop system where the output is denoted by  $y(t)$  and the input is  $r(t)$ . (b) Determine the characteristic equation.



**FIGURE E3.9** Multi-loop feedback control system.

**(Ans)**

Analyzing the block diagram yields

$$\begin{aligned}\dot{x}_1 &= -x_1 + \frac{1}{2}x_2 + r \\ \dot{x}_2 &= x_1 - \frac{3}{2}x_2 - r \\ y &= x_1 - \frac{3}{2}x_2 - r.\end{aligned}$$

Define a state vector  $\mathbf{x}$  like

$$\mathbf{x} = [x_1 \quad x_2]^T.$$

In a state-variable form, we have

$$\dot{\mathbf{x}} = \begin{bmatrix} -1 & \frac{1}{2} \\ 1 & -\frac{3}{2} \end{bmatrix} \mathbf{x} + \begin{bmatrix} 1 \\ -1 \end{bmatrix} r, \quad y = \begin{bmatrix} 1 & -\frac{3}{2} \end{bmatrix} \mathbf{x} - r.$$

The characteristic equation is obtained from  $\det[s\mathbf{I} - \mathbf{A}]$  as follows:

$$s^2 + \frac{5}{2}s + 1 = (s + 2)\left(s + \frac{1}{2}\right) = 0.$$

**E3.11** Determine a state variable representation for the system described by the transfer function

$$T(s) = \frac{Y(s)}{R(s)} = \frac{4(s + 3)}{(s + 2)(s + 6)}.$$

**(Ans)**

Case 1: Phase variable canonical form

The transfer function is

$$T(s) = \frac{4s + 12}{s^2 + 8s + 12}.$$

A state variable representation is

$$\begin{aligned}\dot{\mathbf{x}} &= \mathbf{Ax} + \mathbf{Br} \\ y &= \mathbf{Cx}\end{aligned}$$

where

$$\mathbf{A} = \begin{bmatrix} 0 & 1 \\ -12 & -8 \end{bmatrix}, \quad \mathbf{B} = \begin{bmatrix} 0 \\ 1 \end{bmatrix}, \quad \mathbf{C} = [12 \quad 4].$$

**(Another answer)**

Case 2: Input feedforward canonical form

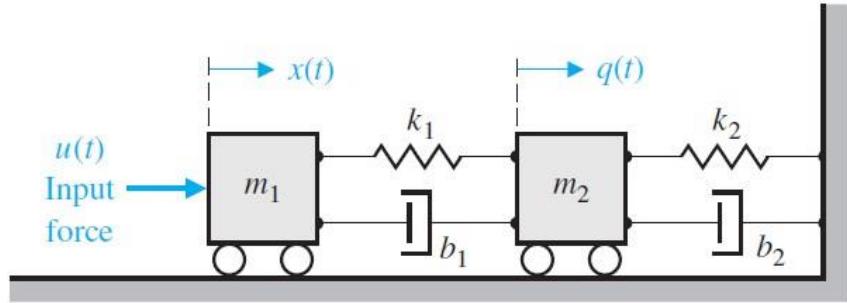
$$\mathbf{A} = \begin{bmatrix} -8 & 1 \\ -12 & 0 \end{bmatrix}, \quad \mathbf{B} = \begin{bmatrix} 4 \\ 12 \end{bmatrix}, \quad \mathbf{C} = [1 \quad 0].$$

**(Another answer)**

Case 3: Diagonal canonical form

$$\mathbf{A} = \begin{bmatrix} -2 & 0 \\ 0 & -6 \end{bmatrix}, \quad \mathbf{B} = \begin{bmatrix} 1 \\ 1 \end{bmatrix}, \quad \mathbf{C} = [1 \quad 3].$$

**E3.16** Two carts with negligible rolling friction are connected as shown in Figure E3.16. An input force is  $u(t)$ . The output is the position of cart 2, that is,  $y(t) = q(t)$ . Determine a state space representation of the system.



**FIGURE E3.16** Two carts with negligible rolling friction.

(Ans)

The governing equations of motion are

$$\begin{aligned} m_1 \ddot{x} + k_1(x - q) + b_1(\dot{x} - \dot{q}) &= u(t) \\ m_2 \ddot{q} + k_2 q + b_2 \dot{q} + b_1(\dot{q} - \dot{x}) + k_1(q - x) &= 0. \end{aligned}$$

Let  $x_1 = x$ ,  $x_2 = \dot{x}$ ,  $x_3 = q$  and  $x_4 = \dot{q}$ . Then,

$$\dot{\mathbf{x}} = \begin{bmatrix} 0 & 1 & 0 & 0 \\ -\frac{k_1}{m_1} & -\frac{b_1}{m_1} & \frac{k_1}{m_1} & \frac{b_1}{m_1} \\ 0 & 0 & 0 & 1 \\ \frac{k_1}{m_2} & \frac{b_1}{m_2} & -\frac{k_1 + k_2}{m_2} & -\frac{b_1 + b_2}{m_2} \end{bmatrix} \mathbf{x} + \begin{bmatrix} 0 \\ 1 \\ \frac{1}{m_1} \\ 0 \end{bmatrix} u(t).$$

Since the output is  $y(t) = q(t)$ , then

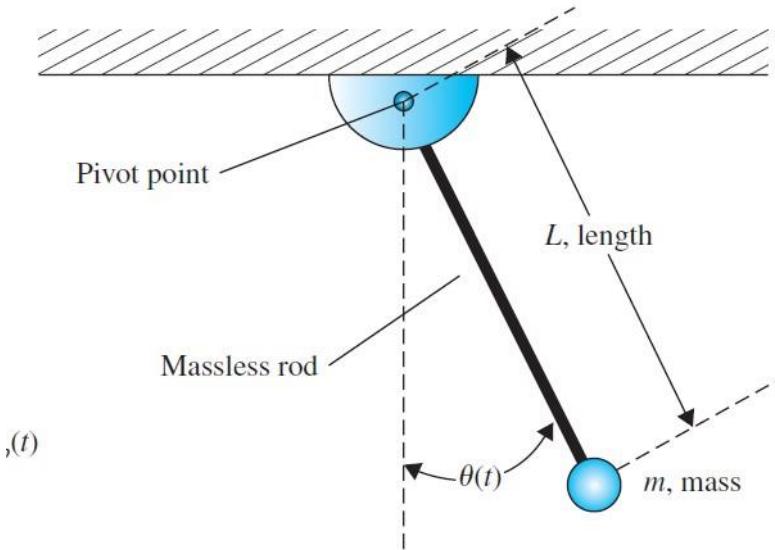
$$y = [0 \quad 0 \quad 1 \quad 0] \mathbf{x}.$$

**E3.20** For the simple pendulum shown in Figure E3.20, the nonlinear equations of motion are given by

$$\ddot{\theta}(t) + \frac{g}{L} \sin \theta(t) + \frac{k}{m} \dot{\theta}(t) = 0,$$

where  $g$  is gravity,  $L$  is the length of the pendulum,  $m$  is the mass attached at the end of the pendulum (assume the rod is massless), and  $k$  is the coefficient of friction at the pivot point.

- (a) Linearize the equations of motion about the equilibrium condition  $\theta_0 = 0^\circ$ .
- (b) Obtain a state variable representation of the system. The system output is the angle  $\theta(t)$ .



**FIGURE E3.20** Simple pendulum.

**(Ans)**

- (a) The linearized equation can be derived from the observation that  $\sin \theta \approx \theta$  when  $\theta \approx 0$ . In this case, the linearized equation is

$$\ddot{\theta}(t) + \frac{k}{m} \dot{\theta}(t) + \frac{g}{L} \theta(t) = 0.$$

- (b) Let the state variable  $\mathbf{x} = \begin{bmatrix} \theta \\ \dot{\theta} \end{bmatrix}$  and system output  $y = \theta$ . Then, the system in state variable form can be represented as

$$\begin{aligned}\dot{\mathbf{x}} &= \mathbf{Ax} \\ y &= \mathbf{Cx}\end{aligned}$$

where

$$\mathbf{A} = \begin{bmatrix} 0 & 1 \\ -\frac{g}{L} & -\frac{k}{m} \end{bmatrix}, \quad \mathbf{C} = [1 \quad 0], \text{ and } \mathbf{x}(0) = \begin{bmatrix} \theta(0) \\ \dot{\theta}(0) \end{bmatrix}.$$

**E3.23** Consider a system modeled via the third-order differential equation

$$\begin{aligned}\ddot{x}(t) + 3\dot{x}(t) + 3x(t) \\ = \ddot{u}(t) + 2\dot{u}(t) + 4u(t).\end{aligned}$$

Develop a state variable representation and obtain a block diagram of the system assuming the output is  $x(t)$  and the input is  $u(t)$ .

**(Ans)**

By applying Laplace Transform, the given differential equation can be expressed as follows:

$$\begin{aligned}(s^3 + 3s^2 + 3s + 1)X(s) &= (s^3 + 2s^2 + 4s + 1)U(s) \\ \rightarrow \frac{X(s)}{U(s)} &= \frac{s^3 + 2s^2 + 4s + 1}{s^3 + 3s^2 + 3s + 1}.\end{aligned}$$

To obtain a block diagram of the system, we can develop the equation as follows:

$$\frac{X(s)}{U(s)} = \frac{s^3 + 2s^2 + 4s + 1}{s^3 + 3s^2 + 3s + 1} \cdot \frac{Z_1(s)}{Z_1(s)}$$

where

$$z_1(t): \text{a new state variable}, Z_1(s) = \mathcal{L}\{z_1(t)\}.$$

Then, we can derive the following equations:

$$\begin{aligned}X(s) &= (s^3 + 2s^2 + 4s + 1)Z_1(s) \\ \rightarrow x(t) &= \ddot{z}_1(t) + 2\dot{z}_1(t) + 4z_1(t) + z_1(t) \quad (8.1)\end{aligned}$$

$$\begin{aligned}U(s) &= (s^3 + 3s^2 + 3s + 1)Z_1(s) \\ \rightarrow u(t) &= \ddot{z}_1(t) + 3\dot{z}_1(t) + 3z_1(t) + z_1(t). \quad (8.2)\end{aligned}$$

Putting (8.2) into (8.1), we get

$$\begin{aligned}\ddot{z}_1(t) &= -3\dot{z}_1(t) - 3z_1(t) - z_1(t) + u(t) \\ x(t) &= -\ddot{z}_1(t) + \dot{z}_1(t) + u(t)\end{aligned}$$

And define a state variable  $\mathbf{z}$

$$\mathbf{z} = \begin{bmatrix} z_1 \\ z_2 \\ z_3 \end{bmatrix} \text{ and } z_2(t) = \dot{z}_1(t), z_3(t) = \dot{z}_2(t) = \ddot{z}_1(t)$$

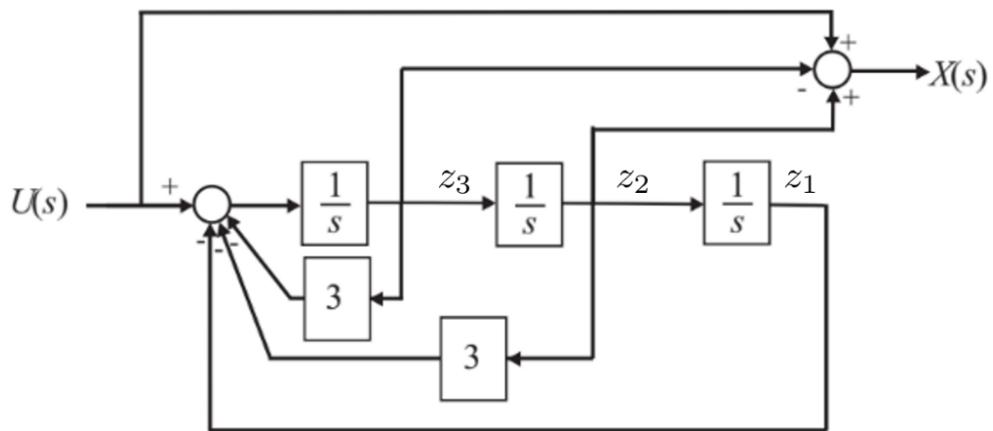
Then, the system in state variable form and block diagram can be represented as

$$\dot{\mathbf{z}} = \mathbf{Az} + \mathbf{Bu}$$

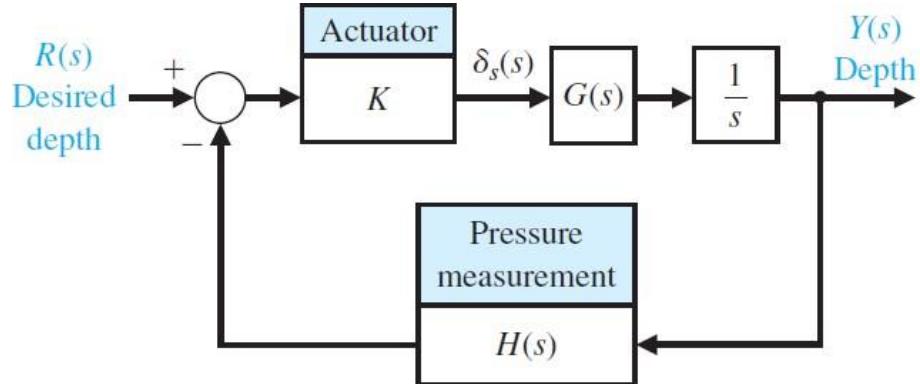
$$x = \mathbf{Cz} + \mathbf{Du}$$

where

$$\mathbf{A} = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -1 & -3 & -3 \end{bmatrix}, \quad \mathbf{B} = \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix}, \quad \mathbf{C} = [0 \quad 1 \quad -1], \quad \mathbf{D} = [1].$$



- P3.7** An automatic depth-control system for a robot submarine is shown in Figure P3.7. The depth is measured



**FIGURE P3.7** Submarine depth control.

by a pressure transducer. The gain of the stern plane actuator is  $K = 1$  when the vertical velocity is 25 m/s. The submarine has the transfer function

$$G(s) = \frac{(s + 1)^2}{s^2 + 1},$$

and the feedback transducer is  $H(s) = 2s + 1$ . Determine a state variable representation for the system.

**(Ans)**

Given  $K = 1$ , we have

$$KG(s) \cdot \frac{1}{s} = \frac{(s + 1)^2}{s(s^2 + 1)}.$$

And from the given block diagram, the transfer function can be represented as follows:

$$\frac{Y(s)}{R(s)} = T(s) = \frac{kG(s)}{s + H(s) \cdot kG(s)}.$$

We then compute the closed-loop transfer function as

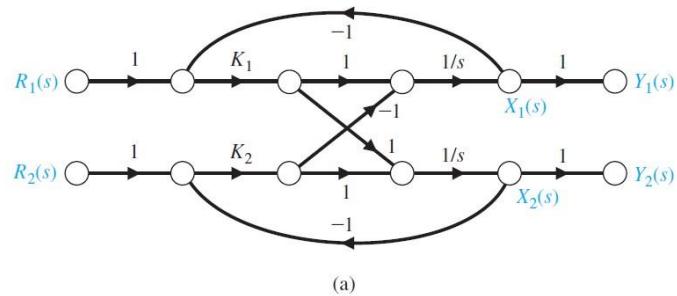
$$T(s) = \frac{s^2 + 2s + 1}{3s^3 + 5s^2 + 5s + 1} = \frac{\frac{1}{3}s^2 + \frac{2}{3}s + \frac{1}{3}}{s^3 + \frac{5}{3}s^2 + \frac{5}{3}s + \frac{1}{3}}.$$

By defining a state vector  $\mathbf{x}$ , the state variable model is

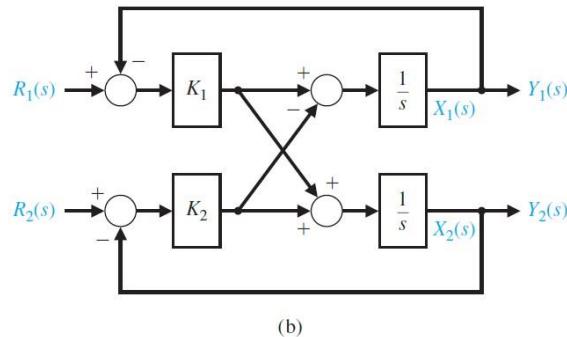
$$\begin{aligned}\dot{\mathbf{x}} &= \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -1/3 & -5/3 & -5/3 \end{bmatrix} \mathbf{x} + \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} r \\ y &= \begin{bmatrix} 1 & 2 & 1 \end{bmatrix} \mathbf{x},\end{aligned}$$

where  $\mathbf{x} = [x_1 \quad x_2 \quad x_3]^T$  and  $x_1 = x(t)$ ,  $x_2 = x(t)'$ ,  $x_3 = x(t)''$ .

**P3.10** Many control systems must operate in two dimensions, for example, the  $x$ - and the  $y$ -axes. A two-axis control system is shown in Figure P3.10, where a set of state variables is identified. The gain of each axis is  $K_1$  and  $K_2$ , respectively. (a) Obtain the state differential equation. (b) Find the characteristic equation from the  $\mathbf{A}$  matrix. (c) Determine the state transition matrix for  $K_1 = 1$  and  $K_2 = 2$ .



(a)



(b)

**FIGURE P3.10**  
Two-axis system.  
(a) Signal-flow graph.  
(b) Block diagram model.

**(Ans)**

(a) From the signal flow diagram, we determine that a state-space model is given by

$$\begin{aligned}\dot{\mathbf{x}} &= \begin{bmatrix} -K_1 & K_2 \\ -K_1 & -K_2 \end{bmatrix} \mathbf{x} + \begin{bmatrix} K_1 & -K_2 \\ K_1 & K_2 \end{bmatrix} \begin{bmatrix} r_1 \\ r_2 \end{bmatrix} \\ \mathbf{y} &= \begin{bmatrix} y_1 \\ y_2 \end{bmatrix} = \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} \mathbf{x}.\end{aligned}$$

(b) The characteristic equation is

$$\det[s\mathbf{I} - \mathbf{A}] = s^2 + (K_2 + K_1)s + 2K_1K_2 = 0,$$

$$\text{where } \mathbf{A} = \begin{bmatrix} -K_1 & K_2 \\ -K_1 & -K_2 \end{bmatrix}.$$

(c) When  $K_1 = 1$  and  $K_2 = 2$ ,

$$\mathbf{A} = \begin{bmatrix} -1 & 2 \\ -1 & -2 \end{bmatrix}.$$

The state transition matrix associated with  $\mathbf{A}$  in  $s$ -domain is

$$\Phi(s) = [s\mathbf{I} - \mathbf{A}]^{-1} = \frac{1}{(s + \frac{3}{2})^2 + (\frac{\sqrt{7}}{2})^2} \begin{bmatrix} s + 2 & 1 \\ -2 & s + 1 \end{bmatrix}.$$

Then, the state transition matrix is finally derived as follows:

$$\begin{aligned} \phi(t) &= \mathcal{L}^{-1}\{[s\mathbf{I} - \mathbf{A}]^{-1}\} \\ &= e^{-\frac{3}{2}t} \begin{bmatrix} \cos(\alpha t) + \frac{1}{2\alpha} \sin(\alpha t) & \frac{2}{\alpha} \sin(\alpha t) \\ -\frac{1}{\alpha} \sin(\alpha t) & \cos(\alpha t) - \frac{1}{2\alpha} \sin(\alpha t) \end{bmatrix}, \text{ where } \alpha = \frac{\sqrt{7}}{2}. \end{aligned}$$