

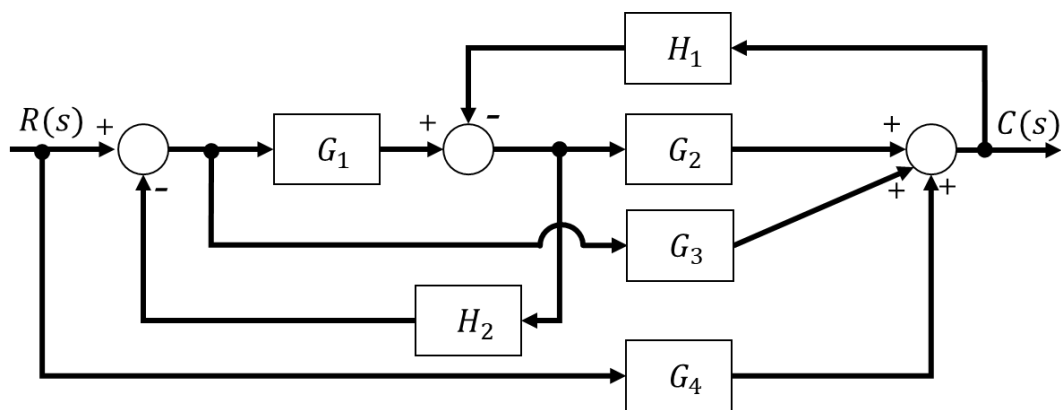
# EE381 Control System Engineering

## Mid-term Exam. (Apr. 22, 2021)

Score ( \_\_\_\_\_ )

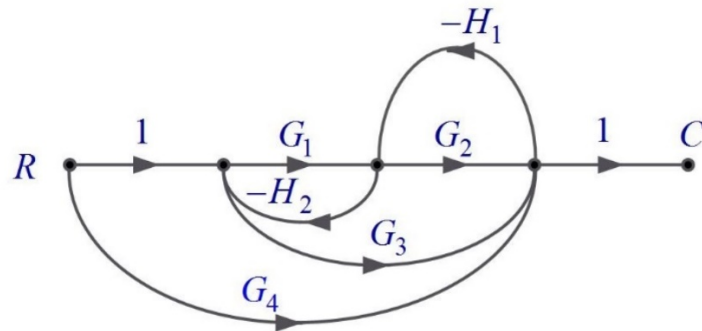
Student ID: \_\_\_\_\_ Name: \_\_\_\_\_

1. For the following block diagram,
  - (a) Draw the corresponding signal flow graph. (5 points)
  - (b) Find the transfer function  $C(s)/R(s)$  using Mason's formula. (15 points)



(Ans)

- (a) The corresponding signal flow graph can be drawn as follows:



- (b) There are three forward paths from  $R$  to  $C$  and three loops, with gains

$$\begin{aligned}
 P_1 &= G_1 G_2 \\
 P_2 &= G_3 \\
 P_3 &= G_4 \\
 L_1 &= -G_1 H_2 \\
 L_2 &= -G_2 H_1 \\
 L_3 &= G_3 H_1 H_2
 \end{aligned}$$

All three loops touch, so  $\Delta$  is 1 minus sum of the loop gains

$$\Delta = 1 - (-G_1 H_2 - G_2 H_1 + G_3 H_1 H_2)$$

$$= 1 + G_1H_2 + G_2H_1 - G_3H_1H_2$$

If all forward paths and **all loops touch each other**, it may be seen that the cofactors are all unity.

In this problem, the forward paths  $P_1$  and  $P_2$  touch all three loops so the corresponding cofactors  $\Delta_1$  and  $\Delta_2$  are unity. However, loop  $L_1$  does not touch path  $P_3$  so,

$$\Delta_3 = 1 + G_1H_2$$

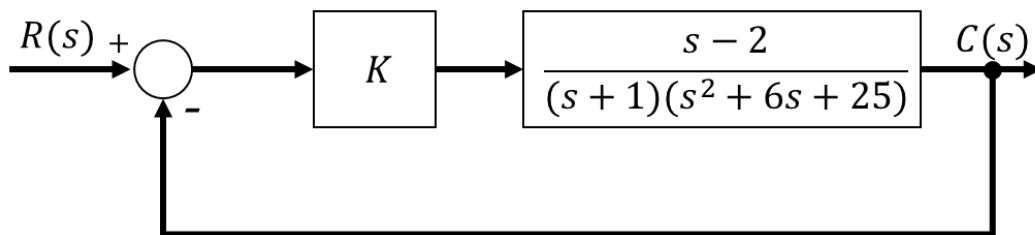
Substituting values from above all three steps into the gain formula yields the closed loop transfer function as follows:

$$T = \frac{P_1\Delta_1 + P_2\Delta_2 + P_3\Delta_3}{\Delta}$$

So,

$$T = \frac{G_1G_2 + G_3 + G_4(1 + G_1H_2)}{1 + G_1H_2 + G_2H_1 - G_3H_1H_2}$$

2. Consider the closed-loop system shown in the following figure. Determine the range of  $K$  for stability. Assume that  $K > 0$ . (20 points)



(Ans)

The closed transfer function  $C(s)/R(s)$  is

$$\frac{C(s)}{R(s)} = \frac{K(s-2)}{(s+1)(s^2+6s+25) + K(s-2)} = \frac{K(s-2)}{s^3 + 7s^2 + (K+31)s + 25 - 2K}$$

For stability, the denominator of this last equation must be a stable polynomial. For the characteristic equation

$$q(s) = s^3 + 7s^2 + (K+31)s + 25 - 2K = 0$$

the Routh array becomes as follows:

$s^3$	1	$31 + K$
$s^2$	7	$25 - 2K$
$s^1$	$\frac{192 + 9K}{7}$	0
$s^0$	$25 - 2K$	

Since  $K$  is assumed to be positive, for stability, we require

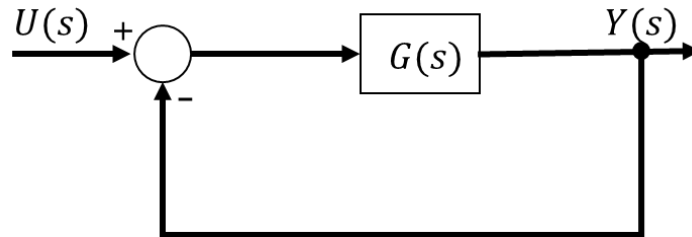
$$0 < K < 12.5.$$

3. In the system below, we have

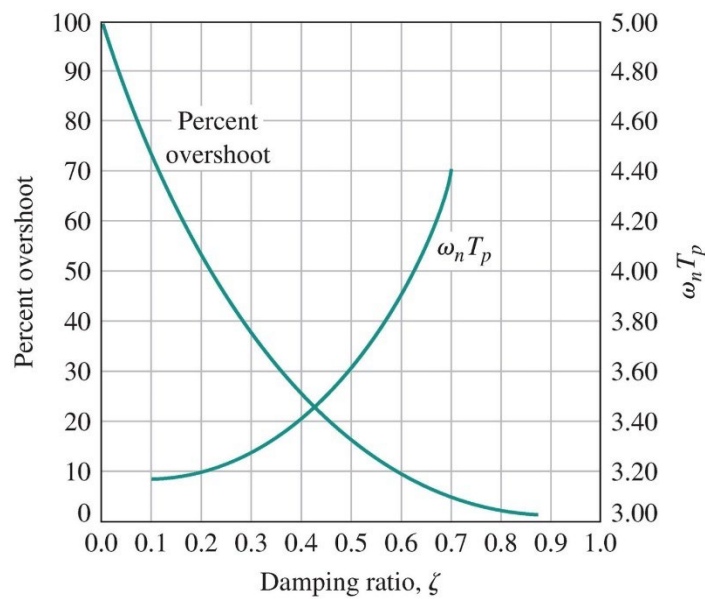
$$G(s) = \frac{K}{s(s+2)}$$

where  $K > 0$ .

- (a) What value of  $K$  should we choose so that the step response of the closed-loop system has a percent overshoot of 5%? (5 points)
- (b) What is the corresponding settling time (2% criterion) for this  $K$ ? (10 points)



Please use the following graph regarding damping ratio vs. percent overshoot.



(Ans)

The closed-loop system has the transfer function

$$T(s) = \frac{G(s)}{1 + G(s)} = \frac{K}{s^2 + 2s + K}$$

which is a standard second order system with the undamped natural frequency  $\omega_n = \sqrt{K}$  and the damping ratio  $\zeta = 1/\sqrt{K}$ .

To have P.O. of 5%, we need  $\zeta = 0.7$  from the figure. From  $\frac{1}{\sqrt{K}} = 0.7$ , we have  $K = 2$ .

For this particular  $K$ , the settling time is  $T_s = \frac{4}{\zeta\omega_n} = \frac{4}{1} = 4$  s.

4. Consider two systems given by the following transfer functions:

$$H_1(s) = \frac{80}{(s+10)(s^2+4s+8)}, \quad H_2(s) = \frac{37}{(s+1)(s^2+12s+37)}$$

Suppose the unit step input is given. For each of the above two systems,

- (a) Estimate the settling time (2% criterion) of the step response. Use  $\ln(50) \approx 4$ .  
(10 points)  
(b) Find the final value  $y(\infty)$  without computing the output  $y(t)$  explicitly. (5 points)

(Ans)

(a)

$H_1(s)$  has three poles:  $p_1 = -10, p_{2,3} = -2 \pm j2$ , where  $p_{2,3}$  are dominant poles. Thus, its step response can be approximated by a second order system

$$H_1(s) \approx \frac{8}{(s^2 + 4s + 8)}$$

with the damping ratio  $\zeta = 1/\sqrt{2}$  and  $\omega_n = 2\sqrt{2}$ . Thus,  $T_s \approx \frac{4}{\zeta\omega_n} = \frac{4}{2} = 2$  s.

$H_2(s)$  has three poles:  $p_1 = -1, p_{2,3} = -6 \pm j1$ , where  $p_1$  is the dominant pole. Thus, its step response can be approximated by a first order system

$$H_2(s) \approx \frac{1}{s+1}$$

with the time constant  $T = 1$ . Thus,  $T_s \approx 4T = 4$  s.

The step response is

$$Y(s) = \frac{1}{s(s+1)} = \frac{1}{s} - \frac{1}{s+1} \rightarrow y(t) = 1 - e^{-t}.$$

The settling time  $T_s$  should satisfy  $e^{-T_s} = 0.02$ . Then  $T_s = -\ln(0.02) = \ln(50) = 4$  s.

(b) Both systems are stable; hence  $y(\infty)$  exists and is given by (by the final value theorem)

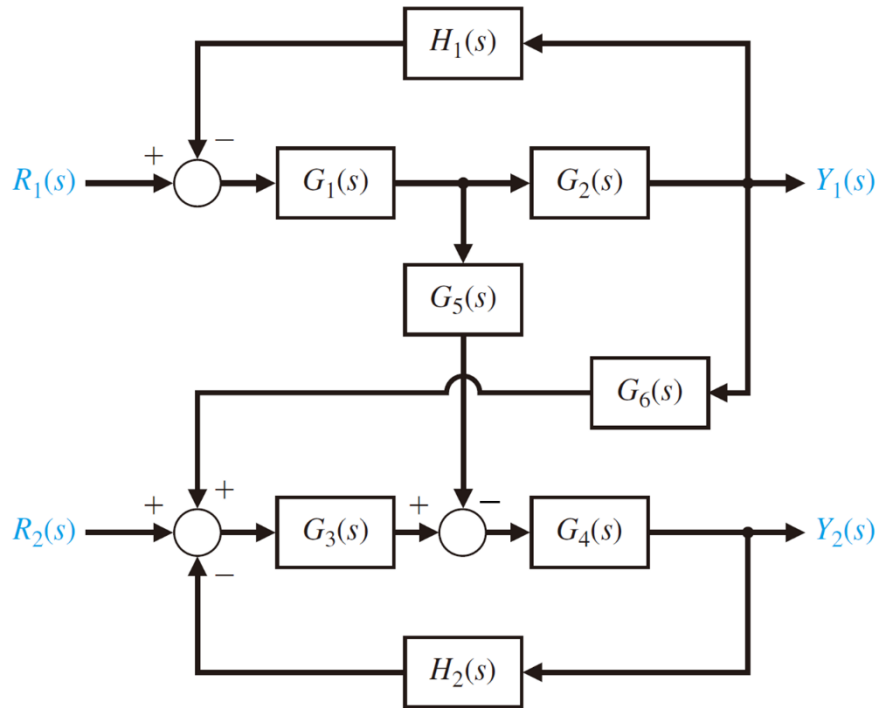
$$\text{For system } H_1(s): \lim_{t \rightarrow \infty} y_1(t) = \lim_{s \rightarrow 0} sY_1(s) = 1$$

$$\text{For system } H_2(s): \lim_{t \rightarrow \infty} y_2(t) = \lim_{s \rightarrow 0} sY_2(s) = 1$$

5. A system has a block diagram as shown in the figure below.

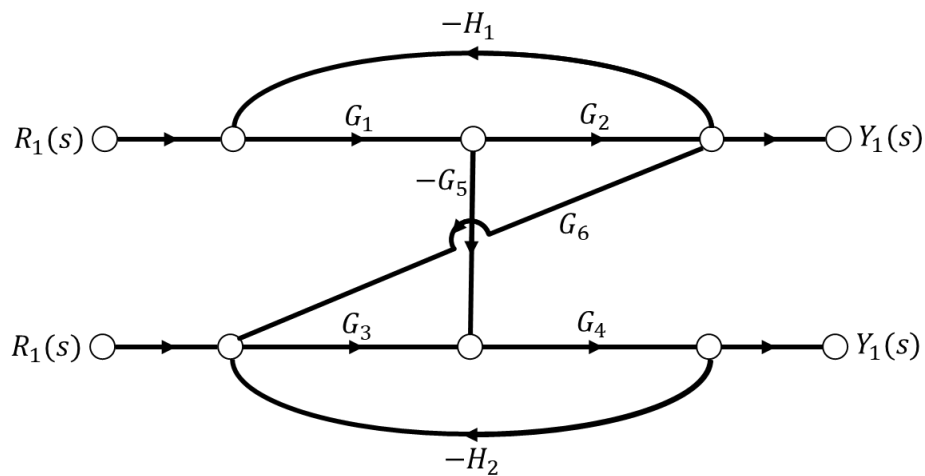
(a) Determine the transfer function  $T_{12}(s) = Y_2(s)/R_1(s)$ . (10 points)

(b) It is desired to decouple  $Y_2(s)$  from  $R_1(s)$ . Select  $G_5(s)$  in terms of the other  $G_i(s)$  to achieve decoupling. (5 points)



(Ans)

(a) The signal flow graph can be drawn as follows:



There are two forward paths from  $R_1(s)$  to  $Y_2(s)$ :

$$P_1: -G_1G_5G_4$$

$$P_2: G_1G_2G_6G_3G_4.$$

There are two loops:

$$L_1: -G_1G_2H_1$$

$$L_2: -G_3G_4H_2.$$

So, from the Mason's gain formula,

$$\begin{aligned}\Delta &= 1 - (L_1 + L_2) + (L_1L_2) = 1 - (-G_1G_2H_1 - G_3G_4H_2) + G_1G_2H_1G_3G_4H_2 \\ &= (1 + G_1G_2H_1)(1 + G_3G_4H_2)\end{aligned}$$

For  $P_1$  and  $P_2$ , there are no non-touching loops, so their gain is 1, i.e.,  $\Delta_1 = \Delta_2 = 1$ . Then, the closed-loop transfer function from  $R_1(s)$  to  $Y_2(s)$  is

$$\begin{aligned} T_{12}(s) &= \frac{Y_2(s)}{R_1(s)} = \frac{P_1\Delta_1 + P_2\Delta_2}{\Delta} = \frac{-G_1G_5G_4 \cdot 1 + G_1G_2G_6G_3G_4 \cdot 1}{\Delta} \\ &= \frac{-G_1G_5G_4 + G_1G_2G_6G_3G_4}{(1 + G_1G_2H_1)(1 + G_3G_4H_2)}. \end{aligned}$$

- (b) To decouple  $Y_2(s)$  from  $R_1(s)$ , the numerator of  $T_{12}(s)$  should be zero. Thus,  $G_5 = G_2G_3G_6$ .

6. Consider the state-space equation

$$\begin{aligned} \dot{\mathbf{x}}(t) &= \mathbf{A}\mathbf{x}(t) + \mathbf{b}u(t) = \begin{bmatrix} -2 & 5 \\ 0 & 3 \end{bmatrix} \mathbf{x}(t) + \begin{bmatrix} 4 \\ 0 \end{bmatrix} u(t) \\ y(t) &= \mathbf{c}\mathbf{x}(t) + du(t) = [7 \quad 8]\mathbf{x}(t) + 1.5u(t) \end{aligned}$$

- (a) When there is no input, i.e.,  $u(t) = 0$ , obtain the characteristic equation for the state  $\mathbf{x}(t)$  and discuss the stability of the state  $\mathbf{x}(t)$ . (5 points)  
 (b) Solve the overall system transfer function and discuss the BIBO stability of this system. (5 points)  
 (c) Is there a difference in stability between (a) and (b)? Discuss why. (5 points)

(Ans)

- (a)  $q(s) = (s + 2)(s - 3)$ . The pole locations are -2, +3. The system state is not stable since one pole is located on the righthand s-plane.

$$\begin{aligned} \text{(b) } (s\mathbf{I} - \mathbf{A})^{-1} &= \begin{bmatrix} s+2 & -5 \\ 0 & s-3 \end{bmatrix}^{-1} = \begin{bmatrix} \frac{1}{s+2} & \frac{5}{(s+2)(s-3)} \\ 0 & \frac{1}{s-3} \end{bmatrix} \\ T(s) &= \mathbf{c}(s\mathbf{I} - \mathbf{A})^{-1}\mathbf{b} + d = [7 \quad 8] \begin{bmatrix} \frac{1}{s+2} & \frac{5}{(s+2)(s-3)} \\ 0 & \frac{1}{s-3} \end{bmatrix} \begin{bmatrix} 4 \\ 0 \end{bmatrix} + 1.5 \\ &= [7 \quad 8] \begin{bmatrix} \frac{4}{s+2} \\ 0 \end{bmatrix} + 1.5 = \frac{1.5s + 31}{s + 2} \end{aligned}$$

There is only one pole at -2. So the system is BIBO stable.

- (c) The state itself is not stable due to the pole at +3. But the overall system is stable due to the unstable pole cancellation.