

Applied Computational Fluid Dynamics Using OpenFOAM

Value Added Course
College/University: AEC
Spring 2025



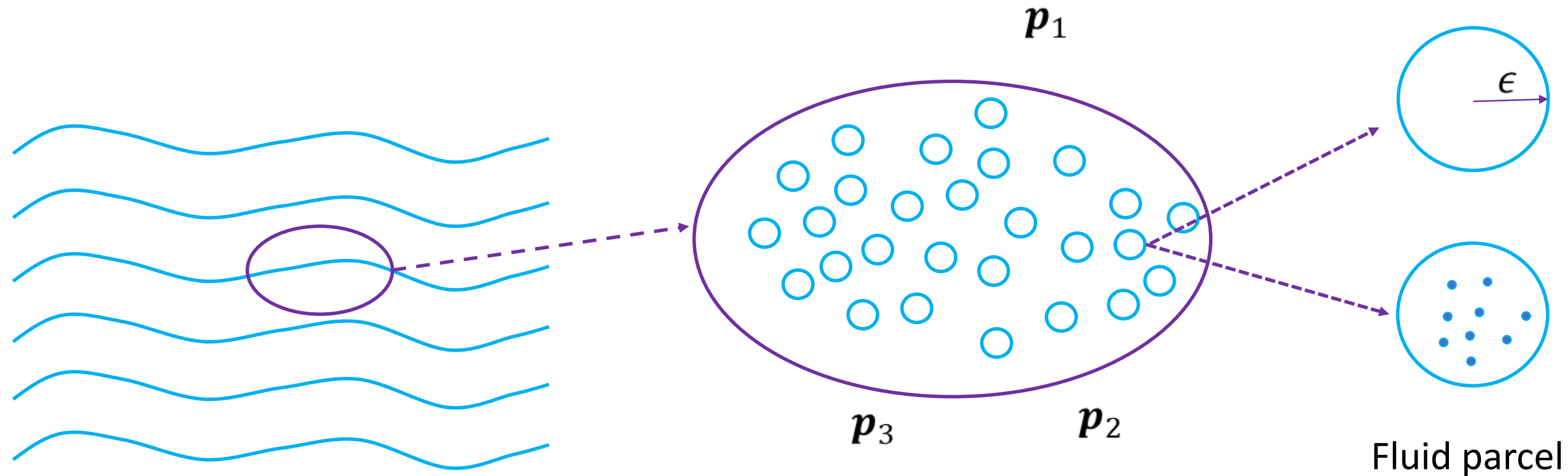
ExaSlate

Develop = Guide = Collab

Contents

- Governing Equations
- Gauss Divergence Theorem
- Reynolds Transport Theorem

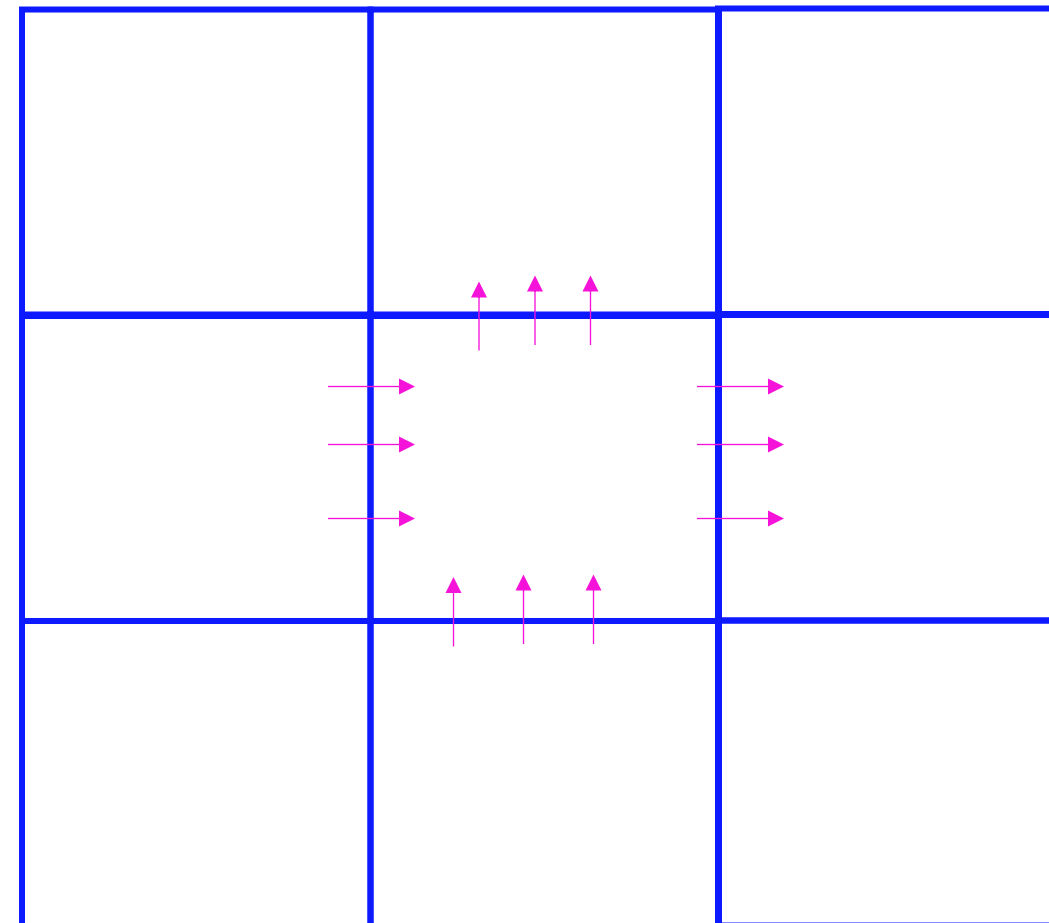
Lagrangian frame – discrete phase



- Follow a fluid parcel ($\mathbf{p}_1, \mathbf{p}_2, \dots$)
- Flow property at a location is obtained from the fluid parcel that happens to be at that location at that time
- Useful to derive conservation laws

Eulerian frame

- Conservation laws are applied around a fixed “**control volume**” in space
- Flux of quantities through the boundary is used to estimate the flow variables
- Useful to take observations at fixed locations



Governing Equations

- The general equation can be written in the form as:

$$\frac{\partial}{\partial t}(\rho\phi) + \nabla \cdot (\rho u \phi) = \nabla \cdot (\Gamma \nabla \phi) + S$$

$$\frac{\partial}{\partial t}(\rho\phi) + \frac{\partial}{\partial x_j}(\rho u_j \phi) = \frac{\partial}{\partial x_j} \left(\Gamma \frac{\partial \phi}{\partial x_j} \right) + S$$

$$\frac{\partial}{\partial t} \iiint \rho \phi dV + \iint \rho \phi (u \cdot dA) = \iint \Gamma \nabla \phi \cdot dA + \iiint S dV$$

1

2

3

4

1

Unsteady/Transient term

3

Diffusion term

2

Advection/Convection term

4

Source term

Governing Equations

$$\frac{\partial}{\partial t}(\rho\phi) + \nabla \cdot (\rho u \phi) = \nabla \cdot (\Gamma \nabla \phi) + S$$

Continuity equation: $\phi = 1, S = 0 \rightarrow \frac{\partial}{\partial t}(\rho) + \nabla \cdot (\rho u) = 0$

Momentum equation: $\phi = u, \Gamma = \mu, S = S_u \rightarrow \frac{\partial}{\partial t}(\rho u) + \nabla \cdot (\rho u u) = \nabla \cdot (\mu \nabla u) - \nabla p + S_u$

Energy equation: $\phi = h, \Gamma = k / C_p, S = S_h \rightarrow \frac{\partial}{\partial t}(\rho h) + \nabla \cdot (\rho u h) = \nabla \cdot \left(\frac{k}{C_p} \nabla h \right) + S_h$

Species equation: $\phi = h, \Gamma = \Gamma_l, S = S_m \rightarrow \frac{\partial}{\partial t}(\rho m_l) + \nabla \cdot (\rho u m_l) = \nabla \cdot (\Gamma_l \nabla m_l) + S_m$

Turbulence equation: $\phi = k(\text{or})\varepsilon, \Gamma = \Gamma_k(\text{or})\Gamma_\varepsilon, S = S_k(\text{or})S_\varepsilon \rightarrow \frac{\partial}{\partial t}(\rho k) + \nabla \cdot (\rho u k) = \nabla \cdot (\Gamma_k \nabla k) + S_k$

Ideal Gas equation: $p = \rho R T$

Integral Form – Differential Form

- Conservation of mass

$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \mathbf{u}) = 0$$

- Integrate over a control volume

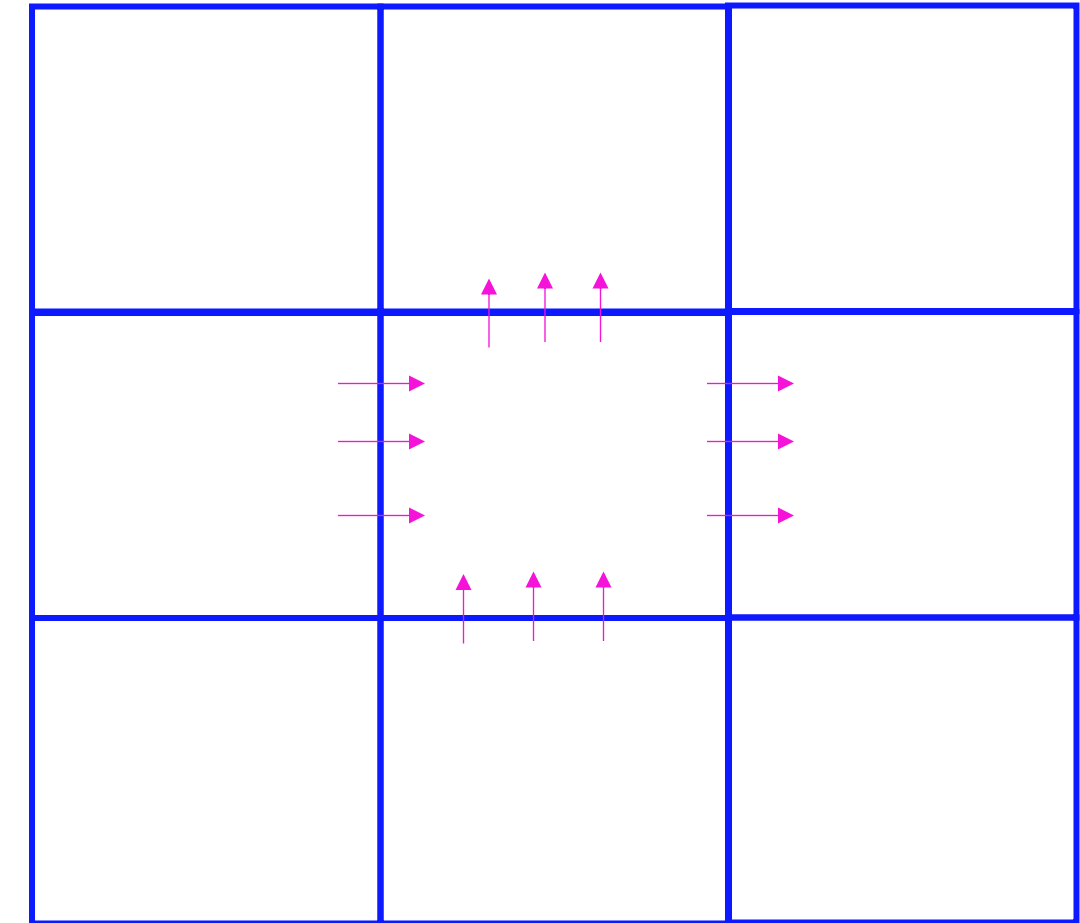
$$\int_V \left(\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \mathbf{u}) \right) dV = 0$$

$$\int_V \frac{\partial \rho}{\partial t} dV + \int_V \nabla \cdot (\rho \mathbf{u}) dV = 0$$

$$\frac{\partial}{\partial t} \int_V \rho dV + \oint_S \rho \mathbf{u} \cdot d\mathbf{S} = 0$$



Gauss – divergence theorem



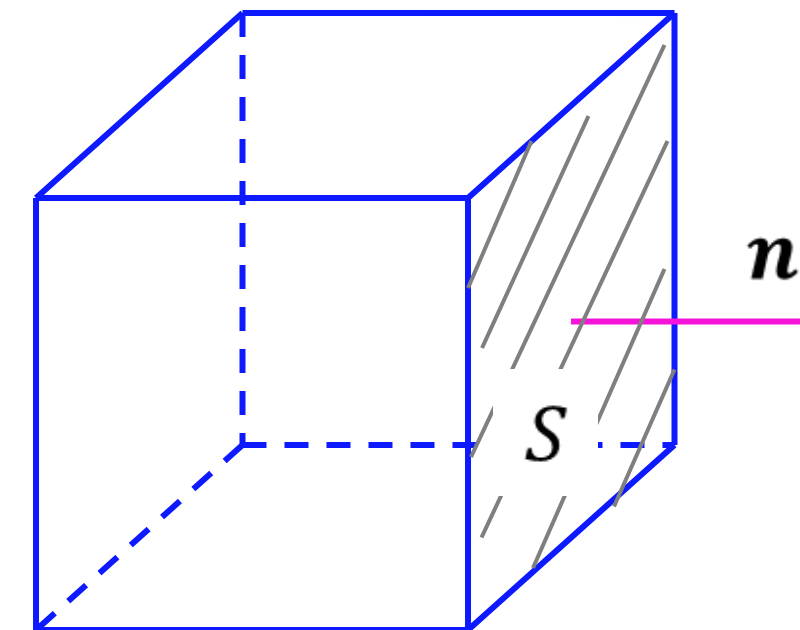
Gauss Divergence Theorem

- Surface Area Vector: \mathbf{S}

$$\mathbf{S} = |\mathbf{S}|\mathbf{n}$$

$$\mathbf{S} = S\mathbf{n}$$

- Extensive property: Φ
- Intensive property: ϕ
 - Conserved property calculated by mass
- Mass: $\rho V = \int_V \rho dV$

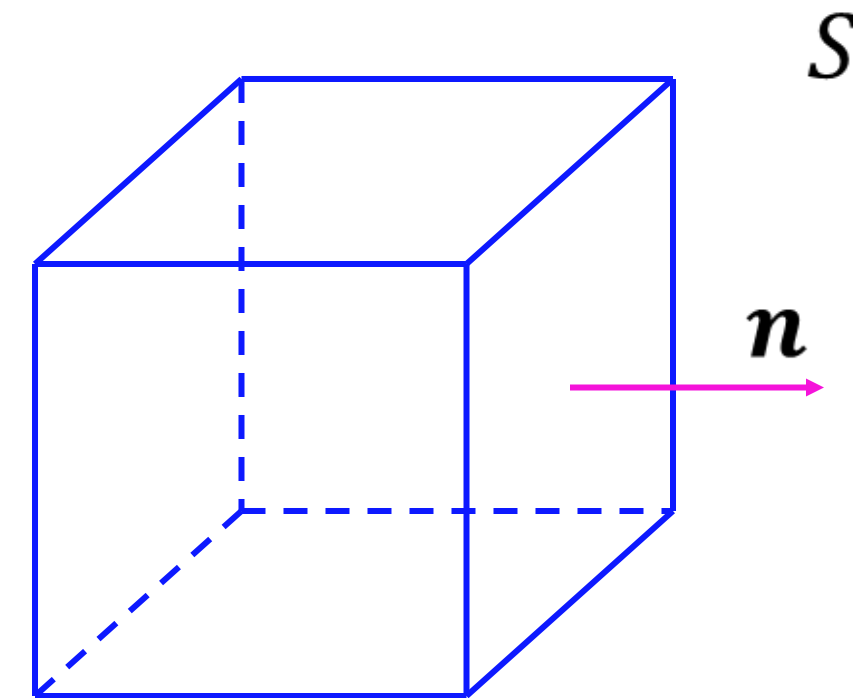


Gauss Divergence Theorem

- For a vector: \mathbf{F}

$$\int (\nabla \cdot \mathbf{F}) dV \approx \sum \mathbf{F} \cdot \mathbf{S}$$

- Rate of change of a quantity over a control volume = Rate of flow through control surface.



Gauss Divergence Theorem

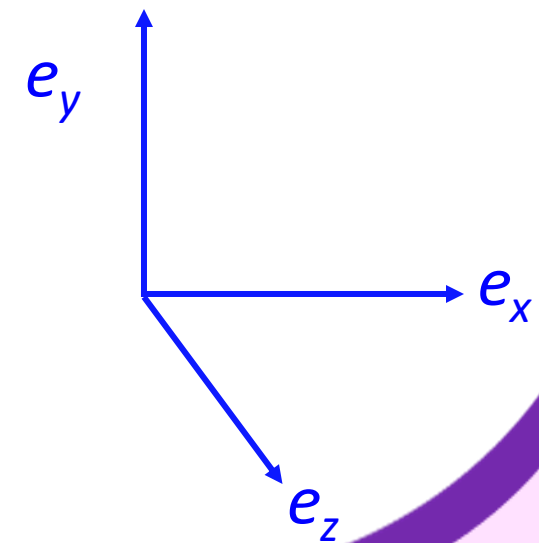
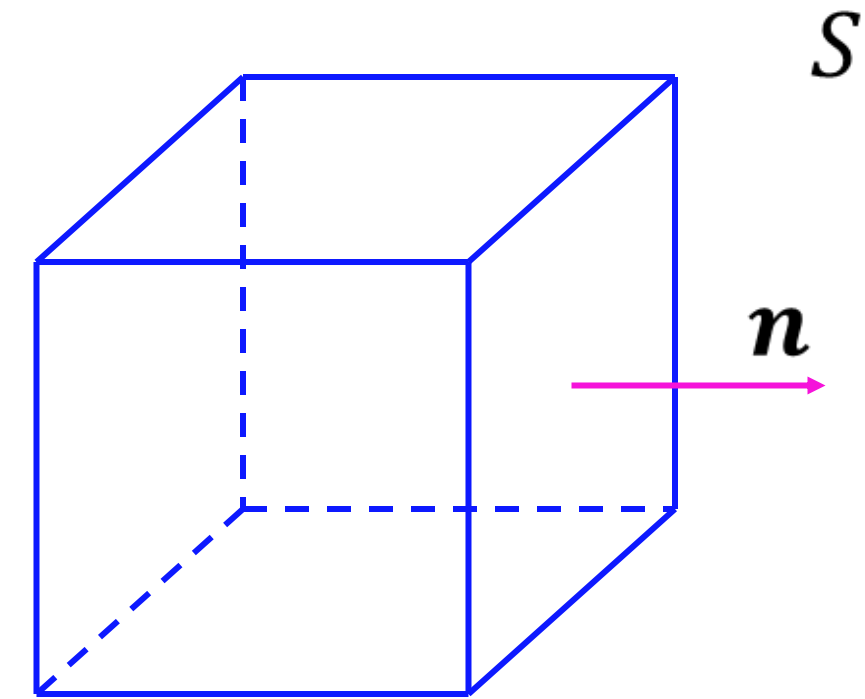
- For a vector: \mathbf{F}

$$\int (\nabla \cdot \mathbf{F}) dV \approx \sum \mathbf{F} \cdot \mathbf{s}$$

Let: $\mathbf{F} = x\mathbf{e}_x + y\mathbf{e}_y$

$$\int (\nabla \cdot \mathbf{F}) dV = \int \left(\frac{\partial}{\partial x} \mathbf{e}_x + \frac{\partial}{\partial y} \mathbf{e}_y \right) \cdot (x\mathbf{e}_x + y\mathbf{e}_y) dV$$

$$\nabla \cdot \mathbf{u} = \left(\frac{\partial}{\partial x} \mathbf{e}_x + \frac{\partial}{\partial y} \mathbf{e}_y + \frac{\partial}{\partial z} \mathbf{e}_z \right) (u\mathbf{e}_x + v\mathbf{e}_y + w\mathbf{e}_z) = \left(\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} \right)$$



Gauss Divergence Theorem

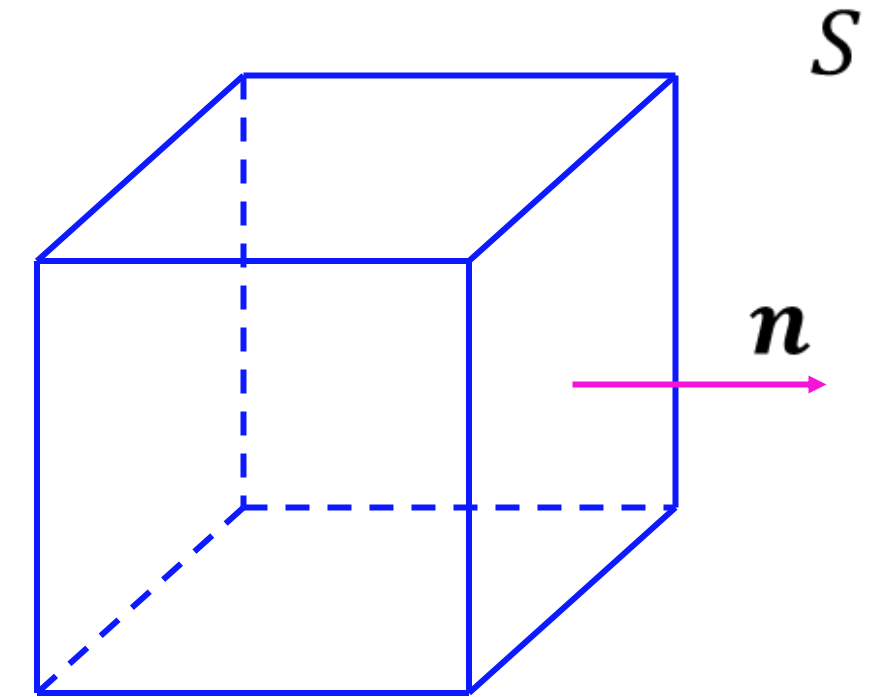
$$\int (\nabla \cdot \mathbf{F}) dV \approx \sum \mathbf{F} \cdot \mathbf{S}$$

Let: $\mathbf{F} = x\mathbf{e}_x + y\mathbf{e}_y$

$$\int (\nabla \cdot \mathbf{F}) dV = \int \left(\frac{\partial}{\partial x} \mathbf{e}_x + \frac{\partial}{\partial y} \mathbf{e}_y \right) \cdot (x\mathbf{e}_x + y\mathbf{e}_y) dV$$

$$= \int \left(\frac{\partial x}{\partial x} + \frac{\partial y}{\partial y} \right) dV = 2V$$

$$\sum \mathbf{F} \cdot \mathbf{S} = \sum (x\mathbf{e}_x + y\mathbf{e}_y) \cdot \mathbf{S}$$

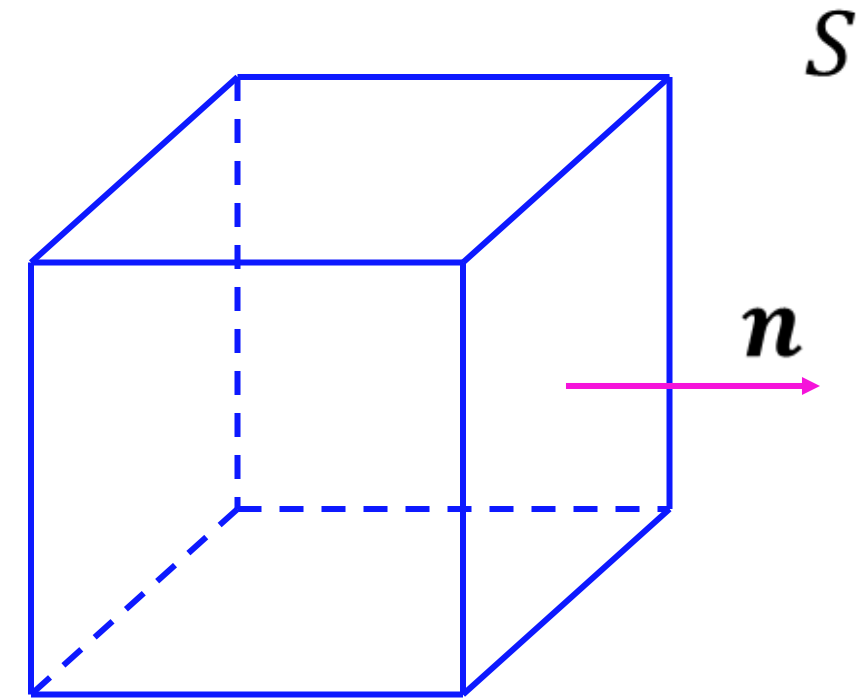


$$S = \Delta x \Delta y$$

$$V = \Delta x \Delta y \Delta z$$

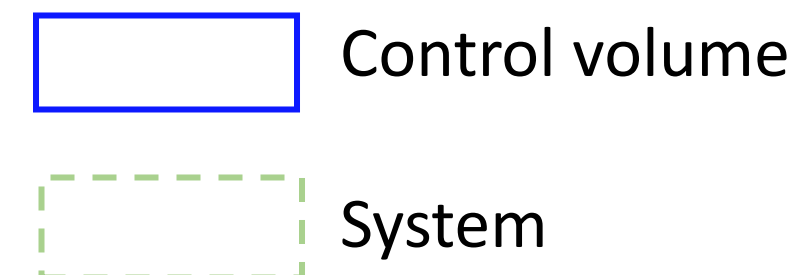
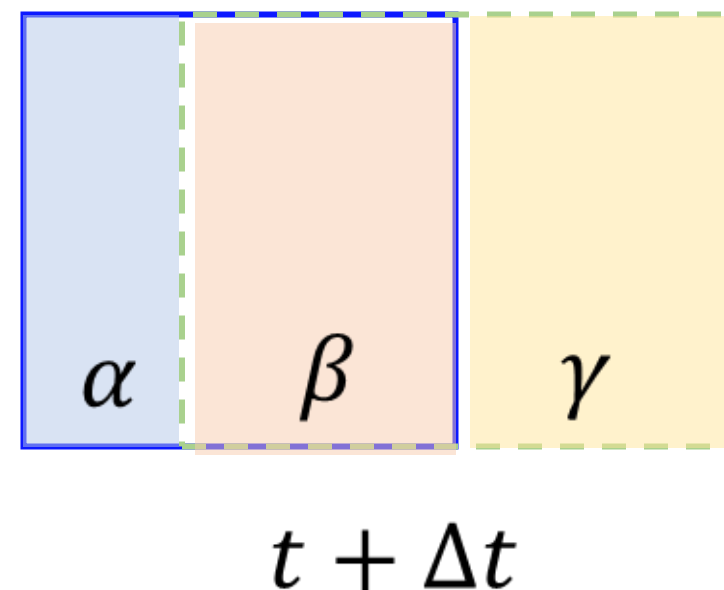
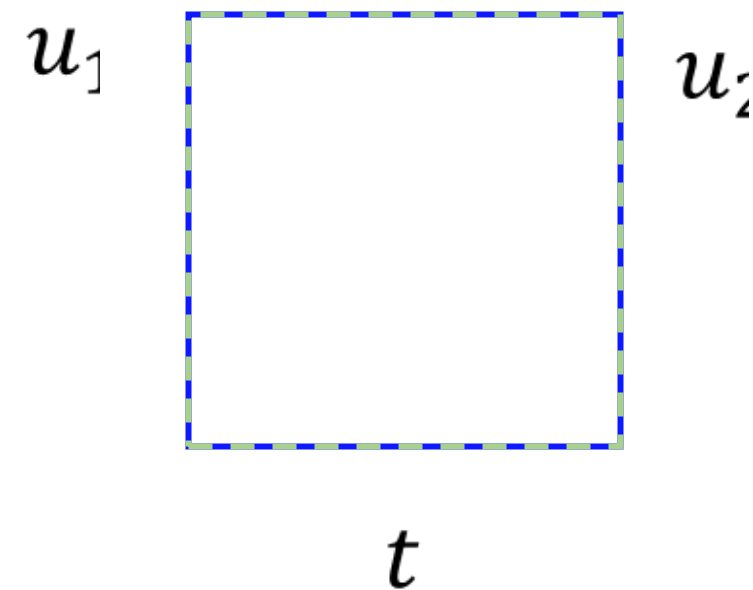
Reynolds Transport Theorem

$$\frac{d}{dt} \int_{V_S} \rho \phi dV = \frac{d}{dt} \int_{V_{CV}} \rho \phi dV + \int_S \rho \phi \mathbf{u} \cdot \mathbf{n} dS$$



Reynolds Transport Theorem

$$\frac{d}{dt} \int_{V_S} \rho \phi dV = \frac{d}{dt} \int_{V_{CV}} \rho \phi dV + \int_S \rho \phi \mathbf{u} \cdot \mathbf{n} dS$$



$$(1) \quad \Phi_S(t) = \Phi_{CV}(t)$$

$$(2) \quad \Phi_S(t + \Delta t) = \Phi_{CV}(t + \Delta t) - \Phi_\alpha + \Phi_\gamma$$

Reynolds Transport Theorem

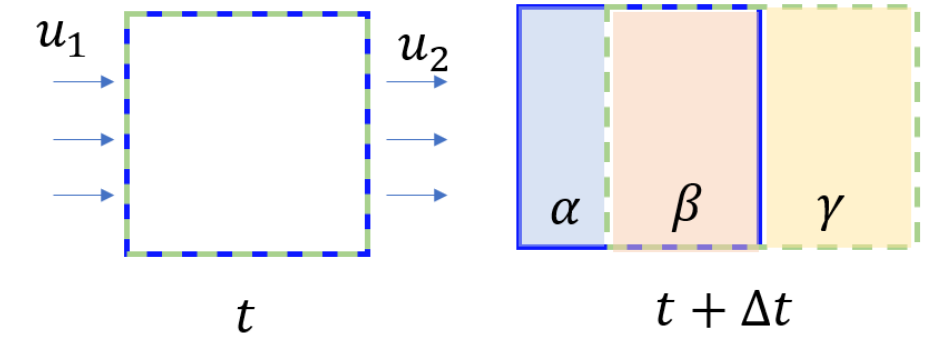
$$(1) \quad \Phi_S(t) = \Phi_{CV}(t)$$

$$(2) \quad \Phi_S(t + \Delta t) = \Phi_{CV}(t + \Delta t) - \Phi_\alpha + \Phi_\gamma$$

Subtract (1) from (2)

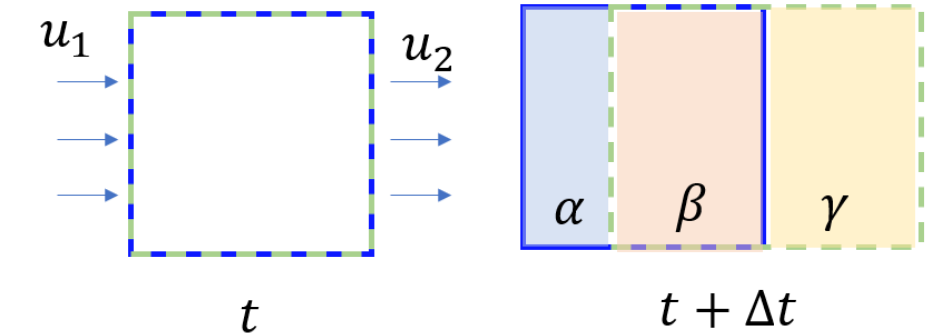
$$\left(\frac{\Phi(t + \Delta t) - \Phi(t)}{\Delta t} \right)_{System} = \left(\frac{\Phi(t + \Delta t) - \Phi(t)}{\Delta t} \right)_{CV} - \dot{\Phi}_\alpha + \dot{\Phi}_\gamma$$

$$\frac{d\Phi}{dt}_{System} = \frac{d\Phi}{dt}_{CV} - \dot{\Phi}_\alpha + \dot{\Phi}_\gamma$$



Reynolds Transport Theorem

$$\frac{d\Phi}{dt}_{system} = \frac{d\Phi}{dt}_{CV} - \dot{\Phi}_{\alpha} + \dot{\Phi}_{\gamma}$$



$$\Phi_{\alpha} = \phi_{\alpha} m_{\alpha} = \phi_{\alpha} \rho_{\alpha} V_{\alpha} = \phi_{\alpha} \rho_{\alpha} (u_1 \Delta t) S$$

Using $\Phi = \int \rho \phi dV$ and net flux as $\int \rho \phi \mathbf{u} \cdot \mathbf{n} dS$

$$\frac{d}{dt} \int_{V_S} \rho \phi dV = \frac{d}{dt} \int_{V_{CV}} \rho \phi dV + \int_S \rho \phi \mathbf{u} \cdot \mathbf{n} dS$$

Conservation Laws

- Conservation of mass

$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \mathbf{u}) = 0; \quad \nabla \cdot (\rho \mathbf{u}) = \frac{\partial(\rho u)}{\partial x} + \frac{\partial(\rho v)}{\partial y} + \frac{\partial(\rho w)}{\partial z}$$

$$\frac{d}{dt} \int_{V_S} \rho \phi dV = \frac{d}{dt} \int_{V_{CV}} \rho \phi dV + \int_S \rho \phi \mathbf{u} \cdot \mathbf{n} dS$$

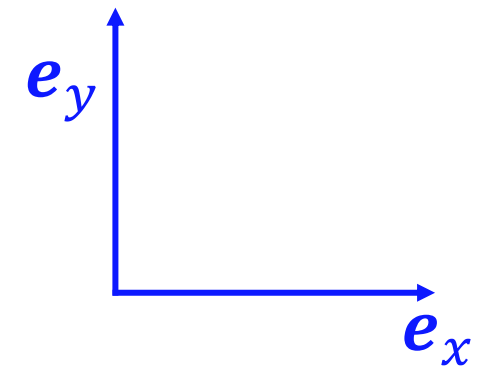
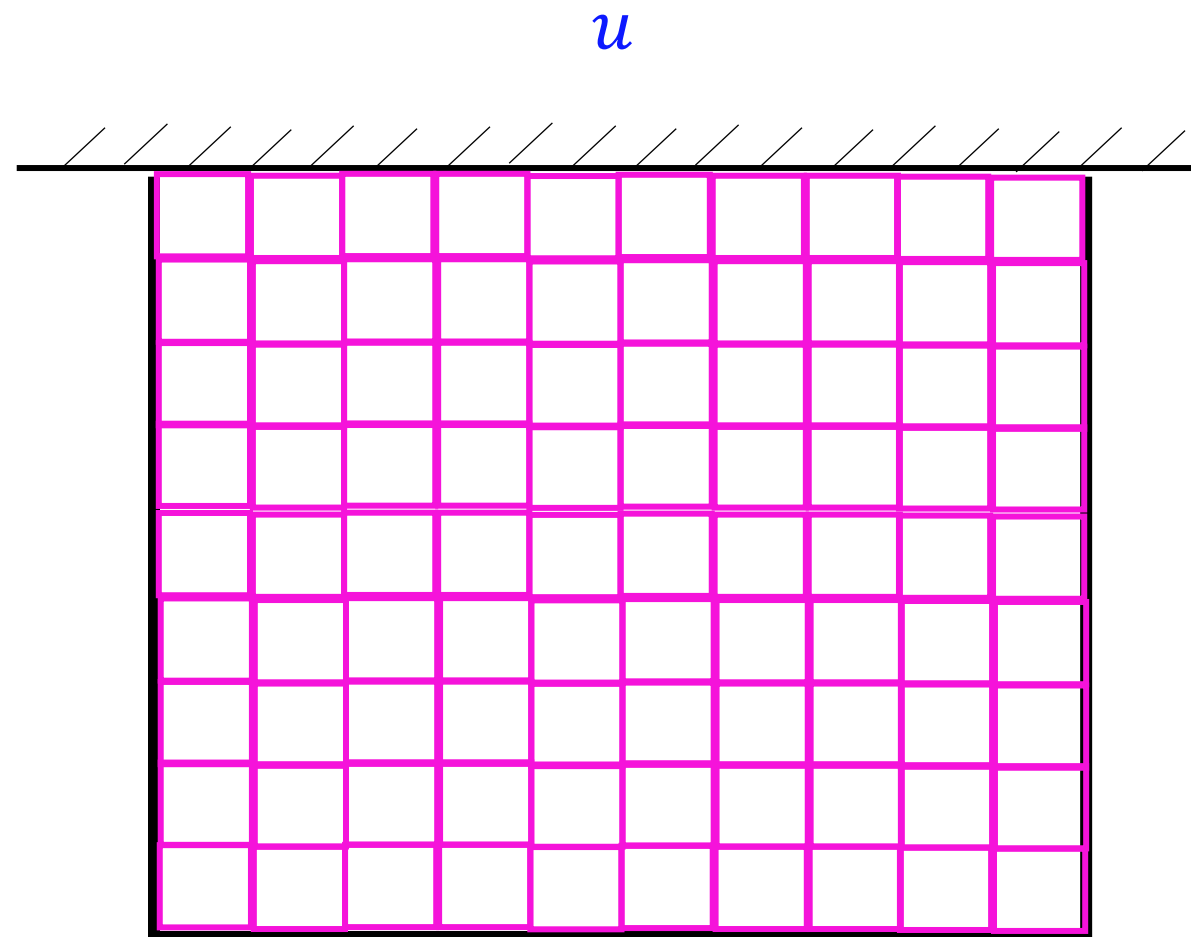
- Conservation of momentum

$$\frac{\partial \rho \mathbf{u}}{\partial t} + \nabla \cdot (\rho \mathbf{u} \mathbf{u}) = -\nabla p + \nabla \cdot \boldsymbol{\sigma} + \rho \mathbf{g};$$

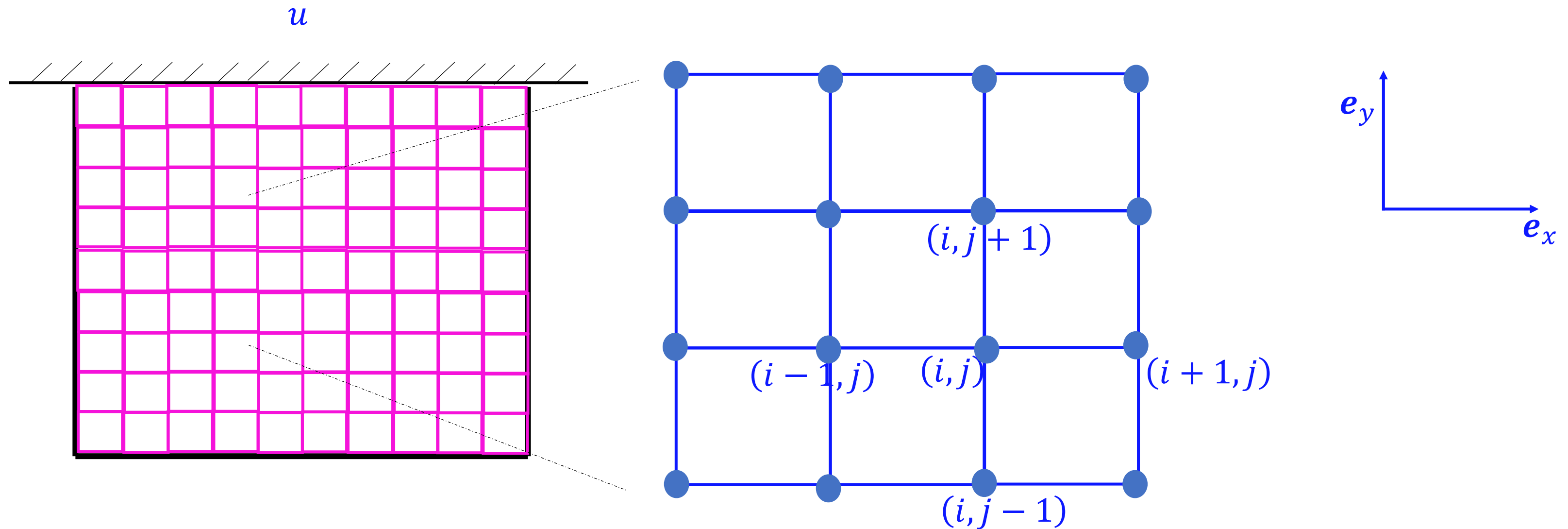
- Scalar conservation law

$$\frac{\partial \rho \phi}{\partial t} + \nabla \cdot (\rho \mathbf{u} \phi) = \nabla \cdot (\Gamma \nabla \phi) + S_\phi$$

Numerical Discretization (Grid layout)

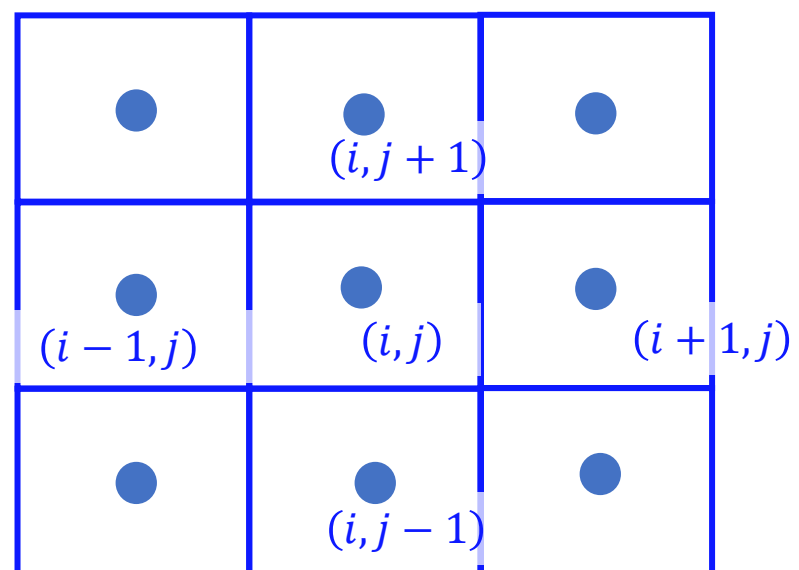
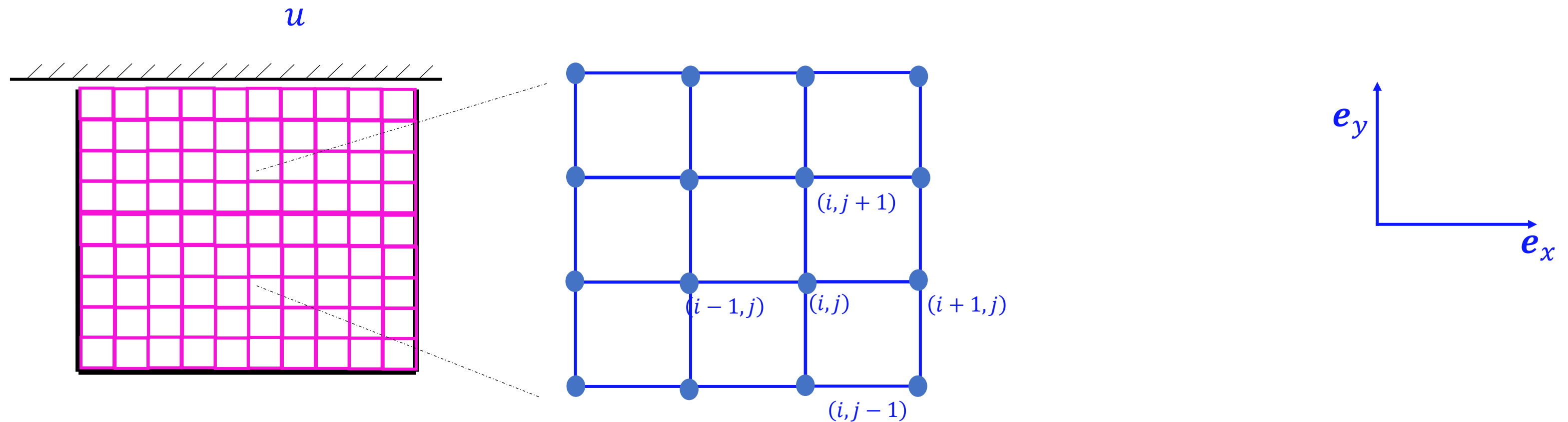


Numerical Discretization (Grid layout)



- Flow properties are assigned at each grid locations.

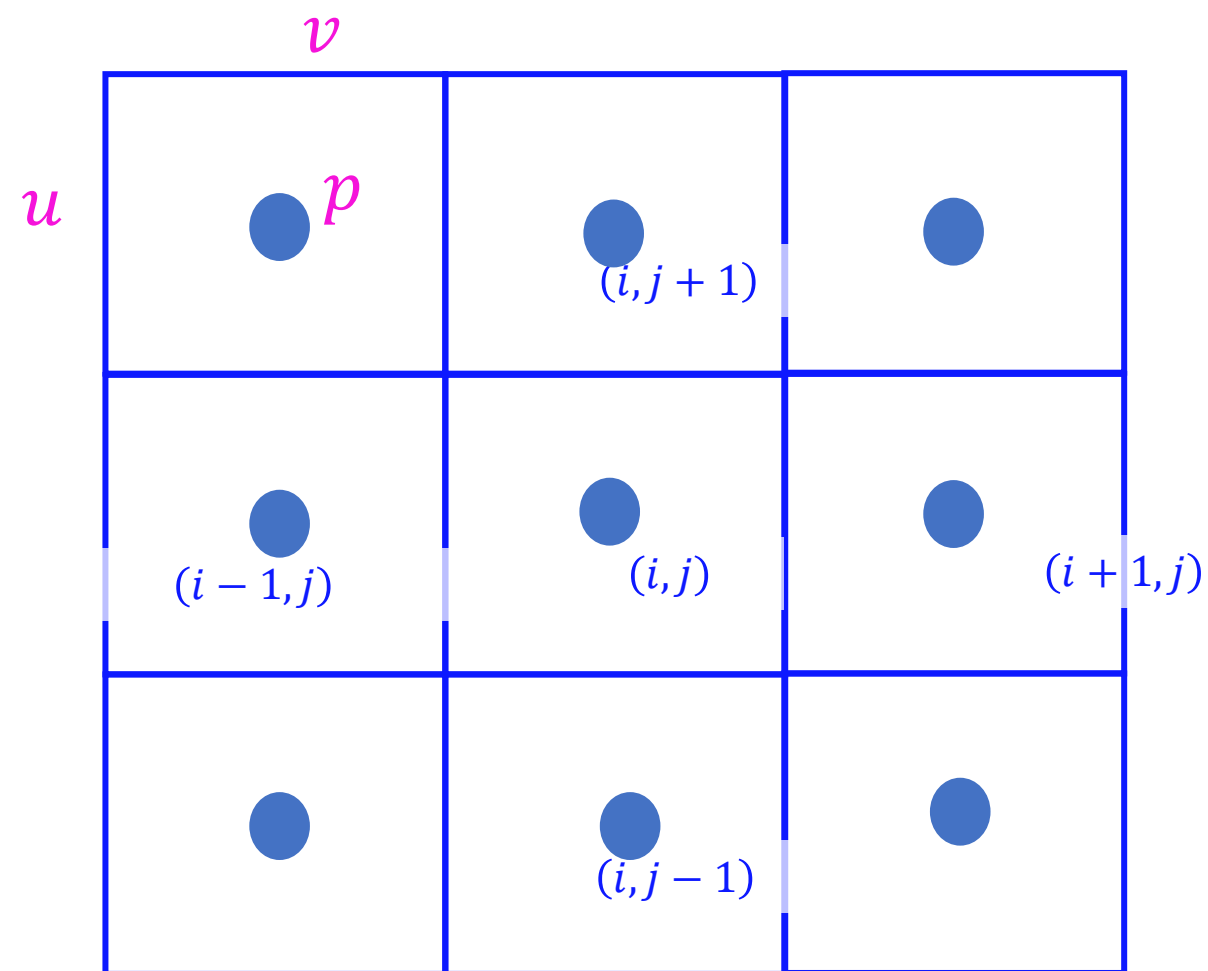
Numerical Discretization (Grid layout)



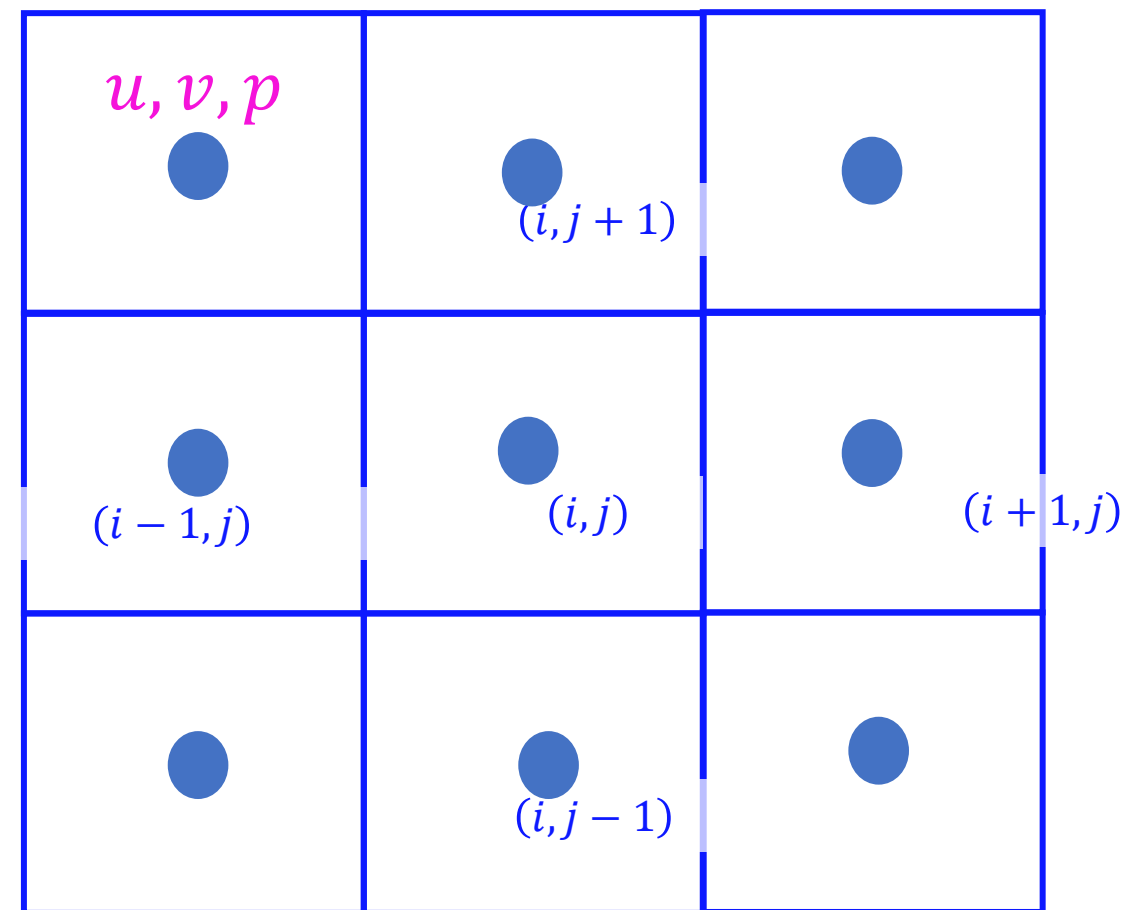
Cell centered representation

Numerical Discretization (Grid layout)

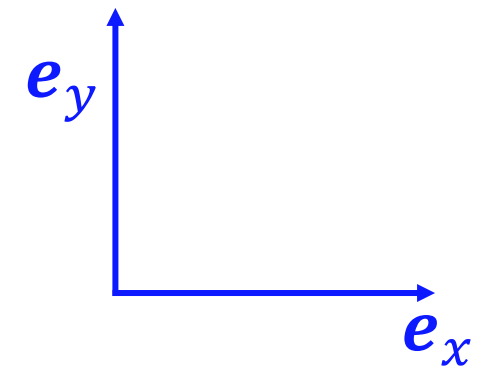
- Cell centered representation



Staggered grid



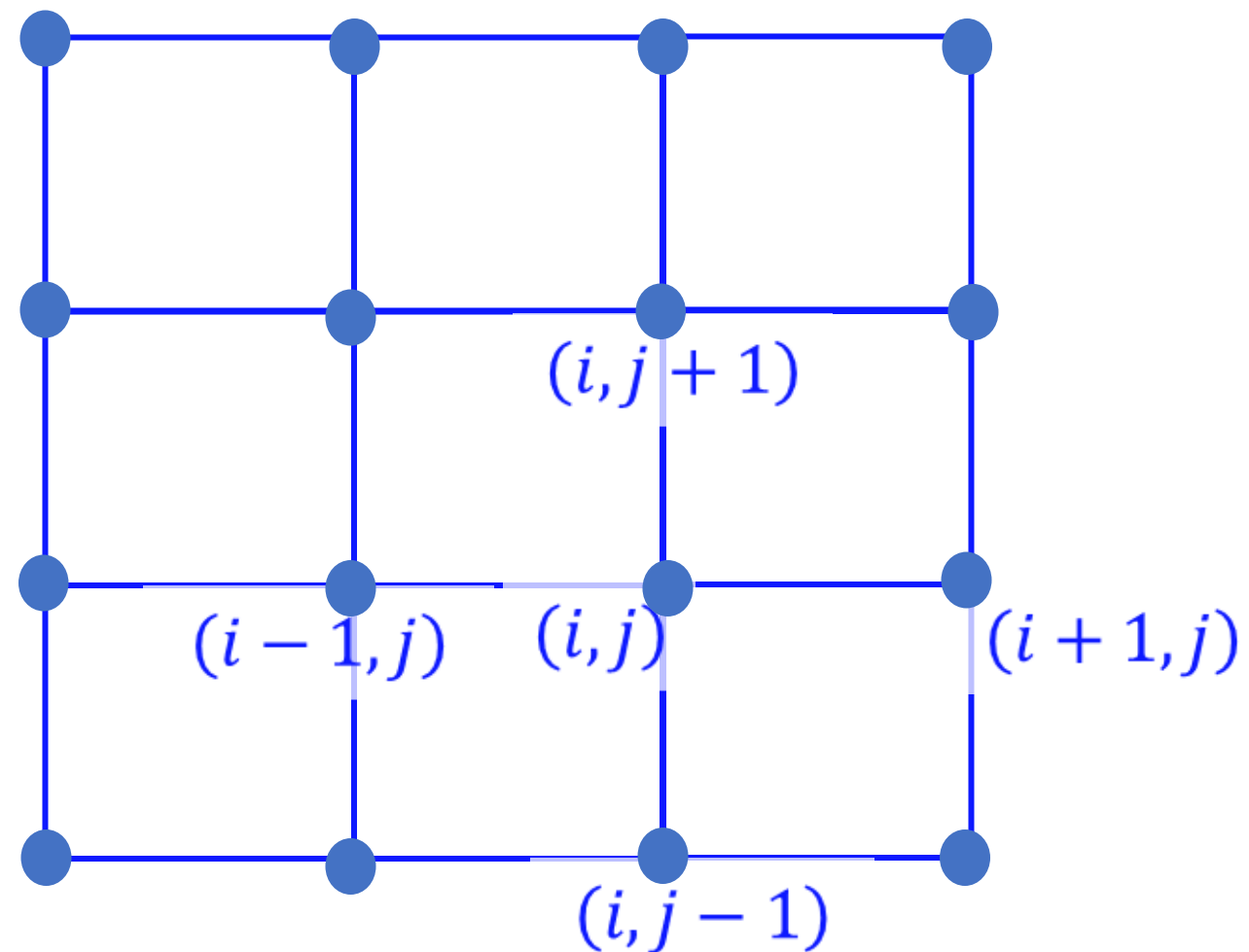
Collocated grid



Finite Difference – Finite Volume

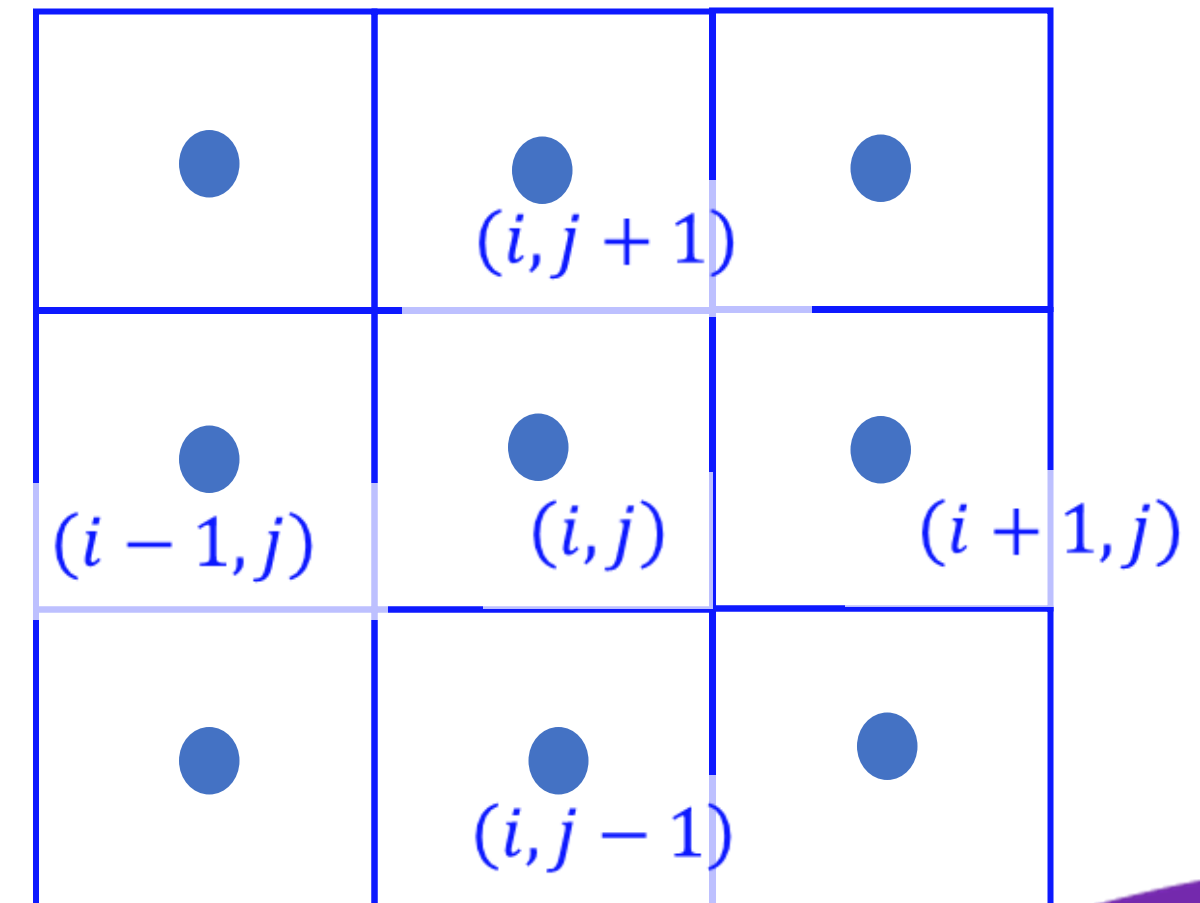
Differential form

$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \mathbf{u}) = 0$$



Integral form

$$\frac{\partial}{\partial t} \int_V \rho dV + \oint_S \rho \mathbf{u} \cdot d\mathbf{S} = 0$$



Taylor series and FDM

Taylor series:

$$\rho(x_{i+1}) = \rho(x_i) + \Delta x_i \left(\frac{\partial \rho}{\partial x} \right)_i + O(\Delta x_i^2)$$

$$\left(\frac{\partial \rho}{\partial x} \right)_i = \frac{\rho(x_{i+1}) - \rho(x_i)}{\Delta x_i} + \frac{1}{\Delta x_i} O(\Delta x_i^2)$$

$$\left(\frac{\partial \rho}{\partial x} \right)_i = \frac{\rho(x_{i+1}) - \rho(x_i)}{\Delta x_i} + O(\Delta x_i)$$

$$\left(\frac{\partial \rho}{\partial x} \right)_i \approx \frac{\rho(x_{i+1}) - \rho(x_i)}{\Delta x_i}$$

First order forward difference scheme

Finite difference

$$\nabla \rho = \left(\frac{\partial}{\partial x} \mathbf{e}_x + \frac{\partial}{\partial y} \mathbf{e}_y + \frac{\partial}{\partial z} \mathbf{e}_z \right) \rho = \left(\frac{\partial \rho}{\partial x} \mathbf{e}_x + \frac{\partial \rho}{\partial y} \mathbf{e}_y + \frac{\partial \rho}{\partial z} \mathbf{e}_z \right)$$

$$\left(\frac{\partial \rho}{\partial x} \right)_i = \frac{\rho(x_{i+1}) - \rho(x_i)}{\Delta x_i} + O(\Delta x_i)$$

Taylor series expansion



$$\rho(x_{i+1}) = \rho(x_i) + (x_{i+1} - x_i) \left(\frac{d\rho}{dx} \right)_i + (x_{i+1} - x_i)^2 \left(\frac{d^2\rho}{dx^2} \right)_i + (x_{i+1} - x_i)^3 \left(\frac{d^3\rho}{dx^3} \right)_i + \dots$$

$$(1) \quad \rho(x_{i+1}) = \rho(x_i) + \Delta x_i \left(\frac{d\rho}{dx} \right)_i + \Delta x_i^2 \left(\frac{d^2\rho}{dx^2} \right)_i + O(\Delta x_i^3)$$

$$(2) \quad \rho(x_{i-1}) = \rho(x_i) - \Delta x_i \left(\frac{d\rho}{dx} \right)_i + \Delta x_i^2 \left(\frac{d^2\rho}{dx^2} \right)_i + O(\Delta x_i^3)$$

Taylor series: Central Difference Scheme (2nd order)

$$(1) \quad \rho(x_{i+1}) = \rho(x_i) + \Delta x_i \left(\frac{d\rho}{dx} \right)_i + \Delta x_i^2 \left(\frac{d^2\rho}{dx^2} \right)_i + O(\Delta x_i^3)$$



$$(2) \quad \rho(x_{i-1}) = \rho(x_i) - \Delta x_i \left(\frac{d\rho}{dx} \right)_i + \Delta x_i^2 \left(\frac{d^2\rho}{dx^2} \right)_i + O(\Delta x_i^3)$$

Subtract (2) from (1)

$$\rho(x_{i+1}) - \rho(x_{i-1}) = 2\Delta x_i \left(\frac{d\rho}{dx} \right)_i + O(\Delta x_i^3)$$

$$\left(\frac{d\rho}{dx} \right)_i = \frac{\rho(x_{i+1}) - \rho(x_{i-1}))}{2\Delta x_i} + O(\Delta x_i^2)$$

Second order central difference scheme

Taylor series: Backward Difference Scheme (1st order)

$$\rho(x_{i-1}) = \rho(x_i) - \Delta x_i \left(\frac{d\rho}{dx} \right)_i + \Delta x_i^2 \left(\frac{d^2\rho}{dx^2} \right)_i + O(\Delta x_i^3)$$

$$\rho(x_{i-1}) = \rho(x_i) - \Delta x_i \left(\frac{d\rho}{dx} \right)_i + O(\Delta x_i^2)$$

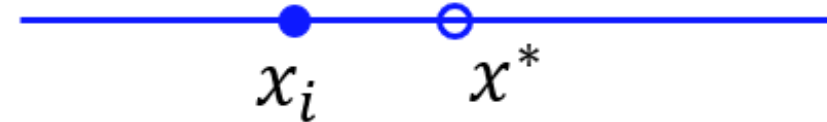
$$\rho(x_{i-1}) = \rho(x_i) - \Delta x_i \left(\frac{d\rho}{dx} \right)_i + O(\Delta x_i^2)$$

$$\left(\frac{d\rho}{dx} \right)_i = \frac{\rho(x_i) - \rho(x_{i-1})}{\Delta x_i} + O(\Delta x_i)$$

$$\left(\frac{d\rho}{dx} \right)_i \approx \frac{\rho(x_i) - \rho(x_{i-1})}{\Delta x_i}$$

First order backward difference scheme

Taylor series: Summary



$$\rho(x^*) = \rho(x_i) + (x^* - x_i) \left(\frac{d\rho}{dx} \right)_i + (x^* - x_i)^2 \left(\frac{d^2\rho}{dx^2} \right)_i + (x^* - x_i)^3 \left(\frac{d^3\rho}{dx^3} \right)_i + \dots$$



First order forward difference

$$\left(\frac{d\rho}{dx} \right)_i \approx \frac{\rho(x_{i+1}) - \rho(x_i)}{\Delta x_i}$$

Second order central difference

$$\left(\frac{d\rho}{dx} \right)_i \approx \frac{\rho(x_{i+1}) - \rho(x_{i-1}))}{2\Delta x_i}$$

First order backward difference

$$\left(\frac{d\rho}{dx} \right)_i \approx \frac{\rho(x_i) - \rho(x_{i-1}))}{\Delta x_i}$$

Approximating Second Order Derivative $\left(\frac{d^2\rho}{dx^2}\right)_i$



$$\rho(x_{i+1}) = \rho(x_i) + (x_{i+1} - x_i) \left(\frac{d\rho}{dx}\right)_i + \frac{(x_{i+1} - x_i)^2}{2} \left(\frac{d^2\rho}{dx^2}\right)_i + \frac{(x_{i+1} - x_i)^3}{6} \left(\frac{d^3\rho}{dx^3}\right)_i + \frac{(x_{i+1} - x_i)^4}{24} \left(\frac{d^4\rho}{dx^4}\right)_i + \dots$$

$$(1) \quad \rho(x_{i+1}) = \rho(x_i) + \Delta x_i \left(\frac{d\rho}{dx}\right)_i + \frac{\Delta x_i^2}{2} \left(\frac{d^2\rho}{dx^2}\right)_i + \frac{\Delta x_i^3}{6} \left(\frac{d^3\rho}{dx^3}\right)_i + \frac{\Delta x_i^4}{24} \left(\frac{d^4\rho}{dx^4}\right)_i + O(\Delta x_i^5)$$

$$(2) \quad \rho(x_{i-1}) = \rho(x_i) - \Delta x_i \left(\frac{d\rho}{dx}\right)_i + \frac{\Delta x_i^2}{2} \left(\frac{d^2\rho}{dx^2}\right)_i - \frac{\Delta x_i^3}{6} \left(\frac{d^3\rho}{dx^3}\right)_i + \frac{\Delta x_i^4}{24} \left(\frac{d^4\rho}{dx^4}\right)_i + O(\Delta x_i^5)$$

Approximating Second Order Derivative

$$(1) \quad \rho(x_{i+1}) = \rho(x_i) + \Delta x_i \left(\frac{d\rho}{dx} \right)_i + \frac{\Delta x_i^2}{2} \left(\frac{d^2\rho}{dx^2} \right)_i + \frac{\Delta x_i^3}{6} \left(\frac{d^3\rho}{dx^3} \right)_i + \frac{\Delta x_i^4}{24} \left(\frac{d^4\rho}{dx^4} \right)_i + O(\Delta x_i^5)$$

$$(2) \quad \rho(x_{i-1}) = \rho(x_i) - \Delta x_i \left(\frac{d\rho}{dx} \right)_i + \frac{\Delta x_i^2}{2} \left(\frac{d^2\rho}{dx^2} \right)_i - \frac{\Delta x_i^3}{6} \left(\frac{d^3\rho}{dx^3} \right)_i + \frac{\Delta x_i^4}{24} \left(\frac{d^4\rho}{dx^4} \right)_i + O(\Delta x_i^5)$$



Add (1) and (2)

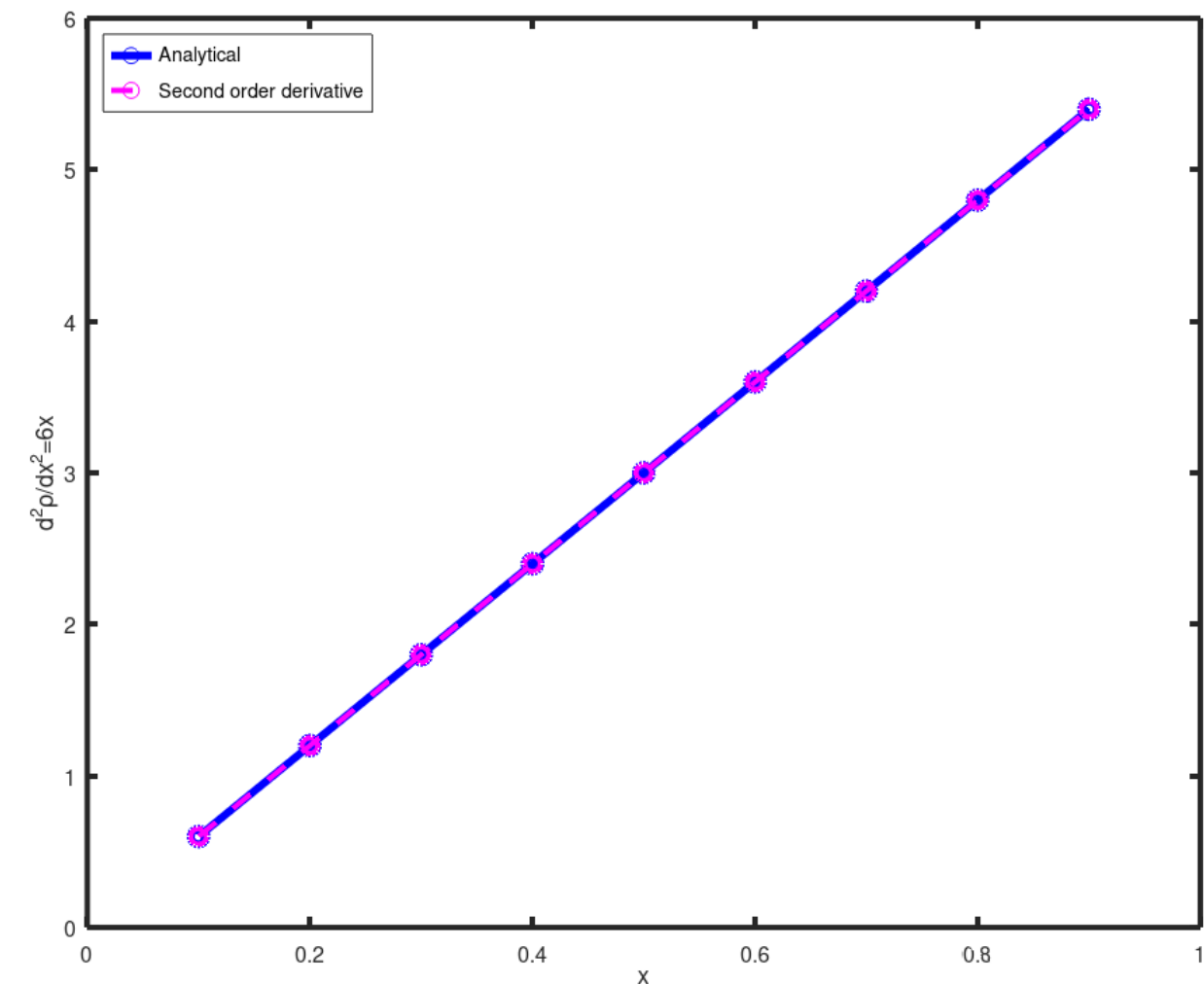
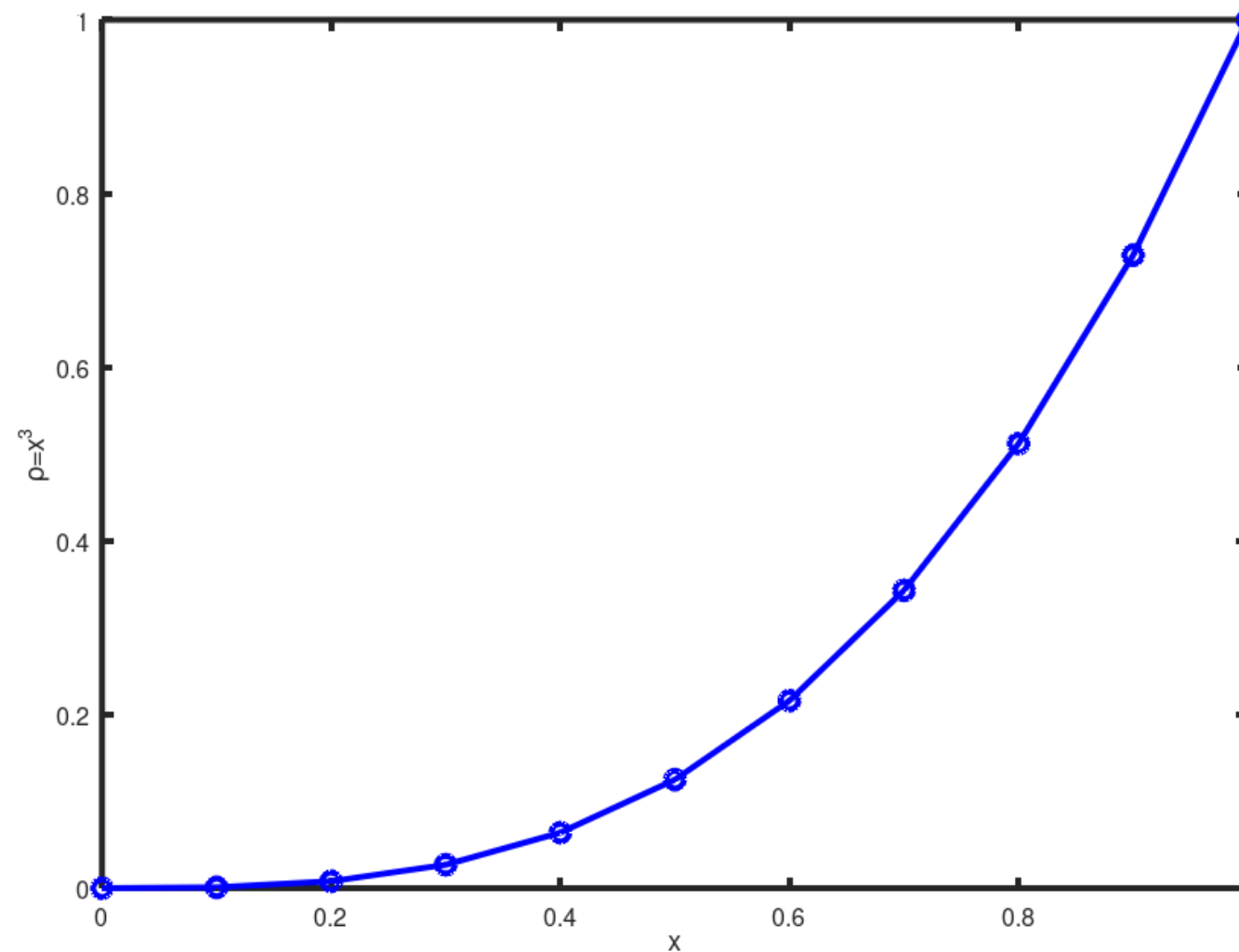
$$\rho(x_{i+1}) + \rho(x_{i-1}) = 2\rho(x_i) + \Delta x_i^2 \left(\frac{d^2\rho}{dx^2} \right)_i + \frac{\Delta x_i^4}{12} \left(\frac{d^4\rho}{dx^4} \right)_i + \dots$$

$$\left(\frac{d^2\rho}{dx^2} \right)_i = \frac{\rho(x_{i+1}) - 2\rho(x_i) + \rho(x_{i-1}))}{\Delta x_i^2} + \frac{\Delta x_i^4}{12\Delta x_i^2} \left(\frac{d^4\rho}{dx^4} \right)_i + \dots$$

$$\boxed{\left(\frac{d^2\rho}{dx^2} \right)_i = \frac{\rho(x_{i+1}) - 2\rho(x_i) + \rho(x_{i-1}))}{\Delta x_i^2} + O(\Delta x_i^2)}$$

Approximating Second Order Derivative

$$\left(\frac{d^2\rho}{dx^2}\right)_i = \frac{\rho(x_{i+1}) - 2\rho(x_i) + \rho(x_{i-1}))}{\Delta x_i^2} + O(\Delta x_i^2)$$



Exercise – 6

[Exercise-6] Estimate second order derivative using second order central difference scheme #7

Edit

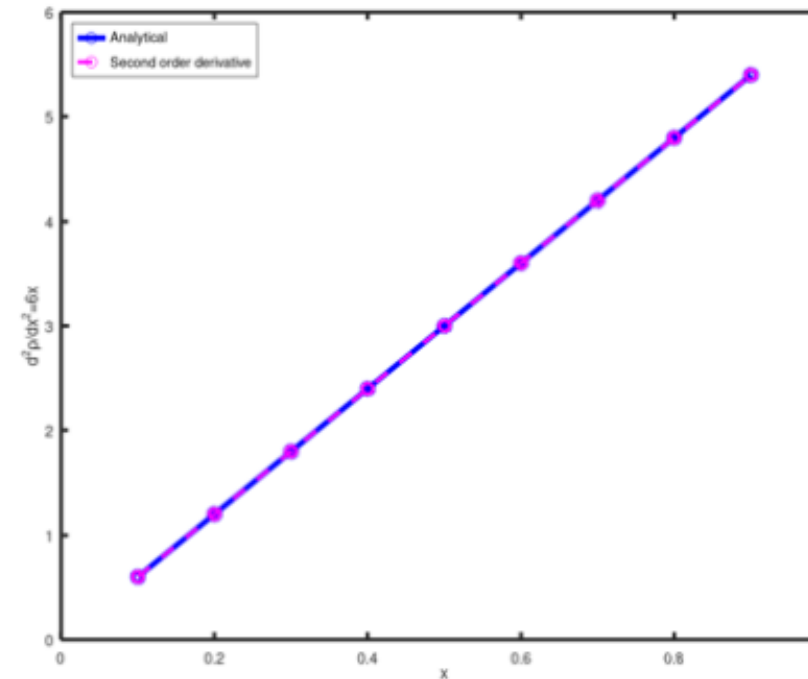
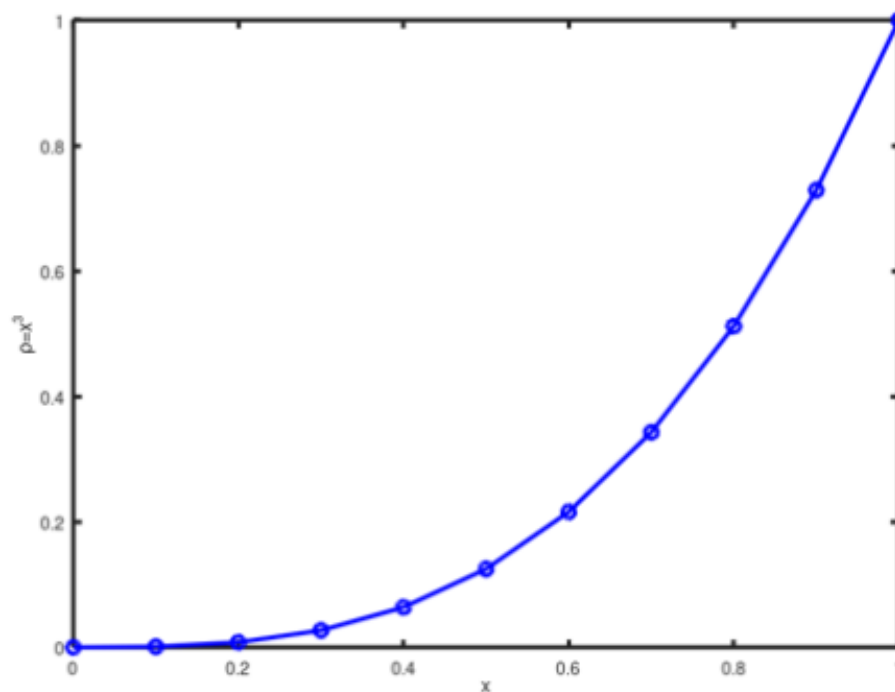
kummi0402 started this conversation in General



kummi0402 yesterday Maintainer

Approximating Second Order Derivative

$$\left(\frac{d^2\rho}{dx^2}\right)_i = \frac{\rho(x_{i+1}) - 2\rho(x_i) + \rho(x_{i-1}))}{\Delta x_i^2} + o(\Delta x_i^2)$$



Category



General

Labels



None yet

1 participant



Notifications

Unsubscribe

You're receiving notifications because you authored the thread.

Lock conversation

Transfer this discussion

Pin discussion

Pin discussion to General

Create issue from discussion

Delete discussion

THANK YOU