

## Transistor Modeling.....

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PEARSON

### Common – Base Configuration

Using a PNP transistor the Common-Base configuration and the  $r_e$  model:

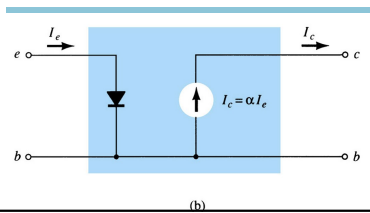
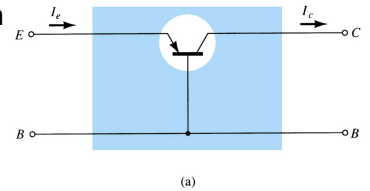
The emitter is the input and the collector is the output.

This model indicates:

$$I_c = \alpha I_e$$

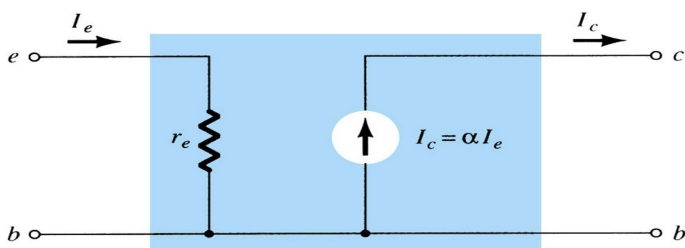
$$r_e = \frac{26\text{mV}}{I_E}$$

where  $I_E$  is the DC current.



### Common Base $r_e$ Model

The diode in the previously shown  $r_e$  model can be replaced by the resistor  $r_e$ .



### Impedance in Common-Base Configuration

The  $r_e$  model indicates:

The input impedance ( $Z_i$ ) is quite small:  $Z_i = r_e$

[Formula 7.12]

The output impedance ( $Z_o$ ) is quite large:  $Z_o \approx \infty \Omega$

[Formula 7.13]

## Gain calculations for the Common-Base using the $r_e$ model

Voltage Gain:  $A_v = \frac{R_L}{r_e} \cong \frac{R_L}{r_e}$   
[Formula 7.14]

Current Gain:  $A_i = -\alpha \cong -1$   
[Formula 7.15]

$$V_o = -I_o R_L = -(-I_e) R_L = \alpha I_e R_L$$

$$V_i = I_e Z_i = I_e r_e$$

$$A_v = \frac{V_o}{V_i} = \frac{\alpha I_e R_L}{I_e r_e}$$

$$A_v = \frac{\alpha R_L}{r_e} \cong \frac{R_L}{r_e} \quad CB$$

$$A_i = \frac{I_o}{I_i} = \frac{-I_e}{I_e} = -\frac{\alpha I_e}{I_e}$$

$$A_i = -\alpha \cong -1 \quad CB$$

The phase relationship between input and output is **0** degrees.

**The npn transistor will use the same calculation. The only difference is that the voltage polarities and current directions will be the opposite.**

For a common-base configuration of Fig. 7.17 with  $I_E = 4$  mA,  $\alpha = 0.98$ , and an ac signal of 2 mV applied between the base and emitter terminals:

- Determine the input impedance.
- Calculate the voltage gain if a load of 0.56 k $\Omega$  is connected to the output terminals.
- Find the output impedance and current gain.

### Solution

(a)  $r_e = \frac{26 \text{ mV}}{I_E} = \frac{26 \text{ mV}}{4 \text{ mA}} = 6.5 \Omega$

(b)  $I_i = I_e = \frac{V_i}{Z_i} = \frac{2 \text{ mV}}{6.5 \Omega} = 307.69 \mu\text{A}$

$$V_o = I_e R_L = \alpha I_e R_L = (0.98)(307.69 \mu\text{A})(0.56 \text{ k}\Omega) = 168.86 \text{ mV}$$

and  $A_v = \frac{V_o}{V_i} = \frac{168.86 \text{ mV}}{2 \text{ mV}} = 84.43$   
or from Eq. (7.14),

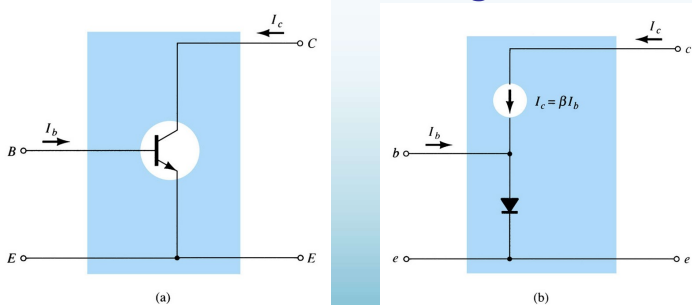
$$A_v = \frac{\alpha R_L}{r_e} = \frac{(0.98)(0.56 \text{ k}\Omega)}{6.5 \Omega} = 84.43$$

(c)  $Z_o \cong \infty \Omega$

$A_i = \frac{I_o}{I_i} = -\alpha = -0.98$  as defined by Eq. (7.15)

## Example

## Common-Emitter Configuration



The base current is the input and the collector is the output.  
This model indicates:

$$I_c = \beta I_b \quad [\text{Formula 7.16}]$$

$$I_e = (\beta + 1) I_b \quad [\text{Formula 7.17}]$$

$$I_e \cong \beta I_b \quad [\text{Formula 7.18}]$$

## Impedance in Common-Emitter Configuration

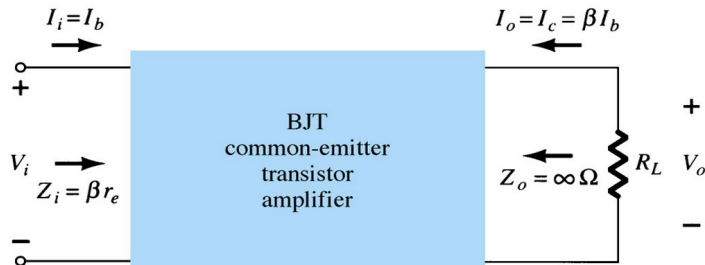
The input impedance ( $Z_i$ ):  $Z_i = \beta r_e$

[Formula 7.19]

The output impedance ( $Z_o$ ):  $Z_o = r_o$   
 $Z_o \cong \infty \Omega$

[Formula 7.20]

### Gain calculations for the Common-Emitter using the $r_e$ model



Voltage Gain ( $A_v$ ):  $A_v = -\frac{R_L}{r_e}$  [Formula 7.21]

Current Gain ( $A_i$ ):  $A_i = \beta / r_o = \infty \Omega$  [Formula 7.22]

**The Common-Emitter Model is used for Common-Collector.**

### Types of Amplifier

**Three** Types of **Amplifiers** are :

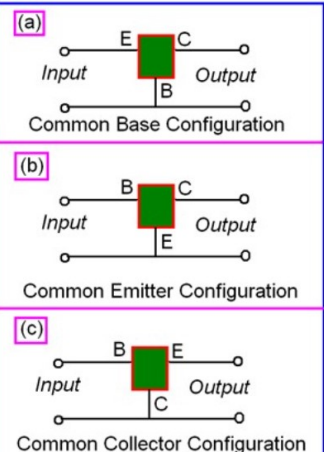
- (i) **CURRENT amplifiers** , with a small load resistance,
- (ii) **VOLTAGE amplifiers** have a high load resistance, and
- (iii) **POWER amplifiers** .

### Classification of Amplifiers

Type of Signal	Type of Configuration	Classification	Frequency of Operation
Small Signal	Common Emitter	Class A Amplifier	Direct Current (DC)
Large Signal	Common Base	Class B Amplifier	Audio Frequencies (AF)
	Common Collector	Class AB Amplifier	Radio Frequencies (RF)
		Class C Amplifier	VHF, UHF and SHF Frequencies

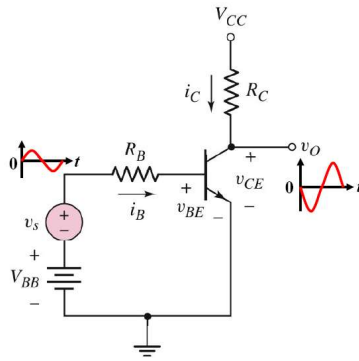
### Biasing Configurations in active region

Three configurations in the active region are shown



## Basic BJT amplifier

- A BJT needs to be biased by a dc voltage source ( $V_{BB}$ ) at a suitable Q-point to ensure that it is operating in **forward-active mode** – the precondition for configuring a BJT as an amplifier.
- A BJT amplifier has a time-varying signal source ( $v_s$ ) in series with the dc voltage source ( $V_{BB}$ ).
- A change in  $v_s$  causes a change in  $i_B$  which, in turn, causes a larger change in  $i_C$  ( $i_C = \beta i_B$ ) & leads to an **inverted & amplified** signal ( $v_o$ ) compared to the original  $v_s$ .



Common-Emitter Amplifier

## Analysis of BJT amplifiers

### Function of each component:

- Capacitors: Acting as an **open circuit** for a **dc** operation but a **short circuit** for an **ac** operation (If  $f = 10 \text{ kHz}$  &  $C = 10 \mu\text{F}$ , then  $|Z_C| = (2 \pi f C)^{-1} = 8 \Omega$ , which is usually smaller than  $R_{TH} = R_1 // R_2$ )
- $R_1$ ,  $R_2$ ,  $R_C$  &  $R_E$ : Setting dc biasing **Q-point**
- $R_C$ : Converting  $i_c$  variation into  $v_{ce}$  (or  $v_o$ ) variation (**signal conversion**)

