

# *ECE 20002: Electrical Engineering Fundamentals II*

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Lecture notes for Purdue's ECE 20002.

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## *Course Introduction*

Continuation of Electrical Engineering Fundamentals I. The course addresses mathematical and computational foundations of circuit analysis (differential equations, Laplace Transform techniques) with a focus on application to linear circuits having variable behavior as a function of frequency, with emphasis on filtering. Variable frequency behavior is considered for applications of electronic components through single-transistor and operational amplifiers. The course ends with a consideration of how circuits behave and may be modeled for analysis at high frequencies.

### *Learning Objectives:*

1. Analyze 2nd order linear circuits with sources and/or passive elements
2. Compute responses of linear circuits with and without initial conditions via one-sided Laplace transform techniques
3. Compute responses to linear circuits using transfer function and convolution techniques
4. Analyze and design transistor amplifiers at low, mid and high frequencies

## Field-Effect Transistor Devices

### MOSFETs

Let us begin where ECE 20001 ended, with metal-oxide semiconductor field-effect transistors (MOSFETs). The rectangle below represent a wafer of silicon. The p - Si label indicates that the wafer is primarily doped with boron and the primary carrier type is holes. The two  $n^+$  rectangles designate regions of phosphorus doping. The grey rectangles above the wafer are dielectric layers of silicon dioxide. The black rectangles are ohmic metals that allow for connecting our phosphorus regions to other components. To these metal contacts we attach a source, a gate, and a drain. The source is the source of electron, and the drain is how the electrons exit. The gate will define a pathway between the source and drain. Since the phosphorus re-



Figure 1: nMOSFET diagram

gions are n-type and ergo have free electrons, the primary carrier of this MOSFET are electrons. The way we allow current to flow from source to drain is by increasing the voltage of the gate  $v_{GS}$  to attract an inversion layer underneath the dielectric separating the gate from the silicon wafer. If the voltage of the gate is high enough ( $v_{GS} > V_T$ ) then enough electrons will be attracted to that area for current to flow between source and drain.

We could create a similar MOSFET by inverting the n-type and p-type regions, as in figure 2. In this case the primary current carrier will be holes.

In the case of the nMOSFET in figure 1, a negative gate voltage will attract holes in the semiconductor, forming two oppositely charged areas separated by a distance  $x$ . This establishes an electric field within the oxide layer given by the equation for a parallel plate capacitor

$$\mathcal{E}_x = -\frac{dV}{dx} \quad (1)$$

Likewise, a positive gate voltage *that is less than*  $V_T$  will attract elec-



Figure 2: pMOSFET diagram

trons in the semiconductor. This also forms a capacitance of  $C_{ox}$  in the oxide layer, but because the semiconductor is n-type, the electrons will be spread out over a wider area and have their own capacitance  $C_d$ . Thus the total capacitance across the oxide and depletion region  $C$  given by

$$\frac{1}{C} = \frac{1}{C_{ox}} + \frac{1}{C_d} \quad (2)$$

If  $0 < V_T < v_{GS}$ , then  $C = f\omega$ , where  $\omega$  is the frequency of our probe.

Figure 3 displays the capacitance-voltage graph of a p-type metal-oxide semiconductor. The capacitance is constant when gate voltage is negative, then falls at the *flat-band voltage*  $V_{GS} = 0V$ , then rapidly rises again after the threshold voltage is reached.

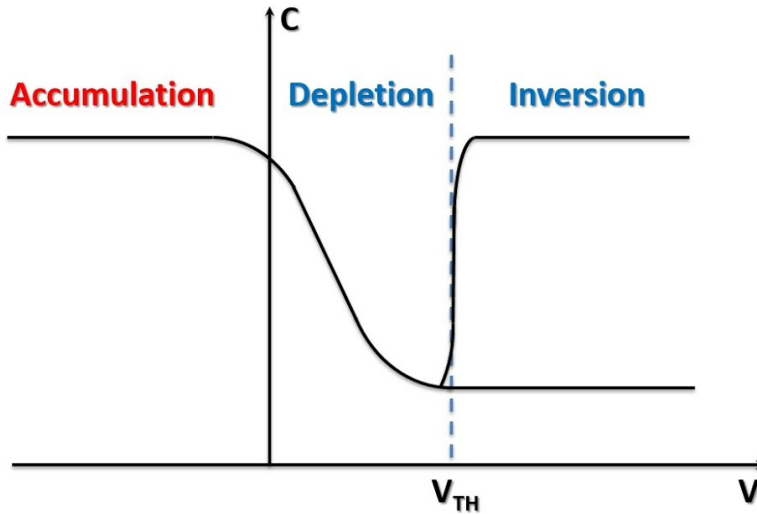


Figure 3: p-type MOS capacitance-voltage characteristic

The resistivity of the inversion channel created by the gate's bias is given by

$$\frac{1}{\rho} = (n\mu_e + p\mu_h)q \quad (3)$$

where  $n$  is the concentration of electrons,  $p$  is the concentration of holes,  $\mu_e$  is the mobility of electrons,  $\mu_h$  is the mobility of holes, and  $q$  is the charge of an electron. The higher the gate voltage, the higher the current between source and drain. Below the threshold voltage there is no current flow because no channel is formed. This relationship is linear provided the drain voltage is less than 150 mV, but above 0.3 V becomes nonlinear. That's because the channel is no longer a regular shape, but narrows in the region of the drain. Below 150 mV, however, this distortion can be assumed negligible. Recall that

$$R = \frac{\rho L}{A} \quad (4)$$

Whereas for small  $v_{DS}$  the area is almost constant, when  $v_{DS} > 0.15V$  the area  $A$  decreases enough that the resistance  $R$  is significantly increased. When the area has decreased to zero at the drain, we reach the *pinch-off* and the drain voltage is at saturation  $v_{DS(sat)}$ . The current still flows constantly for all drain voltage above saturation, however. Before saturation is reached and after the gate voltage is above the threshold, we are in the triode region. In the triode region, the current is given by

$$i_{D(triode)} = \mu C_{ox} \frac{W}{L} \left( (v_{GS} - V_T) v_{DS} - \frac{v_{DS}^2}{2} \right) \quad (5)$$

Sometimes, the constant terms are wrapped up into one constant, like so:

$$i_{D(triode)} = k_n \left( (v_{GS} - V_T) v_{DS} - \frac{v_{DS}^2}{2} \right) \quad (6)$$

In the saturation region,

$$i_{D(sat)} = \mu C_{ox} \frac{W}{L} \frac{(v_{GS} - V_T)^2}{2} \quad (7)$$

$$= k_n \frac{v_{DS(sat)}^2}{2} \quad (8)$$

When we are far away from saturation, the resistance of the channel is given by

$$R_{on} = \frac{\partial v_{DS}}{\partial i_D} \quad (9)$$

$$= \frac{1}{\mu C_{ox} \frac{W}{L} (v_{GS} - V_T)} \quad (10)$$

Figure 4 shows a family of  $i_D$ - $v_{DS}$  curves with differing values of  $v_{GS}$ . Also show as a dashed green line is the saturation current as a function of gate voltage. Let's look at the impact the threshold voltage has by plotting the  $i_D$ - $v_{GS}$  curve for differing values of  $V_T$  in figure 5. Now the green dashed curve corresponds to a threshold voltage of



Figure 4: Transfer characteristics of nMOSFETs

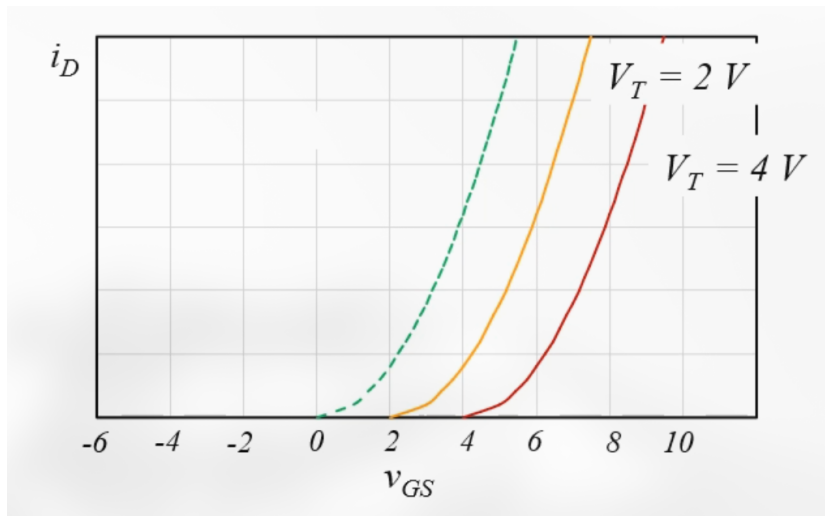


Figure 5:  $i_D$ - $v_{GS}$  curve for select values of  $V_T$

zero. Recall that the threshold voltage is intrinsic to the semiconductor wafer. Doping variations, defect, and shape can all affect the threshold voltage. If we build a depletion-mode nMOSFET, then we allow for negative threshold voltages.

A normally off like in figure 1 has the symbol shown in 6 and is said to be in enhancement mode. If the nMOSFET has an n-channel

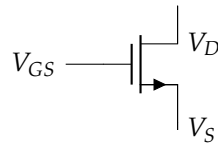


Figure 6: nMOSFET schematic

between the source and drain, as shown in figure 7, then it is normally

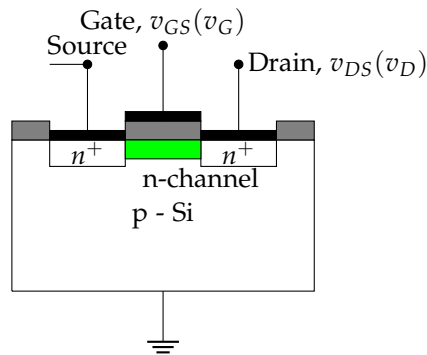


Figure 7: Normally on nMOSFET diagram

on and its symbol is as seen in figure 8. This kind of nMOSFET is said to be in depletion mode. Note the thicker line between source and

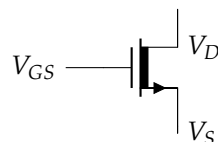


Figure 8: Schematic of normally on nMOSFET

drain representing the n-channel.

Similarly, the pMOSFET shown in figure 2 is a normally off, enhancement mode pMOSFET. A pMOSFET with a p-channel is normally on and in depletion mode.

Let's look at the transfer characteristics of the different types of MOSFETs. figure 4 shows these characteristics for a normally off, enhancement mode nMOSFET. For a normally on, depletion mode nMOSFET the graph is exactly the same, except that the current can flow even when the gate bias is zero since the fabricated channel

allows the flow of electrons from source to drain. The output characteristics for a normally off, enhancement mode pMOSFET are shown in figure 9. A negative bias on the gate will induce a channel of pos-

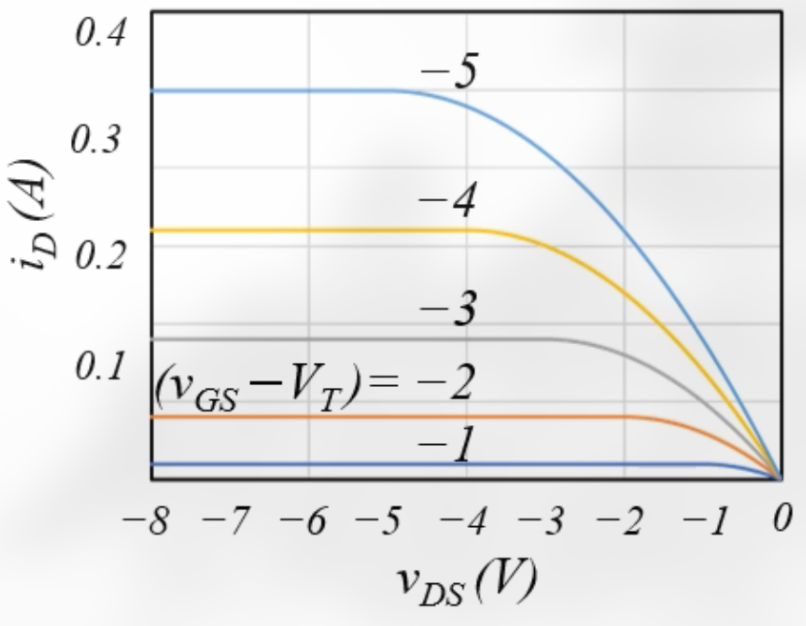


Figure 9:  $i_D$ - $v_{DS}$  curve for select values of  $v_{GS} - V_T$

itive holes in the semiconductor, making the threshold voltage for a pMOSFET negative. Again, the normally on depletion mode pMOSFET graph has the same shape, but since there is an existing channel for current it will flow even for some positive values of  $v_{GS}$ . We need to deplete the channel by pushing away all the holes in it with the bias on the gate in order to turn it off.

To review, there are four kinds of MOSFETs in which we are interested:

- normally off, enhancement mode nMOSFETs
- normally on, depletion mode nMOSFETs
- normally off, enhancement mode pMOSFETs
- normally on, depletion mode pMOSFETs

### Transconductance

Now, let us move on to the topic of transconductance. In the triode region, the transconductance is defined as

$$g_m = \left. \frac{i_D}{v_{GS}} \right|_{Q_{pt}} \quad (11)$$

where

$$Q_{pt} = (I_D, V_{DS}). \quad (12)$$

If we recall equation 5, and substitute for  $i_D$  in equation 11, then we obtain

$$g_m = \mu C_{ox} \frac{W}{L} v_{DS} \quad (13)$$

$$= \frac{i_{D(triode)}}{(v_{GS} - v_T) - \frac{v_{DS}}{2}} \quad (14)$$

In the saturation region,

$$g_m = \frac{di_D}{dv_{GS}}|_{Q_{pt}} \quad (15)$$

and

$$i_{D(sat)} = \mu C_{ox} \frac{W}{L} \frac{(v_{GS} - V_T)^2}{2}. \quad (16)$$

Again combining these two equations,

$$g_m = \mu C_{ox} \frac{W}{L} (v_{GS} - V_T) \quad (17)$$

$$= \frac{2i_{D(sat)}}{(v_{GS} - V_T)} \quad (18)$$

The larger the transconductance, the larger the gain of an amplifier circuit that uses the transistor.

### *Channel length modulation*

By adjusting the voltage of the drain, we can modulate the channel length. Specifically,

$$i_{D(sat)} \propto \frac{1}{L - \Delta L} \quad (19)$$

$$\equiv \frac{1}{L} \left( 1 + \frac{\Delta L}{L} \right). \quad (20)$$

And

$$\Delta L \propto (v_{DS} - v_{DS(sat)}) \quad (21)$$

means that

$$i_{D(sat)} = \frac{1}{2} \mu C_{ox} \frac{W}{L} (v_{GS} - V_T)^2 \left[ 1 + \lambda (v_{DS} - v_{DS(sat)}) \right] \quad (22)$$



where  $\lambda$  is the empirically determined channel length modulation parameter. The output resistance at the drain is given by

$$r_0 = \left[ \frac{\partial i_{D(sat)}}{\partial v_{DS}} \right]^{-1} \quad (23)$$

$$= \left[ \lambda \frac{1}{2} k_n (v_{GS} - V_T)^2 \right]^{-1} \quad (24)$$

$$= \frac{1}{\lambda I_{D(sat)}} \quad (25)$$

$$\approx \frac{V_A}{I_{D(sat)}} \quad (26)$$

Channel length modulation is not important when channel length is relatively large, but it is important on modern transistors where are on the order of nanometers.

### MOSFETs in DC circuits

Consider a circuit with two enhancement mode pMOSFETs. Notice

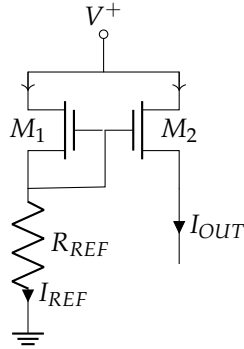


Figure 10: MOSFET DC circuit

that in figure 10, the drain of  $M_1$  is directly attached to the gate. From this we have

$$v_{DS1} = v_{GS1} \quad (27)$$

$$= v_{GS2} \quad (28)$$

We are told  $M_1$  is in saturation. If these are two identical transistors, then

$$I_{REF} = I_{D(sat)} \quad (29)$$

$$= \frac{1}{2} k_{p1} (v_{GS1} - V_{T1})^2 \quad (30)$$

$$= I_{OUT}. \quad (31)$$

From this, we learn that the reference current is mirrored by the drain current if  $k_{p1} = k_{p2}$  and  $v_{GS1} = v_{GS2}$ .

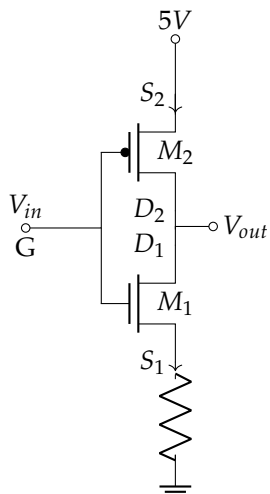


Figure 11: Inverter

Let us now look at the inverter shown in figure 11. Let's try to find  $V_{out}$  for  $V_{in} = 0V$  and  $V_{in} = 5V$ . We are told that  $V_{T(M1)} = 1V$  and  $V_{T(M2)} = -1V$ , because M1 is an enhancement mode nMOSFET and M2 is an enhancement mode pMOSFET. When  $V_{in} = 0V$ , M1 is off because  $v_{GS1} < V_{T(M1)}$ . Likewise, M2 is on because  $v_{GS2} < V_{T(M2)}$  (recall that M2 is a pMOSFET). Since M1 is off, no current flows and  $V_{out} = 5V$ . For  $V_{in} = 5V$ , M1 flips on while M2 is off. Since M2 is off, no current flows. That means that  $V_{out} = 5V$ .

### Transistors as amplifiers

The circuit shown in figure 12 has both AC and DC voltage sources.

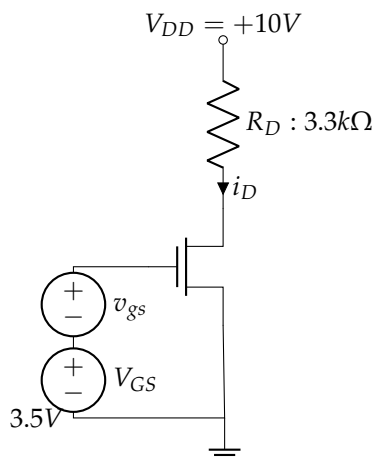


Figure 12: Common-source nMOSFET amplifier circuit

The source labelled by  $V_{GS}$ , all caps, is the DC voltage. The source  $v_{gs}$ , all lowercase, is the AC. This is not to be confused with  $v_{GS}$ , the total

gate bias. The mix of cases indicates we have both AC and DC bias in consideration. The cool thing about this circuit is a small oscillation in the AC input induces a much larger oscillation in the output, hence calling it an amplifier. The output signal is going to be phase shifted by  $180^\circ$ . We can calculate the gain with eq. 32

$$A_v = \frac{v_{ds}}{v_{gs}} \quad (32)$$

In this instance,

$$A_v = \frac{v_{ds}}{v_{gs}} \quad (33)$$

$$= \frac{4.17 \angle 180^\circ}{1 \angle 0^\circ} \quad (34)$$

$$= -4.17 \quad (35)$$

This gain, however, will be somewhat distorted. To reduce distortion we need that  $|v_{gs}| \ll 2(V_{GS} - V_T)$ . The exact value of the "much less" symbol  $\ll$  will depend on the application, but it's common to require  $|v_{gs}| < 0.2(V_{GS} - V_T)$ . If we assume the small signal condition and no channel length modulation, then the transconductance of the amplifier is

$$g_m = \sqrt{2k_n I_{D(sat)}} \quad (36)$$

### Chapter summary

Region	Conditions
Cut-off	$v_{DS} < 0$ or $v_{DS(sat)} < 0$
Triode	$0 \leq v_{DS} \leq v_{DS(sat)}$
Saturation	$v_{DS} > v_{DS(sat)}$

Figure 13: MOSFET regions of operation

nMOSFET	pMOSFET
$v_{GS(on)} > 0$	$v_{GS(on)} < 0$

Figure 14: Differences between pMOSFET and nMOSFET

Equation	Reference
$v_{DS(sat)} = v_{GS} - V_T$	
$i_{D(cutoff)} = 0$	
$i_{D(triode)} = \mu C_{ox} \frac{W}{L} ((v_{GS} - V_T)v_{DS} - \frac{v_{DS}^2}{2})$ $= k_n ((v_{GS} - V_T)v_{DS} - \frac{v_{DS}^2}{2})$	eq. 5
$i_{D(sat)} = \mu C_{ox} \frac{W}{L} \frac{(v_{GS} - V_T)^2}{2}$ $= k_n \frac{v_{DS(sat)}^2}{2}$	eq. 7

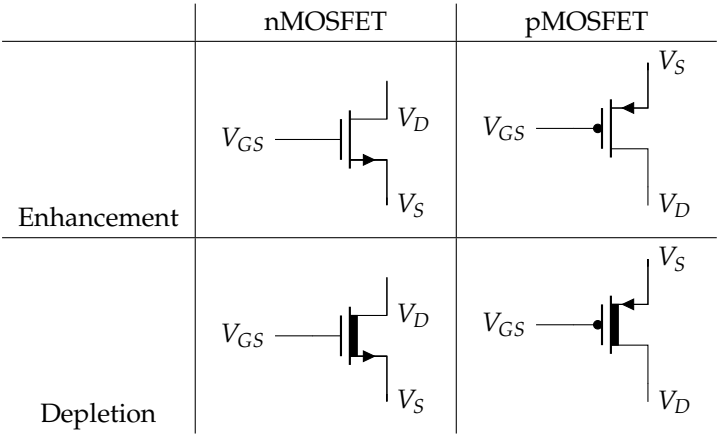


Figure 15: MOSFET schema