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## Enhanced leader particle swarm optimisation (ELPSO): An efficient algorithm for parameter estimation of photovoltaic (PV) cells and modules



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#### ABSTRACT

Today, photovoltaic (PV) systems are generating a significant share of electric power. Parameter estimation of photovoltaic cells and modules is a hot research topic and plays an important role in modelling PV systems. This problem is commonly converted into an optimisation problem and is solved by metaheuristic optimisation algorithms. Among metaheuristic optimisation algorithms, particle swarm optimisation (PSO) is a popular leaderbased stochastic optimisation algorithm. However, premature convergence is the main drawback of PSO which does not let it to provide high-quality solutions in multimodal problems such as PV cells/modules parameter estimation. In PSO, all particles are pulled toward the leader, so the leader can significantly affect collective performance of the particles. A high-quality leader may pull all particles toward good regions of search space and vice versa. Therefore, in this research, an improved PSO variant, with enhanced leader, named as enhanced leader PSO (ELPSO) is used. In ELPSO, by enhancing the leader through a five-staged successive mutation strategy, the premature convergence problem is mitigated in a way that more accurate circuit model parameters are achieved in the PV cell/module parameter estimation problem. RTC France silicon solar cell, STM6-40/36 module with monocrystalline cells and PVM 752 GaAs thin film cell have been used as the case studies of this research. Parameter estimation results for various PV cells and modules of different technologies confirm that in most of the cases, ELPSO outperforms conventional PSO and a couple of other state of the art optimisation algorithms.

#### 1. Introduction

Despite the intermittency of Photovoltaic (PV) power generation and the uncertainty that they add to electric power systems, they are deemed as popular sources for power generation. They are environmentally friendly power generation sources that are usually used as distributed generators near load centers. Photovoltaic systems play an important role in today's electric power systems and their penetration in electric power generation is increasing. For rapid and reliable design of PV systems, an accurate and fast simulator is very crucial (Chin et al., 2015). This simulator can be used for purposes such as design of maximum power point tracking systems and efficiency estimation of PV systems (Chin et al., 2015). PV cell model is the most important component of a PV simulator. It is envisaged to have a model that closely imitates the behavior of real PV cells, i.e. fits its measured I-V data under all operating conditions (Chin et al., 2015). The most commonly used modeling approach for PV cells is to use their electrical equivalent circuit (Chin et al., 2015; Jordehi, 2016a).

Single diode model is the most popular equivalent circuit model for PV cells. It has been illustrated as Fig. 1.

Single diode model has five parameters; photocurrent denoted by  $I_{Ph}$ , diode's ideality factor denoted by a, diode's reverse saturation current denoted by  $I_S$ , series resistance represented by  $R_S$  and shunt resistance denoted by  $R_P$ . For modeling a PV cell, these five parameters must be determined properly.

I-V characteristic of single diode model is given by Eq. (1).

$$I = I_{Ph} - I_{S} \left[ exp \left( \frac{q(V + R_{S}I)}{aKT} \right) - 1 \right] - \frac{V + R_{S}I}{R_{P}}$$

$$\tag{1}$$

where I and V respectively represent current and voltage of the cell and K stands for Boltzmann constant.

Double diode model, is the second most widely used circuit model for PV cells. It has been illustrated as Fig. 2 and its I-V characteristic is represented by Eq. (2) Gow and Manning, 1996; Chowdhury et al., 2007; Gupta et al., 2012. It has seven parameters;  $I_{Ph}$ ,  $R_S$ ,  $R_P$ , a and  $I_S$  of the first diode, a and  $I_S$  of the second diode. For modeling a certain PV cell/module as double diode model, these seven parameters must be found. Double diode model provides higher accuracy than single diode model, but it is more complex.

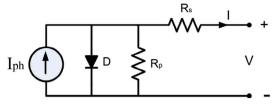


Fig. 1. Single diode model (Jordehi, 2016b).

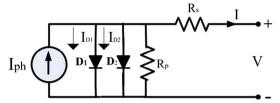


Fig. 2. Double diode model (Jordehi, 2016b).

$$I = I_{Ph} - I_{S_1} \left[ exp \left( \frac{q(V + R_S I)}{a_1 KT} \right) - 1 \right] - I_{S_2} \left[ exp \left( \frac{q(V + R_S I)}{a_2 KT} \right) - 1 \right] - \frac{V + R_S I}{R_P}$$
(2)

For modeling a PV cell/module, its circuit model parameters, i.e. the five parameters of single diode model and seven parameters of double diode model, must be determined in a way that the I-V characteristic of the resultant circuit closely emulates the experimental I-V data of the real PV cell. This problem is known as PV cell/module parameter estimation problem. In this problem, the circuit model parameters are typically determined in a way that root mean square error (RMSE) of model currents and experimentally measured currents are minimised. This represents a nonlinear, multimodal optimisation problem that is typically solved by population-based metaheuristic optimisation algorithms. Metaheuristics includes popular algorithms in solving challenging engineering optimisation problems. These algorithms do not require any preconditions such as differentiability or convexity of the problem and therefore can be employed for solving any optimisation problem. They are probabilistic algorithms that attempt to provide near-global solutions for the optimisation problem in hand.

Metaheuristics has been widely used for solving the PV cell/module parameter estimation problem (Jordehi, 2016b). In Hasanien (2015), shuffled frog leaping algorithm (SFLA), inspired from food foraging behavior of frogs, has been used for modeling PV modules as a single diode model. The absolute error between experimental currents and currents given by model parameters is the objective function. Datasheet information has been used for parameter estimation. The results show the superiority of the SFLA over the genetic algorithm (GA).

In Derick et al. (2017), the wind-driven optimisation (WDO) algorithm has been used for parameter estimation of the PV modules. It is inspired from the microscopic air parcels in a multi-dimensional space. RMSE has been chosen as objective of the optimisation problem. A Kyocera-KC215 module has been used as the case study. The simulation results for the parameter estimation of the used PV module illustrate the outperformance of the wind-driven optimisation algorithm over a diverse set of state-of-the-art algorithms, including pattern search, genetic algorithm, simulated annealing, opposition-based teaching learningbased optimisation, artificial bee swarm algorithm, harmony search and flower pollination algorithm. For a more detailed comparison, the relative error, given by different algorithms has been compared. In Louzazni et al. (2016), a leader-based metaheuristic optimisation algorithm, named as firefly algorithm, has been used for parameter estimation of the photovoltaic modules. A Photowatt-PWP201 module has been used as the case study and the simulation results with singlediode model illustrate the outperformance of the firefly algorithm with respect to the Newton-Raphson, pattern search, simulated annealing and genetic algorithm.

In Oliva et al. (2017a), a chaotic artificial bee colony (ABC) algorithm has been proposed for parameter estimation of the PV panels. In the proposed chaotic ABC, the random number in the onlooker bee phase is replaced by a chaos-generated number. A diverse set of chaotic maps have been investigated and the best one, named as Tent map has been used in the proposed chaotic ABC algorithm. The simulation results with both single and double diode models illustrate the superiority of the proposed chaotic ABC over the conventional ABC, a chaotic variant of PSO, artificial bee swarm optimisation algorithm, simulated annealing, cat swarm optimisation algorithm, teaching learning-based optimisation algorithm and harmony search. An RTC-France PV cell, STM6-120/36 as a polycrystalline panel and STM6-40/36 as a monocrystalline PV panel have been used as the case studies.

In Oliva et al. (2017b), a chaotic variant of whale optimisation algorithm (WOA) has been proposed for parameter estimation of the PV cells and panels. WOA takes inspiration from the behavior of whales. In WOA, at each iteration, in the process of updating the position of the whales, a random number in [0,1] is generated and determines the probability of choosing either spiral model or shrinking encircling mechanism. In the proposed chaotic WOA, this randomly generated number is replaced by a chaos-based generated number. Four different chaotic maps including Singer, Sinusoidal, Logistic and Tent maps have been tested and the best one has been chosen for the proposed chaosbased WOA. Singer map proved to be the best map for the parameter estimation problem. The simulation results with both single and double diode models illustrate the superiority of the proposed chaos-based WOA over some state-of-the-art optimisation algorithms such as the ABC, PSO, artificial bee swarm optimisation algorithm, simulated annealing, bird mating optimisation algorithm, differential evolution and harmony search.

In Mughal et al. (2017), the hybrid of PSO and SA has been proposed for estimating parameters of the PV cells. At each iteration of the proposed PSO-SA, in order to exploit the advantages of both algorithms, both the operators of PSO and the operators of SA are applied to the search agents. RMSE has been used as the objective of the optimisation algorithm. The simulation results on a RTC-France PV cell with both double diode and single diode models show that the proposed hybrid algorithm performs better than the PSO, SA, HS and pattern search. In Gong et al. (2017), PSO with changing acceleration coefficients and inertia weight has been used for estimating parameters of the PV modules. In Fathy and Rezk (2017), the imperialistic competitive algorithm (ICA), has been used for estimating the circuit model parameters of the PV modules. Both the single diode and the double diode models have been used and the simulations have been done for different technologies such as mono-crystalline, polycrystalline, thin film and amorphous. The findings show the outperformance of ICA over the pattern search, a chaos-based PSO, bird mating optimisation algorithm, an adaptive DE, artificial bee swarm optimisation, simulated annealing and harmony search.

In Xu and Wang (2017), a hybrid of flower pollination algorithm and Nelder-Mead algorithm has been used for the parameter estimation of PV modules in both the single and double-diode models. The PV's of mono-crystalline, polycrystalline, thin film technologies have been used in the simulations. The proposed algorithm has been validated by comparing with some state-of-the-art optimisation algorithms such as the ABC, PSO, PS, HS and artificial bee swarm optimisation algorithm. In Jordehi (2016c), the PSO with time-varying acceleration coefficients has been used for estimating the parameters of PV cells and modules. In order to develop a suitable trade-off between explorative and exploitative capabilities of the algorithm, the cognitive acceleration coefficient is linearly decreased during the course of the run, while the social acceleration coefficient is linearly increased. In Jordehi (2017), a gravitational search algorithm with linearly decreasing gravitation constant has been proposed for parameter estimation of PV cells and modules, where the simulation results of the proposed GSA outperformed GSA with a fixed gravitation constant and exponentially-

changing gravitation constant.

Other than the described research works, in Ram et al. (2017), an improved variant of the flower pollination algorithm, in Sudhakar and Babu (2016), the fireworks optimisation algorithm and in Rezk and Fathy (2017) the water cycle algorithm have been used for the parameter estimation of PV cells and modules. Although the advantages of metaheuristics with respect to other parameter estimation strategies cannot be denied, they may get stuck in local optima. This issue is called premature convergence and is more accurate in the PV cell parameter estimation problem as a multimodal problem. This is evidenced by relatively high RMSE values in existing applications of metaheuristics to the PV cell parameter estimation problem. A great deal of effort is being put to mitigate premature convergence problem of metaheuristic optimisation algorithms. In this research, an improved variant of particle swarm optimisation (PSO) with a strong explorative capability is used for solving the PV cell parameter estimation problem. At each iteration of the used PSO variant, five successive mutation operators are used to enhance the swarm leader (Jordehi, 2015a, 2014; Rezaee Jordehi and Jasni, 2015). The synergic effect of diverse employed mutation operators has resulted in an efficient PSO variant with a strong explorative capability that efficiently explores different regions of search space and locates promising regions containing the global optimum. In this way, premature convergence problem is alleviated and high quality solutions are achieved in PV cell/module parameter estimation problem.

The rest of the paper is structured as follows; in Section 2, PV cell/module parameter estimation problem is formulated. In Section 3, the proposed methodology is introduced. Results and analysis are provided in the fourth section. Finally, the concluding remarks are put in Section 5.

#### 2. Formulation of the PV parameter estimation problem

In the PV cell parameter estimation problem, model parameters must be found in a way that the circuit provides an I-V characteristic very close to the experimentally measured I-V data of real PV cell (Jordehi, 2016b, 2016c, 2017).

In the single diode model, for every experimental I-V pair  $(V_{m,j},I_{m,j})$ , using  $V_{m,j}$ , the PV cell current is calculated by solving (3) as a nonlinear equation.

$$I_{est,j} = I_{Ph} - I_S \left[ exp \left( \frac{q(V_{m,j} + R_S I_{est,j})}{aKT} \right) - 1 \right] - \frac{V_{m,j} + R_S I_{est,j}}{R_P}$$
(3)

Since in (3), current has not been explicitly expressed as a function of voltage, the equation is solved by Newton-Raphson (Jordehi, 2016c).

In (3),  $I_{ext,j}$  denotes the estimated current of PV cell, i.e. the PV cell current given by the circuit model.

Using (3), the estimated current is determined for all the experimentally measured voltages, then the root mean square error (RMSE) is used to quantify the proximity of the experimentally measured currents and the estimated currents. RMSE is defined by (4) and is used as the objective of the optimisation problem.

$$RMSE = \sqrt{\frac{\sum_{i=1}^{N} (I_{est,j} - I_{m,j})^2}{N}}$$
 (4)

where *N* represents the number of the experimental I-V pairs (Jordehi, 2016b, 2016c, 2017).

In the single diode model, the decision vector of the optimisation problem is represented as (5).

$$X = [I_{Ph}, I_S, a, R_S, R_P]$$

$$\tag{5}$$

In the double diode model, for every experimental I-V pair  $(V_{m,j},I_{m,j})$ , using  $V_{m,j}$ , the PV cell current is calculated by solving (6) as a nonlinear equation.

$$I_{est,j} = I_{Ph} - I_{S_1} \left[ exp \left( \frac{q(V_{m,j} + R_S I_{est,j})}{a_1 K T} \right) - 1 \right] - I_{S_2} \left[ exp \left( \frac{q(V_{m,j} + R_S I_{est,j})}{a_2 K T} \right) - 1 \right] - \frac{V_{m,j} + R_S I_{est,j}}{R_P}$$
(6)

Then, Newton-Raphson is assisted to solve Eq. (6) (Jordehi, 2016c). In (6),  $I_{est,j}$  denotes the estimated current of PV cell, i.e. the PV cell current given by the circuit model.

Using (6), the estimated currents are determined for all the experimentally measured voltages, then RMSE as the objective function of the optimisation problem, is calculated by (4) (Jordehi, 2016c, 2017).

For the double diode model, the decision vector of the optimisation problem is represented as (7).

$$X = [I_{Ph}, I_{S_1}, a_1, I_{S_2}, a_2, R_S, R_P]$$
(7)

#### 3. Enhanced leader PSO

The particle swarm optimisation (PSO) is a well-known swarm-intelligence-based metaheuristic optimisation algorithm. The number of publications on engineering applications of PSO is very huge (Alfi, 2011; Jordehi, 2015b; Zhao et al., 2012; Yucekaya et al., 2009; Yu and Zhang, 2014). Even some other metaheuristic algorithms such as the firefly optimisation algorithm can be considered as variants of PSO. It is a probabilistic, population-based algorithm wherein each search agent is called a particle. The particles collectively attempt to find the position with the least value of objective function to be minimised. In PSO, during the run, each particle memorises its own best experience, i.e. the position with the least objective value among its visited positions. The best position of a particle is called its personal best. Moreover, the best position found by the whole swarm is memorised and referred to as the global best, swarm leader or leader (Shi and Eberhart, 1998). Let's assume that the swarm includes  $N_P$  particles, and denote the position and velocity of i th particle as  $X_i$  and  $V_i$  respectively.

At the beginning, the particles are randomly dispersed in the search space and their initial velocities are set as zero. The objective function is calculated for all particles. Since, this is the first experience of the particles, the position of each particle will also be its personal best. The particle having the least objective value, the global best or swarm leader.

At each iteration, the velocities of particles are updated by Eq. (8).

$$V_i(t+1) = \omega V_i(t) + C_1 r_1 (P_i - X_i) + C_2 r_2 (P_g - X_i)$$
(8)

where t denotes iteration number,  $V_i$  denotes the velocity of i th particle,  $P_i$  and  $P_g$  respectively represent the position of personal best and global best,  $C_1$  and  $C_2$  are respectively named personal acceleration coefficient and social acceleration coefficient,  $\omega$  representss inertia weight. Eventually,  $r_1$  and  $r_2$  are two uniformly generated random numbers in [0,1] (Shi and Eberhart, 1998).

Eq. (8) explicitly shows that the new velocity of each particle is attracted toward its current velocity, its personal best as well as its global best. The contribution of these three vectors in new velocity can be respectively adjusted by  $\omega$ ,  $C_1$  and  $C_2$ .

After updating velocities, the positions of particles are updated by Eq. (9).

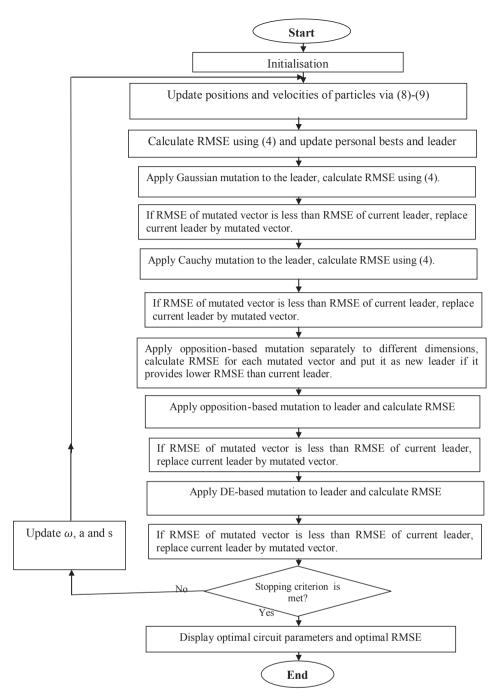
$$X_i(t+1) = X_i(t) + V_i(t+1)$$
(9)

Then, the all particles are re-evaluated and their personal bests and global best are updated.

The process of updating the velocities, positions, personal bests and global best are continued iteration by iteration until stopping criterion is met.

In PSO, due to the following two factors, the premature convergence is likely to happen in multimodal optimisation problems (Jordehi, 2015a, 2014; Rezaee Jordehi and Jasni, 2015). Premature convergence is defined as the convergence of particles to the local optima in lieu of

**Fig. 3.** The flowchart of the application of the ELPSO in the PV cell/module parameter estimation.



the global one.

- Due to the fact that all particles are attracted toward leader, the particles become similar to each other and different regions of search space are not explored efficiently. Weak exploration induces premature convergence.
- After some iterations, as the particles get close to each other, the second and third terms of right hand side of Eq. (8) tend to be zero and particles will have low velocities and will get nearly motionless.
   In this situation, if they stuck in a region with the local optimum, they do not have the capability to jump out from that region. This inherent property of PSO increases premature convergence probability.

In a multimodal optimisation problem, such as the problem considered in this paper, due to existence of multiple optima, premature

convergence is a serious threat that may lead to low-quality solutions. This is evidenced by relatively high values of RMSE in existing research works on the PV cell parameter estimation.

Considering the above-mentioned intrinsic drawbacks of PSO, in Jordehi (2015a), an improved PSO variant, named as enhanced leader PSO (ELPSO) has been developed. In ELPSO, at each iteration, five successive mutation operators are applied to the swarm leader. After applying each mutation, if the mutated  $P_{\rm g}$  has better objective value than the current  $P_{\rm g}$ , it takes the position of current  $P_{\rm g}$ . In this way, the leader is enhanced and pulls all other particles toward better regions in the search space (Jordehi, 2015a).

At the first stage of the mentioned five-staged mutation strategy, a Gaussian mutation is applied to the leader as (10).

$$P_{g1}(d) = P_g(d) + (X_{max}(d) - X_{min}(d))$$
. Gaussian(o,a)ford = 1,2,...,n (10)

where  $X_{\text{max}}(d)$  and  $X_{\text{min}}(d)$  respectively stand for the upper and lower

Table 1
Used ranges of the PV cell parameters in the single diode model (Jordehi, 2016b, 2016c).

| Parameter           | Lower bound | Upper bound |
|---------------------|-------------|-------------|
| I <sub>Ph</sub> (A) | 0           | 1           |
| $I_S$ (A)           | 0           | $10^{-6}$   |
| a                   | 1           | 2           |
| $R_S(\Omega)$       | 0           | 0.5         |
| $R_P(\Omega)$       | 0           | 100         |

bounds of dth decision variable, and a is standard deviation of Gaussian distribution. If the objective value of  $P_{g1}$  is better than that of  $P_{g}$ , then takes the position of  $P_{g}$ . In order to have a decreasing exploration capability during the run, the standard deviation of the Gaussian distribution is linearly decreased during the run.

At the second stage, a Cauchy mutation is used as (11).

$$P_{g2}(d) = P_g(d) + (X_{max}(d) - X_{min}(d))$$
. Cauchy(0,s)ford = 1,2,...,n (11)

where s is a scale parameter of Cauchy distribution which is linearly reduced during the run to have a decreasing explorative capability.

If the mutated vector leads to better objective value than current leader, it takes the position of current leader.

At the third stage, opposition-based mutation is separately applied to all dimensions of  $P_g$  as (12).

$$P_{g3}(d) = X_{min}(d) + X_{max}(d) - P_g(d)$$
(12)

After using (12) for each dimension, the resultant vector is evaluated and if its objective value is less than the objective value of the current leader, it will be the new leader. This means that in this stage, n points are searched in the hope of finding a better leader.

At the fourth stage, opposition-based mutation is applied to the whole  $P_{\nu}$  as (13).

$$P_{g4} = X_{min} + X_{max} - P_g (13)$$

If the mutated vector leads to better objective value, it takes the position of current leader.

At the last stage, DE-based mutation operator is used as (14).

$$P_{g5} = P_g + F(X_e - X_q)$$
 (14)

where e and q are two random unequal particles in swarm and F is a control parameter called scale factor. Again, if the mutated vector leads to better objective value, it takes the position of current leader (Jordehi, 2015a).

The flowchart of the application of the ELPSO to the PV cell parameter estimation problem has been depicted in Fig. 3.

#### 4. Results and analysis

In this section, the results of the application of ELPSO for parameter estimation of three various PV cells/modules PV of different technologies will be presented and analysed. The superior performance of ELPSO is validated by comparing with a couple of state of the art algorithms including conventional PSO (CPSO), artificial bee colony (ABC), genetic algorithm (GA), pattern search (PS), backtracking search algorithm (BSA) and Newton algorithm. RTC France silicon solar cell, STM6-40/36 module with 36 monocrystalline cells and PVM 752 GaAs

thin film cell have been used as the case studies of this research. The parameter estimation is done both for single diode and double diode models. The compared algorithms have been run for 30 times. For CPSO and ELPSO,  $C_1 = C_2 = 2$  and  $\omega$  is linearly decreased from 0.9 to 0.4. For ELPSO, the control parameters have been directly taken from Jordehi (2015a). To make a fair comparison, all the compared algorithms are allocated the same number of function evaluations.

## 4.1. Case study #1: RTC France silicon solar cell at 33 °C and full irradiation

In this subsection, the experimentally measured I-V pairs of RTC France silicon solar cell at 33 °C and full sun (irradiation of  $1000 \ \text{W/m}^2$ ) have been used for estimating the circuit model parameters. The results for single and double diode models are presented below.

#### 4.1.1. Results for case study #1with the single diode model

The results and the analysis of the application of ELPSO and other compared algorithms for the parameter estimation of RTC France PV cell with the single diode model are provided in this subsection. As stated in the problem formulation section, in the single diode model, the number of decision variables (the problem dimension in optimisation problem) is five. In the single diode model, the number of function evaluations (NFE's) allocated for each algorithm is 101,000. The maximum number of iterations is set as 100. The number of individuals for the GA, CPSO and BSA is set as 1000. In the ELPSO, due to the incorporated mutation strategy, the number of function evaluations per iteration is higher than other algorithms. Therefore, to make a fair comparison, in the ELPSO, the number of individuals (particles) must be set lower than other algorithms. To this end, the number of particles in the ELPSO is set as 991. In this way, the number of allocated function evaluations is the same for all used algorithms. Used ranges for the PV cell parameters in single diode model have been tabulated as Table 1. It must be noted here that the above-mentioned ranges of decision variables, number of individuals and maximum number of iterations will be also used for finding the single diode circuit model parameters of the next two case studies.

Table 2 contains the statistics of RMSE values achieved by different algorithms, in 30 runs. This table indicates that in terms of the average of the achieved RMSE values, the ELPSO performs better than the conventional PSO, ABC and other algorithms. In terms of the worst RMSE and standard deviation of achieved RMSE values, ELPSO outperforms all other used algorithms. From the viewpoint of the best achieved RMSE, ELPSO and CPSO outperform all other optimisation algorithms. The best (the most accurate) circuit model parameters achieved by used algorithms have been tabulated as Table 3. Convergence curve of the best run of ELPSO has been plotted as Fig. 4.

In Table 4, for each experimentally measured I-V pair  $(V_{m,j},I_{m,j})$ , the absolute error and relative error of the experimental and estimated currents have been tabulated. The forth column of the table represents the currents calculated by the circuit model parameters of ELPSO. In this table, for jth pair of I-V data, the absolute error and the relative error are respectively calculated by (15) and (16). The error metrics indicate that the estimated currents are in good agreement with the measured currents of the real PV cell.

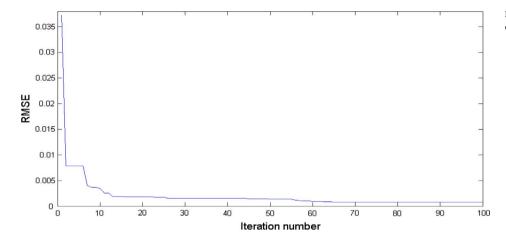
$$AE = |I_{m,j} - I_{est,j}| \tag{15}$$

Table 2
Statistics of the RMSE values, achieved by different optimisation algorithms for the single diode model.

|      | ELPSO       | CPSO (Jordehi, 2016c) | BSA         | ABC       | GA (Jordehi, 2017) | PS (Jordehi, 2016c) | Newton (Easwarakhanthan et al., 1986) |
|------|-------------|-----------------------|-------------|-----------|--------------------|---------------------|---------------------------------------|
| Mean | 7.7314E - 4 | 7.7847E – 4           | 2.7798E - 3 | 0.001089  | 9.8771E - 3        | 2.0502E - 3         | 9.7000E - 3                           |
| Min  | 7.7301E - 4 | 7.7301E – 4           | 1.4436E - 3 | 8.8636E-4 | 4.1020E - 3        | 2.0502E - 3         | 9.7000E - 3                           |
| Max  | 7.7455E - 4 | 9.2832E – 4           | 5.8117E - 3 | 0.0013    | 0.01516            | 2.0502E - 3         | 9.7000E - 3                           |
| Std  | 3.4508E - 7 | 2.8344E – 5           | 9.7202E - 4 | 1.0314E-4 | 2.7197E - 3        | 0                   | 0                                     |

**Table 3**Circuit model parameters for the single diode model, achieved by different optimisation algorithms.

|          | ELPSO       | CPSO (Jordehi, 2016c) | BSA           | ABC         | GA (Jordehi, 2017) | PS (Jordehi, 2016c) | Newton (Easwarakhanthan et al., 1986) |
|----------|-------------|-----------------------|---------------|-------------|--------------------|---------------------|---------------------------------------|
| $I_{Ph}$ | 0.760788    | 0.760788              | 0.761051      | 0.761012    | 0.766535           | 0.760574            | 0.7608                                |
| $I_S$    | 3.106775E-7 | 3.106975E-7           | 4.787662E - 7 | 3.348957E-7 | 7.456099E-7        | 9.809079E-7         | 3.223E - 7                            |
| а        | 1.475256    | 1.475262              | 1.519642      | 1.483057    | 1.570175           | 1.600097            | 0.0364                                |
| $R_S$    | 0.036547    | 0.036547              | 0.034695      | 0.035994    | 0.031438           | 0.031171            | 53.7634                               |
| $R_p$    | 52.889336   | 52.892521             | 79.569251     | 48.784551   | 29.482993          | 100.00              | 1.4837                                |
| RMSE     | 7.7301E-4   | 7.7301E-4             | 1.4436E-3     | 8.8636E-4   | 4.1020E – 3        | 2.0502E - 3         | 9.7000E – 3                           |



**Fig. 4.** The convergence curve of ELPSO for the single diode model at its best run (RMSE = 7.7301E-4).

Table 4
Error metrics for each measurement in the single diode model obtained by ELPSO.

| Number | Voltage | Measured<br>current | Calculated current | Absolute<br>error (AE) | Relative<br>error (RE) |
|--------|---------|---------------------|--------------------|------------------------|------------------------|
| 1      | -0.2057 | 0.7640              | 0.7641             | 0.0001                 | -0.0002                |
| 2      | -0.1291 | 0.7620              | 0.7627             | 0.0007                 | -0.0009                |
| 3      | -0.0588 | 0.7605              | 0.7614             | 0.0009                 | -0.0011                |
| 4      | 0.0057  | 0.7605              | 0.7602             | 0.0003                 | 0.0005                 |
| 5      | 0.0646  | 0.7600              | 0.7590             | 0.0010                 | 0.0013                 |
| 6      | 0.1185  | 0.7590              | 0.7580             | 0.0010                 | 0.0013                 |
| 7      | 0.1678  | 0.7570              | 0.7570             | 0.0000                 | -0.0001                |
| 8      | 0.2132  | 0.7570              | 0.7561             | 0.0009                 | 0.0012                 |
| 9      | 0.2545  | 0.7555              | 0.7550             | 0.0005                 | 0.0006                 |
| 10     | 0.2924  | 0.7540              | 0.7536             | 0.0004                 | 0.0005                 |
| 11     | 0.3269  | 0.7505              | 0.7513             | 0.0008                 | -0.0011                |
| 12     | 0.3585  | 0.7465              | 0.7473             | 0.0008                 | -0.0011                |
| 13     | 0.3873  | 0.7385              | 0.7401             | 0.0016                 | -0.0021                |
| 14     | 0.4137  | 0.7280              | 0.7274             | 0.0006                 | 0.0008                 |
| 15     | 0.4373  | 0.7065              | 0.7070             | 0.0005                 | -0.0007                |
| 16     | 0.4590  | 0.6755              | 0.6754             | 0.0001                 | 0.0001                 |
| 17     | 0.4784  | 0.6320              | 0.6310             | 0.0010                 | 0.0016                 |
| 18     | 0.4960  | 0.5730              | 0.5722             | 0.0008                 | 0.0014                 |
| 19     | 0.5119  | 0.4990              | 0.4995             | 0.0005                 | -0.0011                |
| 20     | 0.5265  | 0.4130              | 0.4135             | 0.0005                 | -0.0012                |
| 21     | 0.5398  | 0.3165              | 0.3172             | 0.0007                 | -0.0021                |
| 22     | 0.5521  | 0.2120              | 0.2120             | 0.0000                 | -0.0001                |
| 23     | 0.5633  | 0.1035              | 0.1026             | 0.0009                 | 0.0083                 |
| 24     | 0.5736  | -0.0100             | -0.0093            | 0.0007                 | 0.0702                 |
| 25     | 0.5833  | -0.1230             | -0.1244            | 0.0014                 | -0.0111                |
| 26     | 0.5900  | -0.2100             | -0.2091            | 0.0009                 | 0.0043                 |

$$RE = \frac{I_{m,j} - I_{est,j}}{I_{m,j}} \tag{16}$$

#### 4.1.2. Results for case study #1 with double diode model

The results and analysis of the application of ELPSO and the other compared algorithms for the parameter estimation of RTC France the PV cell with the double diode model are presented in this subsection. In the double diode model, the number of decision variables or the

 $\begin{tabular}{ll} \textbf{Table 5} \\ \textbf{The ranges of the PV cell parameters in the double diode model (Jordehi, 2016b, 2016c)}. \\ \end{tabular}$ 

| Parameter     | Lower bound | Upper bound |
|---------------|-------------|-------------|
| $I_{Ph}$ (A)  | 0           | 1           |
| $I_{S_1}$ (A) | $10^{-12}$  | $10^{-6}$   |
| $a_1$         | 1           | 2           |
| $I_{S_2}$ (A) | $10^{-12}$  | $10^{-6}$   |
| $a_2$         | 1           | 2           |
| $R_S(\Omega)$ | 0           | 0.5         |
| $R_P(\Omega)$ | 0           | 100         |
|               |             |             |

problem dimension in the optimisation problem is seven. Therefore, in this case, the number of function evaluations (NFE's) allocated for each algorithm is set higher than that for single diode model. The number of function evaluations for each algorithm is set as 151,500. Maximum number of iterations is set as 100. The number of individuals for CPSO, GA and BSA is set as 1500. As stated in the presentation of the results for the single diode model, to make a fair judgment, in ELPSO, the number of search agents must be set lower than other algorithms. To this end, the number of search agents in ELPSO is set as 1489. The ranges used for different PV cell parameters in the double diode model have been tabulated as Table 5. It must be noted here that the abovementioned ranges of the decision variables, number of individuals and maximum number of iterations will be also used for finding the double diode circuit model parameters of the next two case studies.

Table 6 contains statistics of the RMSE values achieved by the used algorithms, in 30 runs. Table 6 clearly shows that in all terms of the average, best, worst and standard deviation of the obtained RMSE values, ELPSO performs better than conventional PSO, ABC and the other algorithms. Such a reduction in the RMSE value(s) is practically significant and this improvement influences practical applications. The best circuit model parameters provided by the used algorithms have been tabulated in Table 7.

In Table 8, based on the best estimated parameters given by ELPSO, for each experimentally measured I-V, the absolute error and relative error of experimental and the estimated currents have been tabulated.

Table 6
Statistics of the RMSE values, achieved by different optimisation algorithms for the double diode model.

|      | ELPSO     | CPSO (Jordehi, 2016c) | BSA         | ABC       | GA (Jordehi, 2017) | PS (Jordehi, 2016c) |
|------|-----------|-----------------------|-------------|-----------|--------------------|---------------------|
| Mean | 7.5904E-4 | 7.902041E – 4         | 2.8606E - 3 | 0.00118   | 8.6115E-3          | 8.1646E-3           |
| Min  | 7.4240E-4 | 7. 4444E-4            | 0.00110851  | 8.0824E-4 | 5.91958E - 3       | 8.1646E-3           |
| Max  | 7.9208E-4 | 0.001220              | 4.6684E - 3 | 0.0016    | 0.014432           | 8.1646E-3           |
| Std  | 9.4291E-6 | 1.0145E-4             | 8.3519E-4   | 1.9721E-4 | 0.001818           | 0                   |

 Table 7

 Circuit model parameters for the double diode model, achieved by different optimisation algorithms.

|          | ELPSO       | CPSO (Jordehi, 2016c) | BSA         | ABC         | GA (Jordehi, 2017) | PS (Jordehi, 2016c) |
|----------|-------------|-----------------------|-------------|-------------|--------------------|---------------------|
| $I_{Ph}$ | 0.760808    | 0.760805              | 0.761617    | 0.760717    | 0.768864           | 0.763353            |
| $I_{s1}$ | 1E - 006    | 9.575723E-7           | 4.163866E-7 | 2.866992E-7 | 6.606207E-7        | 2.86013E-10         |
| $a_1$    | 1.835767    | 1.881069              | 1.505369    | 1.469147    | 1.608739           | 1.000120            |
| $I_{s2}$ | 9.916824E-8 | 1.334501E-7           | 1E - 12     | 2.474846E-7 | 4.551497E-7        | 1E-12               |
| $a_2$    | 1.386091    | 1.407490              | 2           | 1.968374    | 1.628899           | 1.000908            |
| $R_S$    | 0.037551    | 0.037353              | 0.035392    | 0.036659    | 0.029144           | 0.058611            |
| $R_p$    | 55.920471   | 55.441518             | 54.455178   | 58.299556   | 51.116             | 18.210627           |
| RMSE     | 7.4240E-4   | 7.4444E-4             | 0.00110851  | 8.0824E-4   | 5.91958E – 3       | 8.1646E-3           |

Table 8
Error metrics for each measurement in double diode model obtained by ELPSO.

| Number | Voltage | Measured<br>current | Calculated current | Absolute<br>error | Relative error |  |
|--------|---------|---------------------|--------------------|-------------------|----------------|--|
| 1      | -0.2057 | 0.7640              | 0.7640             | 0.0000            | 0.0000         |  |
| 2      | -0.1291 | 0.7620              | 0.7626             | 0.0006            | -0.0008        |  |
| 3      | -0.0588 | 0.7605              | 0.7613             | 0.0008            | -0.0011        |  |
| 4      | 0.0057  | 0.7605              | 0.7602             | 0.0003            | 0.0004         |  |
| 5      | 0.0646  | 0.7600              | 0.7591             | 0.0009            | 0.0011         |  |
| 6      | 0.1185  | 0.7590              | 0.7582             | 0.0008            | 0.0011         |  |
| 7      | 0.1678  | 0.7570              | 0.7572             | 0.0002            | -0.0003        |  |
| 8      | 0.2132  | 0.7570              | 0.7563             | 0.0007            | 0.0010         |  |
| 9      | 0.2545  | 0.7555              | 0.7552             | 0.0003            | 0.0004         |  |
| 10     | 0.2924  | 0.7540              | 0.7537             | 0.0003            | 0.0004         |  |
| 11     | 0.3269  | 0.7505              | 0.7513             | 0.0008            | -0.0011        |  |
| 12     | 0.3585  | 0.7465              | 0.7472             | 0.0007            | -0.0009        |  |
| 13     | 0.3873  | 0.7385              | 0.7399             | 0.0014            | -0.0019        |  |
| 14     | 0.4137  | 0.7280              | 0.7272             | 0.0008            | 0.0011         |  |
| 15     | 0.4373  | 0.7065              | 0.7068             | 0.0003            | -0.0004        |  |
| 16     | 0.4590  | 0.6755              | 0.6753             | 0.0002            | 0.0003         |  |
| 17     | 0.4784  | 0.6320              | 0.6311             | 0.0009            | 0.0015         |  |
| 18     | 0.4960  | 0.5730              | 0.5724             | 0.0006            | 0.0011         |  |
| 19     | 0.5119  | 0.4990              | 0.4997             | 0.0007            | -0.0015        |  |
| 20     | 0.5265  | 0.4130              | 0.4136             | 0.0006            | -0.0015        |  |
| 21     | 0.5398  | 0.3165              | 0.3172             | 0.0007            | -0.0021        |  |
| 22     | 0.5521  | 0.2120              | 0.2119             | 0.0001            | 0.0005         |  |
| 23     | 0.5633  | 0.1035              | 0.1025             | 0.0010            | 0.0100         |  |
| 24     | 0.5736  | -0.0100             | -0.0094            | 0.0006            | 0.0559         |  |
| 25     | 0.5833  | -0.1230             | -0.1244            | 0.0014            | -0.0111        |  |
| 26     | 0.5900  | -0.2100             | -0.2089            | 0.0011            | 0.0051         |  |
|        |         |                     |                    |                   |                |  |

**Table 9**Statistics of RMSE values, achieved by different optimisation algorithms for STM6-40/36 (monocrystalline) at 51 °C and full irradiation with single diode model.

|      | ELPSO       | CPSO        | BSA         | ABC         |
|------|-------------|-------------|-------------|-------------|
| Mean | 2.2503E - 3 | 2.1803E - 3 | 6.0155E - 3 | 3.5460E - 3 |
| Min  | 2.1803E - 3 | 2.1803E - 3 | 3.6289E - 3 | 2.3977E - 3 |
| Max  | 3.7160E - 3 | 2.1803e - 3 | 9.4360E - 3 | 5.6195E - 3 |
| Std  | 2.9211E - 4 | 6.3747E - 9 | 1.4603E - 3 | 7.7909e - 4 |

**Table 10**Circuit model parameters STM6-40/36 at 51 °C and full irradiation, for single diode model, achieved by different optimisation algorithms.

|  | ELPSO   | CPSO  | BSA  | ABC   |
|--|---|---|--|---|
| I <sub>Ph</sub> I <sub>s</sub> A R <sub>S</sub> R <sub>p</sub> | 1.666268<br>4.596141E – 7<br>50.458643<br>0.5<br>497.747315 | 1.666268<br>4.596154E - 7<br>50.458652<br>0.5<br>497.748669 | 1.659404<br>6.335228e - 7<br>51.762752<br>0.527342<br>723.391770 | 1.667181<br>4.656705E - 7<br>50.475178<br>0.5<br>495.520578 |
| RMSE   | 2.1803E-3   | 2.1803E-3   | 3.6289E-3  | 2.3977E-3   |

Table 11 Error metrics for each measurement in single diode model obtained by ELPSO for STM6-40/36 module at  $51\,^{\circ}$ C and irradiation of  $1000\,$ W/m².

| Number | Voltage (V)<br>(Oliva et al.,<br>2017b) | Current (A)<br>(Oliva et al.,<br>2017b) | Calculated<br>current (A) | Absolute<br>error (AE) | Relative<br>error (RE) |
|--------|---|---|---------------------------|------------------------|------------------------|
| 1      | 0.1180                                  | 1.6630                                  | 1.6644                    | 0.0014                 | -0.0008                |
| 2      | 2.2370                                  | 1.6610                                  | 1.6601                    | 0.0009                 | 0.0005                 |
| 3      | 5.4340                                  | 1.6530                                  | 1.6537                    | 0.0007                 | -0.0004                |
| 4      | 7.2600                                  | 1.6500                                  | 1.6499                    | 0.0001                 | 0.0001                 |
| 5      | 9.6800                                  | 1.6450                                  | 1.6444                    | 0.0006                 | 0.0004                 |
| 6      | 11.5900                                 | 1.6400                                  | 1.6383                    | 0.0017                 | 0.0010                 |
| 7      | 12.6000                                 | 1.6360                                  | 1.6331                    | 0.0029                 | 0.0018                 |
| 8      | 13.3700                                 | 1.6290                                  | 1.6271                    | 0.0019                 | 0.0011                 |
| 9      | 14.0900                                 | 1.6190                                  | 1.6187                    | 0.0003                 | 0.0002                 |
| 10     | 14.8800                                 | 1.5970                                  | 1.6040                    | 0.0070                 | -0.0044                |
| 11     | 15.5900                                 | 1.5810                                  | 1.5829                    | 0.0019                 | -0.0012                |
| 12     | 16.4000                                 | 1.5420                                  | 1.5434                    | 0.0014                 | -0.0009                |
| 13     | 16.7100                                 | 1.5240                                  | 1.5219                    | 0.0021                 | 0.0014                 |
| 14     | 16.9800                                 | 1.5000                                  | 1.4994                    | 0.0006                 | 0.0004                 |
| 15     | 17.1300                                 | 1.4850                                  | 1.4852                    | 0.0002                 | -0.0001                |
| 16     | 17.3200                                 | 1.4650                                  | 1.4651                    | 0.0001                 | -0.0000                |
| 17     | 17.9100                                 | 1.3880                                  | 1.3854                    | 0.0026                 | 0.0019                 |
| 18     | 19.0800                                 | 1.1180                                  | 1.1191                    | 0.0011                 | -0.0010                |

 $\begin{tabular}{ll} \textbf{Table 12} \\ \textbf{Statistics of RMSE values, achieved by different optimisation algorithms for STM6-40/36} \\ \textbf{(monocrystalline) at 51 °C and full irradiation with double diode model.} \\ \end{tabular}$ 

|      | ELPSO       | CPSO          | BSA          | ABC         |
|------|-------------|---------------|--------------|-------------|
| Mean | 2.0351E - 3 | 2.0536E - 3   | 6.6880E - 3  | 3.4274E - 3 |
| Min  | 1.8307E - 3 | 1.8343E - 3   | 4.0335E - 3  | 2.0538E - 3 |
| Max  | 2.1178E - 3 | 2.4820E - 3   | 9.1132E - 3  | 5.3626E - 3 |
| Std  | 8.4271E - 5 | 1.3007E - 004 | 1.46600E - 3 | 8.1672E - 4 |

 $\begin{tabular}{ll} \textbf{Table 13} \\ \textbf{Circuit model parameters STM6-40/36 at 51 °C and full irradiation, for double diode model, achieved by different optimisation algorithms.} \end{tabular}$ 

|          | ELPSO       | CPSO        | BSA         | ABC         |
|----------|-------------|-------------|-------------|-------------|
| $I_{Ph}$ | 1.664843    | 1.664746    | 1.661112    | 1.663472    |
| $I_{s1}$ | 1.670160E-8 | 2.529140E-8 | 1.198529E-6 | 8.937775E-6 |
| $a_1$    | 41.993481   | 42.816947   | 100         | 71.464981   |
| $I_{s2}$ | 6.210924E-6 | 8.779822E-6 | 8.916770E-7 | 1E - 12     |
| $a_2$    | 67.344124   | 70.734863   | 52.874278   | 27.790714   |
| $R_S$    | 0.500000    | 0.500000    | 0.500000    | 1.236435    |
| $R_p$    | 606.888301  | 611.747136  | 924.813027  | 938.209991  |
| RMSE     | 1.8307E - 3 | 1.8343E - 3 | 4.0335E - 3 | 2.0538E - 3 |

Table 14 Error metrics for each measurement in double diode model obtained by ELPSO for STM6-40/36 module at  $51\,^{\circ}$ C and irradiation of  $1000\,$ W/m² (Oliva et al., 2017b).

| Number | Voltage (V) | Current (A) | Calculated<br>current (A) | Absolute<br>error (AE) | Relative<br>error (RE) |
|--------|-------------|-------------|---------------------------|------------------------|------------------------|
| 1      | 0.1180      | 1.6630      | 1.6633                    | 0.0003                 | -0.0002                |
| 2      | 2.2370      | 1.6610      | 1.6598                    | 0.0012                 | 0.0007                 |
| 3      | 5.4340      | 1.6530      | 1.6544                    | 0.0014                 | -0.0008                |
| 4      | 7.2600      | 1.6500      | 1.6511                    | 0.0011                 | -0.0006                |
| 5      | 9.6800      | 1.6450      | 1.6458                    | 0.0008                 | -0.0005                |
| 6      | 11.5900     | 1.6400      | 1.6392                    | 0.0008                 | 0.0005                 |
| 7      | 12.6000     | 1.6360      | 1.6335                    | 0.0025                 | 0.0015                 |
| 8      | 13.3700     | 1.6290      | 1.6270                    | 0.0020                 | 0.0012                 |
| 9      | 14.0900     | 1.6190      | 1.6180                    | 0.0010                 | 0.0006                 |
| 10     | 14.8800     | 1.5970      | 1.6029                    | 0.0059                 | -0.0037                |
| 11     | 15.5900     | 1.5810      | 1.5817                    | 0.0007                 | -0.0004                |
| 12     | 16.4000     | 1.5420      | 1.5428                    | 0.0008                 | -0.0005                |
| 13     | 16.7100     | 1.5240      | 1.5217                    | 0.0023                 | 0.0015                 |
| 14     | 16.9800     | 1.5000      | 1.4996                    | 0.0004                 | 0.0002                 |
| 15     | 17.1300     | 1.4850      | 1.4856                    | 0.0006                 | -0.0004                |
| 16     | 17.3200     | 1.4650      | 1.4659                    | 0.0009                 | -0.0006                |
| 17     | 17.9100     | 1.3880      | 1.3871                    | 0.0009                 | 0.0006                 |
| 18     | 19.0800     | 1.1180      | 1.1182                    | 0.0002                 | -0.0002                |

Table 15 Statistics of RMSE values, achieved by different optimisation algorithms for PVM 752 GaAs thin film cell at  $25\,^{\circ}\text{C}$  and full irradiation with single diode model.

|      | ELPSO       | CPSO        | BSA         | ABC         |
|------|-------------|-------------|-------------|-------------|
| Mean | 2.5400E - 2 | 2.5400E - 2 | 3.5990E - 3 | 2.1113E - 3 |
| Min  | 2.5400E - 2 | 2.5400E - 2 | 2.1469E - 3 | 2.0412E - 3 |
| Max  | 2.5400E - 2 | 2.5400E - 2 | 1.0997E - 2 | 2.2427E - 3 |
| Std  | 0           | 0           | 2.2240E - 3 | 5.3438E - 5 |

**Table 16**Circuit model parameters PVM 752 GaAs thin film cell at 25 °C and full irradiation, for single diode model, achieved by different optimisation algorithms.

|          | ELPSO     | CPSO      | BSA          | ABC            |
|----------|-----------|-----------|--------------|----------------|
| $I_{Ph}$ | 0.115016  | 0.116530  | 0.103903     | 0.103312       |
| $I_S$    | 0         | 0         | 8.490000E-11 | 3.200000E - 11 |
| A        | 1.768590  | 1.617093  | 1.858574     | 1.774159       |
| $R_S$    | 0.159052  | 0.346578  | 0.5          | 0.5            |
| $R_p$    | 14.429507 | 14.241982 | 100          | 100            |
| RMSE     | 2.5400E-2 | 2.5400E-2 | 2.1469E-3    | 2.0412E-3      |
|          |           |           |              |                |

The error metrics signify that the estimated currents are in good agreement with the measured currents of real PV cell.

## 4.2. Results for case study #2: STM6-40/36 module at $51^{\circ}$ C and full irradiation

STM6-40/36, manufactured by Schutten Solar, with 36 monocrystalline cells (of size  $38 \text{ mm} \times 128 \text{ mm}$ ) aligned in series, has been

Table 17 Error metrics for each measurement in single diode model obtained by ELPSO for PVM 752 GaAs thin film cell at 25  $^{\circ}$ C and irradiation of 1000 W/m<sup>2</sup>.

| Number | Voltage (V) | Measured<br>current (A) | Calculated<br>current (A) | Absolute<br>error (AE) | Relative<br>error (RE) |
|--------|-------------|-------------------------|---------------------------|------------------------|------------------------|
| 1      | -0.1659     | 0.1001                  | 0.1251                    | 0.0250                 | -0.2501                |
| 2      | -0.1281     | 0.1000                  | 0.1225                    | 0.0225                 | -0.2254                |
| 3      | -0.0888     | 0.0999                  | 0.1198                    | 0.0199                 | -0.1997                |
| 4      | -0.0490     | 0.0999                  | 0.1171                    | 0.0172                 | -0.1724                |
| 5      | -0.0102     | 0.0999                  | 0.1145                    | 0.0146                 | -0.1458                |
| 6      | 0.0275      | 0.0998                  | 0.1119                    | 0.0121                 | -0.1210                |
| 7      | 0.0695      | 0.0999                  | 0.1090                    | 0.0091                 | -0.0911                |
| 8      | 0.1061      | 0.0998                  | 0.1065                    | 0.0067                 | -0.0670                |
| 9      | 0.1460      | 0.0998                  | 0.1038                    | 0.0040                 | -0.0396                |
| 10     | 0.1828      | 0.0997                  | 0.1012                    | 0.0015                 | -0.0154                |
| 11     | 0.2230      | 0.0997                  | 0.0985                    | 0.0012                 | 0.0123                 |
| 12     | 0.2600      | 0.0996                  | 0.0959                    | 0.0037                 | 0.0367                 |
| 13     | 0.3001      | 0.0997                  | 0.0932                    | 0.0065                 | 0.0653                 |
| 14     | 0.3406      | 0.0996                  | 0.0904                    | 0.0092                 | 0.0922                 |
| 15     | 0.3789      | 0.0995                  | 0.0878                    | 0.0117                 | 0.1177                 |
| 16     | 0.4168      | 0.0994                  | 0.0852                    | 0.0142                 | 0.1429                 |
| 17     | 0.4583      | 0.0994                  | 0.0823                    | 0.0171                 | 0.1716                 |
| 18     | 0.4949      | 0.0993                  | 0.0798                    | 0.0195                 | 0.1960                 |
| 19     | 0.5370      | 0.0993                  | 0.0770                    | 0.0223                 | 0.2251                 |
| 20     | 0.5753      | 0.0992                  | 0.0743                    | 0.0249                 | 0.2507                 |
| 21     | 0.6123      | 0.0990                  | 0.0718                    | 0.0272                 | 0.2748                 |
| 22     | 0.6546      | 0.0988                  | 0.0689                    | 0.0299                 | 0.3027                 |
| 23     | 0.6918      | 0.0983                  | 0.0663                    | 0.0320                 | 0.3251                 |
| 24     | 0.7318      | 0.0977                  | 0.0636                    | 0.0341                 | 0.3490                 |
| 25     | 0.7702      | 0.0963                  | 0.0610                    | 0.0353                 | 0.3669                 |
| 26     | 0.8053      | 0.0937                  | 0.0586                    | 0.0351                 | 0.3750                 |
| 27     | 0.8329      | 0.0900                  | 0.0567                    | 0.0333                 | 0.3703                 |
| 28     | 0.8550      | 0.0855                  | 0.0552                    | 0.0303                 | 0.3549                 |
| 29     | 0.8738      | 0.0799                  | 0.0539                    | 0.0260                 | 0.3258                 |
| 30     | 0.8887      | 0.0743                  | 0.0528                    | 0.0215                 | 0.2888                 |
| 31     | 0.9016      | 0.0683                  | 0.0520                    | 0.0163                 | 0.2392                 |
| 32     | 0.9141      | 0.0618                  | 0.0511                    | 0.0107                 | 0.1731                 |
| 33     | 0.9248      | 0.0555                  | 0.0504                    | 0.0051                 | 0.0924                 |
| 34     | 0.9344      | 0.0493                  | 0.0497                    | 0.0004                 | -0.0084                |
| 35     | 0.9445      | 0.0422                  | 0.0490                    | 0.0068                 | -0.1616                |
| 36     | 0.9533      | 0.0357                  | 0.0484                    | 0.0127                 | -0.3562                |
| 37     | 0.9618      | 0.0291                  | 0.0478                    | 0.0187                 | -0.6438                |
| 38     | 0.9702      | 0.0222                  | 0.0473                    | 0.0251                 | -1.1287                |
| 39     | 0.9778      | 0.0157                  | 0.0467                    | 0.0310                 | -1.9769                |
| 40     | 0.9852      | 0.0092                  | 0.0462                    | 0.0370                 | -4.0250                |
| 41     | 0.9926      | 0.0026                  | 0.0457                    | 0.0431                 | -16.5855               |
| 42     | 0.9999      | -0.0040                 | 0.0452                    | 0.0492                 | 12.3055                |
| 43     | 1.0046      | -0.0085                 | 0.0449                    | 0.0534                 | 6.2823                 |
| 44     | 1.0089      | -0.0124                 | 0.0446                    | 0.0570                 | 4.5972                 |

Table 18 Statistics of RMSE values, achieved by different optimisation algorithms for PVM 752 GaAs thin film cell at  $25\,^{\circ}\text{C}$  and full irradiation with double diode model.

|      | ELPSO       | CPSO        | BSA         | ABC         |
|------|-------------|-------------|-------------|-------------|
| Mean | 0.002304    | 0.002320    | 0.002447    | 0.002197    |
| Min  | 0.002075    | 0.002303    | 0.002178    | 0.002044    |
| Max  | 0.0024309   | 0.0024309   | 0.0027557   | 0.0023260   |
| Std  | 5.4011E - 5 | 4.4174E - 5 | 1.2436E – 4 | 7.0060E - 5 |

used as the second case study of this research. The experimental data has been extracted at T = 51 °C and full irradiation (Oliva et al., 2017b). The findings of parameter estimation for this module can be found as Tables 9–14. For the single diode model, from the perspective of the best achieved RMSE in 30 runs, the ELPSO and CPSO surpass the other used algorithms, while from the perspective of the mean of the achieved RMSE values in 30 runs, the CPSO surpasses all other algorithms. Table 11 includes the error metrics, resulted by parameter estimation for single diode model with the ELPSO and Table 14 includes the error metrics, resulted for double diode model with ELPSO. Tables 12 and 13 testify that in the case of double diode model, the ELPSO surpasses all other algorithms, either in the terms of the best achieved

**Table 19**Circuit model parameters PVM 752 GaAs thin film cell at 25° C and full irradiation, for double diode model, achieved by different optimisation algorithms.

|          | ELPSO          | CPSO           | BSA            | ABC            |
|----------|----------------|----------------|----------------|----------------|
| $I_{Ph}$ | 0.103192       | 0.102688       | 0.102497       | 0.103252       |
| $I_{s1}$ | 1.775000e - 10 | 1.000000E - 12 | 1.000000E - 12 | 4.000000E - 11 |
| $a_1$    | 2.000000       | 1.572718       | 1.635590       | 1.792987       |
| $I_{s2}$ | 1.000000E - 12 | 1.000000E - 12 | 8.060000E - 11 | 1.000000E - 12 |
| $a_2$    | 1.571052       | 1.572718       | 1.874265       | 2.000000       |
| $R_S$    | 0.500000       | 0.500000       | 0.500000       | 0.500000       |
| $R_p$    | 100.000000     | 100.000000     | 100.000000     | 100.000000     |
| RMSE     | 0.002075       | 0.002303       | 0.002178       | 0.002044       |

Table 20 Error metrics for each measurement in double diode model obtained by ELPSO for PVM 752 GaAs thin film cell at 25  $^{\circ}$ C and irradiation of 1000 W/m<sup>2</sup>.

|        | mber Voltage (V) Measured Calculated Absolute Relative |             |             |            | D 1 .:     |
|--------|--|-------------|-------------|------------|------------|
| Number | Voltage (V)  | Measured    |             |            | Relative   |
|        |  | current (A) | current (A) | error (AE) | error (RE) |
| 1      | -0.1659  | 0.1001      | 0.1043      | 0.0042     | -0.0422    |
| 2      | -0.1281  | 0.1000      | 0.1040      | 0.0040     | -0.0395    |
| 3      | -0.0888  | 0.0999      | 0.1036      | 0.0037     | -0.0367    |
| 4      | -0.0490  | 0.0999      | 0.1032      | 0.0033     | -0.0327    |
| 5      | -0.0102  | 0.0999      | 0.1028      | 0.0029     | -0.0288    |
| 6      | 0.0275   | 0.0998      | 0.1024      | 0.0026     | -0.0261    |
| 7      | 0.0695   | 0.0999      | 0.1020      | 0.0021     | -0.0209    |
| 8      | 0.1061   | 0.0998      | 0.1016      | 0.0018     | -0.0183    |
| 9      | 0.1460   | 0.0998      | 0.1012      | 0.0014     | -0.0143    |
| 10     | 0.1828   | 0.0997      | 0.1009      | 0.0012     | -0.0116    |
| 11     | 0.2230   | 0.0997      | 0.1005      | 0.0008     | -0.0076    |
| 12     | 0.2600   | 0.0996      | 0.1001      | 0.0005     | -0.0049    |
| 13     | 0.3001   | 0.0997      | 0.0997      | 0.0000     | 0.0001     |
| 14     | 0.3406   | 0.0996      | 0.0993      | 0.0003     | 0.0031     |
| 15     | 0.3789   | 0.0995      | 0.0989      | 0.0006     | 0.0060     |
| 16     | 0.4168   | 0.0994      | 0.0985      | 0.0009     | 0.0088     |
| 17     | 0.4583   | 0.0994      | 0.0981      | 0.0013     | 0.0129     |
| 18     | 0.4949   | 0.0993      | 0.0977      | 0.0016     | 0.0156     |
| 19     | 0.5370   | 0.0993      | 0.0973      | 0.0020     | 0.0200     |
| 20     | 0.5753   | 0.0992      | 0.0969      | 0.0023     | 0.0230     |
| 21     | 0.6123   | 0.0990      | 0.0965      | 0.0025     | 0.0252     |
| 22     | 0.6546   | 0.0988      | 0.0960      | 0.0028     | 0.0285     |
| 23     | 0.6918   | 0.0983      | 0.0954      | 0.0029     | 0.0295     |
| 24     | 0.7318   | 0.0977      | 0.0945      | 0.0032     | 0.0328     |
| 25     | 0.7702   | 0.0963      | 0.0930      | 0.0033     | 0.0339     |
| 26     | 0.8053   | 0.0937      | 0.0906      | 0.0031     | 0.0328     |
| 27     | 0.8329   | 0.0900      | 0.0874      | 0.0026     | 0.0293     |
| 28     | 0.8550   | 0.0855      | 0.0833      | 0.0022     | 0.0252     |
| 29     | 0.8738   | 0.0799      | 0.0786      | 0.0013     | 0.0168     |
| 30     | 0.8887   | 0.0743      | 0.0736      | 0.0007     | 0.0089     |
| 31     | 0.9016   | 0.0683      | 0.0684      | 0.0001     | -0.0019    |
| 32     | 0.9141   | 0.0618      | 0.0625      | 0.0007     | -0.0108    |
| 33     | 0.9248   | 0.0555      | 0.0566      | 0.0011     | -0.0197    |
| 34     | 0.9344   | 0.0493      | 0.0507      | 0.0014     | -0.0284    |
| 35     | 0.9445   | 0.0422      | 0.0438      | 0.0016     | -0.0391    |
| 36     | 0.9533   | 0.0357      | 0.0373      | 0.0016     | -0.0458    |
| 37     | 0.9618   | 0.0291      | 0.0306      | 0.0015     | -0.0506    |
| 38     | 0.9702   | 0.0222      | 0.0234      | 0.0012     | -0.0557    |
| 39     | 0.9778   | 0.0157      | 0.0166      | 0.0009     | -0.0576    |
| 40     | 0.9852   | 0.0092      | 0.0096      | 0.0004     | -0.0457    |
| 41     | 0.9926   | 0.0026      | 0.0023      | 0.0003     | 0.1077     |
| 42     | 0.9999   | -0.0040     | -0.0052     | 0.0012     | -0.2951    |
| 43     | 1.0046   | -0.0085     | -0.0102     | 0.0017     | -0.1954    |
| 44     | 1.0089   | -0.0124     | -0.0148     | 0.0024     | -0.1949    |
|        |  |             |             |            |            |

RMSE or in the terms of the mean of achieved RMSE values. As expected, the RMSE values, given by the double-diode model are lower than those, given by single diode model.

## 4.3. Results for case study #2: PVM 752 GaAs cell at 25 °C and full irradiation

PVM 752 GaAs thin film cell, has been used as the third case study

of this research. The experimental data, including 44 pairs of I-V points has been extracted at T = 25 °C and full irradiation and was kindly provided by the national renewable energy laboratory (NREL). The findings of parameter estimation for this cell can be viewed as Tables 15-20. As per Tables 15 and 16, for the single diode model, the ABC surpasses the other used algorithms. Table 17 includes the error metrics, resulted by parameter estimation for the single diode model with ELPSO and Table 20 includes the error metrics, resulted for the double diode model with ELPSO. Tables 18 and 19 prove that in the case of the double diode model, the ABC and ELPSO surpass other algorithms, both in the terms of the best achieved RMSE and the mean of the achieved RMSE values. Comparing Tables 15-20 with results of RTC France cell and STM6-40/36 module indicate that due to the huge number of I-V pairs, estimating parameters of PVM 752 GaAs cell is more challenging for optimisation algorithms. For instance, the best RMSE, achieved by the ELPSO, in single diode model is as high as 0.0254. Comparing the results of the single diode model and double diode model indicates that, the RMSE values, given by the double-diode model are lower than those, given by the single diode model.

#### 5. Conclusions

The PV cell/module parameter estimation is considered as a multimodal optimisation problem with multiple local optima. In such multimodal problems, metaheuristic algorithms, due to their premature convergence problem, are likely to converge into local optima in lieu of the global one. PSO is a popular metaheuristic optimisation algorithm. In this research, in an attempt to mitigate premature convergence, an improved PSO variant, named as enhanced leader PSO (ELPSO), has been used for solving the PV cell/module parameter estimation problem. At each iteration of the ELPSO, the leader is enhanced by five successive mutation operators. The enhanced leader may attract other particles toward better regions of search space and thereby the premature convergence problem is mitigated. An RTC France silicon solar cell, STM6-40/36 module with 36 monocrystalline cells and PVM 752 GaAs thin film cell have been used as the case studies of this research. The findings show that in RTC France silicon solar cell and STM6-40/36 module, the ELPSO surpasses all the other compared algorithms including the CPSO, GA, ABC, BSA, PS and Newton. In the PVM 752 GaAs cell, the ELPSO surpasses the conventional PSO, although the ABC outperforms all the compared algorithms.

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