

**ENERGY HARVESTING BY EXPLOITING VORTEX-INDUCED VIBRATION
FROM A MODIFIED CRUCIFORM STRUCTURE**

AHMAD ADZLAN FADZLI BIN KHAIRI

UNIVERSITI TEKNOLOGI MALAYSIA

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ENERGY HARVESTING BY EXPLOITING VORTEX-INDUCED VIBRATION
FROM A MODIFIED CRUCIFORM STRUCTURE

AHMAD ADZLAN FADZLI BIN KHAIRI

A thesis submitted in fulfilment of the
requirements for the award of the degree of
Doctor of Philosophy

Malaysia-Japan International Institute of Technology
Universiti Teknologi Malaysia

SEPTEMBER 2021

DECLARATION

I declare that this thesis entitled "*Energy Harvesting by Exploiting Vortex-induced Vibration from a Modified Cruciform Structure*" is the result of my own research except as cited in the references. The thesis has not been accepted for any degree and is not concurrently submitted in candidature of any other degree.

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DEDICATION

My dearest wife and children. Respected supervisor and colleagues at the WEE
iKohza. This is for all of you.

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I would like to first express my highest sense of gratitude to my supervisor Dr. Mohamed Sukri Mat Ali. His knowledge and proficiency in computational fluid dynamics have made my entry into this field of study a little bit more bearable and has since been an excellent tool in making novel discoveries and conclusions. His open stance in receiving ideas and suggestions to strengthen the foundations of this research has been fundamental to the preservation of the originality and timeliness of this work. I have learned a lot from him about the value of logical continuity and how to achieve it throughout the course of completing this work. The relentless effort for logical continuity throughout the thesis has been, in my opinion, crucial towards a manuscript that not only is easily accessible but helps target audiences to build upon this work in the future, hence advancing the field as a whole.

As for my beloved family, especially my wife and two babies, I really cannot think of any way to repay your hardships and understanding throughout the years of my study. Even a lifetime of unconditional love and devotion towards all of you squares only but a small fraction of what you have given up making my studies a reality. To that end I can only trust the Most Merciful to fully even the debt and make all of you among those who are most beloved by the Most Gracious. I pray to the Almighty to accept the fruit of our jihad in finding knowledge and may all the trials and tribulations we have encountered together, physically, psychologically and financially, will stand witness in the hereafter that we have answered His call towards submission, and His call towards success. Aamin ya Rabbal 'alamin.

ABSTRACT

From off-grid charging of electronic devices to energising independent wireless sensor networks, the demand for stand-alone, low-power generators from renewable energy sources is becoming more prevalent. A cruciform energy harvester has been shown to output consistent power in the order of 1 mW when the reduced velocity U^* , exceeds 15. However, this output is insufficient and its onset too late for real-world applications. Thus, this study seeks to remedy these two shortcomings by investigating cruciforms oscillators at various cruciform angles. To fulfill these goals, the Reynolds-Averaged Navier-Stokes simulation were performed, and the results for the 90° cruciform were compared against experimental data for validation. The experiment uses a similar 90° cruciform in an open flow channel. Assessments were made on the vibration amplitude, frequency, lift amplitude and lift frequency at cruciform angles 90°, 67.5°, 45°, 22.5° and 0°. The Reynolds number range was $1.1 \times 10^3 \leq Re \leq 14.6 \times 10^3$ and Scruton number 9.94, which was consistent with similar studies. Hilbert-Huang analysis of the 90° cruciform indicated that a lot of energy from the free stream was wasted in the production of non-performing Karman vortices. A larger lift was possible if streamwise vortices were produced instead. When $45 \leq \alpha(^{\circ}) \leq 67.5$, asymmetries in the vortical structures prevented high-amplitude vibrations from taking place. However, when $0 \leq \alpha(^{\circ}) \leq 22.5$, a high-degree of symmetry among the vortical structures led to an early onset of high-amplitude vibration. Power generated by the cruciform was in the order of 1 mW for a 90° cruciform, below 1 mW when $45 \leq \alpha(^{\circ}) \leq 67.5$, and in the order of 10 mW when $0 \leq \alpha(^{\circ}) \leq 22.5$. Unification of the power generation and energy harvesting efficiency results produced a map that describes the power and efficiency of the harvester in the $\alpha(^{\circ}) - U^*$ parameter space. This uncovers three distinct regions of power generation: pure cruciform region as cruciform angle tends to 90°, steep-angle region between $45 \leq \alpha(^{\circ}) \leq 67.5$, and shallow-angle region between $0 \leq \alpha(^{\circ}) \leq 22.5$. Maximum efficiency occurs close to 0.8 m/s when cruciform angle is 90°, close to 0.2 m/s at 67.5°, and close to 0.4 m/s at 0°. This power and efficiency map makes it possible for future engineers to tailor the design of their cruciform energy harvester to their specific power and efficiency needs.

ABSTRAK

Daripada pengecasan peranti elektronik di luar grid sehingga pentenagaan rangkaian sensor tanpa wayar, permintaan untuk sistem janakuasa berskala kecil dari sumber tenaga boleh diperbaharui adalah semakin meningkat. Sebuah pemungut tenaga krusiform menghasilkan kuasa sekitar 1mW apabila halaju terturun U^* lebih besar daripada 15. Walau bagaimanapun, output ini tidak mencukupi dan permulaannya terlalu lewat untuk aplikasi dunia sebenar. Kajian ini bertujuan untuk mengatasi dua masalah tersebut dengan menyelidik pengayun krusiform pada sudut krusiform yang pelbagai. Simulasi Navier-Stokes Purata-Reynolds telah dijalankan, dan data dari krusiform 90° telah dibandingkan dengan data eksperimen untuk pengesahan. Eksperimen tersebut juga menggunakan krusiform 90° dalam sebuah kanal aliran terbuka. Penilaian dijalankan terhadap amplitud getaran, frekuensi, serta amplitud dan frekuensi daya angkat pada sudut krusiform 90° , 67.5° , 45° , 22.5° dan 0° . Nombor Reynolds adalah $1.1 \times 10^3 \leq Re \leq 14.6 \times 10^3$, manakala nombor Scruton adalah 9.94. Analisis Hilbert-Huang pada sudut 90° menunjukkan terdapat banyak tenaga yang terbazir dalam menghasilkan vortex Karman. Daya angkat yang lebih besar boleh diperoleh sekiranya vorteks arus yang dihasilkan. Pada sudut $45^\circ \leq \alpha (\text{ }^\circ) \leq 67.5$, asimetri pada struktur vortex menghalang penjanaan amplitud getaran yang tinggi. Walau bagaimanapun, apabila $0^\circ \leq \alpha (\text{ }^\circ) \leq 22.5$, simetri yang tinggi pada struktur vorteks menyebabkan getaran amplitud tinggi bermula lebih awal. Penyatuan data output kuasa dan kecekapan menghasilkan peta output kuasa dan kecekapan dalam ruang parameter $\alpha (\text{ }^\circ) - U^*$. Ini membawa kepada penemuan tiga rantau penjanaan kuasa: rantau krusiform asli apabila sudut krusiform menghampiri 90° , krusiform curam apabila $45^\circ \leq \alpha (\text{ }^\circ) \leq 67.5$, dan krusiform cetek apabila $0^\circ \leq \alpha (\text{ }^\circ) \leq 22.5$. Kecekapan maksimum terhasil sekitar 0.8 m/s dan sudut krusiform 90° , sekitar 0.2 m/s pada 67.5° dan sekitar 0.4 m/s pada 0° . Peta kuasa dan kecekapan ini membolehkan jurutera masa hadapan mengubahsuai pemungut tenaga krusiform mereka mengikut keperluan kuasa dan kecekapan yang diperlukan.

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LIST OF ABBREVIATIONS

3D	-	Three-dimensional
ACMI	-	Arbitrarily Coupled Mesh Interface
CFD	-	Computational Fluid Mechanics
CFL	-	Courant-Friedrichs-Lowy
DKSGS	-	Dynamic k-equation Subgrid-scale
DNS	-	Direct Numerical Simulation
EMD	-	Empirical Mode Decomposition
EEMD	-	Ensemble Empirical Mode Decomposition
FIV	-	Fluid-induced Vibration
FSI	-	Fluid-structure Interaction
GAMG	-	Geometric-Algebraic Multi Grid
GCI	-	Grid Convergence Index
HT	-	Hilbert Transform
HHT	-	Hilber-Huang Transform
ICT	-	Information and Communications Technology
IF	-	Intrinsic Function
KVIV	-	Karman Vortex-induced Vibration
MD	-	Molecular Dynamics
PISO	-	Pressure-Implicit with Splitting Operators
PIMPLE	-	PISO-stabilised SIMPLE
PIV	-	Particle Image Velocimetry
POD	-	Proper Orthogonal Decomposition
PTC	-	Passive Turbulence Control
PV	-	Cauchy Principal Value
SIMPLE	-	Semi-implicit Method for Pressure Linked Equations
SVIV	-	Streamwise Vortex-induced Vibration
TrSL	-	Transition in Shear Layer

URANS	-	Unsteady Reynolds Averaged Navier-Stokes
VIV	-	Vortex-induced Vibration

LIST OF SYMBOLS

$a(t)$	-	Instantaneous amplitude
C_l	-	Lift coefficient
C_d	-	Drag coefficient
C_{y^*,y^*}	-	IMF component of y^* with highest correlation to y^*
C_{Cl,y^*}	-	IMF component of C_l with highest correlation to y^*
$C_{Cl,RMS}$	-	Root-mean-square of characteristic IMF of C_l
D	-	Characteristic diameter
F_l	-	Lift force
F_s	-	Safety factor for GCI estimation
$f_{cyl.}$	-	Dominant cylinder vibration frequency
f_{RE}	-	Richardson extrapolation of quantity in GCI study
f_n	-	Natural system frequency
$f_{v,Karman}$	-	Karman vortex shedding frequency
f^*	-	Normalised system frequency
g	-	Gap between upstream cylinder and downstream plate
G	-	Normalised gap
h	-	Average mesh cell size
$l_{cylinder}$	-	Length of upstream cylinder
$m_{eff.}$	-	Effective system mass
O	-	Order of magnitude
P	-	Pressure
p	-	Order of accuracy grid independence study
$P_{Fluid,RMS}$	-	Root-mean-square of fluid power
$P_{Mech.,RMS}$	-	Root-mean-square of mechanical power
Re	-	Reynolds number
r^p	-	Mesh refinement ratio
$S_{grid,i}$	-	Total number of cells in the i^{th} grid

S_{ij}	-	Strain rate
St	-	Strouhal number
$\text{St}_{\text{Karman}}$	-	Strouhal number of Karman vortex shedding
$T_{\text{osc.}}$	-	Period of oscillation
t	-	Time
U	-	Velocity
U_∞	-	Free stream velocity
u'	-	Fluctuating component of velocity
U^*	-	Reduced velocity
V_{in}	-	Input voltage
W_{Cl}	-	Mean work done over one vibration cycle
y	-	Vertical cylinder displacement
y^*	-	Normalised vertical cylinder displacement
y_{RMS}^*	-	Root-mean-square of vertical cylinder displacement
β	-	Porosity
δ	-	Logarithmic damping
λ	-	Mesh deformation velocity and displacement diffusion
ν	-	Kinematic viscosity
ν_T	-	Kinetic eddy viscosity
$\omega(t)$	-	Instantaneous frequency
ϕ	-	Representative phase lag between y and Cl
$\theta y - \text{Cl}$	-	Phase lag between y and Cl
∂	-	Partial differential operator
ρ	-	Fluid density
τ	-	Reynolds stress tensor
$\theta(t)$	-	Instantaneous phase
$\zeta_{\text{tot.}}$	-	Total damping coefficient

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CHAPTER 1

INTRODUCTION

This chapter gives the reader a brief overview of the contents of the thesis. The chapter begins with the Section 1.1 Background of Study. Here, an abridged introduction to the topic of flow-induced vibration (FIV) is provided, specifically, on vortex-induced vibration (VIV) for energy harvesting. Two types of VIV are discussed: Karman VIV and streamwise VIV. This is followed by the prerequisites of their formation and the pros and cons of each in terms of energy harvesting.

Next, the chapter proceeds with Section 1.2 Problem Statement. This lists the main gaps to be closed in this thesis. Then, Section 1.3 Research Questions translates the gaps identified in the preceding section into concrete questions that this work will address in subsequent chapters. Following this, the Thesis Objectives are listed in Section 1.4 and Significance of Study in Section 1.6. Finally, the chapter explains the Scope of Work in 1.5 and ends with the outline of the thesis in Section 1.7 Thesis Organisation.

1.1 Background of Study

The term “flow-induced vibration” refers to a wide range of phenomena. One of the phenomenon is called flutter, which is the flapping of a thin, flexible structure that results from the competition between periodic bending forces due to the shedding of vortices, and the stabilising forces from the structure itself (Xia *et al.*, 2015). Another example is galloping, which is the outcome of aeroelastic instability of an elastically supported cylinder (Kluger *et al.*, 2013). On the other hand, vibration of a structure due to resonance with the frequency of turbulent eddies around it is called turbulence-induced vibration (Nakamura *et al.*, 2013). Finally, there are also structural vibrations that are the result of excitations coming from the wake of another structure, named wake-induced vibration (Derakhshandeh *et al.*, 2014). The vast majority of these

phenomena were studied as part of a program to suppress the vibrations, to prevent structural failure (Khalak and Williamson, 1999).

On the other hand, vortex-induced vibration (VIV) is a type of vibration that grows from instabilities in fluid flows moving past a solid object, i.e. bluff body. When the flow exceeds a critical velocity, the flow develops vortices that are shed alternately downstream the bluff body. This triggers the onset of unsteady lift and drag forces that initiate and sustain its vibration (Bukka *et al.*, 2020). The common denominator for all these examples is the potential damage to the engineering construct experiencing it. Thus, methods are devised and implemented to mitigate the effects of the vibrations by dissipating the vibrational energy or delaying/aborting its onset in the first place.

However, the past decade has seen efforts to instead make the vibration stronger. For example, purposefully maximising the vibration of flexible piezoelectric flags to harvest wind energy from low-speed winds (Mehdipour *et al.*, 2022). Another example is the effort to maximise the vibration of in-tandem VIV nanogenerators for energy harvesting by (Zhang *et al.*, 2022b). Simple circular cylinder oscillators has also been studied to increase its vibration amplitude and efficiency in energy conversion (Zhang *et al.*, 2022a). The simplicity of design and scalability attracts many to contribute to this multidisciplinary field of study, along with the prospect of successful development and subsequent commercialization of a new generation of energy harvester. Also, technical publications since the 2000s saw a surge in contributions toward the subject from the perspective of energy harvesting. A simple search in SCOPUS shown in Fig. 1.1 reveals this trend for keywords [“vortex induced vibration” energy] for the last 4 decades.

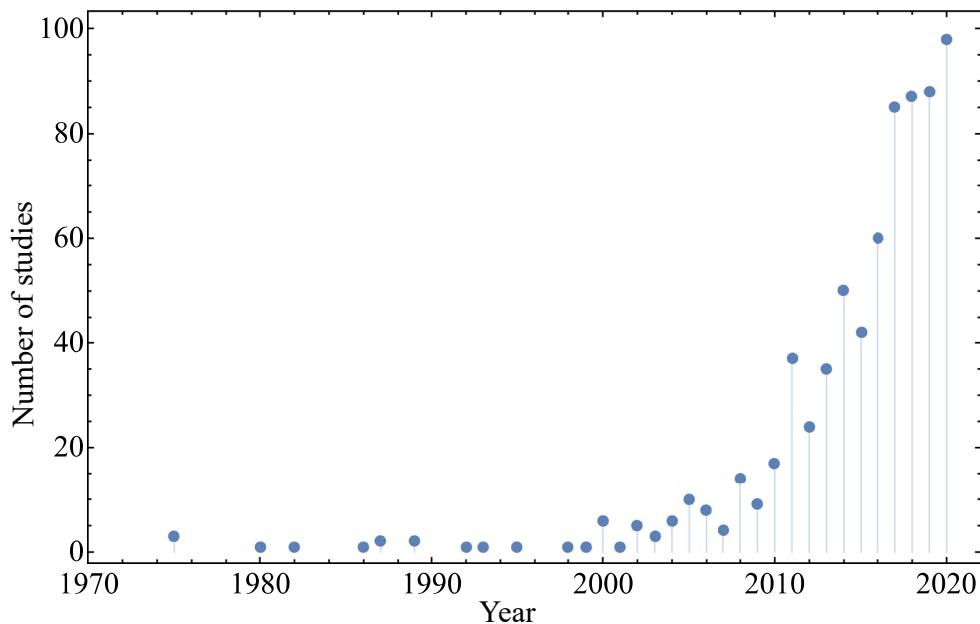


Figure 1.1 Number of publications with keywords ["vortex induced vibration" energy]. Retrieved from SCOPUS.

At the cutting edge of this field of research is a group at The University of Michigan, that has already built prototypes of the energy harvester, named VIVACE (vortex-induced vibration for aquatic clean energy). They compared the cost of power production in USD/kWh between VIVACE and a wide selection of common (pulverised coal, integrated gasification combined cycle, natural gas combined cycle, etc.) and new power generation technologies (anaerobic digester, landfill gas, solar, etc.). In doing so, they found that VIVACE is on par in terms of power production cost with the other conventional technologies, and published their findings in Bernitsas *et al.* (2008). This result demonstrated VIVACE's economic appeal.

The VIV phenomenon utilised by the team at the University of Michigan is of the Karman VIV type (KVIV), capable of producing power in the order of MW when installed as a large-scale energy farm (Raghavan, 2007). Karman VIV - or KVIV for short - is a form of VIV that is induced and sustained by the periodic shedding of Karman vortices from opposite surfaces of a cylinder. The periodic shedding of these vortices creates a pressure fluctuation from the opposing surfaces (Mei *et al.*, 2021). This produces a net fluctuating force acting on the cylinder, which is the lift that

drives its vibration. Karman vortices fall into the category of spanwise vortices, and structurally, a single cylinder is all one needs to trigger its formation (Liu *et al.*, 2022).

However, as pointed out by Koide *et al.* (2013) the reduced velocity (U^*) range within which KVIV can be relied upon for power generation is about one order of magnitude smaller than what can be expected from another form of VIV namely the streamwise VIV (SVIV). Reduced velocity U^* is a nondimensional characteristic velocity that allows comparison of results between similar systems vibrating in a flow. Reduced velocity is defined as follows.

$$U^* = \frac{U_\infty f_n}{D}, \quad (1.1)$$

where U_∞ , f_n and D refers to the freestream velocity, natural frequency of the system and diameter of the cylinder respectively. Using U^* to express flow velocity allows the reader to gauge how fast the flow is, with respect to the speed of vibration at f_n .

Streamwise VIV - or SVIV for short - has its vorticity vector parallel to the direction of the flow. This is different from KVIV whose vorticity vector is perpendicular to the direction of the flow, and is instead parallel to the axis of the cylinder. Structurally, unlike a single cylinder like KVIV, SVIV needs two cylinders in cruciform to trigger its formation. This cruciform is made by placing one cylinder upstream and another downstream. The axes of the two cylinders are at right angles to each other. The midpoint of the cylinders overlap one another, forming a plus sign, i.e. “+”. This type of cruciform, where the two cylinders are at 90° to each other is called the pure cruciform.

Streamwise vortices that drive the vibration of the cylinder appear in pairs, one on the left, and another on the right of the “+”. The streamwise vortex on the left of the “+” rotates in the opposite direction to the streamwise vortex on the right. This means that the streamwise vortex pair is a counter-rotating pair of vortex. This counter-rotation produces the alternating lift on the upstream cylinder. Since SVIV power generation is

possible for a large range of U^* , it is better suited for deployment in flows with large velocity changes. to each other is called the pure cruciform.

Unlike KVIV-based energy harvesters, the oscillating upstream cylinder of SVIV-based energy harvesters have both Karman and streamwise vortices shed from it (Koide *et al.*, 2017). This presents a challenge to the measurement of the phase lag between the lift and vibration signals. The closer the phase lag is to 90° , the higher the power output (Koide *et al.*, 2013; Raghavan, 2007). Hence it is favourable to be able to measure the phase lag as it can help explain an observed improvement or deterioration of the power output. Since both Karman and streamwise vortices are shed from SVIV-based energy harvesters, distinguishing which part of the lift signal is due to either, is difficult. A time-resolved signal processing method is needed and in this study, the Hilbert-Huang Transform (HHT) analysis is employed.

The HHT analysis involves two steps: the first is decomposing a time-series signal into components of decreasing mean frequency, and second, to apply the Hilbert transform on the components to obtain the instantaneous phase (de Souza *et al.*, 2022). The application of HHT analysis enables this work to distinguish the dominant components of the lift signal, identify which of these is actually driving the vibration of the cylinder, and compute its phase lag against the vibration signal.

One shortcoming of a SVIV-based harvester is its maximum power output which is demonstrated at the current stage of development to cap at a mW scale for a single-cylinder setup. An isolated cylinder setup for KVIV produces a maximum power in the order of 10 W (Bernitsas *et al.*, 2009). The apparent power P_a (W) for both KVIV and SVIV is shown in Fig. 1.2. Following this present limitation of the unoptimized SVIV energy harvesters, their application is currently limited to mW electronics e.g., sensors and signal transmitters.

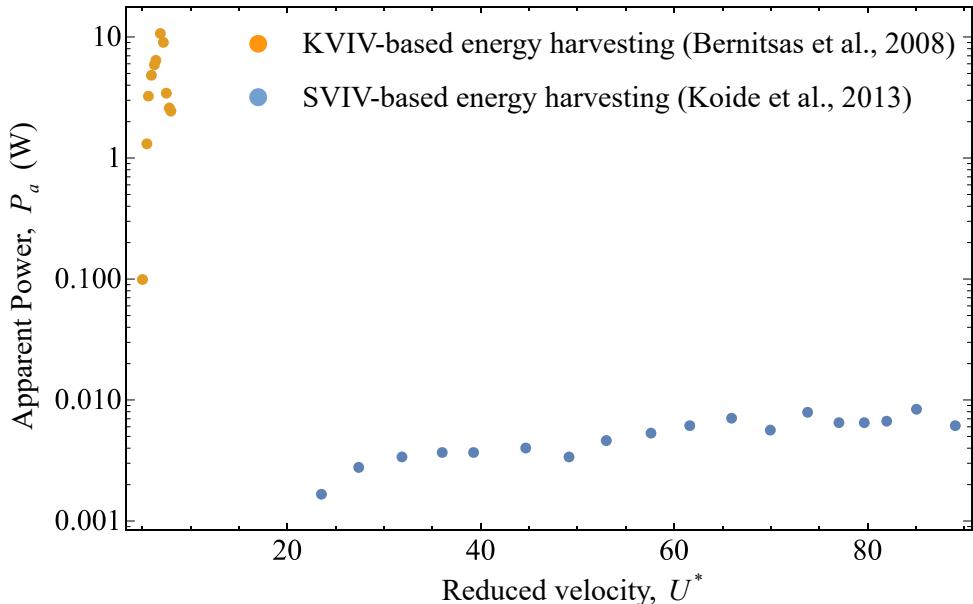


Figure 1.2 Apparent power P_a (W) versus reduced velocity U^* for cases of KVIV and SVIV. Adapted from Koide *et al.* (2013).

Nevertheless, these sensors and signal transmitters can make up environment-monitoring sensor networks to monitor the water level in rivers and irrigation canals that benefit flood forecasting efforts. The sensor network can also be used to monitor the level of pollution of the river or canal. This is possible by installing concentration sensors for specific contaminants. Finally, low-power batteries can also benefit from this energy harvesting technology, especially in the context of off-grid charging.

To expand the usability of the cruciform oscillator in energy harvesting, efforts should be made to improve its power output. Hence, this thesis seeks to identify the cause that limits the power output to its current value. This includes the identification of vortical structures in the flow, their location, and strength. The thesis also looks into the modulation of the lift signal by the shedding of vortical structures. Then, this thesis seeks to explore a new parameter in the study of the cruciform oscillator, which is the cruciform angle. This study documents the effects of the various cruciform angles on the vortical structures present in the flow in terms of their location and strength. In addition, this work also studies their effects on the lift and vibration signal, and ultimately, estimated power output and efficiency.

1.2 Problem Statement

The preceding section has established the viability of harnessing energy from a flow by exploiting the VIV phenomenon. Multiple modes of VIV have been observed, and SVIV stands out as better oriented for deployment in fluid flows that vary greatly in terms of free-stream velocity. Even with very rudimentary optimisations, SVIV from a cruciform harvester has the ability to generate power in the order of mW consistently over a large range of free-stream velocities (Koide *et al.*, 2013).

To achieve this, the problems outlined below must be addressed to close relevant gaps in the current body of knowledge.

1. A lack of understanding on the transition mechanism from Karman to streamwise vortex-induced vibration.
2. A paucity in the knowledge on what contributes to the magnitude of the alternating lift force acting on the cylinder, and its vibrational frequency components.
3. A deficiency of new methods to control the flow perturbation which gives rise to a strong, stable and periodic forcing of the cylinder vibration, sustainable over the desired operating range of U^* .

Problem statement one stems from the realisation that although past studies have shown that SVIV in a cruciform harvester begins around $U^* = 18$ (Koide *et al.*, 2013), none has ever looked into how the transition actually occurs from KVIV. This is especially the case in terms of the distribution of vortical structures around the cruciform, the lift signal: its frequency, amplitude and phase lag relative to the cylinder vibration signal. Removing this lack of understanding can help to trigger the desired mode of vibration at a lower U^* .

Problem statement two stems from the observation by Zhao and Lu (2018) on sectional lift, which drew attention to the effect a vortical structure has on the lift acting on the cylinder. Particularly in the case where several types of vortices are being shed simultaneously - like the cruciform harvester - the paucity in the knowledge on how

the different vortical structures affect the lift signal is a hindrance to improving the maximum lift that can be possible obtained from the cruciform harvester.

Finally, problem statement three comes from the realisation that recent studies in the field of cruciform energy harvester seems to be hard-pressed in finding new parameters to explore, focusing time and again on the gap between the cylinder and the downstream plate, the plate width and other dimensions of the system (Sakamoto *et al.*, 2021).

To date, the upstream and downstream cylinder (or plate) in cruciform harvesters have always been assumed to be at 90° to each other. It is possible that keeping the cruciform at a right angle prevents the discovery of other configurations that are capable of outputting higher power at better efficiencies. With enough cruciforms studied between angles 0° and 90° , one can synthesise a map of power and efficiency of cruciform harvesters at various cruciform angles α ($^\circ$) that can advise on the selection of the cruciform harvester for a given design constraint.

1.3 Research Questions

The answer to several questions is sought in this proposed study. These questions are meant to drive the study towards its objectives.

1. How does the lift signal evolve as the flow transitions from being driven primarily by Karman vortex to streamwise vortex?
2. How does the ratio of energy transferred from the flow to the lift components evolve with respect to U^* ?
3. Compared to a pure cruciform, what are the differences the Karman or streamwise vortical structures experience under the condition of a modified cruciform?
4. How do the differences mentioned in 3 affect the lift magnitude, and by extension the frequency-amplitude response?
5. Where in the power envelope can maximum (minimum) power be obtained with the largest (narrowest) operability range, and how does this translate into a new

mode of flow control to suit the operating conditions of the cruciform energy harvester?

1.4 Thesis Objectives

Following the problems outlined in the previous section, the objectives that define the scope of work in this proposal are listed below.

1. To identify the causes of the difference in amplitude and frequency response of the lift and vibration signals when the dominant vortical structure changes from Karman to streamwise vortex, in a pure cruciform.
2. To distinguish the dominant components of the lift signal and how the components interact to modify the amplitude and frequency response of cylinder vibration, in a pure cruciform.
3. To synthesise a map for each of the amplitude, power, and efficiency, summarised in the cruciform angle α ($^{\circ}$) - reduced velocity U^* parameter space.

As mentioned previously in Section 1.2, there is a lack of understanding on how the transition from KVIV to SVIV takes place in a cruciform energy harvester, which is the first problem statement. The first objective is thus to establish the relationship between the amplitude and frequency response of the lift and vibration signals and the vortical structures that are present at that time. The amplitude response is computed by taking the root-mean-square of the signals, both lift and vibration, and plotting them against U^* . The frequency response is computed by finding the dominant frequency in the FFT spectrum of the signals, both lift and vibration. Vortical structures are identified by computing the vorticity field.

Then, the second objective of distinguishing the dominant components of the lift signal is to answer problem statement two. As the reason behind the modulation of the lift signal remains unknown, this objective seeks to analyse the lift signal. The method of analysis to be employed here is HHT, through which the signal can be decomposed and the dominant components identified. Once the components of lift

have been identified, the study can explain how they interact to produce the amplitude and frequency response of the cylinder vibration being observed.

Lastly, the third objective of synthesising a map of the vibration amplitude, power and efficiency in the α ($^{\circ}$) - reduced velocity U^* parameter space is stated to answer problem statement three. As mentioned in problem statement three, the fact that studies have always assumed the cruciform oscillator to have a cruciform angle of 90° has prevented the investigation of a generalised cruciform oscillator. By computing the amplitude response, power and efficiency of a few cruciforms between $0 \leq \alpha$ ($^{\circ}$) < 90 , this study will be able evaluate the feasibility of varying the angle of the cruciform as a method to control flow perturbations due to the arrangement of vortical structures around the cruciform. This also provides a guideline for the optimal cruciform angle for a given design constraint such as vibration clearance, structural integrity and operating range of U^* , in addition to power output and efficiency.

1.5 Scope of Works

This work is a mainly a computational fluid dynamics (CFD) study of a particular version of VIV-based energy harvester that comprise of an elastically supported, horizontally constrained smooth circular cylinder of diameter 1 cm and a passive flow control mechanism that is a strip of rectangular plate at a right angle downstream the cylinder, forming a cruciform. The range of Reynolds number investigated in this thesis is between $1.1 \times 10^3 \leq Re \leq 14.6 \times 10^3$ and the mass-damping parameter, expressed by the nondimensional Scruton number Sc , is 9.94. This work limits itself to examining a cruciform where the width of the strip plate is equal to the diameter of the cylinder D , and the primary data collected from the simulation runs are the time evolution of the cylinder displacement and the corresponding lift coefficient C_l .

The baseline numerical results, i.e. results from a pure cruciform (a cruciform where the cylinder and strip plate are 90° to each other) are validated against experimental results of a similar system in a custom-made recirculating open flow channel. This experiment to validate the baseline numerical results also used a 1 cm diameter circular cylinder. A strip plate of width 1 cm was placed downstream the circular cylinder at a 90° angle. Data collected from the experiment is limited to the

vibration signal (i.e., cylinder displacement) only, and only between $1.1 \times 10^3 \leq \text{Re} \leq 11.2 \times 10^3$. The vibration signal is then post-processed into their respective amplitude and frequency responses.

The simulation in this study collects data on the three-dimensional pressure and velocity fields, and also cylinder displacement data. The pressure field is then post-processed to obtain lift signal acting on the cylinder, while the velocity field is post-processed to obtain the vorticity field. This is in relation to objective one that seeks to establish the amplitude and frequency responses of the lift and cylinder vibration signals. This is different from the parameters studied in Koide *et al.* (2017), as in their experiment, they only seeked to visualise the different vortical structures that appear between $1.2 \times 10^3 \leq \text{Re} \leq 5.7 \times 10^3$ for cruciforms with different cross-sectional shapes.

On the other hand, the study by Zhao and Lu (2018) only looked into the visualisation of the vortical structures around the cruciform and the distribution of lift along the vibrating cylinder. The range of Reynolds number they studied was between $1 \times 10^2 \leq \text{Re} \leq 5 \times 10^2$. This distribution of lift along the length of the vibrating cylinder reveals the location of dominant vortical structures and helps to visualise their strength with respect to time. Instead, this thesis used the FFT of the transverse (direction parallel to the vibration of the cylinder) velocity component downstream the cylinder to visualise dominant vortical structures and their strength.

This thesis looks to discover the relationship between the vortical structures present in the flow and how they modulate the resulting lift acting on the vibrating cylinder of the pure cruciform. Special focus is given to the high flow velocity region where SVIV takes place. This is done by conducting a time-series analysis of both cylinder displacement and lift coefficient signals using the Hilbert-Huang transform (HHT). The motivation behind this is to understand why the amplitude of cylinder displacement is limited to the order of magnitude observed not only by the author, but also in numerous studies within the last ten years. This part of the study concludes with the discovery of a particular route through which a significant amount of energy from the freestream is lost during the energy harvesting process, and the amount by which

the power output can be improved if this loss is eliminated. This scope is related to objective two.

The second part of this thesis is the author's attempt to eliminate the loss mentioned previously. This is done by generalising the cruciform system, through the variation of the relative angle between the cylinder and the strip plate. The study then proceeds to investigate the generalised cruciform system by examining the vortical structures present in the flow, how they affect the resulting lift acting on the cylinder, the amplitude of cylinder displacement itself, and ultimately the power output. The dynamics between the lift and cylinder displacement are explained through the computation of instantaneous phase lag between the two, which in turn is made possible by HHT.

The thesis concludes with the unveiling of a mechanical power and efficiency map, within a parameter space consisting of the cruciform angle and U^* . Useful recommendations can be deduced from the map, which highlights regions of high and low power output, and also regions of high and low efficiency, in order to obtain the desired power output and efficiency for any given power consumption requirement. This scope is related to objective three.

1.6 Significance of Study

The aim of objective 1 is to get a better understanding on SVIV in a pure cruciform. A better understanding of SVIV in a pure cruciform is important because this is the baseline case, to which the performance of other cruciforms at different cruciform angles will be compared. Achieving this objective can demonstrate how the inception of streamwise vortical structures perturb the amplitude and frequency of lift, which directly modifies the amplitude and frequency of the cylinder vibration.

Next, achieving objective 2 is desirable because it allows the establishment of a direct link between the different branches of KVIV or SVIV and how the vortices modulate the lift signal of a pure cruciform. Apart from that, distinguishing the dominant components of lift allows us to quantify how much energy from the flow is consumed by each of the Karman or streamwise vortices, and in return, how much

do they contribute towards driving the vibration of the cylinder. Investigating this for the pure cruciform lay the grounds to understand how power generation is affected by the configuration of vortices in the flow for more complex situations, i.e., when the cruciform angle is no longer 90°.

Finally, objective 3 is significant because in achieving it, one is able to evaluate and recommend the optimal cruciform angle for the designated specifications for vibration clearance, power output and efficiency. This holds the key as to how the cruciform angle should be varied to cater to a particular flow environment and structural integrity - much like the performance curves associated with engines and pumps.

1.7 Thesis Organisation

This thesis is organised into eight chapters. The author introduces the study and gives a general overview of the research in Chapter 1. In Chapter 1, gaps in the research are identified and thesis objectives are formulated based on those gaps. Chapter 1 also outlines the questions the author seeks to address, details the scope of this study and provide concrete examples as to the significance and merit of this work. Chapter 2 reviews relevant literature that gives an overview of the progress made up to the present day, on the subject of VIV energy harvesting, by exploiting an isolated circular cylinder as the oscillator. The chapter then introduces the cruciform oscillator and the studies on the vibration characteristics of a number of variations of the cruciform oscillator.

Chapter 3 discusses the methodology taken by the author to attain the objectives listed in Chapter 1. In Chapter 3, the author details the numerical model implemented in the CFD undertaking and this includes the domain size, critical dimensions of the cruciform, boundary conditions and solution method to the unsteady, three-dimensional (3D) Reynolds-averaged Navier-Stokes equation governing the flow. Apart from that, the author also discusses the turbulence modelling adhered to in the numerical studies. The author also introduces the Hilbert-Huang transform (HHT) and explains the ensemble empirical mode decomposition (EEMD) algorithm that drives the decomposition of a time series signal into a finite number of orthogonal components. Finally, the author explains the Hilbert transform and how the transform

is able to compute instantaneous phase or frequencies of a decomposed component of the signal.

Chapter 4 first takes into account the validation of the numerical setup in two ways: by way of a grid independency study, and by way of experimental comparison. The grid independency study utilises the Richardson extrapolation and grid convergence index (GCI) as the primary tool to ensure spatial convergence of the numerical results. In the experimental validation, this work showcases a simple contactless method of measuring the cylinder displacement using a camera and an open-source image tracking software. After the processing of the experimental data to compute the uncertainty and present them as error bars, the author concluded that the numerical results of the pure cruciform (90° cruciform) is in fair agreement with the experimentally obtained values, providing an added layer of confidence in the numerical results.

This is then followed by the vibration characteristics of a pure cruciform. In this section, the author studies in detail the lift-displacement dynamics that results from the kind of vortical structures that appear in this setup. This section concludes with the discovery of a path to energy loss that has never been considered before in the literature and estimated the amount of improvement possible for the power output if said loss is eliminated.

Then, the chapter continues to discuss the vortical structures and lift-displacement dynamics of a steep-angled cruciform ($45 \leq \alpha(^{\circ}) \leq 67.5$), followed by the vortical structures and lift-displacement dynamics of a shallow-angled cruciform ($0 \leq \alpha(^{\circ}) \leq 22.5$). Here, the study found out that for shallow-angled cruciforms, the onset of meaningful power generation is brought down significantly to from $U^* = 18.2$ in the pure cruciform, to $U^* = 9.1$ when the cruciform angle is 0° . At $\alpha = 0^\circ$, the maximum power also improves by approximately a power of two.

Finally, the author computes the mechanical power and efficiency of each of the cruciform variants for all flow velocities studied. From it, this work is able to produce a mechanical power and efficiency map, in essentially a cruciform angle-flow velocity parameter space.

Chapter 5 details the conclusions that follow the discussions made in Chapter 4. Here, the four main findings of this work are summarised and the chapter ends with some remarks on potential future works for this study.

CHAPTER 2

LITERATURE REVIEW

The alternate shedding of vortices from opposing sides of a cylinder introduces an alternating lift and drag which, unless constrained, will induce the vibration of the cylinder. This vibration energy can be converted into electrical power via the piezoelectric effect or electromagnetic induction. This is the basis of vortex-induced vibration (VIV) energy harvesting, and in this chapter, the author goes through the body of work done on the subject of vortex shedding, vortex-induced vibration and finally energy harvesting from the many variants of cylindrical oscillators, to determine the limits of the current knowledge and pinpoint where this work resides within the web of research done by the community.

2.1 Vortex Shedding from a Cylinder

Numerous occurrences of VIV are readily observable in the field of engineering. In the ocean, marine currents give rise to the vibration of risers and offshore drilling platforms. For example, the marine risers reviewed by Liu *et al.* (2020) in their review paper on recent progress in the research on vibration control of marine risers. Marine risers are also the subject of the study by Zhang *et al.* (2020), where they investigated the feasibility of applying tension to the top of the riser as a method to control its vibration. Another example of marine risers in the study of VIV can be found in Meng *et al.* (2020), where they looked into the modes of VIV that manifest themselves in flexible risers.

On dry land, VIV is observed to produce vibration of power transmission lines. This can be found in the study by Gómez-Ortega *et al.* (2019b), where they studied the vibration of transmission lines experimentally, that is caused by VIV. Power transmission line vibration also appeared in the analytical work by Gómez-Ortega *et al.* (2019a), where they proposed a mathematical model that describes the vibration of the transmission line. These studies demonstrate the usual motivation that drives the

study of VIV. As exemplified by these studies, VIV phenomenon is so common in the engineering field that a huge amount of effort goes into suppressing it. This availability of VIV that is so common in engineering initiated the movement to instead maximise it, and use it for energy harvesting (Barati *et al.*, 2022).

As the name suggests, VIV is the result of the periodic shedding of vortices. This chapter will thus begin with a review of the most common form of vortex shedding: Karman vortex shedding.

2.1.1 Karman Vortex Shedding

The formation of Karman vortex is the direct result of flow separation over a body submerged in a fluid flow. At low Reynolds numbers, the streamline is still able to follow the contour of the submerged body due to viscosity. Here, the Reynolds number Re of the flow is defined as

$$Re = \frac{UD}{\nu}, \quad (2.1)$$

where U , D , and ν are the characteristic velocity, characteristic length, and the kinematic viscosity of the fluid, respectively. For the case of the flow around a circular cylinder, U denotes the flow velocity and D the diameter of the circular cylinder.

As the Reynolds number increases, the higher inertial forces in the flow overpower the viscous forces that kept the streamline along the surface of the body, causing it to separate. This separation creates a bubble downstream the body. With further increase in Reynolds number, the bubble destabilises, leading to the formation of vortices that are shed alternately from the top and bottom surfaces of the body. This evolution of vortex shedding behaviour with respect to Re is summarised in Fig. 2.1. For creeping flows with $Re < 5$, the flow streamline follows the curvature of the circular cylinder submerged in the flow. Then, between $5 \leq Re < 40$, a small recirculation bubble forms at the downstream side of the circular cylinder. Further increasing the value of Re destabilises the bubble, leading to the the shedding of Karman vortices. Karman vortex shedding becomes turbulent between $150 \leq Re < 30 \times 10^5$.

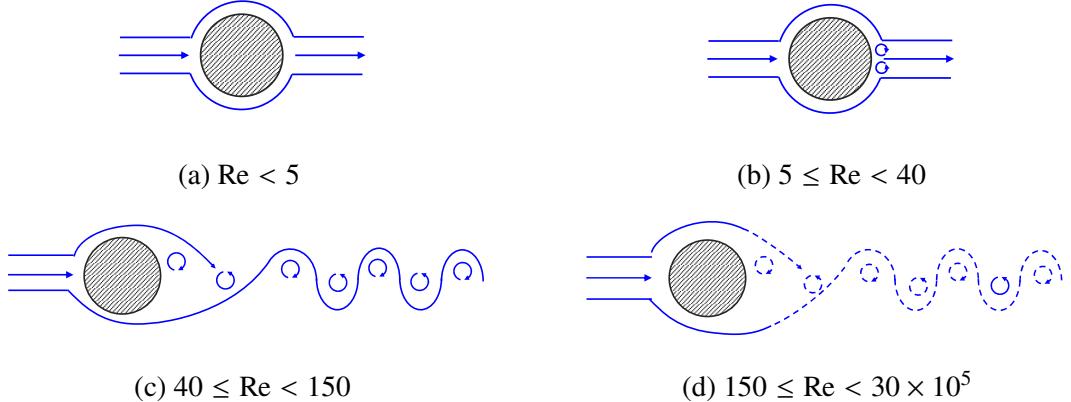


Figure 2.1 Evolution of Karman vortex shedding from a two-dimensional circular cylinder at increasing Reynolds number.

In the study of Karman vortex shedding, seldom is the case where one does not find reference being made to a chart on lift and drag coefficients for a stationary circular cylinder between $10^0 < \text{Re} < 10^8$ in Zdravkovich (1997). The lift coefficient C_L acting on the body is defined as

$$C_L = \frac{F_L}{\frac{1}{2}\rho U^2 A}, \quad (2.2)$$

where F_L , ρ , A , and U are total lift force acting on the body, density of fluid in which the body is submerged, area of the surface of the body, and characteristic velocity, respectively. Similarly, its drag coefficient is defined as

$$C_D = \frac{F_D}{\frac{1}{2}\rho U^2 A}, \quad (2.3)$$

where F_D is the total drag force acting on the body instead. By convention, the direction of the lift and drag are defined relative to the mean direction of the flow, i.e., the freestream. The lift force is normal to the freestream, while the drag force, parallel to the freestream.

The observation by Zdravkovich (1997) that both lift and drag coefficients (C_L and C_D) have their high and low regions within $10^0 < Re < 10^8$ is of extreme utility to engineers. From the preservation of risers to the improvement of power output for VIV-based energy harvesters, the chart in Zdravkovich (1997) gives a rough outline to the range of Reynolds number suitable for a particular engineering operation. This chart is presented in Fig. 2.2, with the highlighted region showing the Re range studied in this thesis. That being said, the chart remains silent on why C_L and C_D evolve the way they do with respect to Re , leaving the gap to be filled by later researchers.

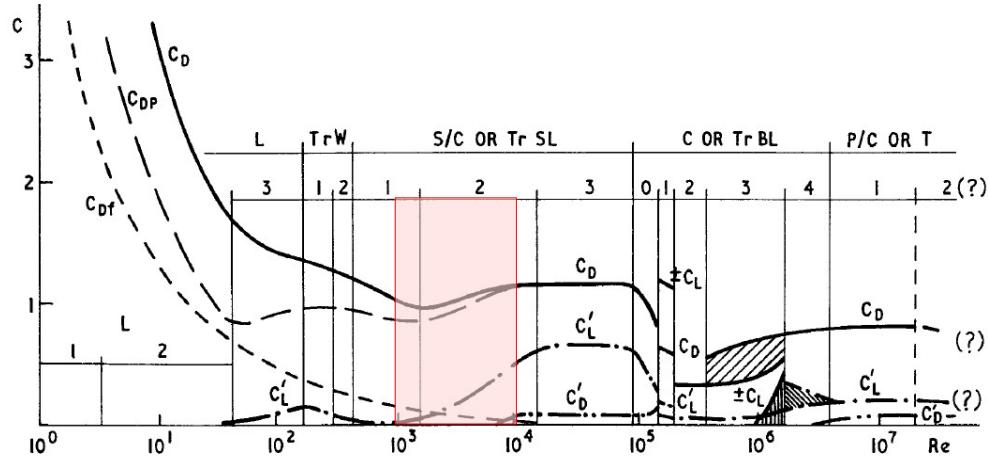


Figure 2.2 Force coefficients versus Re summarised by Zdravkovich (1997).

For example, Desai *et al.* (2020) tackled the question why is there a reduction in C_L and C_D as the cylinder goes through the upper boundary of subcritical flow ($1.49 \times 10^5 < Re < 3.55 \times 10^5$). Their study is experimental, using tools such as particle image velocimetry (PIV) for a quantitative visualisation of the two-dimensional (2D) flow field, and proper orthogonal decomposition (POD) for identification of dominant flow structures. In doing so, they have identified two modes of shedding - the antisymmetric and symmetric modes - which takes place one after another, albeit in no well-defined cycle. The antisymmetric mode corresponds to the “normal” shedding of Karman vortices while the symmetric mode a weaker form of shedding with a higher energy level in its low-frequency components. The symmetric mode gains strength with increasing Re , which entails a weaker form of shedding taking over the flow. This ultimately reduces the magnitude of C_L and C_D of the cylinder. Depending on which side of the divide one is, an engineer may opt to amplify the symmetric mode

to protect the integrity of a structure, or augment the antisymmetric mode to improve the conversion efficiency of energy from the freestream into cylinder vibration. In other words, a deeper understanding into the mechanics of Karman vortex shedding invariably leads to better strategies in cylinder motion control.

Expanding on the topic of flow control, Durhasan *et al.* (2019) conducted an experimental study of the shedding process under the following setup: the circular cylinder is placed in a larger hollow cylinder with varying pore spacing - quantified by their porosity - β - and submerged in a water flow at Reynolds number $Re = 5000$. What they found out is the stunting of the wake from the inner cylinder when $\beta \leq 0.5$, while for porosities $\beta \geq 0.6$, a reduction of 21% to 87% in drag is observed. It is worth noting that both lift and drag forces are equally able to initiate the vibration of the cylinder.

Another exploitation of porous material in the control of Karman vortex shedding is in the work of Geyer (2020). In Geyer (2020), they work to test a method of noise reduction by wrapping certain parts of the cylinder surface with a porous material. This is because, at velocities in the order of $O(10^1)$ m/s, Karman vortex shedding also exacerbates the level of noise generated by the cylinder. They discovered that the higher the air resistance of the material, and the higher the porosity, the bigger the improvement will be in terms of noise reduction. In addition, the porous wrapping reduces turbulence intensity in the wake near-field, hence making it more uniform. This goes to show that the vibration that results from Karman vortex shedding can manifest itself at different scales. First, on the high-amplitude, low-frequency scale, where it is observed as the motion of the cylinder. The second in on the low-amplitude, high-frequency scale, where it is observed as noise generation. It should be stressed, however, that both are simply the different scales of vibration that results from the shedding of Karman vortex.

In studying a flow around a solid object, one quickly finds that experimental methods employed in the investigation is never absolutely independent of the phenomenon being studied. The use of probes, for example, means that the researcher is introducing additional elements into the flow that cannot be fully isolated from

affecting the flow, however careful the design of the experiments are. To compensate this shortcoming, studies have employed numerical methods to model the flow under consideration, and track the evolution of quantities of interest in the flow to a degree of resolution limited only by the computational power available. Taking note of the expediency of porous media buffering the cylinder to temper flow behaviour, Ledda *et al.* (2018) made use of numerical methods to simulate Karman vortex shedding from a square cylinder to gain a deeper insight on how the flow interacts with the porous media to produce the flow responses discussed previously. In this study, the authors observed the efficacy of a porous cylinder surface in not only detaching the recirculation region in the near-wake, but in purging it altogether, at higher porosity values. If a technique can be found to vary the porosity of the surface, perhaps through the use of smart materials (Arsh, 2020), an engineer can basically switch Karman vortex shedding on and off at will.

Other than the usual methods of numerical investigation that work to solve the continuity and Navier-Stokes equations directly (DNS) (Alves Portela *et al.*, 2020), or those that employ some form of simplification (Shao and Li, 2016), methods that model molecular dynamics (MD) have also found their way in the arsenal of tools available to researchers in the field of fluid-structure interaction. One such example is the study by Asano *et al.* (2020). In it, the authors employed the Lennard-Jones potential to model represent the molecular dynamics of a flow around one or two circular cylinders. The Lennard-Jones potential models the fluid particle distribution, and all physical quantities are then expressed in terms of energy, length and time. What they discovered was, cavitation, although undesirable in normal operation of turbomachineries, can be a determining factor in the onset of Karman vortex shedding. As they decreased the fluid temperature, the cavitation bubbles interact with the shear layer of the cylinder in a manner that pushes the wake further downstream than usual. Eventually, wake where the vortex shedding resides is pushed far enough downstream that the alternating lift that normally acts on a cylinder during Karman vortex shedding vanishes.

Another method for Karman vortex shedding control that imposes some form of modification to the shear layer of the cylinder is through the affixing of fairings on the surface of the cylinder. A recent example of this can be found in the work of Kang

et al. (2020). In Kang *et al.* (2020), the fairings affixed to the cylinder surface caused a reduction in both lift and drag acting on the cylinder, although the strength of this effect varies with respect to the actual flow velocity being imposed on the cylinder.

Apart from tempering the shear layer of the cylinder, one can also - similar to Yokoi (2016) - alter the downstream region of the cylinder to achieve a desired response. In their study, Yokoi (2016) introduced a splitter plate on the trailing edge of a circular cylinder and discovered a rich collection of flow patterns that one can achieve simply by varying the following variables: splitter plate length, cylinder forcing amplitude and cylinder forcing frequency. By doing this, one can even achieve a symmetric shedding of Karman vortices from the top and bottom surfaces of the cylinder. To appreciate the significance of this result, one simply needs to recall that alternating C_L and C_D acting on the cylinder is the consequence of Karman vortices shedding alternately from the top and bottom of the cylinder. The fact that one can force the shedding to take place simultaneously from the top and bottom of the cylinder means that the amplitude of both C_L and C_D can be significantly diminish, if not altogether.

To be clear, the splitter plate method is not particularly new in near-wake control; splitter plates have been studied in the past under a similar setup (Mat Ali *et al.*, 2012), although under completely different flow conditions and cylinder geometry. However, one may find it difficult not to rely to some extent on the studies by Mat Ali *et al.* (2012), since unlike Yokoi (2016), they study flow patterns that are self-induced and does not rely on external forcing. This is particularly pertinent as in nature and man-made settings, self-induced vibrations is the norm rather than the exception.

2.1.2 Streamwise Vortex Shedding

In the real world, Karman vortex shedding is almost never a two-dimensional phenomenon. Once Re exceeds 150, Karman vortices can no longer be considered a purely two-dimensional vortical structure, with its vortex line parallel to the axis of the cylinder from which it is shed. The stretching of Karman vortex lines in the direction of flow breaks the two-dimensionality as there are now sections of the vortex line that points in the direction of the flow. The sections of the vortex line that now points in the

direction of the flow - or stream - create structures that are called streamwise vortices. A schematic of this vortex line stretching is presented in Fig. 2.3.

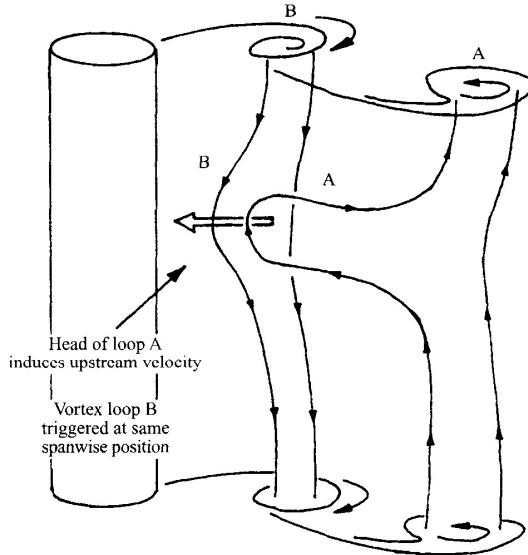


Figure 2.3 Stretching of the vortex line on a Karman vortex creates streamwise vorticity. Adapted from Williamson (1996b).

Among the studies on Karman vortex three-dimensionality are the works of Williamson (1996b) and Williamson (1996a). The author discusses two main modes of three-dimensionality: modes A and B. Mode A has a spanwise wavelength of three to four diameters and appears at $Re = 200$. Mode A of Karman vortex shedding is visualised in Fig. 2.4. The streamwise vortices are the vortical structures whose axis is parallel to the freestream.

However, as Re is increased, another mode with a smaller wavelength appears, designated as mode B. The modes consist of vorticities that point in the streamwise direction. The shedding of these modes are therefore a simple representative case of streamwise vortex shedding. On the other hand, mode B Karman vortex shedding is shown in Fig. 2.5.

Noticeably, a lot of studies on streamwise vortex shedding discuss the process as a secondary process that is the offspring of the vortical structure that actually dominates the flow field - the spanwise Karman vortex. This trend in viewing streamwise vortex shedding as a secondary process is also found in Agbaglah and Mavriplis (2019). In



Figure 2.4 Three-dimensional visualisation of mode A of Karman vortex shedding.
Adapted from Thompson *et al.* (1994).

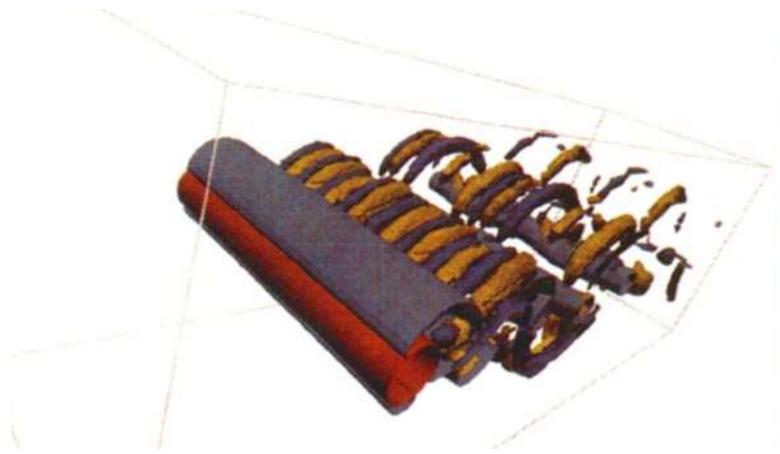


Figure 2.5 Three-dimensional visualisation of mode B of Karman vortex shedding.
Adapted from Thompson *et al.* (1994).

their numerical study of an isolated square and circular cylinder, they considered two Reynolds number, $Re = 205$ and $Re = 225$, and noted that the shedding frequencies of the two cylinders are quite similar. The Strouhal number St for the square cylinder is 0.152 and is 0.149 for the circular cylinder. Here, the Strouhal number St is defined as

$$St = \frac{fD}{U}, \quad (2.4)$$

where f , D and U are the characteristic frequency, characteristic length, and characteristic velocity of the flow. For a circular cylinder, D becomes the diameter of the cylinder.

It is interesting to note that not only do they differ from each other only by two percent, but also that they differ by less than 20% from the empirical equation (see, Eq. 2.5) describing the shedding Strouhal number of Karman vortices from a smooth circular cylinder (Blevins, 1990).

$$St_{\text{Karman}} = 0.198 \left(1 - \frac{19.7}{Re} \right) \quad (2.5)$$

Furthermore, rearranging Eq. 2.5 gives the Karman vortex shedding frequency, shown in Eq. 2.6.

$$f_{v,\text{Karman}} = 0.198 \left(1 - \frac{19.7}{Re} \right) DU \quad (2.6)$$

Here, $f_{v,\text{Karman}}$, D and U are the vortex shedding frequency, diameter of the isolated circular cylinder and U the freestream velocity respectively. The fact that St for the square and circular cylinders of Agbaglah and Mavriplis (2019) differs less than 20% of the value estimated using Eq. 2.5 indicates that the shedding process of streamwise vortex is overshadowed by Karman vortices, which are larger in scale. Perhaps this is an artefact of using an isolated cylinder, and as long as one uses a similar system, Karman vortex shedding will remain the primary process governing the flow.

More recent works on streamwise vortex shedding have shifted away from a simple isolated circular cylinder configuration to slightly more complex layouts, perhaps to recreate models that are more faithful to real engineering situations. For example, in Gibeau *et al.* (2018), an elongated body is studied in the range $3.5 \times 10^3 \leq Re \leq 7.0 \times 10^3$. Through this study, Gibeau *et al.* (2018) found that the average strength of the streamwise vortices in the upstream boundary layer is ten times smaller than in the wake. They also observed that the wavelength reaches between 0.7 and 0.8 of the elongated plate thickness, h .

In another study, Gibeau and Ghaemi (2019) swapped the isolated circular cylinder for a blunt trailing edge body. This blunt trailing edge (BTE) body is made from a leading edge that is a 5:1 ellipse connected to a plate with thickness h . This experimental study in the range $2.6 \times 10^2 \leq \text{Re} \leq 2.58 \times 10^4$, reveals that the rotational direction of the streamwise vortices are conserved during the shedding cycle, and their wavelength is close to mode B of Williamson (1996b).

Knowledge on the spatial distribution and key dimensions of streamwise vortices may be insufficient to highlight how one can exploit them to one's advantage. To exploit streamwise vortex shedding to fulfil engineering objectives, one needs insight on the effects of streamwise vortex shedding on the flow. This is demonstrated in the work by Rai (2018), in which the author published numerical results of flow around a flat plate with a circular trailing edge. The Reynolds number varies from $250 \leq \text{Re} \leq 10000$. Rai (2018) discovered that streamwise vortices are responsible for generating steep spanwise velocity gradients that affect the strength of the dominant vortical structure of the flow, i.e. the Karman vortex. The author also found that fluctuations in the streamwise velocity within the boundary layer leads to variation in the shedding period of the dominant Karman vortex. Finally, streamwise vortex shedding is observed to affect the shedding frequency of the spanwise Karman vortices through the speed of their streaks in the boundary layer.

In an evaluation of a passive method to control flow around a circular cylinder, Lin *et al.* (2018) inserted the cylinder inside a conical shroud and assessed its effect on the vortical structures shed around it. Their conical shroud is shown in Fig. 2.6. A very low $\text{Re} = 100$ was chosen to keep the flow as two-dimensional as possible.

Lin *et al.* (2018) tested two types of conical shroud. One shroud is with perforations of varying diameter and placement angle along the peak of the cone, and the other without. The authors also varied the wavelength and outer diameter of the conical shroud. By doing so, the study essentially discovered a method to prevent the energising of Karman vortex when the disturbance brought about by the conical shroud is large enough. Energy from the freestream is redirected away from Karman vortices, to form strong Ω -shaped vortices in the neighbourhood of the conical valley, some examples of

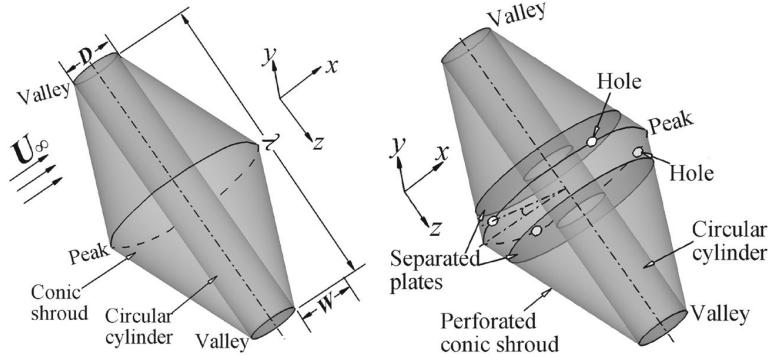


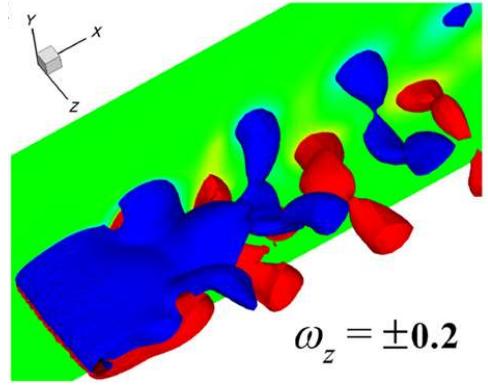
Figure 2.6 The conical shroud used by Lin *et al.* (2018).

which are given in Fig. 2.7. The name Ω -vortex comes from the fact that the vortices being shed downstream the cylinder resembles the uppercase Greek letter “omega” (Ω), when viewed from the direction of +y of their coordinate system.

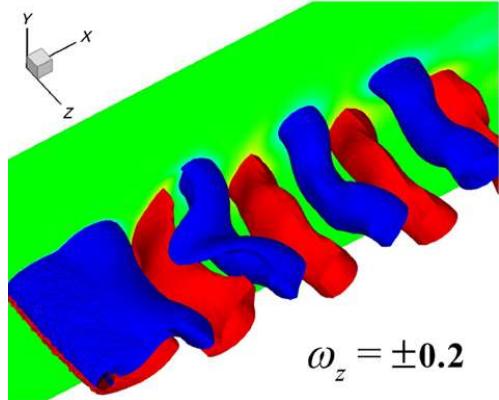
This results in partial to full suppression of Karman vortex shedding. The ability to refocus energy to a vortical structure of choice is indispensable, especially to engineers who may either want to minimise cyclic force acting on a structure, or maximise it to improve vibration energy harvesting potential of the structure.

Other examples of energy redirection can be found in Zhang *et al.* (2016) and Zhang *et al.* (2019). In these studies, the authors examined two methods to control Karman vortex shedding from a model bridge. The first method in Zhang *et al.* (2016) employs suction on the bottom of the bridge to disrupt the homogeneity of the Karman vortex along the span of the bridge. When suction is applied, streamwise vortex - which is considered a secondary process by the authors - becomes energised. The energised streamwise vortex then destabilises the primary vortical structure - the Karman vortex - hence reducing the net force resulting from it.

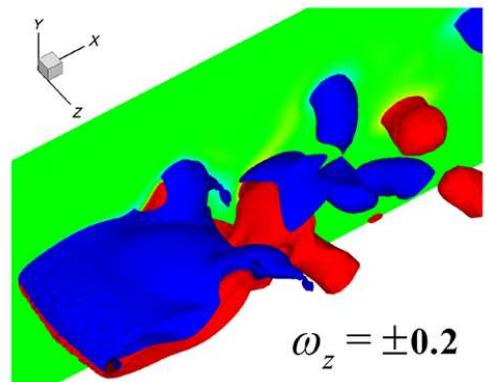
Providing suction on the bottom of the bridge is an active flow control method. This is because an active supply of energy is required to power the suction from the designated holes. As an alternative, Zhang *et al.* (2019) proposed using vortex generators affixed similarly to the bottom of the bridge, and evaluates the degree to which a similar result can be achieved. In the final analysis, they demonstrated that the disruption of Karman vortex homogeneity is possible through the use of vortex



(a) Omega vortex at $t = 470$ s.



(b) Omega vortex at $t = 500$ s.



(c) Omega vortex at $t = 900$ s.

Figure 2.7 Some examples of the Ω -vortices from Lin *et al.* (2018), taken at different times of the simulation.

generators. However, they did not specify quantitatively how much weaker does the Karman vortices get in expense of stronger streamwise vortices.

Attachment of a plate (Gibeau and Ghaemi, 2019) or placement of the cylindrical object inside a conical casing (Lin *et al.*, 2018) - even the deployment of vortex generators on the surface of the cylinder (Zhang *et al.*, 2019) - are all methods of flow control that add another layer of complexity to the cylindrical object. In situations where an engineer seeks to retrofit a flow control method to existing systems with cylindrical objects, direct modification of the cylinder can be difficult and downright undesirable. What if there exists an accessible flow control method that requires only a minimum amount of effort from the end used to install, but is still powerful enough to significantly alter the dominant vortical structures of the flow? The deployment of another cylindrical object downstream the main cylinder seems to be a promising technique.

Flow control using a secondary cylinder placed downstream the main cylinder dates back nearly three decades. Originally, the authors investigating it (Shirakashi *et al.*, 1989) is focussed on reducing the magnitude of cyclic forces acting on an isolated circular cylinder system. They placed a secondary circular cylinder downstream the original circular cylinder and explored how, among others, root-mean-square lift coefficient of the original cylinder varies as the gap between the original and secondary cylinders are varied. The secondary cylinder is placed downstream the original in a way such that the axes are perpendicular to each other, creating a cruciform. In doing so, they discovered that while the root-mean-square of lift coefficient can be reduced as the downstream cylinder is brought closer to the original one, when the normalised gap between two cylinders g/D is < 0.25 the lift coefficient rises again and peaks close to ≈ 0.7 before dropping off again as $g/D \rightarrow 0$. This is a significant finding in that it demonstrates how the flow around an existing isolated cylinder system can be altered in hindsight by simply forming a cruciform structure with another cylinder.

The dominant vortical structure in such a cruciform when $0 < g/D < 0.5$ is dominated by a pair of streamwise vortices, shed alternately from the top and bottom of the primary cylinder (Koide *et al.*, 2017). Two types of streamwise vortices are observed, the necklace vortex when $0.25 < g/D < 0.5$, and the trailing vortex when $0 < g/D < 0.25$. This is illustrated in Fig. 2.8. Although both types of vortices form close to the cruciform juncture, the necklace vortex dominates a region that is closer to

the juncture than the trailing vortex (Takahashi *et al.*, 1999), which forms a little further away from the juncture. The streamwise vortex pair that forms due to the cruciform does not seem to be secondary to the Karman vortex that is also shed from the upstream cylinder. Instead, the streamwise vortices seem to have its own mechanics which is independent from the cycle of Karman vortex shedding.

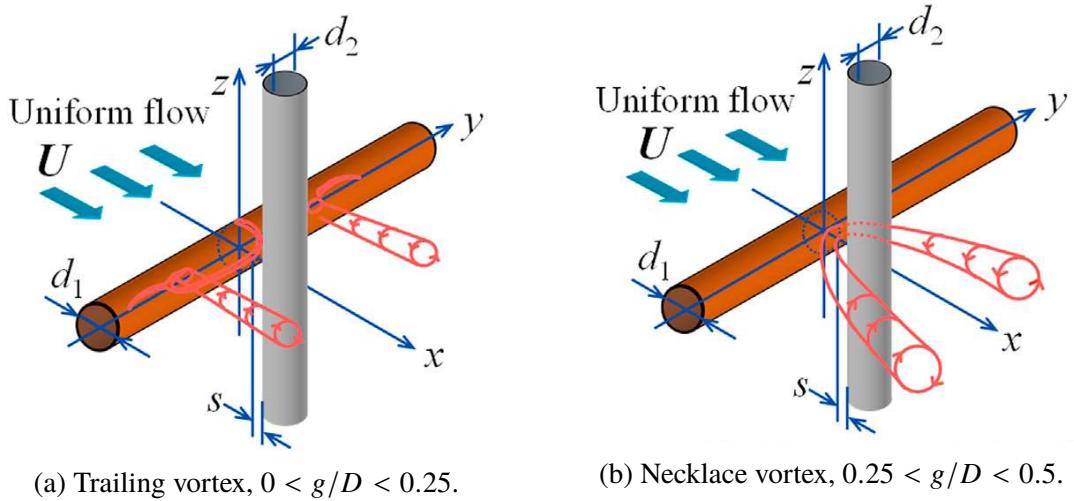


Figure 2.8 A schematic of streamwise vortex shedding, adapted from Hemsuwan *et al.* (2018a).

One obvious example is the deference to Eq. 2.5. Streamwise vortices such as those discussed earlier (Zhang *et al.*, 2016; Rai, 2018; Agbaglah and Mavriplis, 2019; Zhang *et al.*, 2019) develop as three-dimensional instabilities of Karman vortex shedding, and as such, have a base shedding frequency that loosely obeys Eq. 2.5. However, streamwise vortices in Takahashi *et al.* (1999), and even in Shirakashi *et al.* (2001) and Bae *et al.* (2001) do not. Streamwise vortices from these studies are shed at an increasing St as Re is increased within the region $\text{Re} < 10000$. When $\text{Re} > 10000$, St for the streamwise vortex becomes more or less constant with $\text{St} \approx 0.04$ for the necklace vortex and nearly twice that value for the trailing vortex.

Domination of the cruciform flow field by the streamwise vortex pair does not imply that the Karman vortex completely disappears from the experimental domain. This is demonstrated in Koide *et al.* (2006) and Kato *et al.* (2006). According to the frequency spectra of the upstream cylinder vibration, the Karman shedding frequency still exist in the system, only far smaller in magnitude compared to the amplitude attained

by the streamwise vortex structures. The flow field is thus dominated by the streamwise vortex pair close to the cruciform juncture, while the influence of the Karman vortex only grows as one moves towards the ends of the upstream cylinder. This begs the question whether the streamwise vortex-dominant flow is simply a consequence of two circular cylinders at right angles to each other - placed some distance away from each other - or is it something universal to cruciforms structures?

To answer this, Kato *et al.* (2007) and Nguyen *et al.* (2010) tested several variations of the cruciform, to see whether a similar occurrence of streamwise vortex shedding can be observed. For example, Kato *et al.* (2007) swapped the downstream circular cylinder with a strip plate, and observed that similar streamwise vortices do appear in the flow. They are shed at very similar values of St as the two-cylinder cruciform, but the frequency spectra of velocity fluctuations revealed a noisier pattern with less discernable peaks compared to the frequency spectra computed from a two-cylinder cruciform. More recent flow visualisations suggest that the noisier pattern is due to an increased turbulence level in the flow as streamwise vortices are produced from the circular cylinder-strip plate system (Koide *et al.*, 2017). Streamwise vortices produced from the two-cylinder system however, is less turbulent and thus one finds less distortion in the vortical structures compared to the circular cylinder-strip plate cruciform.

Distortion of the vortical structures discussed in Kato *et al.* (2007) and Koide *et al.* (2017) are self-induced: the result of an increasing level of turbulence in the flow. An increased level of turbulence is something that is internal to the flow being considered. It remains to be seen whether external factors such as the type of medium used as the ambient fluid, or configuration of the experimental rig can affect the shedding behaviour of the streamwise vortices. The work by Nguyen *et al.* (2010) partially answers this question. In their study, the two-circular cylinder cruciform is tested under various settings. They tested the system in wind and water tunnels of various sizes and ascribing different dimensions to the cruciform. The dimensions Nguyen *et al.* (2010) vary in their experiments are the circular cylinder diameter, cylinder length and aspect ratio. At the end of their study, Nguyen *et al.* (2010) concluded that nearly all major characteristics of streamwise vortex shedding are observed under the various test

conditions. There are, however, some discrepancies namely reduction by 30% to 50% of streamwise vortex shedding St in the largest wind tunnel, and the vanishing of the necklace vortex in the water tunnel as $\text{Re} > 22400$.

Clearly, streamwise vortex shedding that results from the deployment of a cruciform structure is robust and induces as much force on the upstream cylinder as Karman vortex shedding on an isolated cylinder, if not more. This makes the cruciform structure a good oscillator candidate for the purpose of converting energy from the free stream in to vibration energy. In the next section, the author reviews the recent developments in VIV and discusses how a cruciform oscillator ties into the overall work done to induce a larger, but predictable vibration from fluid flows, including that which depends on Karman vortex.

2.2 Vortex-induced Vibration of a Cylinder

In this section, the thesis looks into the literature on vibration that is induced from the vortex being shed from a cylinder whose axis is perpendicular to the direction of the freestream. In particular, the following sections are going to collect and synthesise information on the transverse oscillation response of the cylinder and summarise how it evolves with respect to parameters such as the Reynolds number and reduced velocity.

2.2.1 Single Cylinder Oscillator Unit

Since Karman vortex shedding has been demonstrated to produce alternating lift and drag on an isolated cylinder system, replacing motion constraints with elastic supports allows oscillatory motion to take place. Typically, the oscillation is constrained to a one-dimensional transverse motion against the direction of the free stream. Following the success of Raghavan (2007) and Bernitsas and Raghavan (2008a) in achieving a high amplitude response from an isolated circular cylinder oscillator, experimental studies for such an oscillator are increasingly done in the $2 - 4 \times 10^4 \leq \text{Re} \leq 1 - 2 \times 10^5$ range.

Numerical studies provide a non-intrusive method to collect high-resolution data on flow quantities. Following the trend in experimental studies of VIV, an increasing number of works have been pushing through the $\text{Re} \sim O(10^5)$ barrier, and collect

time-resolved flow quantities that lay the groundwork for advancing VIV flow theory. Additionally, if one is able to develop a working numerical model of VIV at a particular range of Re that is in good agreement with experimental findings, scholars can then use that model to automate the variation of parameters. This automation enables efficient exploration of the parameter space of interest and rapid product prototyping.

However, for numerical works to accurately depict what is going on in the flow at $Re \sim O(10^5)$, investigators need to abandon one of the most commonly made assumption to simplify the KVIV phenomenon: that the flow is two-dimensionally reducible. Reducing KVIV to a two-dimensional domain greatly reduces computational requirements and allows the researcher to focus the computational effort on resolving the shear layer of the cylinder and the near-wake region. However, three-dimensional effects exists throughout the flow field as soon as $Re > 150$, and an accurate representation of KVIV necessitates taking these effects into account.

Kinaci *et al.* (2016) proposed a tip-flow correction factor to reduce deviation of a two-dimensional CFD simulation from experimental results. The tip-flow correction factor is computed from three-dimensional simulation of flow around a cylinder within the Re range of interest, in essence providing the reader with a new “effective length” of the cylinder. The success of this method is however quite limited as it only scales the lift magnitude from a two-dimensional simulation, but not the phase lag between the lift and cylinder displacement. This means that to conduct a meaningful study of KVIV in the TrSL3 regime ($2 - 4 \times 10^4 \leq Re \leq 1 - 2 \times 10^5$) one must rely on experiments and three-dimensional simulations to explore the bulk of parameter space.

One of the recent developments in the control of KVIV is by affixing passive turbulent stimulations on the surface of the cylinder. For example, Park *et al.* (2016) deploys surface roughness on the cylinder and observed their effect on KVIV. They identified several location on the cylinder that produces weak to high reduction in the amplitude response. They reasoned that this is due to the reduction of vorticity in the shear layer that forestalls vortex roll-up, hence trim the vibration amplitude by at least a factor of three. This forestalling of vortex shows that surface roughness on the scale

of the shear layer thickness can alter the vorticity and thus the lift production process of the cylinder.

The altering of vorticity in the shear layer is also what enables the bridging of KVIV and galloping in single cylinder systems with surface roughness. At low angles of attachment of the roughness strip (Park *et al.*, 2013), the flow separates at the strip upstream but reattaches further downstream the cylinder surface. At high angles of attachment, there is not enough distance along the cylinder surface for the separated flow to reattach, hence vorticity cancellation between Karman vortices shed from the top and bottom of the cylinder becomes comparatively more aggressive. The absence of this aggressive cancellation of spanwise vorticity is the reason why placement of the roughness strip is able to, in contrast to Bernitsas and Raghavan (2008b) and Park *et al.* (2016), enhance KVIV and improve the amplitude response of the single cylinder oscillator.

In Section 2.1.2, this work discussed how the cruciform system has its origin as a simple method that can be retrofitted to an existing single cylinder oscillator unit to control Karman vortex shedding. As such, the effect of the downstream cylinder/stripe plate is targeted towards the upstream cylinder and not itself. However, within the last five years, the VIV research community has increasingly realised that there is no reason for the conversion of energy from the free stream into vibration to strictly be a one-stage process. Excess energy that is not eludes capture by a single cylinder should simply be recovered with another cylinder downstream.

Bearing this in mind, Ding *et al.* (2017) investigated the system response of a two-circular cylinder system, one in front of the other and with their axes parallel to each other. This system is illustrated in Fig. 2.9.

Then, they measured the amplitude/frequency responses of the system and observed the following, compared against a single cylinder system with passive turbulence control (PTC). The amplitude response of the upstream cylinder seems to improve in this serial arrangement of cylinders, and they experience only a small influence from centre-to-centre distance variation. On the other hand, the downstream cylinder experiences

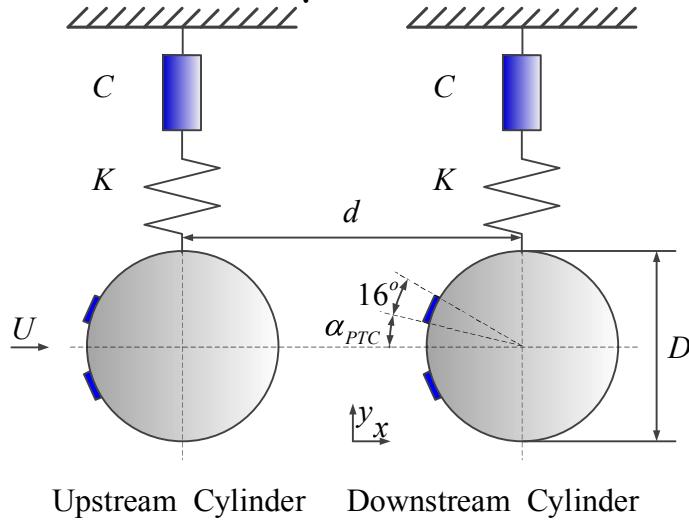


Figure 2.9 The two-circular cylinder system of Ding *et al.* (2017).

a reduction in the amplitude response compared to a single cylinder system and is more sensitive to the centre-to-centre distance between the two cylinders. The reduced amplitude response of the downstream cylinder is the result of the acquisition of downstream cylinder vorticity by the upstream cylinder in proximity. Proximity between the two cylinders determine how much downstream cylinder vorticity is carried away by the upstream vortex, and this reduces the net lift acting on the downstream cylinder. The reduction of lift finally results in the reduction of downstream vibration amplitude.

There is however, a countermeasure to improve the amplitude response of the downstream cylinder. The improvement is achieved by imposing a smaller damping on the downstream cylinder (Xu *et al.*, 2017). When Xu *et al.* (2017) reduced damping for the downstream cylinder, the amplitude response of the downstream cylinder becomes more similar to the amplitude response of the upstream cylinder. Nevertheless, because harnessed power is proportional to damping - specifically damping in the mechanical to electrical power converter - a reduced total damping just to achieve a higher amplitude vibration is simply contrary to the engineer's main objective of energy harvesting Bernitsas *et al.* (2009).

Spacing between the two cylinders play an important role in obtaining maximum vibration amplitude from both the upstream and downstream cylinders. This much is already known from the works of Park *et al.* (2016) and Ding *et al.* (2017). However,

recently, Yuan *et al.* (2020) utilised the Hilbert transform on the cylinder displacement time series of both upstream and downstream cylinders. In doing so, they identified five major responses of the two-cylinder oscillator that depends primarily on the centre-to-centre distance between the two cylinders, and secondarily on other parameters such as spring coefficient and total damping.

The use of Hilbert transform enabled Yuan *et al.* (2020) to compute instantaneous frequency and phase lag between the upstream and downstream cylinders and identified the five major response regimes of the system. Although Yuan *et al.* (2020) have essentially demonstrated the utility of Hilbert transform in analysing complex and interdependent systems of vibration, the signals they analysed are for the most part monocomponent signals with more or less a symmetrical signal envelope. For signals that lack these features, the pre-processing step of empirical mode decomposition (EMD) or ensemble empirical mode decomposition (EEMD) is necessary to produce meaningful physical results (Chen *et al.*, 2019).

2.2.2 Cruciform Oscillator Unit

Streamwise vortex-induced vibration (SVIV) is a type of vortex-induced vibration (VIV) driven by vortical structures whose vorticity vector points in the direction of the free stream. In its early days, the cruciform oscillator is nothing but two circular cylinders perpendicular to each other, overlapping at their midpoints (Zdravkovich, 1985). A cruciform oscillator unit, as shown in Fig. 2.10, derives its vibration from the streamwise vortex pairs discussed in Section 2.1.2.

When the upstream cylinder as shown in Fig. 2.10 is no longer fixed and is supported elastically through some form of spring, the shedding of streamwise vortices causes SVIV to occur. Investigators observed the upstream cylinder acquiring significant vibrations in the order of $O(10^{-1}D)$, as the reduced velocity of the flow U^* exceeds 14. Notice that there is a gap between the upstream and downstream cylinders.

Interestingly, however, the latest published research on a zero-gap circular cylinder cruciform system between $300 \leq Re \leq 1800$ revealed that no streamwise vortex cell are formed and shed from the structure (Tang *et al.*, 2021). This work by

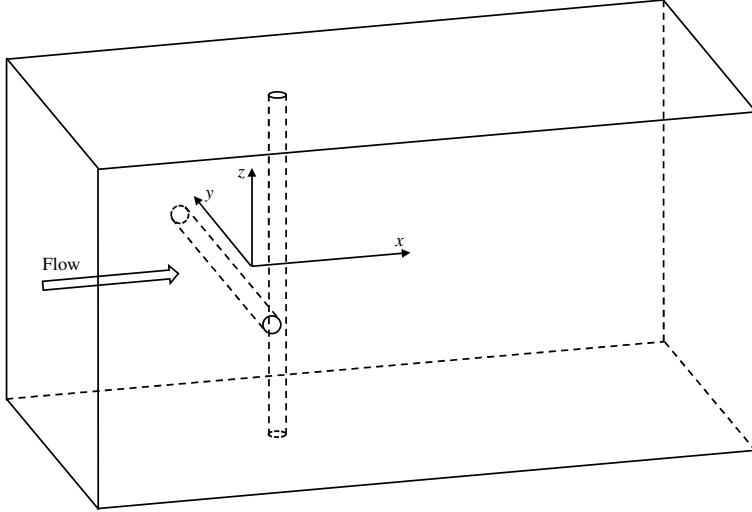


Figure 2.10 The two-circular cylinder cruciform of Zhao and Lu (2018).

Tang *et al.* (2021) was a numerical one, employing large eddy simulation (LES) with the dynamic k -equation subgrid-scale (DKSGS) model. Even the time history of the drag and lift coefficients did not show significant levels of periodicity, similar to those found in Deng *et al.* (2007), although they both simulate flow in the same Reynolds number magnitude of $O(10^2)$. In fact, Deng *et al.* (2007) simulated the flow around a circular cylinder cruciform at a much lower Re and still were able to observe the formation of the streamwise vortex cells and their footprint, manifesting themselves as the periodic oscillation of the drag and lift coefficients. What can be deduced from this is the gap between two cylinders forming a cruciform is essential for the formation of streamwise vortices and ultimately the vibration induced by it.

In their study of the two-circular cylinder cruciform, Shirakashi *et al.* (2001) observed the vibration of the upstream cylinder hitting the top boundary of the wind tunnel between $20.5 \leq U^* \leq 35.9$. The height of the wind tunnel in Shirakashi *et al.* (2001) is 320 mm and the diameter of both upstream and downstream cylinders are 26 mm. The fact that the reported vibration amplitude reaches the top extent of the wind tunnel means that it is able to achieve at least $(320 \text{ mm}/2)/26 \text{ mm} = 6D$ within $20.5 \leq U^* \leq 35.9$. This alone is far bigger than any of the amplitude attained by the single cylinder oscillator units reviewed in Section 2.2.1. However, there seems to be a finite range within which the cruciform oscillator is able to sustain this high amplitude response, which is approximately 15 units of U^* . Past this, the amplitude of the cylinder drops to about $0.1D$ and stayed there up to the maximum U^* tested. In contrast, single

cylinder oscillators of Section 2.2.1 is able to sustain its vibration through galloping for seemingly an infinite range of U^* .

More recent iterations of the system such as in Koide *et al.* (2007) and Kato *et al.* (2007) employs a thin, rectangular plate of width $w = D$ in place of the fixed downstream cylinder, and showed that the region of high-amplitude vibrations of the system is enlarged from 15 units of U^* for a two-circular cylinder cruciform to approximately 40 units of U^* for the circular cylinder-strip plate oscillator studied in Koide *et al.* (2007). Nevertheless, the shortcoming of this configuration is a lower amplitude of vibration, which attains only a maximum of close to $y_{\text{RMS}}^* = 0.35$. The vibration amplitude in Koide *et al.* (2007) and Kato *et al.* (2007) is given as the root-mean-square of nondimensionalised vibration amplitude $y_{\text{RMS}}^* = y_{\text{RMS}}/D$. Here, y denotes the coordinate pointing in the transverse direction of the flow, i.e. the direction of cylinder vibration. The effect of circular cylinder-strip plate gap g/D on y_{RMS}^* was also examined, and the results were consistent with the trend of high lift generation discussed in Section 2.1.2: y_{RMS}^* jumps to a high-amplitude regime as g/D is decreased to < 0.5 , especially when $g/D < 0.25$.

However, at $G = g/D = 0.16$, researchers have found that the circular cylinder-strip plate oscillator managed to sustain its vibration over a very large range of U^* . In relative terms, the vibration of this variant of the cruciform is sustained over a range of U^* 15 times the width observed in an isolated, smooth circular cylinder oscillator of similar diameter. This has been observed in Koide *et al.* (2009) and Koide *et al.* (2013). The reason behind this is the vortical structure driving the vibrations: vibration of the cruciform is driven by a pair of counter-rotating streamwise vortex shed a short distance from the cruciform juncture (refer Fig. 2.11), while vibration of the isolated, smooth circular cylinder is driven by Karman vortices shed alternately from the top and bottom surface of the cylinder.

The upside of this discovery is the fact that this wide synchronisation range is due to vortex shedding i.e., vortex-induced vibration (VIV) instead of galloping, as in Sun *et al.* (2019), Xu *et al.* (2019) and Ding *et al.* (2019), as VIV-based energy

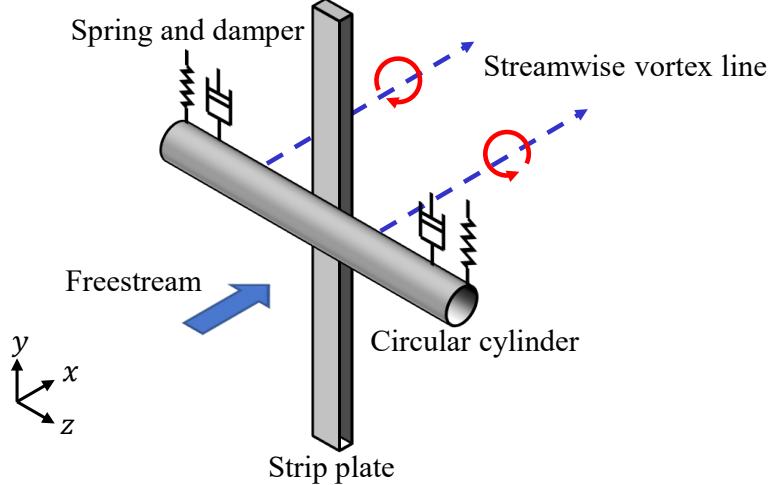


Figure 2.11 Schematic of the base configuration of the oscillator system used in this study, i.e. the pure cruciform.

harvesters of similar scale operate at higher efficiencies compared to galloping-based ones. Sun *et al.* (2016) and Ma *et al.* (2016) also obtained a similar result.

In their study, Deng *et al.* (2007) examined the flow field of a twin circular cylinder cruciform using computational fluid dynamics (CFD). Their domain stretches $28D$ in the streamwise direction, $16D$ in the transverse direction and $12D$ in the spanwise direction. They studied an Re range yet another order of magnitude smaller than that studied by Koide *et al.* (2017), possibly to get an even clearer visualisation of the vortical structures with less turbulence, and to ease computational requisites. At a fixed $Re = 150$, streamwise vortices form even at a gap ratio of 2. This result differs quite strikingly from Koide *et al.* (2006) and Koide *et al.* (2007), conducted at an Re twice the order of magnitude of Deng *et al.* (2007), an indication that the minimum gap ratio needed for the onset of streamwise varies with respect to Re .

They also observed that when the gap ratio G , which they denote as L/D in their paper, increases from 3 to 4, the maximum amplitude of the lift coefficient increases by almost threefold. This can be attributed quite easily to the current vortex pair shed by the upstream cylinder. The downstream cylinder immediately disturbs the pair shed from the upstream cylinder when $G = 3$. The lift coefficient increases by about a factor of 3 when this immediate disturbance diminishes at $G = 4$. The visualisation of three-dimensional (3D) vorticity isocontours enables the present work to quickly

establish this link vis-à-vis the lift coefficient signal. The authors use of CFD made this possible.

A similar study in the order of magnitude $\text{Re} \sim O(10^2)$ by Zhao and Lu (2018) particularly highlighted the immense utility of CFD as a tool to research SVIV or flow around a cruciform in general. They computed the sectional lift coefficient along the upstream cylinder, and the time history of this sectional lift coefficient revealed two different modes of vortex shedding, namely, parallel and K-shaped. They also paid attention to the local flow patterns that vary along the length of the upstream cylinder such as the trailing vortex flow, necklace vortex flow and flow in the small gap (denoted as SG flow). The discontinuities in the phase angle of the sectional lift coefficient along the upstream cylinder seems to suggest the inadequateness of attributing the lift coefficient to streamwise vortex shedding alone, particularly when Karman vortex streamlines were also observed some distance away from the junction of the cruciform.

Shirakashi *et al.* (1989) also made a similar observation in their experimental work. These observations lead the present author to hypothesise that the lift signal is more appropriately viewed as the streamwise and Karman vortex-induced composite lift signal. The present work, nevertheless, could neither find studies that took this viewpoint, nor work out its consequence on power generation. It is worth mentioning that there was a recent development in this field of study, which investigated a square cylinder and a square plate downstream of it (Mohamed *et al.*, 2021). This is essentially a variant of the canonical cruciform structure where the upstream circular cylinder is swapped for a square one, and the downstream strip plate is shortened to the same height of the upstream square cylinder. From all the experimental conditions tested, Mohamed *et al.* (2021) found only one setup that enhances the KVIV amplitude of the system, which is when the side ratio and gap ratio of the system is $(B/D, g/D) = (1.0, 1.17)$, while other setups cut down the KVIV amplitude by a factor of two. Galloping however, receives a boost in the root-mean-square amplitude at $(B/D, g/D) = (1.2, 1.15)$ and $(1.4, 1.15)$, making this setup a galloping-oriented oscillator and ultimately, energy harvester.

2.3 Energy Harvesting from a Vibrating Cylinder

The field of energy harvesting has witnessed exponential growth in the past two decades, particularly those which are based on alternating lift mechanisms. Following the same method used in the previous Section 2.2, the author reviews the progress in the single cylinder energy harvesting unit first, followed by the recent advances in the cruciform systems.

2.3.1 Single Cylinder System

Recent advances in energy harvesting from a single cylinder system builds upon the body of work done on single cylinder oscillators. One of the overarching themes in power output improvement from a single cylinder system is the operating range of Re . Ever since the work done by Bernitsas *et al.* (2008) and Bernitsas *et al.* (2009), prototyping studies have planted their foot firmly in the high lift regime of TrSL3. In doing so, studies such as Ding *et al.* (2019) and Park *et al.* (2017) managed to demonstrate an amplitude response with an upper branch sustained over a wider range of U^* compared to amplitude responses of single cylinder systems in TrSL1 or TrSL2. A higher vibration amplitude will elicit a higher harnessed power from the harvester.

Here, TrSL1, TrSL2 or TrSL3 refers to the classification system in Zdravkovich (1997) to characterise the flow around a smooth circular cylinder. The classification system uses abbreviations of the flow description as labels for different flow behaviours. For example, the flow around the circular cylinder undergoes a number of transitions in the shear layer between $350 - 500 \leq Re \leq 1 \times 10^5 - 2 \times 10^5$. The first transition in the shear layer, occurring between $350 - 500 \leq Re \leq 1 \times 10^3 \times 2 \times 10^3$, is the development of transition waves. Zdravkovich (1997) labeled this regime as TrSL1, formed by joining the abbreviations of “transition”, “shear”, “layer”, and the numerical equivalent of “first”, which is the number one (1). Similarly, the second transition in the shear layer occurring between $1 \times 10^3 - 2 \times 10^3 \leq Re \leq 2 \times 10^4 - 4 \times 10^4$, which is the formation of free vortices, is labeled as TrSL2. The shear layer becomes fully turbulent between $2 \times 10^4 - 4 \times 10^4 \leq Re \leq 1 \times 10^5 - 2 \times 10^5$. This regime is thus labeled TrSL3.

Now with the single cylinder system firmly planted in the TrSL3 regime, researchers worked to push the single cylinder harvesting system even further by tweaking its mechanical parameters. For example, Sun *et al.* (2018) and Ma *et al.* (2018) used as the restorative force, i.e. springs, of the nonlinear variant. This is achieved by connecting the vibrating cylinder not to a physical spring and damper, but instead to a computer-controlled motor, for example as shown in Fig. 2.12. This motor can be programmed to act like a spring and damper, each with its own coefficients k and c . So instead of modelling the spring linearly as

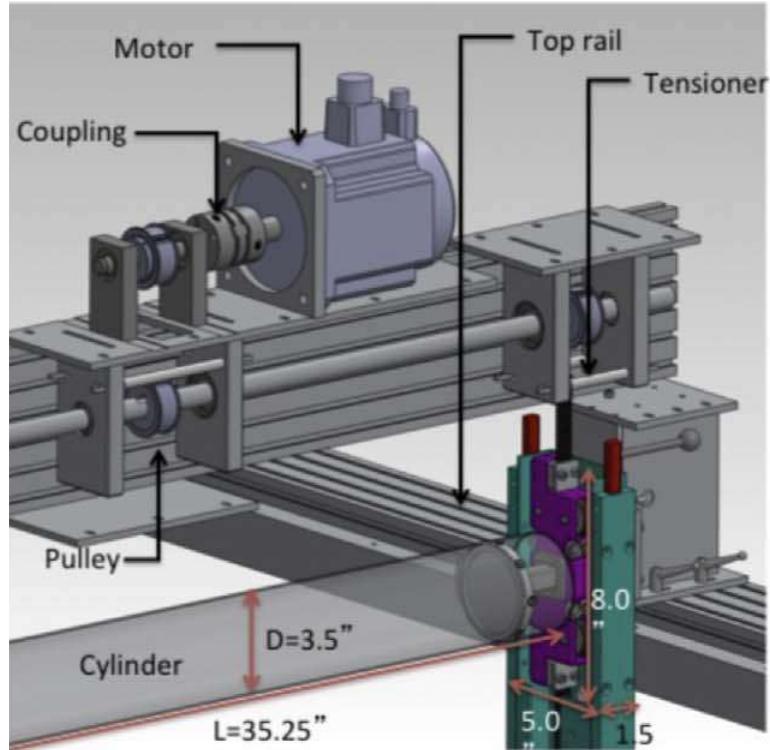


Figure 2.12 A three-dimensional drawing of the system to control the mechanical parameters of the system. Adapted from Ma *et al.* (2018).

$$F(t) = kx(t), \quad (2.7)$$

where $F(t)$ is the restorative force, k the spring coefficient and $x(t)$ the displacement of the object fixed to the end of the spring, they experimented with $F(t)$ that is given as a cubic function and an $F(t)$ that is given as a piecewise linear function. The cubic spring of Eq. 2.8

$$F(t) = ky(t) + ky(t)^3, \quad (2.8)$$

is found to significantly improve energy harvesting in all branches of amplitude response. Most significantly, however, is the improvement in the transition from VIV lower branch to galloping branch. In systems with a linear restorative force, the VIV lower branch is out of sync with the lift and also vortex shedding. This causes the net power harnessed in this regime to drop up to a factor of three, compared to the power harnessed in the upper branch of VIV (Sun *et al.*, 2018; Ma *et al.*, 2018). In contrast, when a cubic restorative force is applied to the system, energy harvesting improves by up to 78% during the transition from lower branch to galloping. Furthermore, once the system enters the galloping regime, the cubic restorative force improves energy harvesting up to 12%. In fact, the only branch where the original linear restorative force outperforms the cubic spring system in terms of energy harvesting is the upper branch.

Differently, a piecewise linear spring such as in Eq. 2.9, in essence enables switching of system stiffness and natural frequency according to the cylinder displacement.

$$F(t) = \begin{cases} k_1y(t), & \text{if } |y(t)| \leq y_0 \\ k_1y(t)y_0 + k_2(y(t) - y_0), & \text{if } |y(t)| > y_0. \end{cases} \quad (2.9)$$

Through this modification, the system is able to automatically switch to a lower stiffness when the lift acting on the cylinder is small, and to a higher stiffness otherwise. A higher stiffness results in a higher system natural frequency. Consequently, when the system is in sync with the alternating lift and vortex shedding, thus producing a large vibration amplitude, the frequency of vibration also switches to a larger value. This switch to a larger value is valuable as the harnessed power from such a system is proportional to the square of its angular frequency (Ma *et al.*, 2018).

Apart from this, the piecewise linear spring is able to harness energy even when $Re < 25000$, which is lower than the usual linear spring system of Eq. 2.7 (Sun *et al.*, 2016). In terms of damping, although it is proportional to the net harnessed power (Ma *et al.*, 2018), there is a trade-off with the size of the stall zone during transition from VIV to galloping. The width of the stall zone increases with increasing system damping, and this reduces the system's range of operability. Furthermore, in a single cylinder system with a linear spring, simply increasing the damping reduces the maximum vibration amplitude.

Interestingly, this suppression effect on vibration amplitude due to increased damping can be kept in check when one uses the in-tandem arrangement of cylinders. The in-tandem system is similar to that discussed in Section 2.2.1, and Sun *et al.* (2019) observed that the amplitude reduction is not as severe in the in-tandem system compared to the single cylinder unit. This highlights the potential of exploiting the synergy between the two cylinders to counter vibration amplitude reduction that is otherwise striking, provided that the two cylinders are optimally spaced. The results also brought attention to the concept of synergy between single cylinder oscillators in order to harness more energy from the flow.

Kim and Bernitsas (2016) took the idea of synergy and investigated a four-cylinder system for energy harvesting. Overall, what they found out was the net energy harvested by the four-cylinder system can exceed the total energy harvested by four isolated cylinder, provided that the four-cylinder system adhere to the optimised system parameters of centre-to-centre cylinder spacing, mass ratio, spring stiffness and damping. They also postulated an energy harvesting unit that consists of stacked arrays of single cylinder oscillators, thus maximising the footprint of the unit and increase power-to-volume density of the system. In summary, Kim and Bernitsas (2016) highlighted the need for the research community to widen their perspective and pay greater attention to multi-component energy harvesting systems as there is a high chance that one can discover practical arrangement of the components that increases the net harnessed energy. The next subsection explores one such system: the pure cruciform energy harvester.

2.3.2 Pure Cruciform System

A pure cruciform (Zou *et al.*, 2021) system is an example of a multicomponent energy harvester where the presence of the downstream plate perpendicular to the upstream cylinder alters the flow such that the vibration response of the upstream cylinder becomes different from the single cylinder oscillator. In such an energy harvesting system, there exists two vortical structures regulating the flow around the cruciform: the Karman and streamwise vortices. However, as the present study discussed in Section 2.1.2, only the shedding of streamwise vortex is able to synchronise with the alternating lift and cylinder displacement, thus producing a cylinder response fit for energy harvesting.

An example the cruciform system is given in Fig. 2.11. In broad terms, the literature on SVIV-based energy harvesting from pure cruciform oscillators are either one of these two categories: studies that investigate how the mass ratio, spring stiffness and damping affect the system response, and studies that put into the spotlight the details of flow that regulates the lift acting on the elastically supported cylinder, hence its amplitude/frequency response, which directly influences the system's energy harvesting capabilities.

For example, Koide *et al.* (2009) investigated such an energy harvesting system by varying a number of parameters defining the vibration-to-electrical energy converter. The energy converter schematic is given in Fig. 2.13.

Damping, similar to single cylinder systems in Section 2.3.1, decreases the magnitude of amplitude attained by the cylinder during vibration. Hence, Koide *et al.* (2009) pointed out the possibility of reduced harnessed power due to this reduction in vibration amplitude. Koide *et al.* (2009) also measured the power and current generated by their pure cruciform system. From these measurements, they computed the phase angle between power and current to estimate the power factor of the system. The evolution of the power factor, however, seems to indicate that there is a lot of room for improvement for their vibration-to-electrical energy converter as the power factor varies significantly from reduced velocity to reduced velocity without any prominent trend.

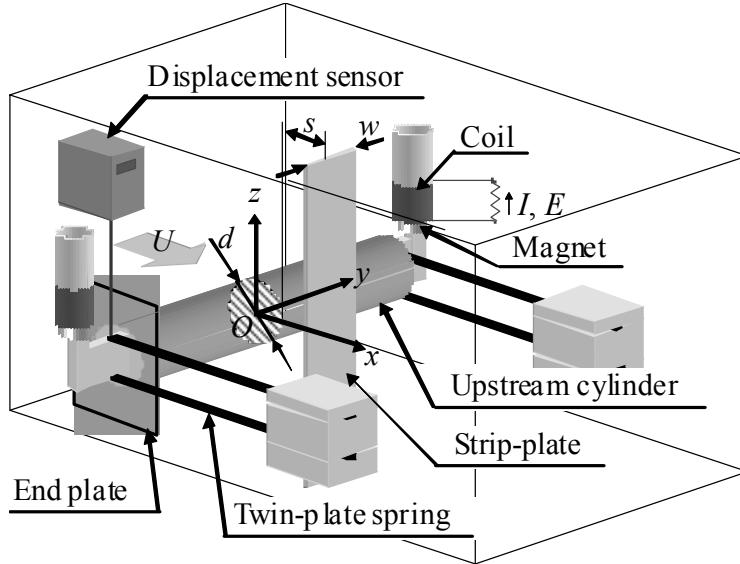


Figure 2.13 The vibration-to-electrical energy converter of Koide *et al.* (2009).

In Nguyen *et al.* (2012), the authors attempted to unravel the effect of mass ratio and damping on a pure cruciform oscillator. However, since they are unable to independently vary either of the two parameters, the conclusions one can draw from their study is fairly limited. Taking this handicap into account, they proposed a crude model of the system response with respect to U^* by assuming a strong linearity underpinning the cylinder vibration. According to this model, the synchronisation range of an oscillator is larger when the total damping is higher. This seems to contradict the experimental observations of Sun *et al.* (2016), whose data indicates that an increased total damping diminishes the range of U^* capable of sustaining VIV and delays the onset of galloping. Furthermore, only the experimental data from the single cylinder oscillator of Nguyen *et al.* (2012) showed some semblance of agreement with the model, but even this agreement is objectively poor as it incapable in capturing the actual trend and magnitude of the experimentally measured amplitude responses. The study did, however, confirm that resonance in VIVs are highly nonlinear, while also suggesting the nonlinearity of SVIV to be qualitatively higher than KVIV.

Such a shortcoming can be overcome using a host of techniques such as the sensor-based virtual spring and damper system in Garcia and Bernitsas (2018) and Sun *et al.* (2018), application of machine learning to fill in the gaps missing from a full factorial study (Hu and Kwok, 2020), and quite conventionally through the use of computational fluid dynamics (CFD) (Zhang *et al.*, 2018b).

In the second focus area, investigators turned their attention to the details of the flow where streamwise vortex shedding occurs. One such study carefully shot motion pictures of the dye-injected flow (Koide *et al.*, 2017) at Reynolds number in the order of $\text{Re} \sim O(10^3)$. A lower Reynolds number (Re) reduces the amount of turbulence in the flow, allowing a clearer shot of the vortex structures. Their study also highlights the higher level of turbulence produced by the circular cylinder-strip plate cruciform in contrast to the twin circular cylinder cruciform, which diminishes the periodicity of vortex shedding.

Although visually enlightening, this and other more qualitative studies contribute little towards improving the understanding of the relationship between vortex shedding and the resulting lift. Deng *et al.* (2007) demonstrated a way to overcome such a shortcoming. In their study at Reynolds number 150, they changed the natural frequency of the system at certain points in their transient simulation and observed how the cylinder amplitude and the force coefficients evolve with respect to the changes. In doing so, the authors found that a higher lift amplitude does not simply translate into a higher amplitude in cylinder displacement. Other factors such as the phase lag between the lift and cylinder displacement plays a significant role in predicting the outcome amplitude of the cylinder. They also verified the previous findings of Shirakashi *et al.* (1989), Koide *et al.* (2009) and Koide *et al.* (2017), that points to the coexistence of both Karman and streamwise vortex shedding in a cruciform system. The fact that only one of the two vortex shedding mechanisms actually govern the cylinder's vibration is viewed by this present work as hinting towards an untapped potential in improving the output and efficiency of the cruciform energy harvester.

Despite this, there is a marked lack in efforts to propose and evaluate new types of cruciform oscillators, particularly on the hidden potential of the strip plate as an effective vortical structure regulator. There are, however, some recent studies on the generalisation of the strip plate in the effort to produce steady lift over the surface on the cylinder. For example, the study by Hemsuwan *et al.* (2018a), Hemsuwan *et al.* (2018b), Hemsuwan *et al.* (2018c) and Hemsuwan *et al.* (2018d). In these studies, there are not one, but two circular cylinders placed at the ends of a small rod, as shown in Fig. 2.14.

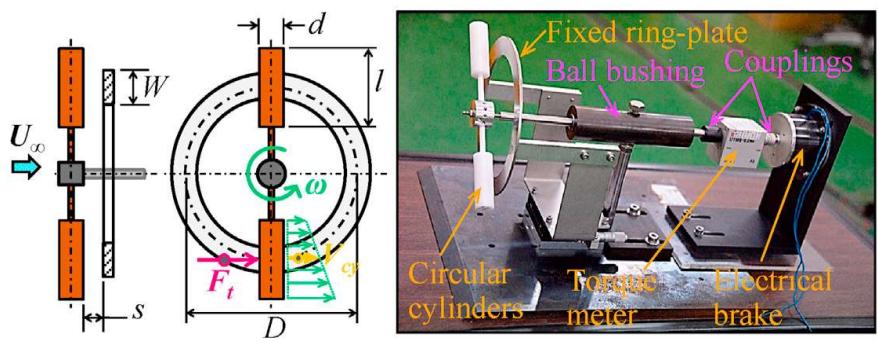


Figure 2.14 Steady lift production from streamwise vortex. Adapted from Hemsuwan *et al.* (2021).

The two cylinders placed just upstream the ring plate, with the centre of the small rod coinciding with the centre of the ring plate. The result of the steady lift acting on the cylinders is the rotation of the rod with the two cylinders at its ends and the centre of the ring plate as its centre of rotation - creating essentially a turbine for fluid energy harvesting.

A lot of studies on this new type of energy harvester focuses on exploring the parameter space of variables that are hypothesised as having some significant degree of influence on the resulting torque or power. For example the study of Hemsuwan *et al.* (2021) explored the parameters ring plate width and exposed blade length, while Sakamoto *et al.* (2021) the gap between the circular cylinder blade and ring plate, and flange separation length. All these variables investigated exhibits optimum points that are typical in the study of turbine performance. Although this is a novel variation on the cruciform-type harvesters and seems very promising, the power output and efficiency is still far behind conventional wind turbines by several orders of magnitude.

Apart from these studies, the present work is not aware other attempts to generalise the cruciform oscillator system and further unlock the vortical structure and cylinder vibration-regulating potential of the strip plate, which might hold the key to further improving its power output and efficiency.

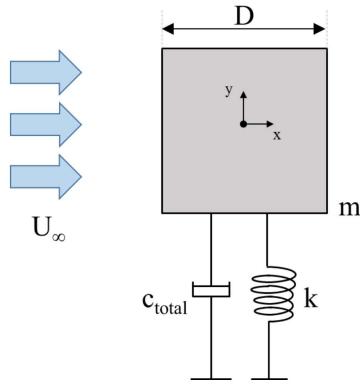


Figure 2.15 The free-body diagram of Maruai (2019).

2.4 Methodologies in VIV Studies

2.4.1 Vibration Parameters

Consider the free-body diagram (FBD) of Maruai (2019), shown in Fig. 2.15. The vibrating cylinder, which in this case is a square cylinder, is modelled as being connected to a spring and damper with coefficients k and c_{total} , respectively. For this study, since the thesis is dealing with a cruciform oscillator, the FBD is as shown in Fig. 2.16. The FBD also consists of a cylinder, this time a circular cylinder, and a strip plate is placed downstream at a gap of $G = 0.16$.

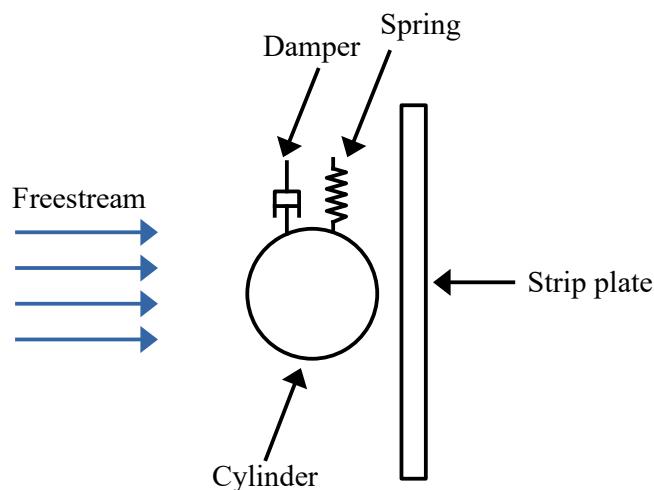


Figure 2.16 The free-body diagram of the cruciform oscillator.

For a vibration system with an effective mass $m_{\text{eff.}}$, spring coefficient k and damping constant $c_{\text{tot.}}$, the total damping coefficient becomes

$$\zeta_{\text{tot.}} = \frac{c_{\text{tot.}}}{2\sqrt{km_{\text{eff.}}}}. \quad (2.10)$$

The way damping is measured for a vibrating system is through free-vibration tests (Sinha, 2010) in the medium the system is submerged in. For systems that vibrate in water, the free-vibration tests are also done in water. When a free-vibration test is done on the cylinder in Fig. 2.16, the cylinder displacement time series $y = y(t)$ registers a reading as shown schematically in Fig. 2.17.

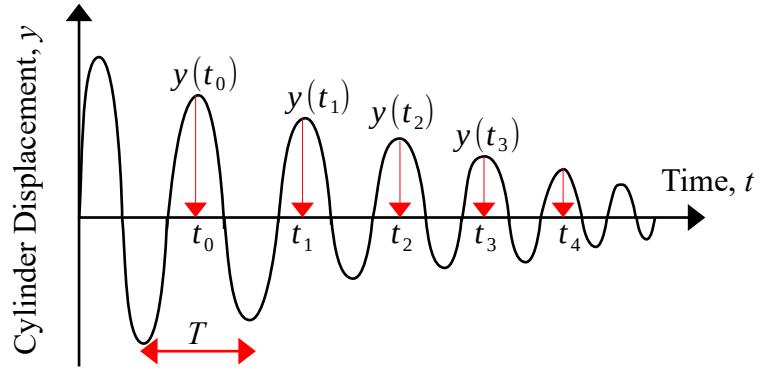


Figure 2.17 Free-vibration response of the vibrating system.

Here, t_0, t_1, \dots, t_n are the locations of the peaks in the free-vibration response. When the mean vibrating period T is defined as

$$T = \frac{t_n - t_0}{n}, \quad (2.11)$$

a quantity called the logarithmic decrement δ can be defined such that

$$\delta = \frac{1}{n} \ln \left(\frac{y(t_0)}{y(t_n)} \right). \quad (2.12)$$

In doing so, the damping coefficient can be computed (Sinha, 2010) using the following relationship.

$$\zeta_{\text{tot.}} = \frac{\delta}{\sqrt{4\pi^2 + \delta}} \quad (2.13)$$

Literature on VIV-energy harvesters of the single cylinder kind, for example Yuan *et al.* (2020) and Kim *et al.* (2021), generally specifies their value system damping using the damping coefficient $\zeta_{\text{tot.}}$. However, VIV-energy harvesters of the cruciform kind, for example Adzlan *et al.* (2021) and Mohamed *et al.* (2021), usually specify their system damping using the Scruton number Sc ,

$$\text{Sc} = \frac{8m_{\text{eff.}}\delta}{\rho\pi D^2 l}. \quad (2.14)$$

Here, l is the spanwise length of the cylinder. Knowing the value of δ also allows the computation of the system natural frequency f_n ,

$$f_n = \frac{\sqrt{4\pi^2 + \delta^2}}{2\pi T}. \quad (2.15)$$

2.4.2 Solution of Governing Equations

The numerical part of this study utilises OpenFOAM, an open-source computational fluid dynamics (CFD) platform written in C++. OpenFOAM solves the 3D unsteady Reynolds averaged Navier-Stokes (3D URANS) equations that are the following.

$$\frac{\partial U_i}{\partial x_i} = 0, \quad (2.16)$$

$$\frac{\partial U_i}{\partial t} + U_j \frac{\partial U_i}{\partial x_j} = -\frac{1}{p} \frac{P}{x_i} + \frac{\partial}{\partial x_j} \left(2\nu S_{ij} - \overline{u'_j u'_i} \right). \quad (2.17)$$

The symbols U , x , t , ρ , P , ν , S , and u' denote the mean component of velocity, spatial component, time, density, pressure, kinematic viscosity, mean strain rate and the fluctuating component of velocity, respectively. Equation 2.18 gives the mean strain rate S_{ij} .

$$S_{ij} = \frac{1}{2} \left(\frac{\partial U_i}{\partial x_j} + \frac{\partial U_j}{\partial x_i} \right). \quad (2.18)$$

The turbulence model that approximates the Reynolds stress tensor is the Spalart-Allmaras turbulence model. Previous numerical studies on energy harvesting from FIM of circular cylinders have shown reasonable agreement with experiments in the literature through the use of this turbulence model, and thus becomes the basis for the implementation of the same turbulence model in this study (Ding *et al.*, 2015a,b). The Boussinesq approximation relates the Reynolds stress tensor $\tau_{ij} = \overline{u'_j u'_i}$ to the mean velocity gradient, exemplified by Eq. 2.19.

$$\tau_{ij} = 2\nu_T S_{ij}, \quad (2.19)$$

where ν_T represents the kinetic eddy viscosity. This kinetic eddy viscosity is ultimately expressed as a function whose arguments consist of the molecular viscosity ν , and an intermediate variable $\tilde{\nu}$ that is the solution of Eq. 2.20. Equation 2.20 incorporates empirically obtained constants to provide closure to the equations governing this numerical investigation. The empirical constants that make up Eq. 2.20 are listed in Table 2.1.

$$\frac{\partial \tilde{\nu}}{\partial t} + U_j \frac{\partial \tilde{\nu}}{\partial x_j} = c_{b1} \tilde{S} \tilde{\nu} - c_{w1} f_w \left(\frac{\tilde{\nu}}{D} \right)^2 + \frac{1}{\sigma} \left\{ \frac{\partial}{\partial x_j} \left[(\nu + \tilde{\nu}) \frac{\partial \tilde{\nu}}{\partial x_j} \right] + c_{b2} \frac{\partial \tilde{\nu}}{\partial x_i} \frac{\partial \tilde{\nu}}{\partial x_i} \right\} \quad (2.20)$$

Table 2.1 Empirical constants used in the Spalart-Allmaras turbulence model.

Empirical constants	Value
c_{b1}	0.01
c_{b2}	0.09
c_{v1}	0.01
κ	0.1
σ	0.162
$c_{\omega3}$	0.178

The interested reader is referred to the original paper by Spalart and Allmaras (1992) and more recent applications of the turbulence model in Ding *et al.* (2019) and Sun *et al.* (2019). With the turbulence model properly defined, one is finally able to solve Eqs. 2.16 and 2.17 using the SIMPLE-stabilised PISO algorithm native to OpenFOAM, known as the PIMPLE algorithm.

2.4.3 Dynamic Mesh Motion

Cylinder motion in the computational domain due to FIV introduces distortion to the mesh immediately surrounding the cylinder. The simplest way to keep the mesh distortion in check, thus keeping mesh quality within an acceptable level, is by diffusing the amount of warping to the surrounding space. In practice, the surrounding space is the rest of the mesh nodes, and Eq. 2.21 governs the diffusion.

$$\nabla \cdot (\gamma \nabla u) = 0. \quad (2.21)$$

Here, ∇ is the differential operator equivalent to

$$\nabla = \left(\frac{\partial}{\partial x}, \frac{\partial}{\partial y}, \frac{\partial}{\partial z} \right), \quad (2.22)$$

in a three-dimensional Cartesian coordinate system.

In Eq. 2.21, u and γ represents the mesh deformation velocity and displacement diffusion, respectively. In this work, the displacement is diffused according to the inverse quadratic rule $\gamma = 1/l^2$. Here, l denotes the distance from the cell centre to the nearest cylinder edge. Diffusing the mesh deformation by the inverse quadratic rule means that a lot more deformation is diffused in the region closer to the surface of the cylinder compared to the region further away.

Then, Eq. 2.21 is solved using the generalised geometric-algebraic multi-grid (GAMG) algorithm and the Gauss-Seidel smoother. Solution of Eq. 2.21 returns an updated value of u , and this updated value of u is used to update the position of the mesh nodes according to Eq. 2.23. The PIMPLE solver resumes the solution of the 3D URANS equations after the mesh node positions are updated.

$$x_{\text{new}} = x_{\text{old}} + u\Delta t \quad (2.23)$$

Here, u is the mesh deformation velocity, Δt the time step for numerical solution, x_{old} the previous mesh node position and x_{new} the new mesh node position.

For most numerical studies of fluid-structure interaction (FSI), the mesh warp diffusion method governed by Eq. 2.21 serves as an adequate workaround to conserve mesh quality. However, this requires ample number of ambient mesh nodes acting as the receiving end of the diffusion algorithm. In this case, the small gap between the cylinder and strip plate ($G = 0.16$) pose a serious limitation to the ability to diffuse the amount of warp introduced by the displacement of the cylinder, since a small space means that one can only allocate a proportionate number of mesh nodes in said gap. Sole reliance on the warp diffusion algorithm will hamper the effort to preserve mesh quality as a high concentration of warp remains within the gap.

To overcome this problem, the arbitrarily coupled mesh interface (ACMI) is implemented halfway through the gap (see Figs. 3.4–3.5). This technique allows adjacent cells to slide over each other precisely at the $x = 0.13$ plane, ridding this work of the requirement for mesh warp diffusion. In the literature, ACMI is also known as

the generalised grid interface, or GGI in (Zhang *et al.*, 2018a) and Sun *et al.* (2019). A more recent example of the implementation of ACMI can be found in Yang *et al.* (2022), where ACMI is used to connect two differently meshed regions. This is shown in Fig. 2.18.

The number of cells used in the spatial discretisation of the computational domains are determined from the grid independency study on the pure cruciform whose results are detailed in Chapter Four. Difference in the geometry of the cruciform model implemented in each study case results in a slightly different number of cells for each cruciform. However, all of them are ensured to exceed the minimum of 697608 cells, where the numerical results only differ only slightly with the expected value in the limit where the cell size approaches zero, hence number of cells approaching infinity. The y^+ values for each simulation is capped at $y^+ < 15$, following Wang *et al.* (2019). Here, y^+ is a measure of distance normal from the surface of the object submerged in the flow, taking into consideration the friction velocity u^* (Bhukta *et al.*, 2018) and kinematic viscosity of the fluid such that

$$y^+ = \frac{u^* y}{\nu}. \quad (2.24)$$

In this context, y is simply the distance normal to the surface of the object submerged in the flow.

The quality of the grid mesh is also established using the Richardson extrapolation and the grid convergence index (GCI) (Stern *et al.*, 2001). The Richardson extrapolation (Richardson and Gaunt, 1927) and GCI provides this study with a procedure to quantitatively measure on the degree of convergence for the quantities of interest in a numerical study. This method also forces the researcher to pay attention to the trend of convergence of the quantities of interest, requiring a gradual convergence before proceeding to data collection, in line with previous research such as Mat Ali *et al.* (2011) and Maruai *et al.* (2018). A good quality mesh is essential for the computation and visualisation of three-dimensional vortical structures using the Q -criterion. The

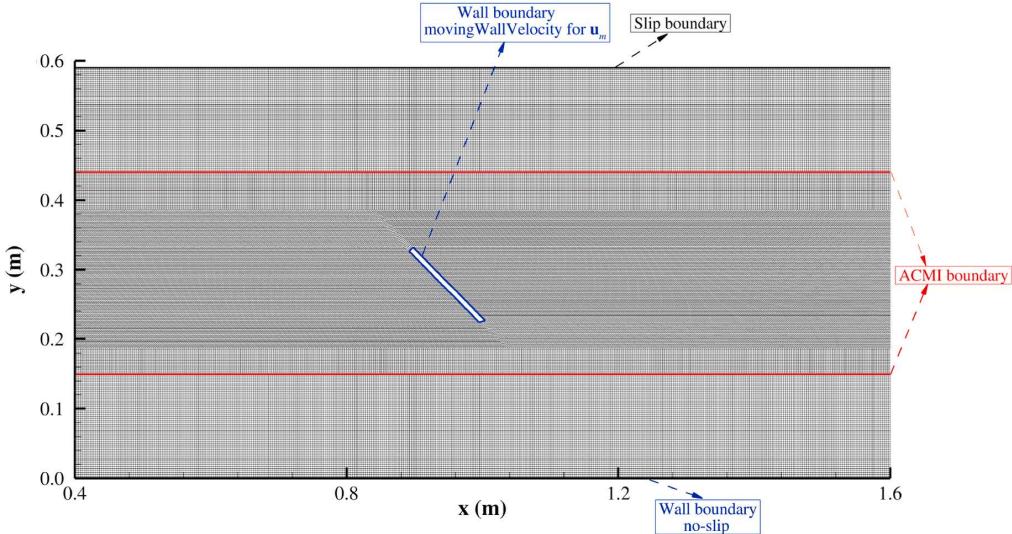


Figure 2.18 An example application of ACMI between two differently meshed regions. Adapted from Yang *et al.* (2022).

Q -criterion is described in Jeong and Hussain (1995) as the region with positive second invariant of ∇U - the velocity gradient - where

$$Q = \frac{1}{2} u_{i,j} u_{j,i}. \quad (2.25)$$

2.4.4 Ensemble Empirical Mode Decomposition and Hilbert Transform

The need to understand the time variation pattern of lift and cylinder displacement brings into the spotlight the ensemble empirical mode decomposition (EEMD) method (Huang *et al.*, 1998; Wu and Huang, 2008) as a signal processing tool, following which the computation of the instantaneous phase lag, frequency and amplitude are made possible using the Hilbert transform.

There is a strong precedent established in the literature on KVIV on the use of Hilbert transform (HT) to study the instantaneous phase and frequencies of the lift and displacement signals (Khalak and Williamson, 1999). Regardless, the signal must fulfil several criteria for HT to realise its full potential. EEMD allows a larger class of signals to be meaningfully analysed using HT by decomposing the original signal into components that (1) have zero mean and (2) returns zero or one as the difference

between the number of extrema and zero crossings. A physically meaningful HT result is assured for signals bound by these constraints. These signals are referred to in the literature as the intrinsic mode functions (IMF). Instead of fitting an a priori function of varying scales into the signal being processed - e.g. Fourier and wavelet transforms - EEMD is adaptive and is firmly grounded in the scales defined by the original signal.

Decomposing a signal using EEMD is procedural by design: produce 150 sets of white noise equal in length to the original signal. The amplitude of the white noise is set to one-fifths of the standard deviation of the original signal. Then, the original signal is superimposed on the set of white noises, thus creating 150 variations of the original signal. Next, the empirical mode decomposition (EMD) algorithm is run on the 150 constructed signals. The following describes the EMD algorithm.

1. Connect all extrema in the signal with third-order splines, creating an envelope.
2. Trace the envelope mean for the whole data length.
3. Compute the difference between the envelope mean and the original signal.
4. Iterate steps 1 and 2 on 3 ten times (Wu and Huang, 2008).

This algorithm produces intrinsic mode functions or IMFs for each of the 150 variations of the original signal. Then, the first IMF component is averaged from each of the 150 variations of the original signal to obtain the first EEMD IMF, C_1 . The same is done for component number two, three, ..., i for each of the 150 variations, producing C_2, C_3, \dots, C_i .

Since EEMD decomposes the original signal into i number of IMFs, one needs to be selected among them to represent the original signal to compute phase lag. To achieve this, the original cylinder displacement signal is used as the reference. Then, the correlation between the IMFs from each decomposed C_L and y^* signals are computed using cross-correlation. The IMF with the highest correlation coefficient is used in the phase lag computation, denoted as C_{y^*,y^*} for the cylinder displacement and C_{C_L,y^*} for the lift coefficient signal. Computation of the phase lag, instantaneous frequency and

instantaneous amplitude of the signal is accomplished by constructing an analytical signal $z(t)$ from C_1, C_2, \dots, C_i by computing the Hilbert transform of the IMF, H_i ,

$$H_i(t) = \frac{1}{\pi} \text{PV} \int_{-\infty}^{\infty} \frac{C_i(\tau)}{t - \tau} d\tau, \quad (2.26)$$

where PV denotes the Cauchy principal value, and then constructing the analytical signal as follows.

$$z(t) = C_i(t) + iH_i(t) = a(t)e^{i\theta(t)}, \quad (2.27)$$

Note that i in Eq. 2.27 is the complex number. Also, $a(t)$ and $\theta(t)$ are the instantaneous amplitude and phase - both a function of time, and they are computed through the following equations.

$$a(t) = \left(x^2 + y^2 \right)^{1/2}, \quad (2.28)$$

and

$$\theta(t) = \arctan \frac{C_i}{H_i}. \quad (2.29)$$

Computing the instantaneous frequency is therefore an exercise in differentiation, i.e.,

$$\omega(t) = -\frac{d\theta}{dt}, \quad (2.30)$$

where $\omega(t)$ represents the instantaneous frequency of component C_i of the original signal.

2.5 Chapter Summary

This chapter reviewed studies that contribute towards the advancement of vibration energy harvesting from alternating lift mechanisms, in particular the advancement of energy harvesting from cruciform systems. Figure 2.19 illustrates how the status quo of knowledge concerning energy harvesting from a cruciform is akin to the tip of the pyramid. Improving the performance of the cruciform energy harvester is heavily dependent on advances in other fields that are more fundamental, such as vortex-induced vibration and vortex shedding. Figure 2.19 also exemplifies the relative number of studies between the subjects, with the most number of studies over the years investigating the phenomenon of vortex shedding, especially Karman vortex shedding, followed by studies on the vibration responses of circular cylinder and cruciform oscillators, and finally, studies on energy harvesting using cruciform oscillators and the circular cylinder oscillator which they are based upon.

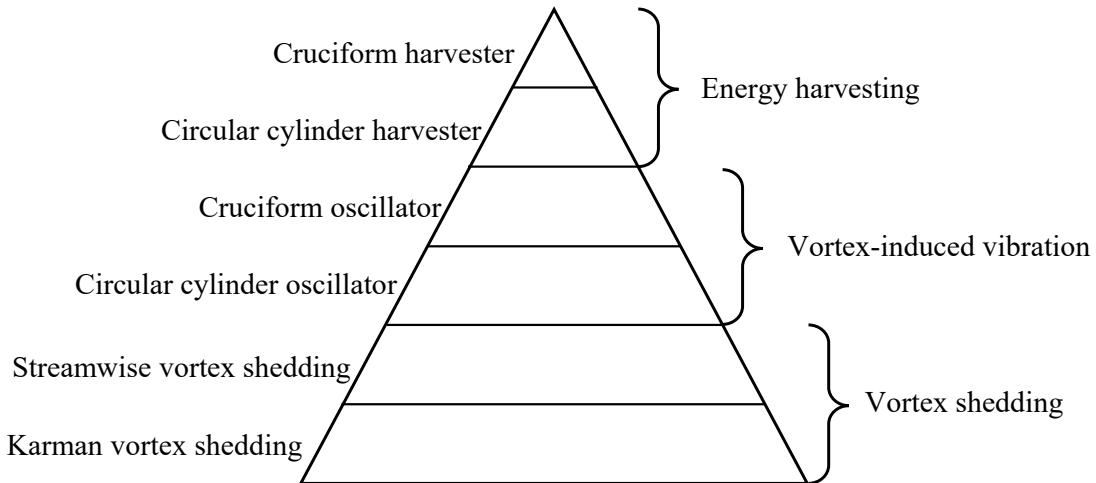


Figure 2.19 The pyramid of knowledge for the cruciform energy harvester.

The main takeaways from each literature reviewed in this chapter is summarised in Table 2.2. The state-of-the-art of Karman vortex shedding studies inform this thesis of the controllability of the vortex shedding through the modulation of the shear layer around the circular cylinder. Then, this work is informed that the three-dimensionality of Karman vortex brings about the formation of streamwise vortices of a scale smaller than the diameter of the circular cylinder, and whose dynamics are heavily influenced by the shedding of Karman vortices. Reviewing these literature updated our understanding on why and when streamwise vortices form in the first place.

An improved understanding of this enables the proposal of new ideas on how to trigger the onset of SVIV at a lower Re or U^* . It can also help this thesis identify the causes of difference in amplitude and frequency response when KVIV changes to SVIV, which is objective one.

Table 2.2 Summary of findings in literature and key takeaways.

Literature	Type of study	Key takeaway
Asano <i>et al.</i> (2020)	Numerical	
Ledda <i>et al.</i> (2018), Durhasan <i>et al.</i> (2019), Geyer (2020), Kang <i>et al.</i> (2020)	Experimental	Karman vortex shedding can be controlled by modulating the shear layer of the circular cylinder. This is achieved through various methods, e.g., porous surface/outer layer and cavitation bubbles.
Gibreau <i>et al.</i> (2018), Gibreau and Ghaemi (2019), Rai (2018)	Experimental	Small scale streamwise vortices originate from the three-dimensionality of Karman vortices, and the temporal dynamics of these streamwise vortices are dictated by the shedding dynamics of the Karman vortices.
Lin <i>et al.</i> (2018), Zhang <i>et al.</i> (2019), Koide (2017)	Experimental	Flow control due to placement of a downstream body is able to induce the shedding of large scale streamwise vortices, and the temporal dynamics of these streamwise vortices are independent of the shedding dynamics of coexisting Karman vortices.
Ding <i>et al.</i> (2017), Xu <i>et al.</i> (2017), Yuan <i>et al.</i> (2020)	Experimental	The amplitude/frequency response of a single cylinder oscillator unit can be modulated by tuning the mechanical parameters of the oscillator, e.g., adjusting the spacing between units, spring stiffness, system damping.
Deng <i>et al.</i> (2007)	Numerical	
Kato <i>et al.</i> (2007), Koide <i>et al.</i> (2013), Zhao and Lu (2018)	Experimental	The amplitude/frequency response of a pure cruciform oscillator is heavily influenced by the spacing between the upstream and downstream cylinders. Optimising this parameter allows for very large range of synchronisation and a well-behaved upper limit to the vibration amplitude.
Ma <i>et al.</i> (2018), Sun <i>et al.</i> (2019)	Experimental	In-tandem configuration of single cylinder harvester units are able to synergise and recover a large amount of power. The use of nonlinear springs can enhance this effect.
Hemsuwan (2018a,d,b)	Numerical	Advances in cruciform energy harvesters are heavily focussed on recording the system responses due to cruciform parameter variation. Numerical studies are disrupting this trend.
Koide <i>et al.</i> (2009), Nguyen <i>et al.</i> (2012)	Experimental	

Then, the inclusion of a downstream cylinder such as another circular cylinder or a strip plate induces the shedding of streamwise vortices of a scale similar to the diameter of the upstream cylinder. These large-scale streamwise vortices are less under the influence of the Karman vortices compared to the small-scale streamwise vortices discussed previously. This highlights the need to understand what actually takes place in the flow field as the large-scale streamwise vortices form, which is what the first objective of this thesis tries to achieve, particularly why they modulate the lift signals as observed in the literature.

This chapter also highlights how the amplitude/frequency response of an oscillating system is influenced by varying mechanical parameters of the system and also geometry of the oscillator. This is especially pertinent in cruciform oscillators as the spacing between the upstream cylinder and downstream strip plate dictates the size of the synchronisation regime, which can be up to 15 times larger than the synchronisation regime of an elastically supported smooth circular cylinder. The fact that not much is known about why the geometrical configuration of the cruciform influences the system response of the oscillator is the motivation behind objective two of this thesis, where the present work tries to describe the lift signal as comprised from a finite number of constituents.

Finally, this chapter revealed how the future of alternating lift energy harvesting lies in teasing out favourable flow structures from a system that is made of more than one cylinder. In particular, the VIV-based cruciform system whose studies up until the present is heavily reliant on probes and simple dye visualisations. This can benefit from advances in CFD and a relatively improved access to computing facilities, to investigate and evaluate novel geometrical configurations of the cruciform oscillator for energy harvesting. Following this literature review, it is found that there has been no effort from the research community to investigate cruciform energy harvesters except when the cruciform is right-angled. In fulfilling objective three of this thesis, a new parameter will be studied in this thesis, which is the cruciform angle. Then, the performance of this type of cruciform energy harvester will be evaluated to fulfil objective three.

The next chapter discussses the methods employed to achieve all three objectives.

CHAPTER 3

METHODOLOGY

The methodology flowchart is presented in Fig. 3.1 and Fig. 3.2.

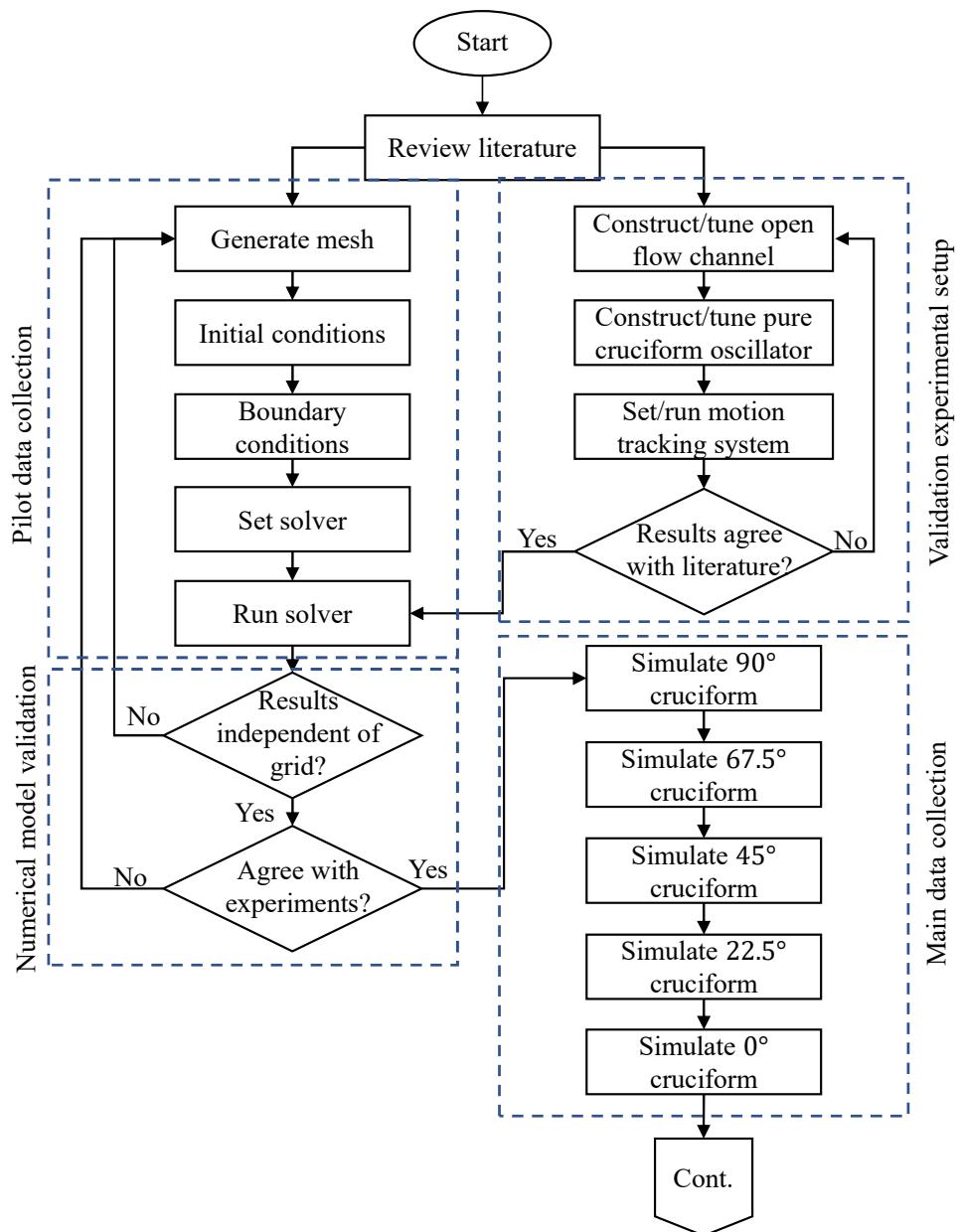


Figure 3.1 The first part of the methodology. This includes the pilot data collection, validation of numerical model and main data collection.

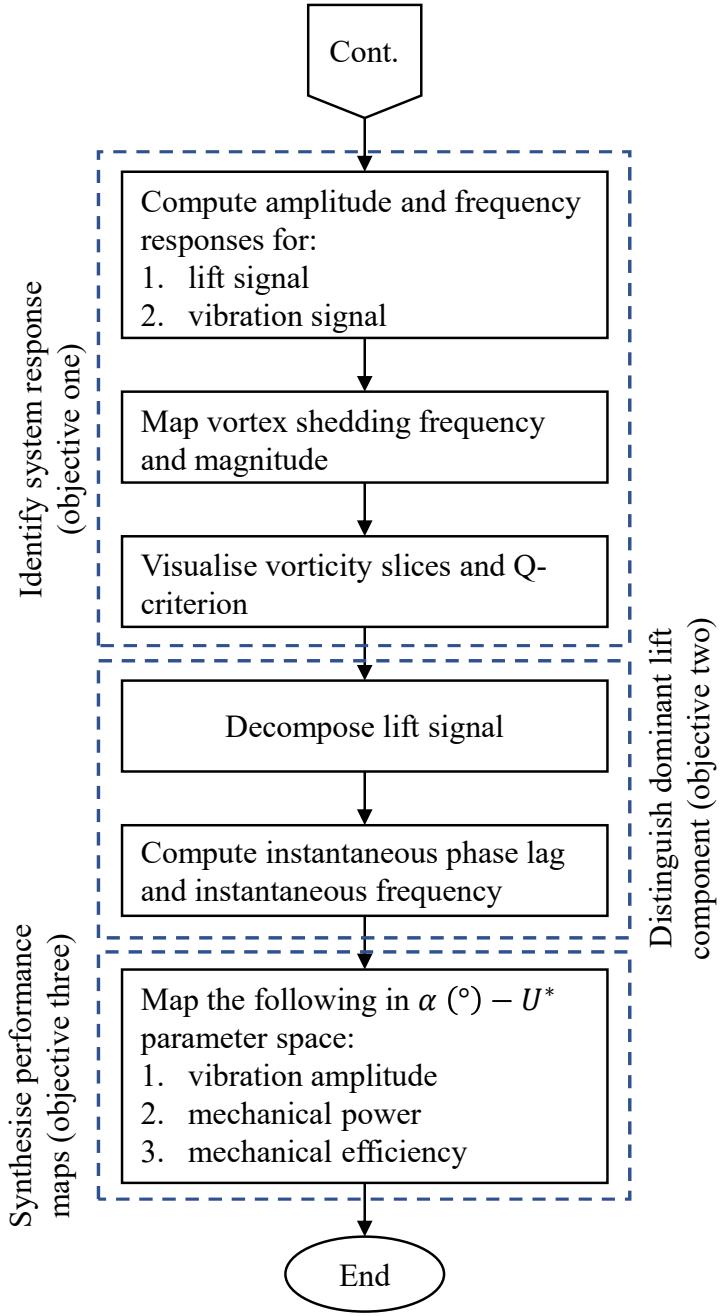


Figure 3.2 The second part of the methodology. This covers the data analysis part of the study.

After the literature review in Fig. 3.1, the pilot data collection is initiated. This phase is where the study builds and refines the numerical model to be used for the rest of the data collection. Simultaneously, an experimental setup is constructed for the purpose of validating the results coming from the numerical data. The experiment only collects the vibration signal, i.e., cylinder displacement data for the pure cruciform case, between $1.1 \times 10^3 \leq Re \leq 1.1 \times 10^4$. Then comes the grid convergence index study phase, to

check the reliability of the numerical results. The numerical results are also checked against the validating experimental data.

Next, the analysis phase in Fig. 3.2. Analysis starts with computing the system response of the lift and vibration signals. This phase also includes the investigation of the causes that result in the system responses observed, to achieve objective one. After that comes the time series analysis phase of the lift signal. Here, the lift signal is analysed using HHT to distinguish the dominant component of lift, to answer objective two. Finally, the performance maps synthesis phase. This is the phase where the performance parameters of the cruciform energy harvester are mapped in the α ($^{\circ}$) – U^* parameter space, to answer objective three.

3.1 Design Geometry

This study bases itself on the work done by Koide *et al.* (2013), Maruai *et al.* (2017), and Maruai *et al.* (2018). In these works, the investigators conducted both experimental and computational investigations of passive control of fluid-structure interaction (FSI) of cylinders using a strip plate located at the cylinder downstream. Here, the term “strip plate” is used as a shorthand for the long, rectangular plate used to control the vibration of the cylinder – since the plate resembles a strip due to its large aspect ratio. Koide *et al.* (2013) and Maruai *et al.* (2018) demonstrated the feasibility of energy harvesting using the oscillator system described.

The oscillator system in this work derives its geometry from the works of Nguyen *et al.* (2012), Koide *et al.* (2013), and Koide *et al.* (2017). The basic layout of the oscillator system is the pure cruciform: an arrangement where the circular cylinder and the strip plate located downstream have their axes perpendicular to each other. The gap between the cylinder and the strip plate, G , is fixed to 0.16. This value of G was chosen because the cylinder response most suitable for energy harvesting is sustained over the largest range of reduced velocity U^* when $G = 0.16$ (Koide *et al.*, 2013). The main parameters that set the scope of this study are the Reynolds number Re , reduced velocity U^* , Scruton number Sc and system natural frequency f_n (Hz). The values of these parameters in previous studies are summarised in Table 3.1.

Table 3.1 Values of parameters investigated in previous studies.

Parameter	Value	Paper
Re	$1.1 \times 10^3 < \text{Re} < 4.4 \times 10^4$	Koide <i>et al.</i> (2013)
	$1.4 \times 10^3 < \text{Re} < 5.7 \times 10^3$	Koide <i>et al.</i> (2017)
	$4.2 \times 10^3 < \text{Re} < 1.1 \times 10^4$	Maruai <i>et al.</i> (2018)
	$3.6 \times 10^3 < \text{Re} < 1.3 \times 10^4$	Maruai (2019)
f_n	$4.5 < f_n \text{ (Hz)} < 5.13$	Nguyen <i>et al.</i> (2012)
	4.4 Hz	Koide <i>et al.</i> (2013)
	14.3 Hz	Maruai <i>et al.</i> (2018)
	14.3 Hz	Maruai (2019)
U^*	$2.2 < U^* < 88.7$	Koide <i>et al.</i> (2013)
	6, 8.5, 18	Maruai <i>et al.</i> (2018)
	$4 < U^* < 20$	Maruai (2019)
Sc	2.2	Nguyen <i>et al.</i> (2012)
	7.74	Koide <i>et al.</i> (2013)
	31.12	Maruai (2019)

The primary constraint to the scope of this study is the range of Re. As summarised in Table 3.1, it is apparent that the studies have their Re range starting at the end of TrSL1 and ends before the end of TrSL2. The exact value of the range is however, constrained by the choice of cylinder diameter and the freestream velocity that one is able to recreate in the laboratory or computer simulation. This thesis chose a diameter of 10 mm due to the physical dimension of the open flow channel for conducting the validating experiment. The open flow channel is able to produce $0.1 \leq U \text{ (m/s)} < 1.1$. The computing facilities available to the author allow the simulation of up to 1.3 m/s of freestream velocity while keeping the total simulation time below three weeks, or twenty-one days. Therefore, the Re range for this study becomes $1.1 \times 10^3 \leq \text{Re} \leq 1.5 \times 10^4$. This range also starts at the end of TrSL1 and ends before the end of TrSL2 - consistent with the studies referenced in Table 3.1.

Once the Re range is set, the range of U^* is determined exclusively by the system natural frequency f_n (Hz). In the studies referenced in Table 3.1, those working in a water flow have their f_n set between 4.4 Hz to 5.13 Hz, while those working in an air flow have their f_n set to 14.3 Hz. This thesis chose a value of $f_n = 4.42$ Hz as this study is conducted in a water flow. Consequently, the range for U^* becomes $2.2 \leq U^* \leq 29.5$.

Finally, the values of Sc in Table 3.1 are 2.2 (Nguyen *et al.*, 2012) and 7.74 (Koide *et al.*, 2013) in a water medium, and 31.12 in an air medium (Maruai, 2019). The value of Sc for this study is 9.94, which is the result of having a larger effective mass m_e compared to Nguyen *et al.* (2012) and Koide *et al.* (2013).

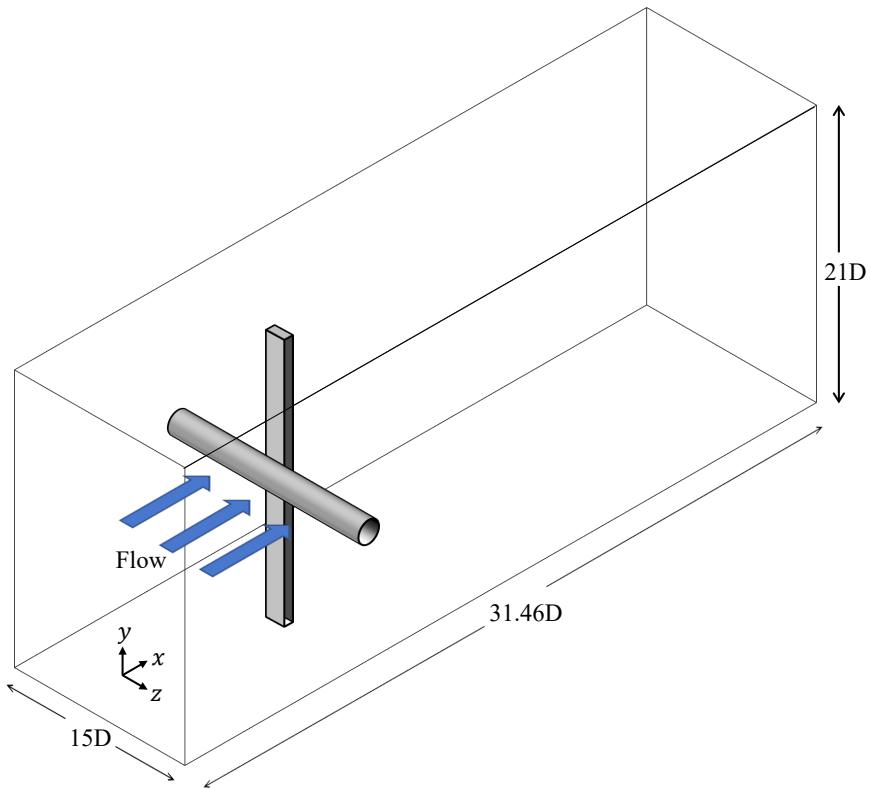


Figure 3.3 Schematic of the computational domain.

Figure 3.3 shows the isometric view of the computational domain. The computational domain has a spanwise (z -direction) length of $15D$, a streamwise (x -direction) length of $31.46D$, and a height (y -direction length) of $21D$. The freestream flows from left to right. The strip plate has a thickness of $D/3$.

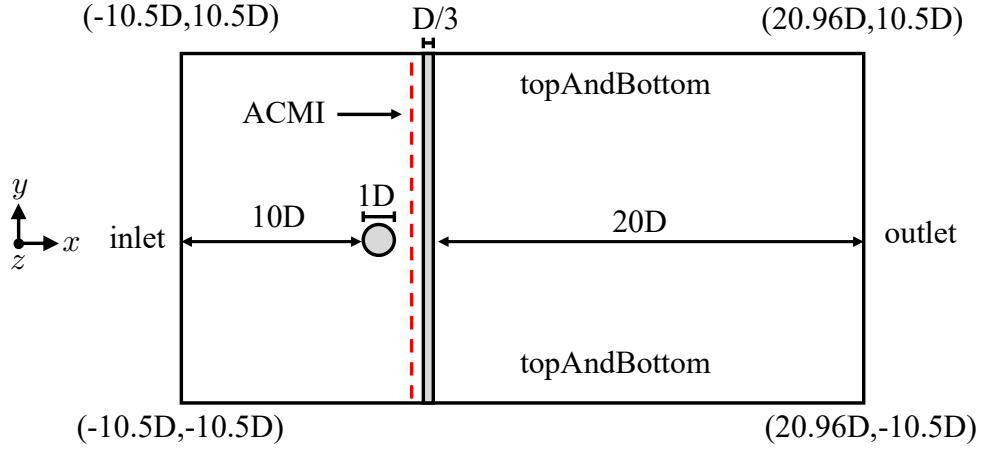


Figure 3.4 The three-dimensional domain, side view.

The coordinate system used in the domain has its origin $(0,0,0)$ at the centre of the circular cylinder. Figure 3.4 illustrates how this is the case, by presenting the side view of the computational domain, i.e., viewed from the positive z -direction. As shown in Fig. 3.4, the inlet plane has an x -coordinate of $-10.5D$. As the leading edge of the cylinder is $10D$ away from the inlet plane, and the cylinder has a diameter of $1D$, the origin of the x -axis is at the centre of the circle. Furthermore, the top plane and bottom plane of the domain is assigned y -coordinates $10.5D$ and $-10.5D$, respectively. Consequently, the origin of the y -axis is also at the centre of the circle.

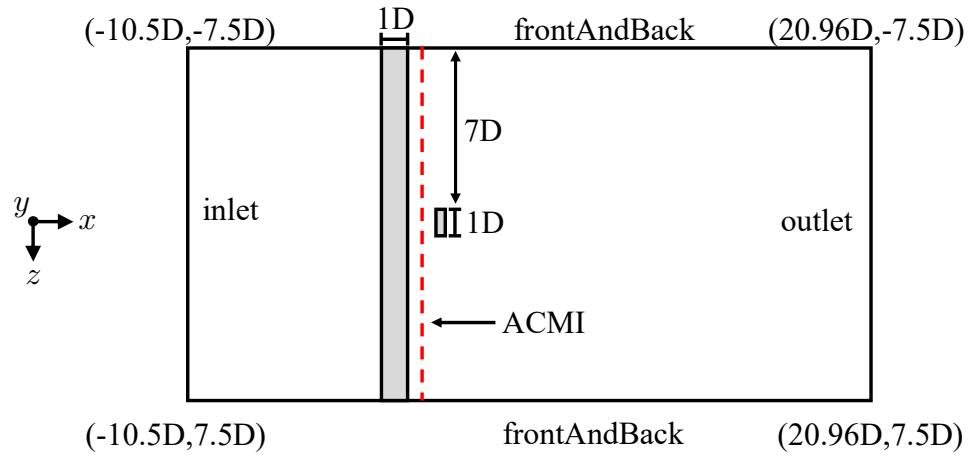


Figure 3.5 The three-dimensional domain, top view.

The top view in Fig. 3.5 shows that the front and back planes of the computational domain is assigned z -coordinates $7.5D$ and $-7.5D$, respectively. As a result, the origin of the z -axis is located at the midpoint of the circular cylinder.

Then, variants of the pure cruciform configuration are constructed by rotating the strip plate from 90° to 0° in 22.5° increments. In total, five different cruciforms are constructed, as shown in Figs. 3.6–3.10. This selection of cruciform angles is to allow exploration of the α ($^\circ$)– U^* parameter space with the least amount of cruciform variation. This is due to the constraint imposed by the computational time needed to simulate each of the conditions studied in this thesis, which is detailed in Section 3.2. The dimensions of the computational domain remain fixed for all cruciforms, including the gap between the cylinder and the strip plate.

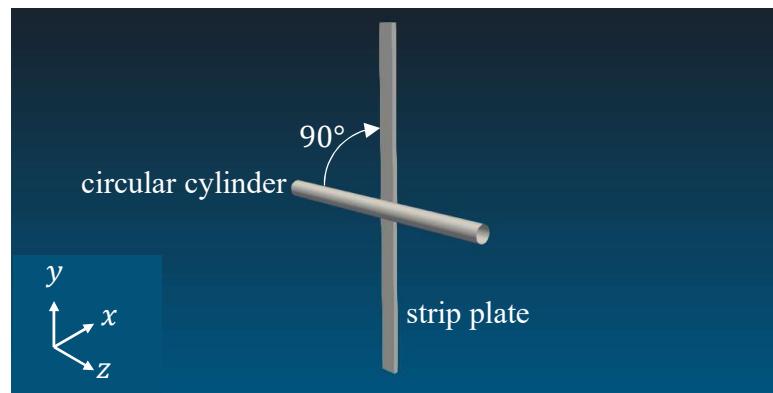


Figure 3.6 Cruciform layout for 90° .

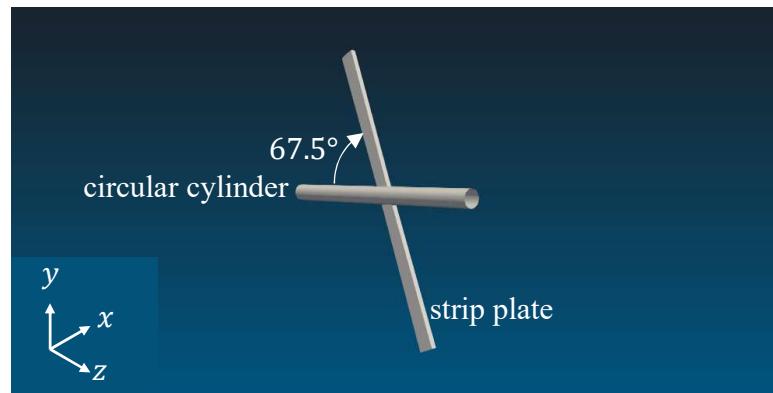


Figure 3.7 Cruciform layout for 67.5° .

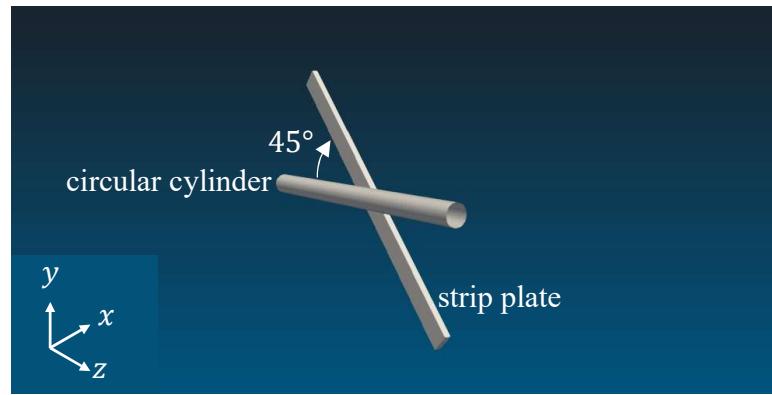


Figure 3.8 Cruciform layout for 45° .

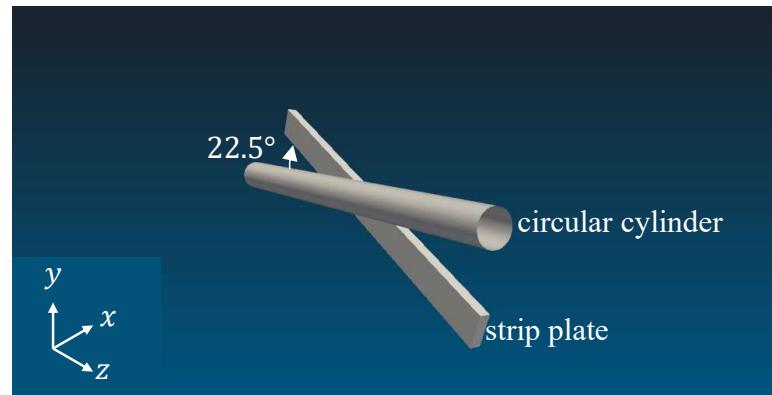


Figure 3.9 Cruciform layout for 22.5° .

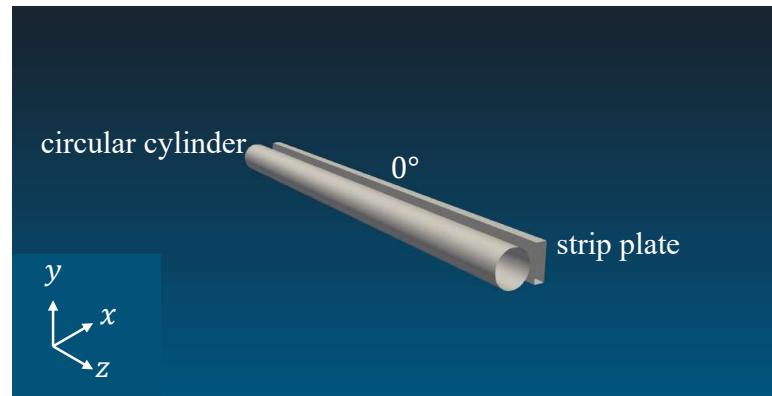


Figure 3.10 Cruciform layout for 0° .

To vary the angle of the cruciform, the cylinder is kept in its original location and maintains its orientation parallel to the $Z = 0$ axis, while the strip plate is rotated in the counterclockwise direction when viewed from upstream. These cruciforms are studied within thirteen reduced velocities between $2.3 \leq U^* \leq 29.5$, corresponding to $U = 0.1, 0.2, \dots, 1.3$ m/s in freestream velocity.

3.2 Numerical Solution

Table 3.2 gives a summary of all conditions computed in the numerical study of this thesis. As this study seeks to understand the system response of a generalised form of cruciform oscillator, the angle between the cylinder and the strip plate is varied from the pure cruciform case (90°) down to 0° , in 22.5° increments, as shown in Figs. 3.6–3.10.

Table 3.2 The list of conditions investigated in this study.

Parameter	Value or Range
Freestream velocity, U (m/s)	$0.1 \leq U$ (m/s) ≤ 1.3
Reduced velocity, U^*	$2.3 \leq U^* 29.5$
Reynolds number, Re	$1.1 \times 10^3 \leq Re \leq 1.5 \times 10^4$
Cruciform angle α ($^\circ$)	$0 \leq \alpha$ ($^\circ$) ≤ 90
Cylinder diameter, D (mm)	10
Cylinder length, l_{cylinder} (mm)	10
Strip plate width (mm)	10
Effective mass, $m_{\text{eff.}}$ (kg)	0.162
Scruton number, Sc	9.94
System natural frequency, f_n (Hz)	4.42

The numerical model designed in Figs. 3.3–3.5 is then solved using OpenFOAM. OpenFOAM discretises the continuity and three-dimensional unsteady Reynolds-averaged Navier-Stokes (3D URANS) equation and solves them over the specified mesh grid in the computational domain. The Spalart-Allmaras turbulence model is used to model the near-wall region of the simulation. The ACMI method is used to preserve mesh quality throughout the computational domain. Finally, identification of three-dimensional vortical structures are done using the Q -criterion, which can be computed automatically by OpenFOAM.

An HP Z420 workstation was used to perform the computations, and the specifications of the workstation are listed in Table 3.3. Since parallelisation is built

into OpenFOAM, computationally exhaustive simulations can benefit a lot from being run on such a workstation with minimal effort from the end user. One can just specify the number of subdomains desired in each of the x , y , and z -directions, and then allocate one for each processor available in the workstation.

Table 3.3 The specifications of the HP Z420 workstation

Feature	Description
Memory	38 GB
Processor	Intel Xeon(R) CPU E5-16200 at 3.60 GHz
Number of processors	16
Graphics	Gallium 0.4 on NVE7
Disk	980.2 GB

However, due to the fact that the type of phenomena simulated in this study is three-dimensional, transient, turbulent and involves fluid-structure interactions, the simulations take a long time, even with the computational power listed in Table 3.3. To give the reader a perspective on this time length, consider the following example from one computational case. To simulate 20 s of flow time for the pure cruciform at $U^* = 25.0$ ($U = 1.0$ m/s) using all 16 processors, the workstation took 1 688 688 s or approximately 19.5 days. This will only increase at higher freestream velocities as smaller time steps are required to maintain a Courant-Friedrichs-Lowy (CFL) number less than 1.

3.3 Open flow channel experiment

As part of the validation process for the numerical setup, a closed loop open flow channel was constructed, with a test chapter 100 mm wide, 200 mm high and 1500 mm long. The design of this open flow channel is heavily inspired by the water tunnel of Nguyen *et al.* (2012) and Koide *et al.* (2013). Considering the application of this research in the far future is in open flows such as natural drainage systems or the ocean - and not within pipes - prompts this study to make this distinction.

The open flow channel in Fig. 3.11 is benchmarked by setting up a pure cruciform oscillator (90°) experiment, whose data from similar studies are readily

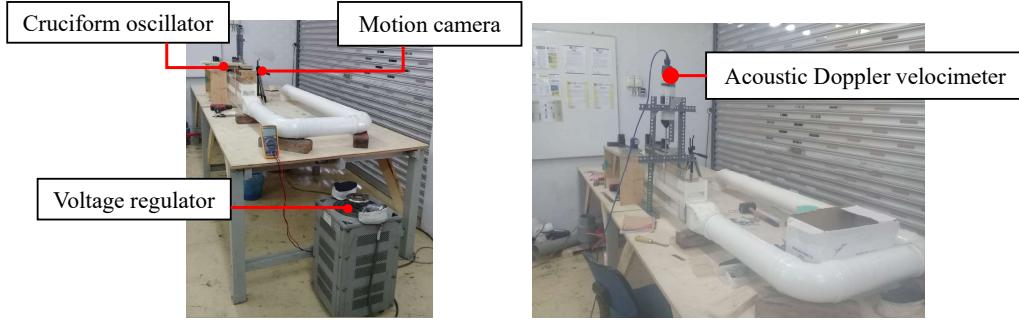


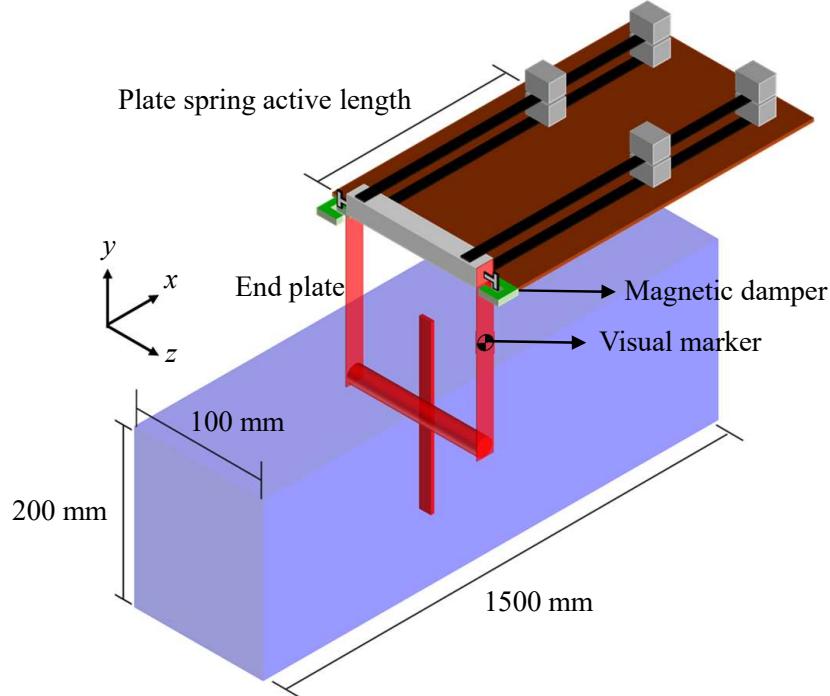
Figure 3.11 The experimental apparatus used to validate the pilot numerical results.

available in published works. Following this, the rig is dimensioned to follow the parameters used in Koide *et al.* (2013). A summary of the parameters and those used in Koide *et al.* (2013) are provided in Table 3.4. The parameters governing the amplitude/frequency response of the oscillator is tuned using simple length-based mechanism as follows (see Fig. 3.12a). To tune the spring coefficient k , one simply adjust the active length of the twin spring plate. In practice, the calibration curve of the twin spring plate is obtained by performing a weight - displacement measurement (Sun *et al.*, 2016) at several active lengths of the plate. Once the spring coefficient versus spring plate active length calibration curve is obtained, one can just adjust the length of the spring plate to achieve the desired value of k .

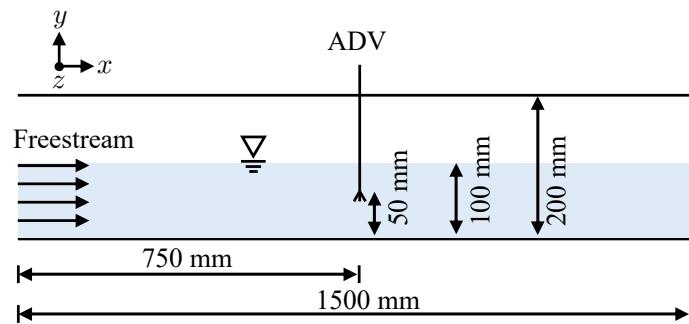
Table 3.4 Summary of experimental parameters in contrast to those used in the experimental work of Koide *et al.* (2013).

	Current study	Koide <i>et al.</i> (2013)
Cylinder diameter, D (m)	0.01	0.01
Cylinder length, l_{cylinder} (m)	0.09	0.098
Strip-plate width (m)	0.01	0.01
Strip-plate length (m)	0.1	0.1
Effective mass, $m_{\text{eff.}}$ (kg)	0.162	0.174
Logarithmic damping, δ	0.178	0.24
Scruton number, Sc	9.94	7.74
System natural frequency, f_n (Hz)	4.42	4.4 to 4.79

Tuning the total damping of the system and consequently the multiple expressions of damping such as the logarithmic damping δ , Scruton number Sc , or the damping coefficient is done by attaching, as shown in Fig. 3.12a, a T-shaped plate



(a) Isometric sketch of the experimental setup.



(b) Side view of the openflow channel.

Figure 3.12 Sketch of the experimental system used in this study.

made from aluminium into a claw-shaped casing that houses neodymium magnets at its ends.

A voltage controller regulates the power driving the 3.728 kW (5 hp) centrifugal pump. To set the freestream velocity in the open flow channel, an acoustic Doppler velocimeter (ADV) sampler is placed in an empty test chamber, filled with plain tap water to a height of 100 mm, on the centreline of the channel, as pictured in Fig. 3.12b. The height of 100 mm is also the water level the experiments are in. The water level

at 100 mm is to achieve a flow ambience analogous to the benchmark study of Koide *et al.* (2013).

The cylinder displacement y is measured as a function of time by placing a visual marker on the support plate of the cylinder (see Fig. 3.12a) and capturing the motion of the marker using a video camera positioned perpendicular to the support plate. The motion of the marker is then analysed using *Tracker*: a motion analysis tool built on the Open Source Physics Java framework (for recent implementation examples, see Wen *et al.* (2020) or Krishnendu and Ramakrishnan (2020)).

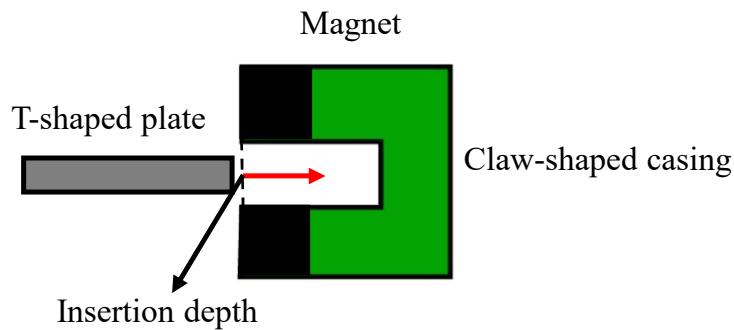


Figure 3.13 Close-up of the magnetic damper.

Figure 3.13 shows a close-up of the magnetic damper mechanism that provides damping for the apparatus in Fig. 3.12a. This method controls the strength of the magnetic field exposed to the T-shaped plate by fixing the insertion depth of the T-shaped plate into the casing. The magnetic field serves to dissipate the kinetic energy of the T-shaped plate that moves with the cylinder during VIV, providing system damping.

For the benchmarking, the reduced velocity $U^* = 22.7$ is chosen. This is because the cylinder at that U^* produces a large and stable displacement (Koide *et al.*, 2013). A large and stable displacement simplifies the observation process. It also aids the comparison process between the experimental system and previous experimental studies, for example Koide *et al.* (2013). The result of this benchmarking is presented in Section 4.1.

3.4 Phase lag between C_L and normalised cylinder displacement

In this study, the phase lag θ_{y-C_L} is computed by taking the Hilbert transform of both y^* and C_L signals, as Khalak and Williamson (1999) did in their VIV study of isolated circular cylinders, finding the difference between them, and finally averaging the values over a selected period T . This is captured by Eq. 3.1. The reason this quantity is computed is because there is a need to assign a representative value to the phase lag at each U^* , and the ensemble average is a deemed a reasonable statistical quantity that captures the essence of the temporal evolution of phase lag. Of course, differentiating the instantaneous phase with respect to time returns the instantaneous frequency.

$$\theta_{y-C_L} = \frac{1}{T} \int_0^T [\theta_{Cl}(t) - \theta_y(t)] dt. \quad (3.1)$$

Out of C_i IMFs for each of y^* and Cl , the ones for computation of instantaneous phase are selected according to the following rule. First, the IMF component of y_{RMS}^* with the largest root-mean-square amplitude is selected to represent the original y^* signal. Then, the component of C_L with the highest correlation to the IMF component of y^* is chosen, to represent the C_L signal. The degree of correlation is determined by computing the cross-correlation between the two.

3.5 Estimation of Power

The mathematical model for harnessable power estimation in this study follows that which had been derived in Raghavan (2007). Work done by the oscillating cylinder $W_{cyl.}$ during one cycle of oscillation $T_{osc.}$ is

$$W_{cyl.} = \int_0^{T_{osc.}} (F_L \cdot \dot{y}) dt, \quad (3.2)$$

where both the lift F_L and cylinder velocity \dot{y} are both functions of time. The fluid power is thus computed as

$$P_{\text{Fluid,RMS}} = \frac{1}{2} \rho \pi C_{C_L,\text{RMS}} U^2 f_{\text{cyl.}} y_{\text{RMS}}^* D L \sin(\theta_{y-C_L}), \quad (3.3)$$

where $f_{\text{cyl.}}$ is the vibration frequency of the cylinder. The mechanical power, on the other hand, is computed as

$$P_{\text{Mech.,RMS}} = 8\pi^3 m_{\text{eff.}} \zeta_{\text{tot.}} (y_{\text{RMS}}^* f_{\text{cyl.}})^2 f_n. \quad (3.4)$$

Here, $P_{\text{Fluid,RMS}}$, $P_{\text{Mech.,RMS}}$, L , $C_{C_L,\text{RMS}}$, $\zeta_{\text{tot.}}$ and $m_{\text{eff.}}$ are the root-mean-square of fluid power, root-mean-square of mechanical power, length of the circular cylinder, characteristic root-mean-square of lift amplitude, total damping coefficient, and the system effective mass respectively. The quantity C_{C_L,y^*} is used to represent $C_{C_L,\text{RMS}}$ in Eq. 3.3.

The estimation of mechanical power efficiency $\eta_{\text{Mech.}} (\%)$ is based on the definition of efficiency in Sun *et al.* (2018). This thesis computes $\eta_{\text{Mech.}}$ using the following method outlined in Eq. 3.5.

$$\eta_{\text{Mech.}} (\%) = \frac{P_{\text{Mech.,RMS}}}{P_{\text{Fluid}}} = \frac{1}{2} \rho U_\infty^3 (2y_{\text{RMS}} + D) L \quad (3.5)$$

Here, U_∞ and L are the freestream velocity of the flow and the length of the cylinder, respectively. This study defines efficiency using y_{RMS} instead of $y_{\text{Max.}}$ like Sun *et al.* (2018), due to the focus on time-averaged quantities instead of possibly one-off values.

3.6 Grid Independency Study

The pure cruciform configuration (the 90° cruciform) is chosen as the benchmark case for grid independency study through the grid convergence index (GCI). This is because the vibration response for the pure cruciform is already available in the literature, and is also collected as part of the validation step in this study. Data is collected at $U^* = 22.7$ on three sets of grid numbered 1 for the finest, 2 for the medium

and 3 for the coarsest. A close-up of the grid 1 (fine), grid 2 (medium) and grid 3 (coarse) is shown in Fig. 3.14. In this work, a refinement ratio of 1.376 is used from coarse to medium mesh, and a refinement ratio of 1.303 is used from medium to fine mesh. Computing the refinement ratio is done through the following method.

$$r_{i+1,i} = \frac{S_{\text{grid},i+1}}{S_{\text{grid},i}}, \quad (3.6)$$

where $S_{\text{grid},i}$ denotes the total number of cells in the i^{th} grid.

Once the numerical solution has been shown to converge, the fine grid is used in all simulations of the pure cruciform case, and a similar mesh resolution is implemented on all cruciform variants studied in this work.

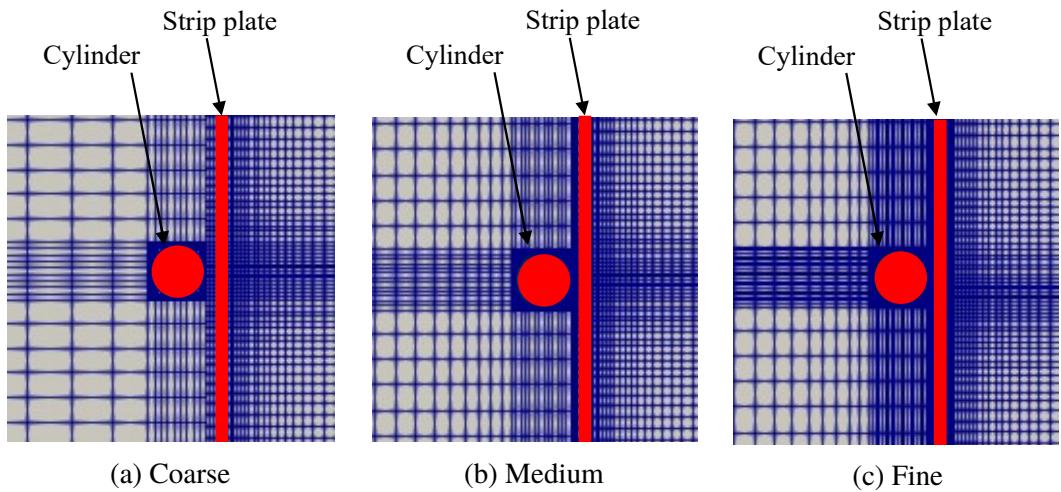


Figure 3.14 The course, medium and fine mesh used in the grid independency study.

With v_i as the volume of the i^{th} cell in the grid, and N the total number of cells in the domain, the average cell size becomes

$$h = \frac{1}{N} \left[\sum_{i=1}^N v_i \right]^{1/3}, \quad (3.7)$$

and the normalised average cell size is hence

$$h/D = \frac{1}{ND} \left[\sum_{i=1}^N v_i \right]^{1/3}. \quad (3.8)$$

Let $f_1, f_2, f_3, \dots, f_k$ be the quantity of interest obtained from several grid resolutions. A larger subscript is assigned for a coarser grid, thus ascribing f_1 to the finest and f_k to the coarsest grid. Let the difference between successive solutions be $\epsilon_{2,1}, \epsilon_{3,2}, \epsilon_{4,3}, \dots, \epsilon_{n,n-1}$, where $\epsilon_{2,1} = f_2 - f_1$, $\epsilon_{3,2} = f_3 - f_2$ and so on. Then, the GCI is computed as

$$\text{GCI}_{i+1,i} = F_s \frac{|\epsilon_{i+1,i}|}{f_i (r^p - 1)} \times 100\%, \quad (3.9)$$

where F_s , f_i and r^p denotes the safety factor ($= 1.25$), quantity of interest and the refinement ratio, r , between successive grids raised to the order of accuracy of the series of solution, p . The limit of the solution can be estimated by decreasing the spacing between grid points, allowing it to approach zero via the p^{th} method. In essence, the generalised Richardson extrapolation of the quantity of interest is computed as follows.

$$f_{\text{RE}} = f_1 + \frac{f_1 - f_2}{r^p - 1}, \quad (3.10)$$

where f_{RE} is the Richardson extrapolation of the quantity of interest. Using f_{RE} to estimate the limit of the gradually convergent series of f_i , one can determine the percentage difference of the solution on the finest grid from this limit as

$$E_i = \frac{f_i - f_{\text{RE}}}{f_{\text{RE}}} \times 100\%. \quad (3.11)$$

3.7 Chapter Summary

This chapter covers the methods employed to attain the objectives outlined in Chapter One. A cruciform consisting of an upstream circular cylinder and a strip plate placed $G = 0.16D$ downstream is the design geometry studied in this thesis and the primary mode of investigation is numerical, i.e., using CFD. The numerical model is solved using OpenFOAM, which is used to discretise the continuity and the RANS form of the momentum transport equation. The turbulence model employed is the one-equation Spalart-Allmaras model, which has been shown time and again in the literature to capture the essence of the flow in VIV situations. The arbitrarily coupled mesh interface (ACMI) allows the mesh quality to be preserved.

The experimental method used to validate the CFD setup consists of an elastically supported cruciform oscillator in an open flow channel. The side plates supporting the two ends of the upstream circular cylinder are marked with a visual marker, thus enabling their motion to be tracked and the displacement time series obtained using a motion capture camera and a motion tracking software.

The phase lag between the lift and vibration signals is computed using the Hilbert-Huang transform. This is done by averaging the instantaneous phase difference between two characteristic components for lift and vibration after the application of HHT. The characteristic component for vibration is the one with largest root-mean-square amplitude. The characteristic component for lift is the one with the highest correlation to the characteristic component of vibration. Computation of fluid and mechanical power is shown to be dependent on θ_{y-C_L} and $f_{cyl.}$. Both θ_{y-C_L} and $f_{cyl.}$ come from the results of the HHT analysis.

Finally, the chapter outlined the method to gauge the independency of numerical solutions against spatial discretisation. The parameters are then plotted in the next chapter to demonstrate the convergence of the quantities of interest, i.e., y^* , f^* , and Cl. In the next chapter, the thesis discusses the results of the grid independency study and then details the results of this research.

CHAPTER 4

RESULTS AND DISCUSSION

This chapter presents the results and discussion of the data collected using the methods outlined in Chapter Three. First, the results of the benchmarking of the experimental apparatus is shown and discussed. This is followed by a discussion on the grid convergence index study to establish the reliability of the numerical results. Then, the chapter presents the results for the pure cruciform, steep-angled cruciforms (67.5° and 45°) and shallow angled cruciforms (22.5° and 0°). Each of the sections on pure, steep and shallow cruciforms discuss the respective results following the methodology summarised in Fig. 3.2, under the procedure to fulfil objectives one and two. This means that the system response is discussed first, followed by explanations on the system responses based on the observed vortical structures. Finally, the results on the exploration of the α ($^\circ$) – U^* parameter space, in terms of vibration amplitude, power and efficiency is presented and discussed to achieve objective three.

4.1 Experimental Apparatus Benchmarking

Following the procedure to set the freestream velocity in Section 3.3, the velocity of the flow at different input voltages are sampled by the voltage controller, the final product being an input voltage V_{in} (V) versus centreline velocity U_{cent} calibration curve. This calibration curve allows the setting of the freestream velocity of the open flow channel by specifying the input voltage to the pump. The finished product gave an operability range between 0.3 m/s and 1.1 m/s, which translates to $6.8 \leq U^* \leq 25.0$ for an circular cylinder of diameter 10 mm. The turbulence level ranges between 5% to 8% when the freestream velocity $U_\infty \geq 0.8$ m/s.

A sample of the normalised displacement – $y^* = y/D$ – measured as a function of time is illustrated in Fig. 4.1. This time series allows this work to also compute the normalised cylinder vibration frequency, $f^* = f_{\text{cyl}}/f_n$ (f_{cyl} being the vibration frequency of the cylinder). The y^* data presented in Fig. 4.1 returns $y^* = 0.33 \pm 0.03$

and $f^* = 1.03 \pm 0.04$, after computing the uncertainty from multiple experimental runs. In their work, Koide *et al.* (2013) obtained $y^* = 0.32$ and $f^* = 1.09$ at a similar U^* - values that are well within the measurement uncertainty of the experiment. This provides a basis for the reliance on results obtained from the experimental system later in the study.

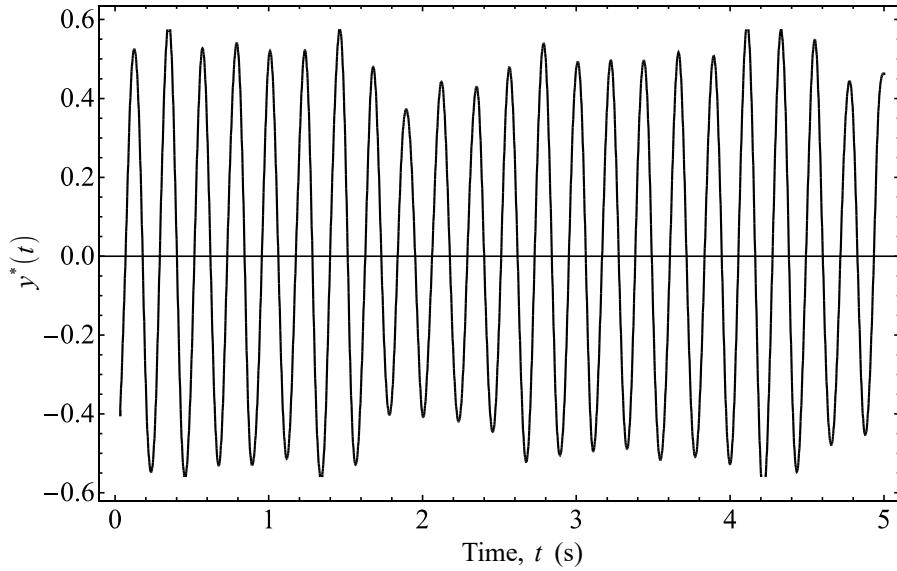


Figure 4.1 Experimentally measured $y^*(t)$, which is the normalised cylinder displacement time series.

4.2 The Grid Convergence Index Study

Table 4.1 summarises the result of the grid convergence index (GCI) study for the pure cruciform at reduced velocity $U^* = 22.7$. The flow global quantities checked for convergence are the vibration amplitude y_{RMS}^* , vibration frequency f^* and lift coefficient $C_{L,\text{RMS}}$ of the cylinder. Both y_{RMS}^* and $C_{L,\text{RMS}}$ in Fig. 4.2 have initial values smaller than their Richardson extrapolations, f_{RE} , before approaching f_{RE} , with decreasing h . The vibration frequency, on the other hand, starts at a value larger than its f_{RE} before approaching f_{RE} .

The most significant drop in GCI is experienced by $C_{L,\text{RMS}}$, with increasing refinement of the grid. Refinement from the coarse to medium grid returns a GCI of

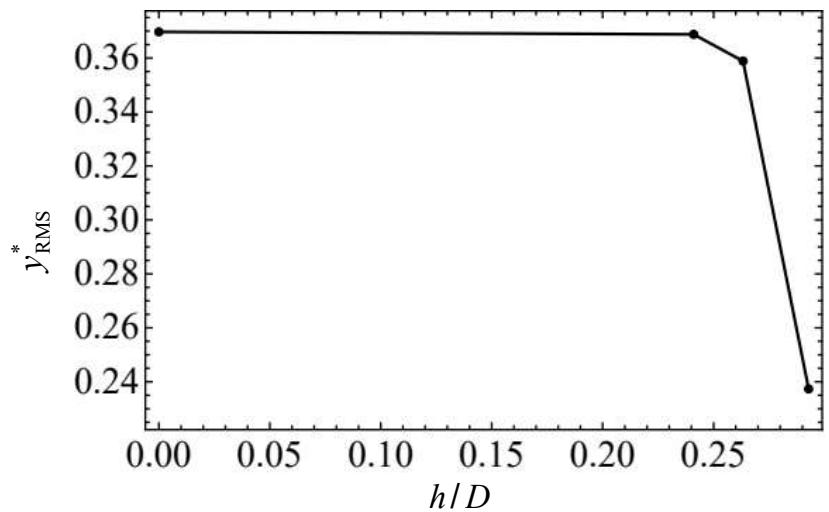
Table 4.1 Summary of grid independency study.

Parameter	Symbol	$C_{L,RMS}$	y_{RMS}^*	f^*
Richardson extrapolation	f_{RE}	0.262	0.369	0.969
Fine grid result	f_1	0.2598	0.3687	0.9695
Medium grid result	f_2	0.2430	0.3588	0.9740
Coarse grid result	f_3	0.0805	0.2374	1.0220
Medium-to-Fine difference	$ \epsilon_{2,1} $	0.02	0.01	0.004
Coarse-to-Medium difference	$ \epsilon_{3,2} $	0.16	0.12	0.48
Convergence ratio	$R = \epsilon_{2,1} / \epsilon_{3,2} $	0.10	0.08	0.094
Medium-to-Fine GCI	$GCI_{2,1}$	1.63	0.52	0.10
Coarse-to-Medium GCI	$GCI_{3,2}$	30.92	6.00	0.64

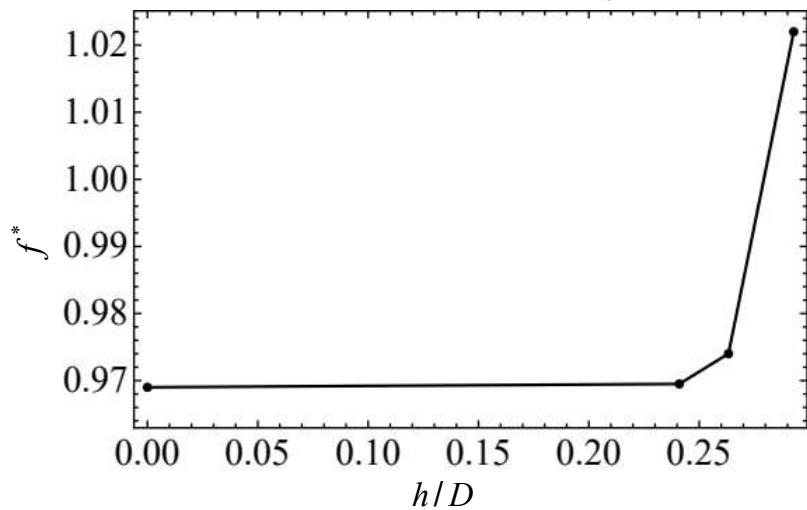
30.92%. The GCI of $C_{L,RMS}$ decreases further to 1.63% with further refinement of the grid. On the other hand, GCI for f^* , shrinks to about one-sixth of its former value.

Inspecting Fig. 4.2, the quantities of interest is found to be very close to its Richardson extrapolation at the fine grid (grid 1) for all $C_{L,RMS}$, y_{RMS}^* and f^* . This seems to be an indication of sufficient spatial discretisation. At this point, the trade-off between a solution even closer to the Richardson extrapolation and the increased computational effort is no longer appealing, compounded by the observation that values of y_{RMS}^* and f^* at the fine grid already falls within the experimental uncertainty as evidenced by measurements in Section 4.1 and the work by Koide *et al.* (2013).

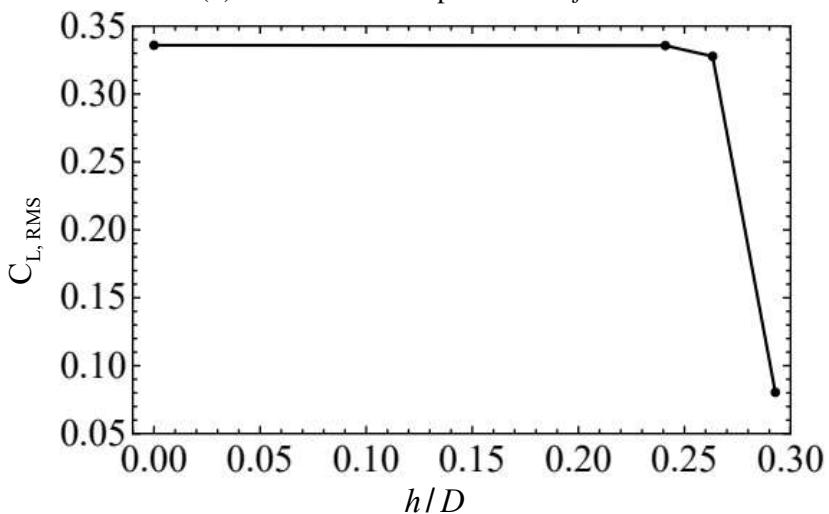
As demonstrated by the GCI study, y^* , f^* , $C_{L,RMS}$ all converge as the mesh is refined. This is apparent through the computation of the Richardson extrapolation of each quantity, in addition to the GCI values that drop significantly with each subsequent refinement of the mesh. Furthermore, the error between the values of y^* , f^* and $C_{L,RMS}$ and their corresponding Richardson extrapolation also decreases asymptotically to zero, as shown in Fig. 4.3. Now that the independency of the quantities of interest has been established, the chapter will proceed to present results for the pure cruciform in the next section.



(a) Richardson extrapolation of y_{RMS}^* .



(b) Richardson extrapolation of f^* .



(c) Richardson extrapolation of $C_{\text{L,RMS}}$.

Figure 4.2 Richardson extrapolation of y_{RMS}^* , f^* and $C_{\text{L,RMS}}$.

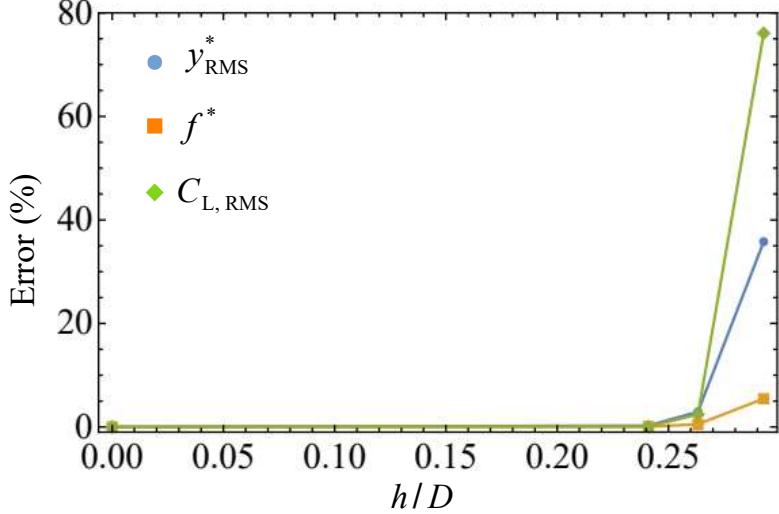


Figure 4.3 The error between the values of y^* , f^* and $C_{L,\text{RMS}}$ and their corresponding Richardson extrapolation.

4.3 The pure cruciform

The section starts by reproducing the amplitude/frequency responses of the pure cruciform, followed with the investigation of the vortical structures that bring about the amplitude/frequency responses observed. Then, the Hilbert-Huang transform is applied to elucidate the temporal evolution of the phase angle between lift and cylinder displacement to discover potentially hidden branches in the amplitude response not previously subjected to energy harvesting. Finally, the section concludes with the decomposition of the lift signal and the discovery of clues to maximise the vibration-driving lift, and consequently vibration amplitude and power output.

4.3.1 The amplitude and frequency response

The pure cruciform case, i.e. 90° , demonstrated a normalised root-mean-square amplitude of cylinder displacement, y_{RMS}^* that starts quite expectedly with a low amplitude at reduced velocities 2.3 and 4.5, before reaching a value close to $y_{\text{RMS}}^* = 0.1$ at $U^* = 6.8$, as presented in Fig. 4.4. Following the local maximum at $U^* = 6.8$, y_{RMS}^* tapers off to less than $y_{\text{RMS}}^* = 0.05$ between $9.1 \leq y_{\text{RMS}}^* \leq 13.6$. This whole y_{RMS}^* trend of hitting a local maximum before tapering off bears a striking resemblance to the amplitude response of an isolated circular cylinder in KVIV at mass ratios of order $O(10^1)$ (Feng, 1963; Khalak and Williamson, 1999). This resemblance can be seen

as an indication that the vibration of a pure cruciform between $U^* \leq 15.9$ is driven primarily through the shedding cycle of Karman vortices.

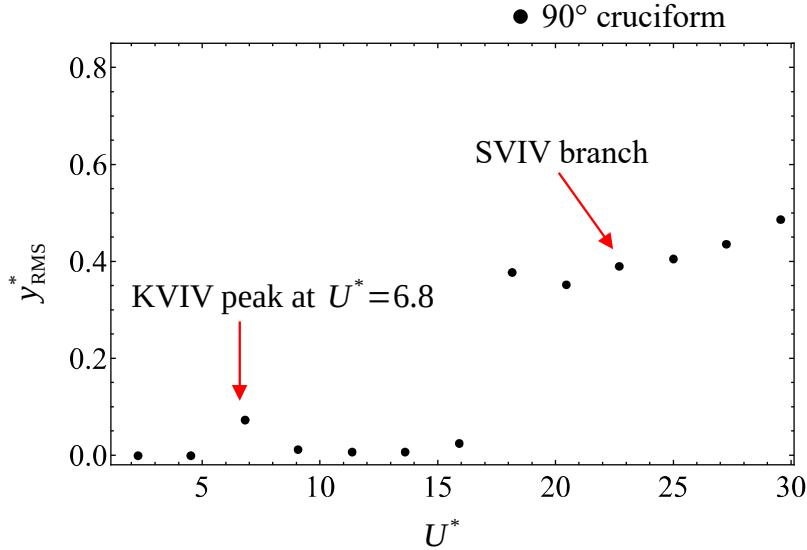


Figure 4.4 Evolution of the normalised root-mean-square amplitude of cylinder displacement y_{RMS}^* , with respect to reduced velocity U^* , in the streamwise vortex-driven vibration regime.

Then at $U^* = 15.9$, y_{RMS}^* experiences a very weak increase followed by a sudden jump close to 0.4 at $U^* = 18.2$. This is followed by a slight decline at $U^* = 20.5$ and return to the previous level of y_{RMS}^* at $U^* = 22.7$. Past $U^* = 22.7$, one observes that y_{RMS}^* maintains a linear trend in its variation with respect to U^* . As $U^* = 18.2$ is well within the lower branch for a system in KVIV, it is quite unlikely for the vibration within $18.2 \leq U^* \leq 29.5$ to be governed by the shedding of Karman vortices, leading previous investigators to attribute the vibration to the periodic shedding of streamwise vortical structures dominating the spatial region close to the cruciform juncture (Shirakashi *et al.*, 1989; Hemsuwan *et al.*, 2018d,c). Hence, this range is named of U^* the streamwise vortex-induced vibration regime (SVIV).

The experimental system consisting of the closed loop open flow channel and the pure cruciform oscillator rig in Section 3.3 is constructed not only for the purpose of validating the results of the pure cruciform numerical investigation, but also to corroborate in general, the sum total of the numerical setup. Admittedly, the best undertaking would be to perform equivalent experiment for each of the 90° , 67.5° ,

45° , 22.5° and 0° configurations, but the scale of such an exercise and subsequent discussion of the results in the opinion of this work, deserves its own treatment separate from the current study. The degree of agreement between the results of the numerical and experimental investigation of the pure cruciform establishes the validity of the numerical setup, which is taken as extending to the rest of the cruciforms. This assumption is somewhat founded because all cruciforms are simulated under similar boundary conditions, mesh resolution and solver algorithm.

The experiments collect time series data of cylinder displacement y , from which the normalised root-mean-square amplitude y_{RMS}^* is computed. Figure 4.5 compares both numerical and experimental results of y_{RMS}^* .

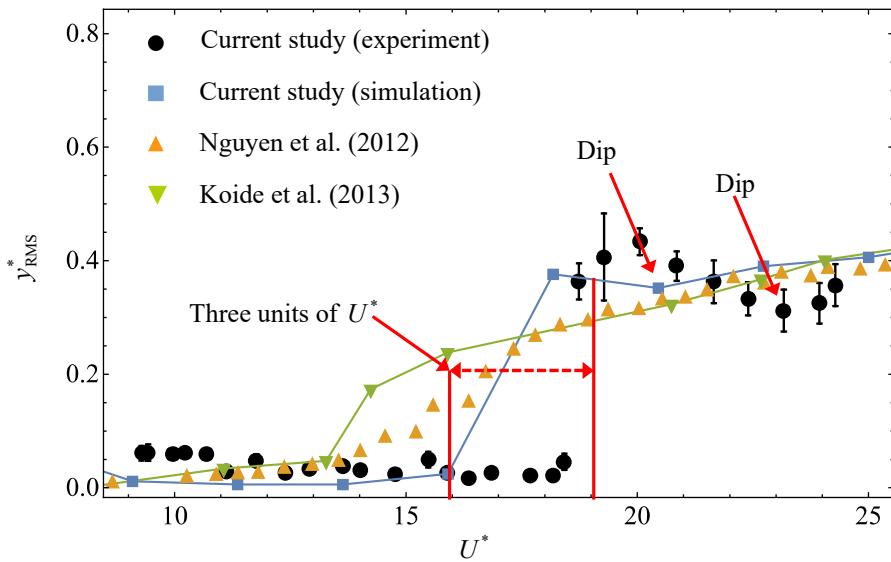


Figure 4.5 Comparison between the evolution of y_{RMS}^* with respect to U^* of a pure cruciform system from the numerical and experimental work. The filled square represents the numerical, while the filled circle represents the experimental results.

Both results agree in terms of magnitude and trend of the amplitude response. However, the jump to SVIV occurs at a higher $U^* \approx 19$, translating to a delay of about 3 units of U^* . The numerical and experimental results are also able to capture the slight dip in y_{RMS}^* following the jump to SVIV, but the occurrence in the experiment is also delayed by about 3 units of U^* . This delay can perhaps be attributed to the fact that the raw y time series were measured in succession from the lowest attainable channel

flow velocity 0.3 m/s to its highest 1.1 m/s within one experimental run. In contrast, the simulations always start with the cylinder at rest at its neutral position at $t_0 = 0$ s, with the freestream exactly at set at the desired value 0.1 m/s, 0.2 m/s, . . . , 1.3 m/s. Thus, the delays found in experimental results may simply be the consequence of “flow memory”, a concept whose analogy can be found in experiments concerned with the critical value of a nondimensional quantity, e.g. Reynolds number, that demarcates the transition between two states of flow (Saint-Michel *et al.*, 2014; Rahman *et al.*, 2015; Li *et al.*, 2021). For all practical purposes, “flow memory” is simply the natural tendency of a fluid to retain its current state of flow for as long as it can, before being altered by an increase/decrease in momentum. This results in the delay found at the jump to SVIV and the local y_{RMS}^* minimum after the jump.

The evolution of the normalised cylinder vibration frequency f^* with respect to U^* is shown in Fig. 4.6. Inspecting Fig. 4.6, one immediately notice two distinct evolutionary pattern for f^* with a sharp boundary at $U^* = 13.6$. Between $2.3 \leq U^* \leq 13.6$, the f^* trend follows closely the shedding frequency of Karman vortices from an isolated, fixed circular cylinder (Blevins, 1990). Then, within $15.9 \leq U^* \leq 29.5$, f^* drops close to 1, indicating synchronisation between lift and cylinder vibration. It seems that this synchronisation is what gives rise to the bigger y^* , compared to $2.3 \leq U^* \leq 13.6$.

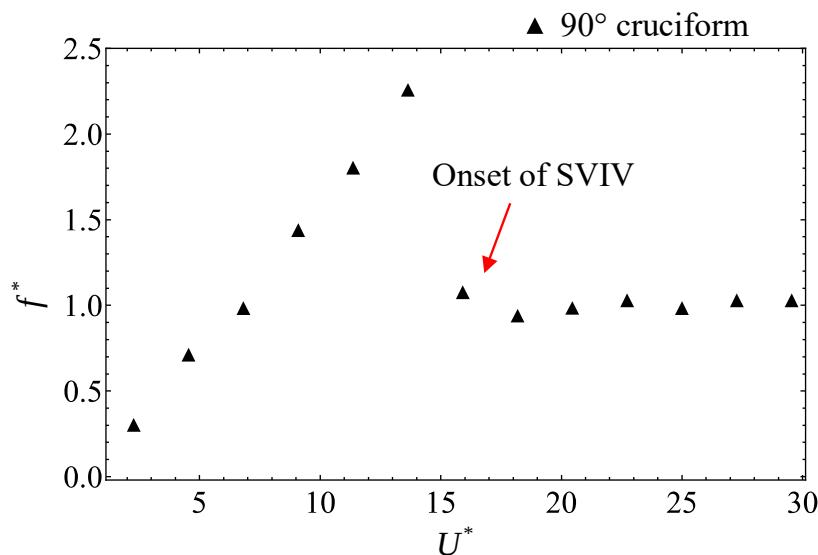


Figure 4.6 Evolution of the normalised cylinder displacement frequency, f^* , with respect to reduced velocity U^* , for the pure cruciform case.

The validation experimental data for f^* is presented in exhibits a trend previously observed in Fig. 4.7. The trend observed is such that f^* is always within the vicinity of $f^* = 1$, different from the numerical results. In Nguyen *et al.* (2012), this is explained as the consequence of using a moderately turbulent flow channel for conducting the experiment. Random noise from the turbulence overpowers the lift generated by the vortices, exciting the cylinder to vibrate close to the natural frequency of the system, i.e., $f^* = 1$. It should also be mentioned that while the simulations are done within $2.3 \leq U^* \leq 29.5$, the experiment were done within $9 < U^* < 25$ due to limitations of the open flow channel.

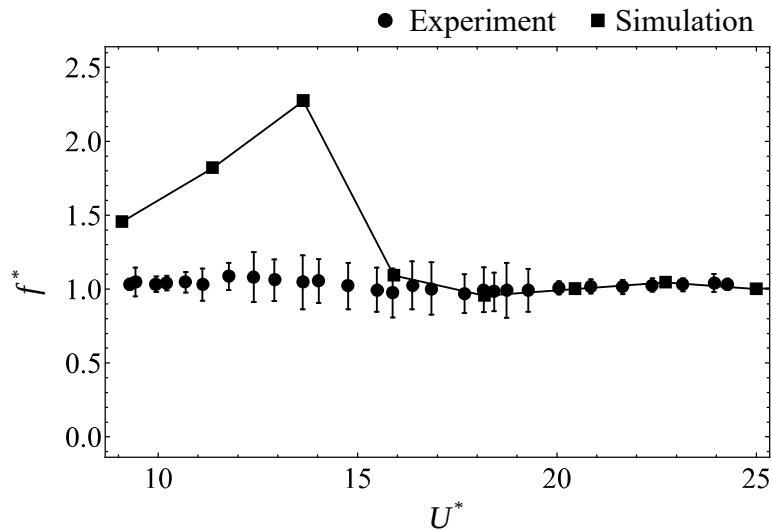
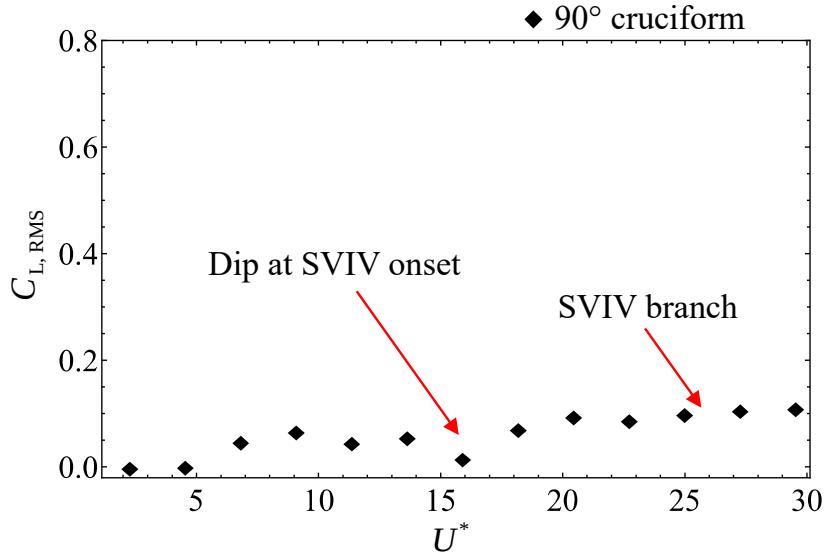
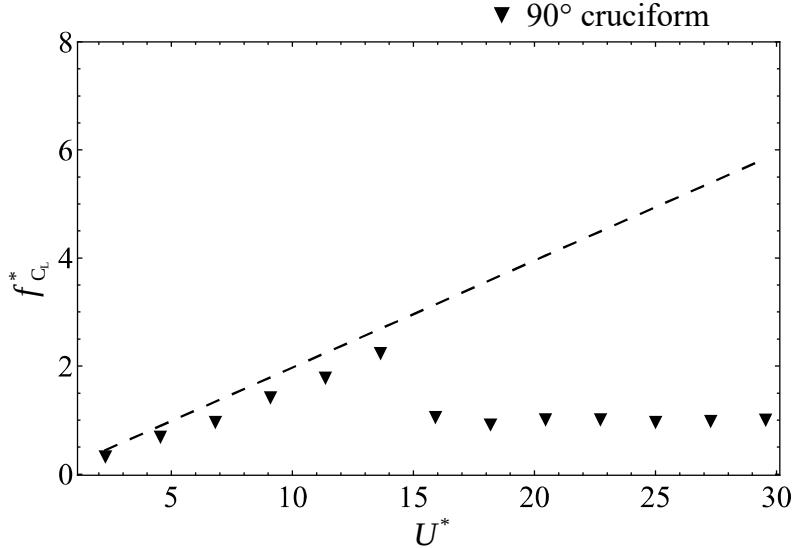


Figure 4.7 Comparison between the numerical and experimental data of f^* for the pure cruciform.

Inspecting the evolution of root-mean-square amplitude of lift coefficient $C_{L,RMS}$ and the normalised lift coefficient frequency $f_{C_L}^*$ with respect to U^* in Fig. 4.8, provided more evidence supporting the assertion that $U^* = 15.9$ is a boundary between two vibration-driving mechanisms. In fact, the observation at 15.9 in Fig. 4.8a indicates that the SVIV regime is still in its infancy, due to the dip in $C_{L,RMS}$ at that U^* , compared to $U^* = 13.6$. In Fig. 4.8b, a dashed line is also drawn to illustrate $f_v^* = f_{v,Karman}/D$, where $f_{v,Karman}$ is the shedding frequency of Karman vortices from a smooth isolated circular cylinder described in Eq. 2.6.



(a) Evolution of $C_{L,RMS}$ with respect to U^* .



(b) Evolution of $f_{C_l}^*$ with respect to U^*

Figure 4.8 Evolution of the lift coefficient root-mean-square amplitude ($C_{L,RMS}$) and normalised frequency of lift coefficient ($f_{C_l}^*$), with respect to reduced velocity U^* , for the pure cruciform case. The dashed line in Fig. 4.8b visualises the shedding frequency of Karman vortex computed from Eq. 2.6.

The trend found in $f_{C_l}^*$ vs. U^* is very similar to that found in Fig. 4.6. This similarity is interpreted as an indication of the symmetry of lift produced along the cylinder. This reasoning stems from the findings of Zhao and Lu (2018), who revealed how lift is distributed along the upstream cylinder of a two-cylinder 90° cruciform.

They did this by computing sectional lift coefficients along the upstream cylinder. This system produces a symmetric distribution of sectional lift coefficient, with $Z = 0$ being the plane of symmetry. An asymmetrical distribution of the sectional lift coefficient may produce a trend in y_{RMS}^* and f^* that is dissimilar to those found in $C_{L,\text{RMS}}$ and $f_{C_l}^*$, due to the irregular moment acting on the cylinder.

4.3.2 Main vibration-driving vortical structure

Recall Figs. 4.4 and 4.6. Out of all thirteen variants of U^* studied in the pure cruciform case, seven within $15.9 \leq U^* \leq 29.5$ sustain high-amplitude vibrations with no foreseeable upper limit within the observation window. For a more complete understanding of the mechanism driving the vibration, one needs to know what are the vortical structures dominating the flow are and how they interact with each other.

Let the coordinates of the simulation domain be defined in the following manner: $(X, Y, Z) = (\frac{x}{D}, \frac{y}{D}, \frac{z}{D})$. The y -component velocity fluctuations are sampled on the $(X, Y) = (1.96, 0)$ line, along the span of the cylinder in $0.5D$ increments, i.e. at coordinates $(1.96, 0, 7.5), (1.96, 0, 7.0), \dots, (1.96, 0, -7.5)$. The distance $X = 1.96$ from the origin is equivalent to $1D$ downstream the trailing edge of the strip plate, and this location is chosen as it is not too close to the cruciform that the vortical structures have not fully formed, and not too far, obfuscating meaningful observation of the structures.

The shedding of vortical structures leave their footprint on the flow field in the form of velocity fluctuations. The choice of analysing the fluctuations of the y -component of velocity is made due to the fact that the oscillator is constrained to move only in the transverse direction. Then, the velocity fluctuations are processed with FFT to obtain the Fourier transform of the fluctuation signals at each spanwise location. The combined Fourier transforms are presented using a colour map in Fig. 4.9. In this figure, every point is a result of that FFT giving the observer a spatial understanding of the vortical structures present in the flow. The abscissa and ordinate denotes f^* and Z coordinates respectively, while the bar legend gives the amplitude of the FFT result.

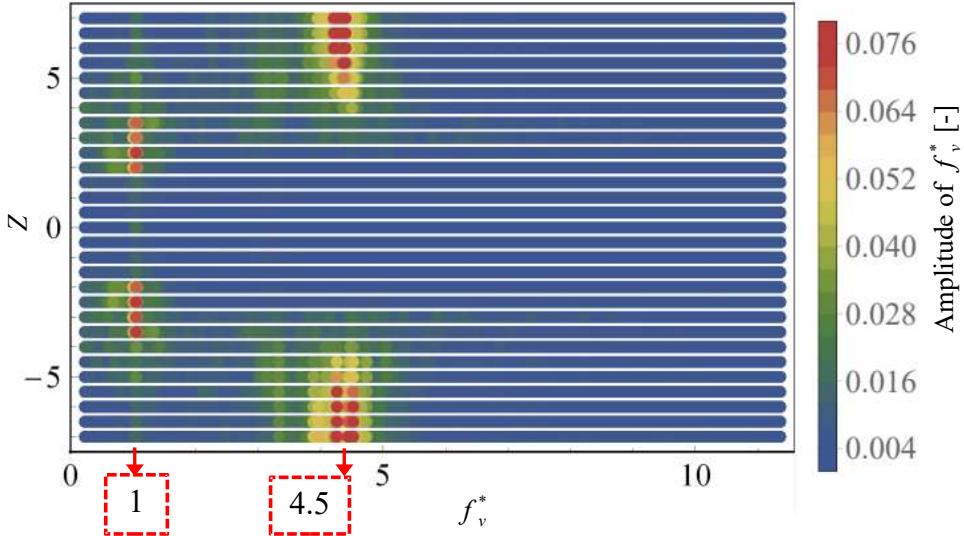


Figure 4.9 Distribution of normalised frequency of vortex shedding, along the span of the cylinder of the pure cruciform at $U^* = 22.7$.

Through inspection, one immediately notices two frequency bands with high amplitudes namely $f^* \approx 1$ and $f^* \approx 4.5$. The locations of these bands are between $3 \leq Z \leq 4.5$ for the former and $4.5 < Z \leq 7$ for the latter. Aided with this visualisation, one can give meaning to the x and z -components of vorticity visualised in Fig. 4.10.

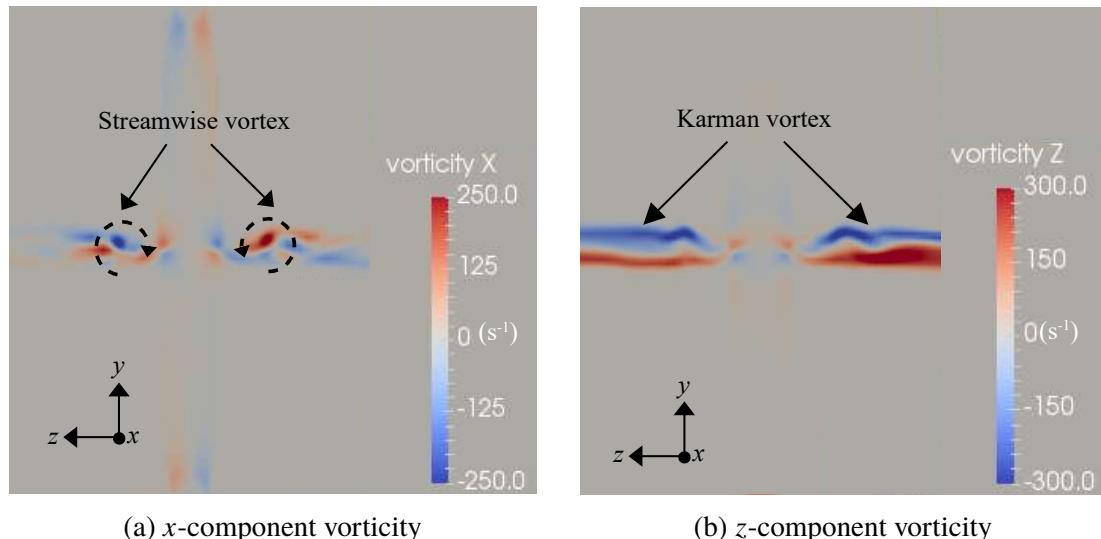
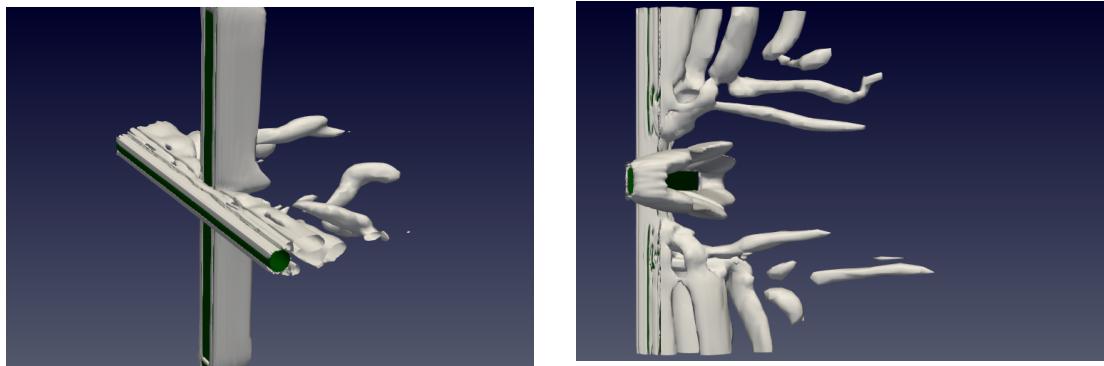


Figure 4.10 Dominant vortical structures at $U^* = 22.7$ observed in the pure cruciform case.

The slices in Fig. 4.10 visualise the distribution of the x (streamwise) and z (Karman) components of vorticity at the $X = 1.96$ plane. The plane is viewed from downstream (viewer standing at $X = 1.96$, looking towards the cruciform), and the vorticities are presented in units of s^{-1} . Furthermore, the visualisations are made when the lift coefficient C_L is at a maximum ($C_{L\max}$).

Comparing Fig. 4.9 with Fig. 4.10 suggests that the $f^* \approx 1$ band is actually due to the shedding of streamwise vortex of a scale close to $1D$ while the $f^* \approx 4.5$ seems to be due to the shedding of Karman vortices. Contrary to the vortical structure commonly observed in studies of isolated circular cylinders (Deng *et al.*, 2007; Kinaci *et al.*, 2016; Duranay and Kinaci, 2020), in the pure cruciform case, two distinct vortical structures take shape in the flow, namely streamwise and Karman vortices. This is consistent with the findings in Koide *et al.* (2017) or Zhao and Lu (2018), where they observed a pair of streamwise vortices on a scale of $\approx 1D$ form in the vicinity of the cruciform juncture, and Karman vortices further away in the spanwise direction. Note that the vibration-driving streamwise vortices forming close to the cruciform juncture exist in pairs: in Fig. 4.10a, one is observed to rotate in the clockwise direction when $Z > 0$ and the other in the counter-clockwise direction when $Z < 0$. What results from this counter-rotating vortex pair is a thrust, propelling the cylinder upwards. This is consistent with the fact that the vorticity field visualisations are produced when the C_L is at a maximum. This work also observe the core of both streamwise vortices lie approximately on the same Y -plane, parallel to the axis of the cylinder.

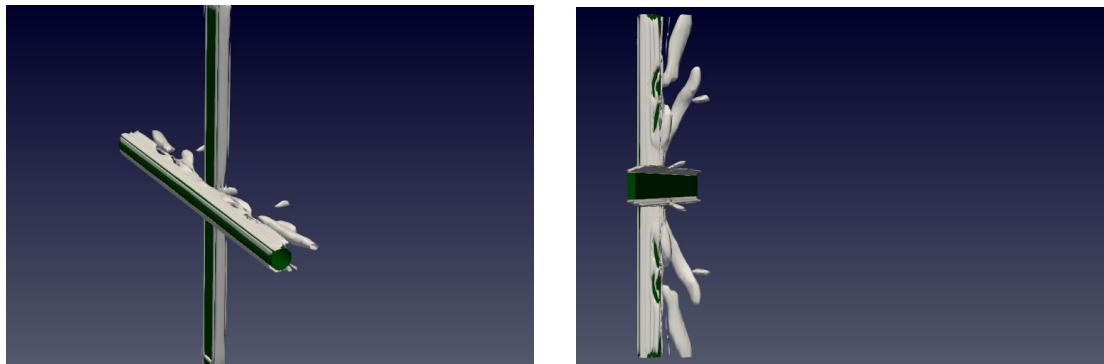
Figures 4.11 and 4.12 highlights the three-dimensionality of the vortical structures during SVIV and KVIV, respectively. This shows additional proof that the vibration of the pure cruciform at 22.7 is due to the shedding of streamwise vortices, while the vibration at 4.5 is due to the shedding of Karman vortices. Results of this Section 4.3.2 and the previous Section 4.3.1 answers objective one of the thesis.



(a) Isometric view of the Q-criterion.

(b) Plan view of the Q-criterion.

Figure 4.11 The Q-criterion for the 90° cruciform at $U^* = 22.7$: the isometric (4.11a) and plan view (4.11b).



(a) Isometric view of the Q-criterion.

(b) Plan view of the Q-criterion.

Figure 4.12 The Q-criterion for the 90° cruciform at $U^* = 6.8$: the isometric (4.12a) and plan view (4.12b).

4.3.3 Temporal evolution of the lift coefficient

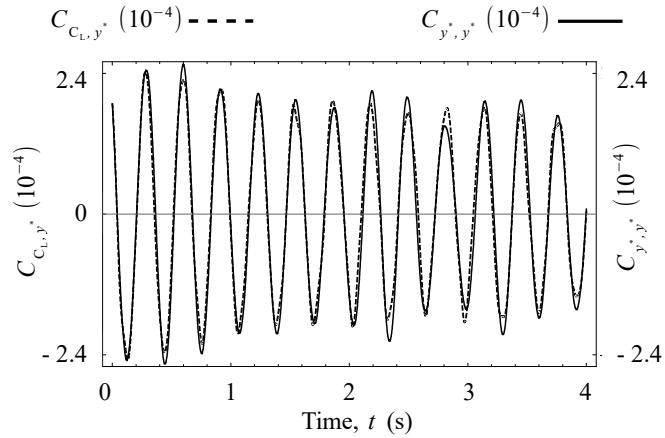
As one can see from the previous section, the streamwise vortex-induced vibration energises the oscillation of the cylinder from within the lower branch of KVIV. However, the amplitude response seems to only increase slightly with each increase of U^* , bordering on tapering off. This is different from oscillators that operate

in the galloping mode, which exhibits a perceptible increase for as long as the reduced velocity U^* is increased. The following sections attempt to uncover the reason for this observation, which can help to improve the power output in subsequent iterations of the cruciform energy harvester by investigating the temporal evolution of the lift coefficient.

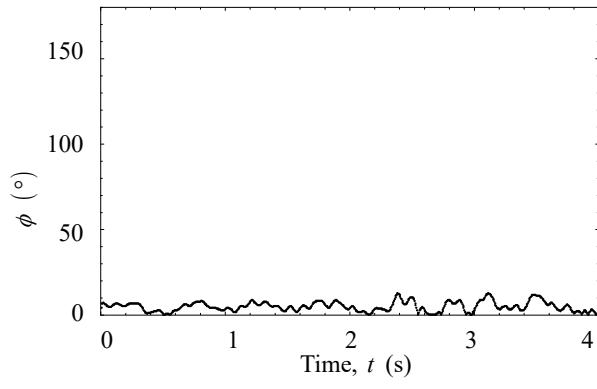
4.3.3.1 The KVIV regime (reduced velocity below 13.6)

At reduced velocities $U^* = 2.3$ and 4.5 , the phase lags ϕ (deg.) between C_L and U^* are practically zero throughout the whole observation time. The characteristic intrinsic mode functions (IMFs) of C_L and y^* at $U^* = 4.5$ exemplifies this trend, as showcased in Fig. 4.13. Here, Fig. 4.13a shows the temporal evolution of C_{y^*,y^*} and C_{C_L,y^*} , which are the characteristic IMFs of y^* and C_L , respectively. Figure 4.13b shows the phase lag between C_{y^*,y^*} and C_{C_L,y^*} , and Fig. 4.13c presents the Hilbert-Huang transform (HHT) spectrogram of C_L .

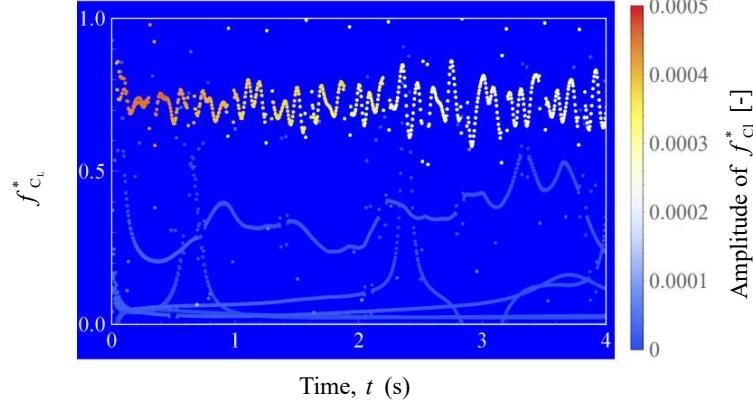
The HHT spectrogram visualises the instantaneous frequency and amplitude of the decomposed C_L signal. The trend in Fig. 4.13b is similar to what was observed by Khalak and Williamson (1999) which also employs the Hilbert transform to compute the instantaneous phase. It is worth noting that the signals dealt with in Khalak and Williamson (1999) are more or less gradual, rendering empirical mode decomposition (EEMD) irrelevant. The dominant IMF component of the lift coefficient has a normalised frequency $f_{C_l}^* = f_{C_l}/f_n$ (Fig. 4.13c) centred at approximately $f_{C_l}^* = 0.75$. Here, the dominant IMF component refers to the component of IMF with the highest amplitude during the whole observation time.



(a) Comparison between C_{C_L,y^*} and C_{y^*,y^*} .



(b) Phase lag between C_{C_L,y^*} and C_{y^*,y^*} .



(c) Hilbert-Huang spectrogram of C_L .

Figure 4.13 Temporal analysis of C_L and y^* at $U^* = 4.5$.

Once the cylinder enters the upper branch of KVIV at $U^* = 6.8$, ϕ jumps to approximately 110 deg. This jump in ϕ is commonly observed in the transition to the upper branches (Maruai *et al.*, 2018). Both C_{C_L,y^*} and C_{y^*,y^*} signals are highly

periodic, and the dominant frequency band of C_L is centred at ≈ 1 , as demonstrated in Fig. 4.14c.

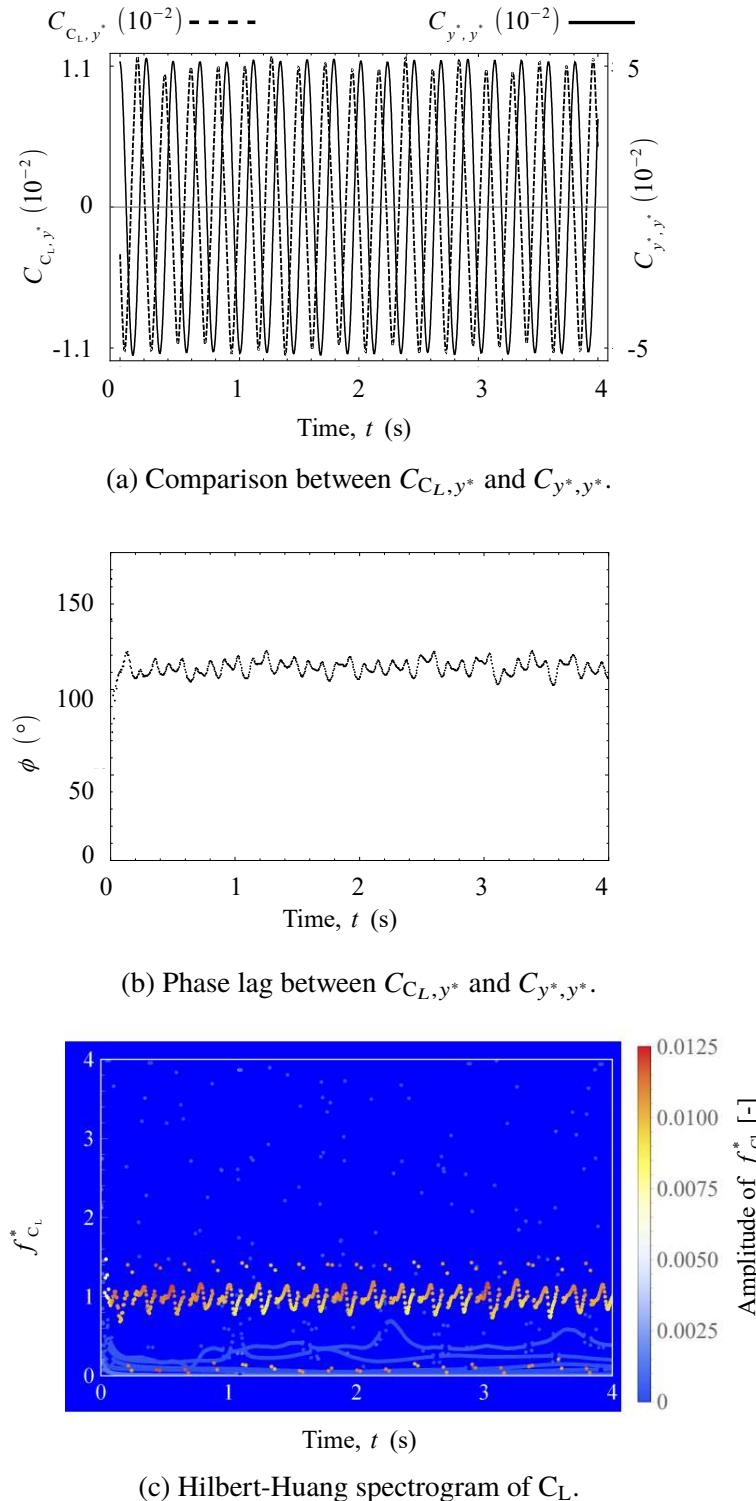
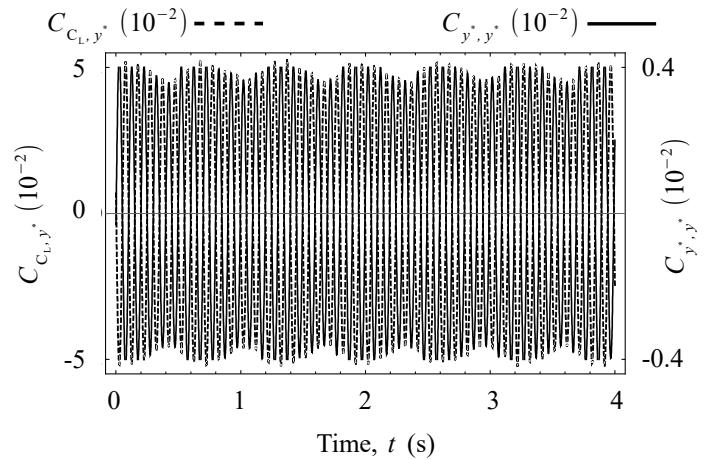
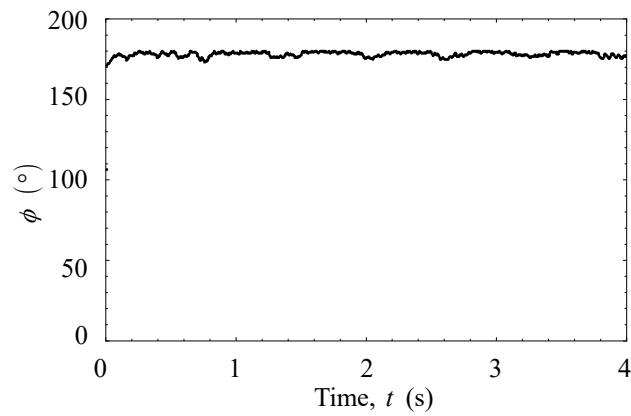


Figure 4.14 Temporal analysis of C_L and y^* at $U^* = 6.8$.

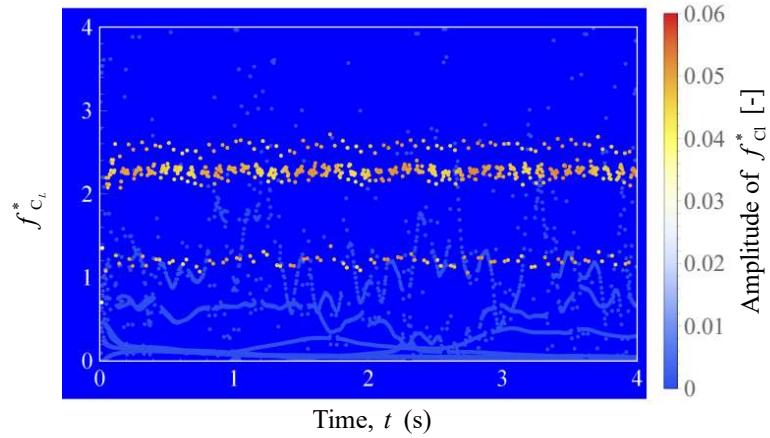
As U^* is increased even further up to $U^* = 13.6$, a similar trend is spotted for all $U^* = 9.1, 11.4, 13.6$ examined: C_{y^*,y^*} and C_{C_L,y^*} are both qualitatively very periodic. Their phase lags are very close to 180 deg. The dominant C_L frequency bands exhibit a time-averaged value that increases linearly for U^* while keeping the Strouhal number of $C_L \approx 0.16$. The representative case of $U^* = 13.6$ is shown in Fig. 4.15. Note how ϕ in this range of U^* varies less against time, compared to ϕ at $U^* = 6.8$, and the dominant frequency band of C_L is much narrower compared to the dominant frequency band at $U^* = 6.8$, indicating a highly periodic and self-similar oscillation of lift.



(a) Comparison between C_{C_L,y^*} and C_{y^*,y^*} .



(b) Phase lag between C_{C_L,y^*} and C_{y^*,y^*} .



(c) Hilbert-Huang spectrogram of C_L .

Figure 4.15 Temporal analysis of C_L and y^* at $U^* = 13.6$.

4.3.3.2 Transition to SVIV (reduced velocity between 15.9 and 18.2)

Previously in the $U^* \leq 13.6$ range, the temporal profile of both C_L and y^* are very similar, except that C_L leads y^* by a certain amount. This similarity in profile supports the assertion that the vibration within $U^* \leq 13.6$ is driven exclusively by the shedding of Karman vortices, which brings the onset of the alternating lift. Similarly, a similar profile between C_L and y^* is expected when streamwise vortices drive the vibration. This presupposition, however, seems to disagree with observation.

Once U^* reaches 15.9, it has become difficult to argue that the profile of y^* is just a lagged version of the profile of C_L . This is shown in Fig. 4.16a, with the enlarged version in Fig. 4.16b. The profile of C_L is akin to the superposition of a plurality of signals. This observation is driven by the presence of two types of maxima with differing amplitude heights. A red dashed line, and a red dashed-dot line is put in Fig. 4.16b as visual cues indicating the two amplitude heights. Through EEMD, some evidence supporting the compound signal hypothesis is brought to light.

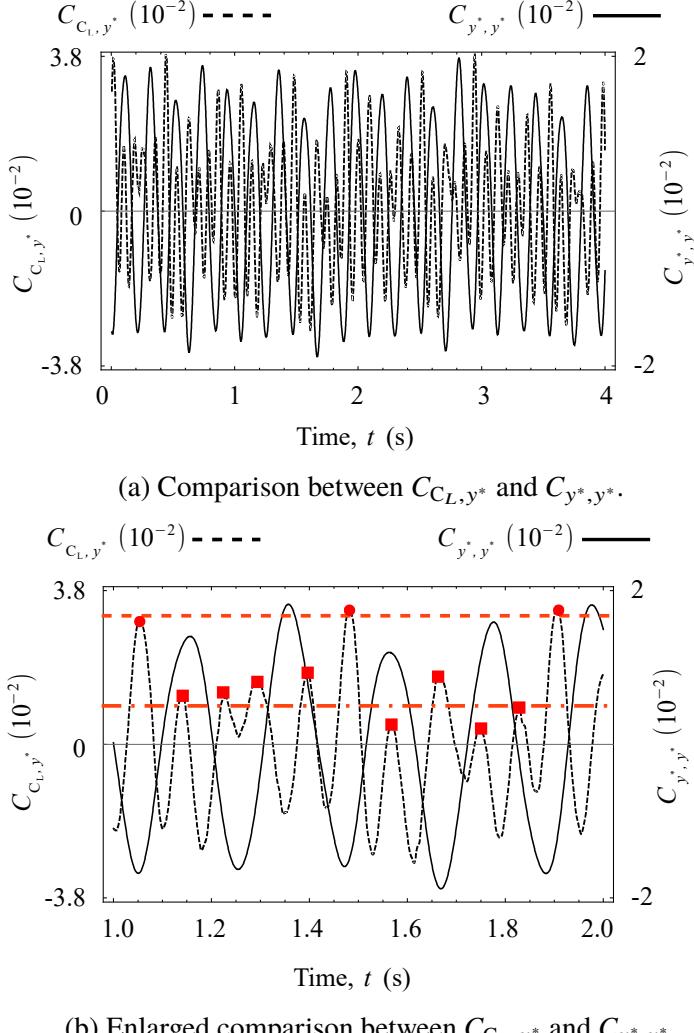
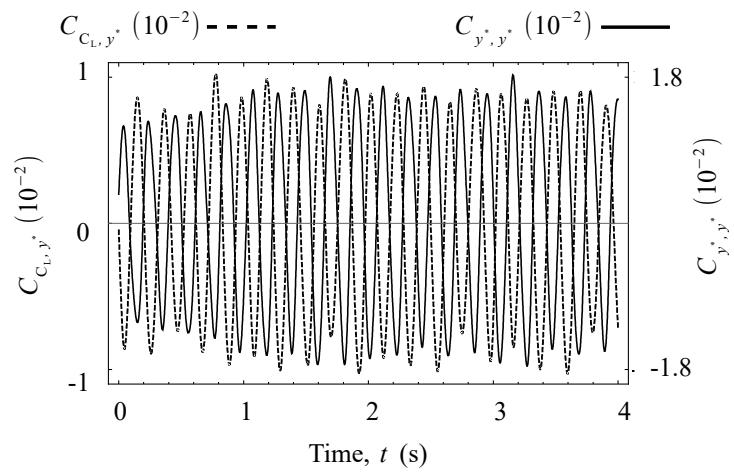
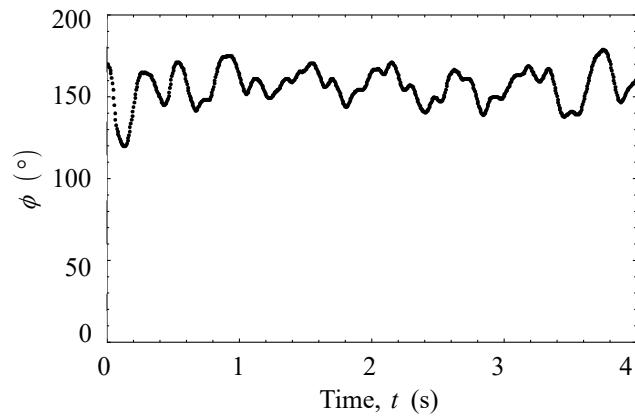


Figure 4.16 Temporal evolution of y^* and C_L at $U^* = 15.9$.

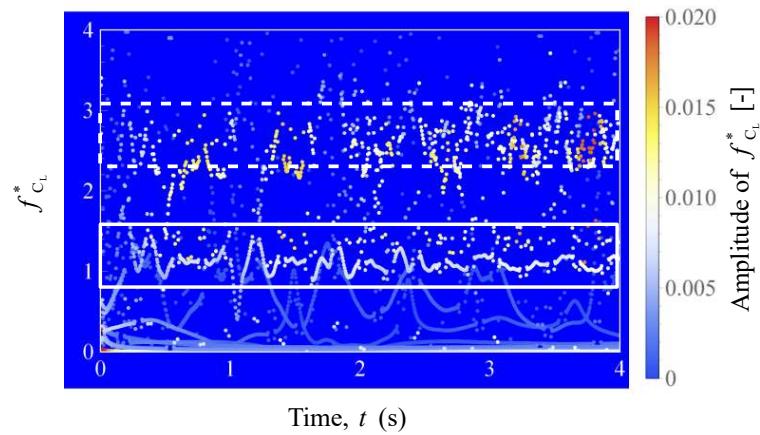
Once the signal is decomposed using EEMD, Fig. 4.16a is replotted using C_{C_L,y^*} and C_{y^*,y^*} in Fig. 4.17a. One can clearly see that the part of C_L signal responsible for driving the vibration at $U^* = 15.9$ is embedded in the original C_L signal (Fig. 4.17a), and decomposition via EEMD managed to recover this signal, which leads C_{y^*,y^*} by approximately 150 deg. on average, throughout the whole observation time (Fig. 4.17b). This decline from $\phi \approx 180$ deg. at reduced velocities $9.1 \leq U^* \leq 13.6$, to $\phi \approx 150$ deg. at $U^* = 15.9$ is quite sizeable, suggesting a fundamental change in flow dynamics, particularly in terms of vortical structure.



(a) Comparison between C_{C_L,y^*} and C_{y^*,y^*} .



(b) Phase lag between C_{C_L,y^*} and C_{y^*,y^*} .



(c) Hilbert-Huang spectrogram of C_L .

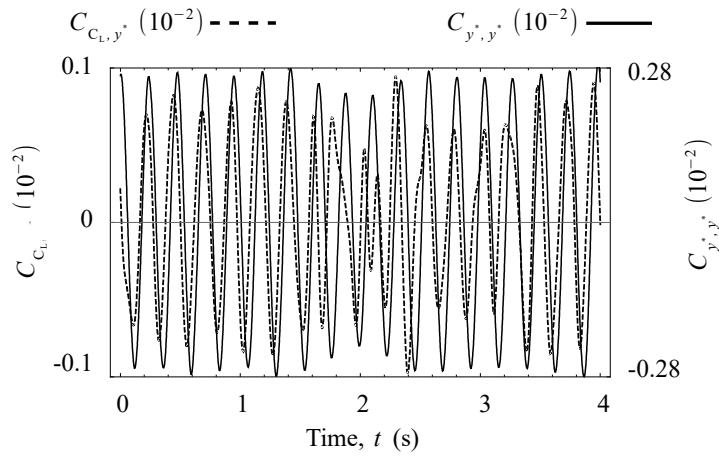
Figure 4.17 Temporal analysis of the C_L and y^* signal at $U^* = 15.9$.

Another significant change is the increased scatter in ϕ from its time-averaged value, different from the evolution of ϕ in the range $9.1 \leq U^* \leq 13.6$, which varies only slightly throughout the observation time.

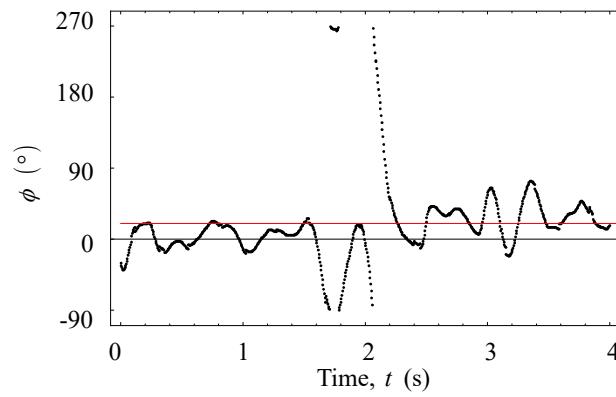
Inspecting the HHT spectrogram in Fig. 4.17c reveals two dominant bands in the frequency domain. The first one, denoted by a white rectangular frame, is the instantaneous frequency for the IMF component of lift shown in Fig. 4.17a, and its mean frequency lies close to the natural frequency of the system ($f_{C_l}^* \approx 1$). Simultaneously, a second frequency band with similar amplitude is marked with a white dashed rectangular frame around $f_{C_l}^* \approx 2.7$. The Strouhal number from this frequency is $St = 0.20$, which is tenuously close to the Strouhal number for Karman vortices as predicted by Eq. 2.6 for $Re = 7.9 \times 10^3$. This second band of frequency is thus attributed to the footprint left by the shedding of Karman vortices and the first band as the result of streamwise vortex shedding. Through visual inspection of Fig. 4.17c, both of these dominant frequency bands are markedly wider, and the individual values are more scattered from their time-averaged values than any of their counterparts within $U^* \leq 13.6$.

Observing Karman vortices shedding from a cruciform structure during SVIV is not new in the literature. However, pinpointing how the streamwise and Karman vortex shedding modulates the lift signal from a cruciform structure in SVIV has no precedence. The vibration of the cylinder remains steadfast near the system natural frequency, even though both Karman and streamwise vortices are comparable in terms of amplitude. The underlying cause is probably the shedding frequency of the Karman vortex, which is too distant from the system's natural frequency f_n . The shedding frequency of the streamwise vortex is much closer to f_n and is thus preferred by the cylinder.

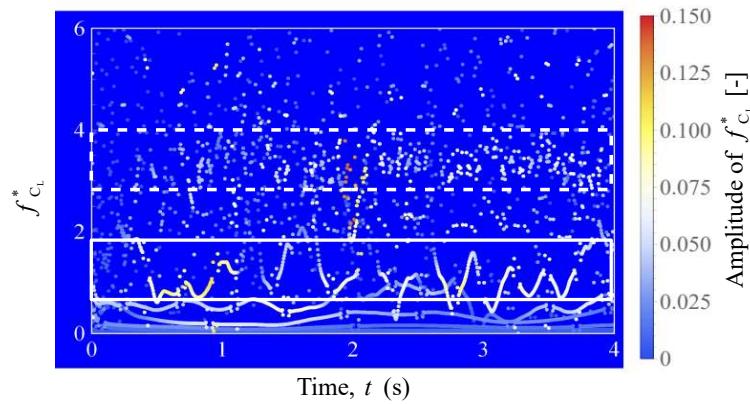
The transition to SVIV is considered complete at $U^* = 18.2$ when the time-averaged phase lag drops further to ≈ 20 deg. Figure 4.18a and 4.18b documents this observation. The instantaneous phase lag is observed to slip through 360 deg. a little past the two second (2 s) timestamp. By inspecting Fig. 4.18a, one finds that a little past 2 s is when distortions in the periodicity of C_{C_L,y^*} occur.



(a) Comparison between C_{C_L,y^*} and C_{y^*,y^*} .



(b) Phase lag between C_{C_L,y^*} and C_{y^*,y^*} .



(c) Hilbert-Huang spectrogram of C_L .

Figure 4.18 Temporal analysis of the lift coefficient and normalised cylinder displacement signal at $U^* = 18.2$.

The slipping through 360 deg. was also mentioned by Khalak and Williamson (1999) in their work on KVIV, drawing attention to the quasi-periodic nature of the signal. For Khalak and Williamson (1999), the slip occurs in the initial branch of KVIV. The overall low value of ϕ (≈ 20 deg. for the whole observation time at $U^* = 18.2$), coupled with the presence of ϕ slippage, is suggestive of the possibility for $U^* = 18.2$ being the initial branch of SVIV. This is a new discovery and it demonstrates the usefulness of CFD in exploring parameter spaces. Using CFD, the researcher can explore new parameter spaces just by setting new values for them in the numerical code. The sensitivity and resolution of data collection can be easily adjusted unlike previous studies such as those by Koide *et al.* (2009) and Koide *et al.* (2013). Their data simply was collected at a lower resolution, thus losing their chance to observe this initial branch of SVIV.

4.3.3.3 The stable SVIV regime (reduced velocity greater than 20.5)

As U^* is increased to 20.5, a jump is observed in ϕ from a mean value of approximately 20 deg. to about 120 deg., shown in Fig. 4.19a. The phase slippage discussed previously is also observed, indicating the quasi-periodic nature of the lift coefficient signal at this U^* . Incidentally, this quasi-periodicity seems to be the norm for the lift signals up to $U^* = 27.3$, as suggested by the phase slippages evident in Figs. 4.19b, c and d. The slippage halts once U^* reaches 29.5, suggesting the emergence of a more periodic lift signal relative to $20.5 \leq U^* \leq 27.3$. Although the instantaneous phase between $20.5 \leq U^* \leq 27.3$ implies a quasi-periodic nature, their time-averaged values at each U^* are contained in the narrow region $114 < \phi$ (deg.) < 135 , as is the value for ϕ at $U^* = 29.5$. This finding can be interpreted as the dominant vortical structures becoming more resilient against external excitations. Hence, $20.5 \leq U^* \leq 29.5$ is classified as the upper branch of SVIV.

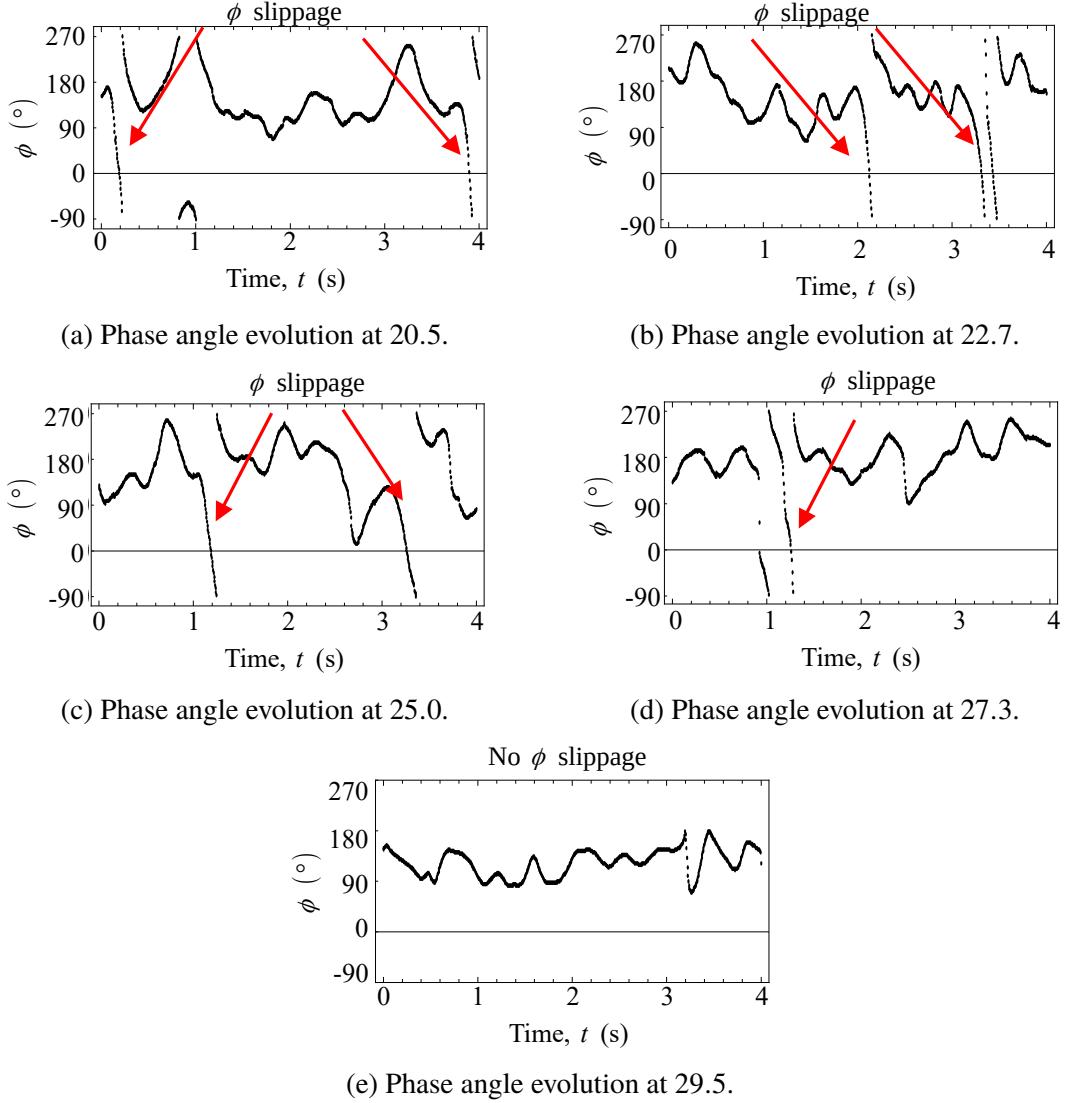


Figure 4.19 The instantaneous phase lag ϕ of C_{C_L,y^*} in the range $20.5 \leq U^* \leq 29.5$.

The $\phi(t)$ data makes it possible to visualise the vibration ‘‘branches’’ within the U^* range investigated. As the branches are mapped against U^* , a representative value of ϕ is needed at each U^* . To achieve this, the time-averaged values of ϕ is taken, i.e. ϕ_{mean} , and plotted them against U^* in Fig. 4.20. Region A indicates the initial branch of KVIV, where ϕ_{mean} is close to zero. Region B denotes the upper/lower branch of KVIV, where the system jumps from $\phi_{\text{mean}} \approx 0$ to greater than 110 deg. The value of ϕ_{mean} saturates near 180 deg. towards the end of this upper/lower branch.

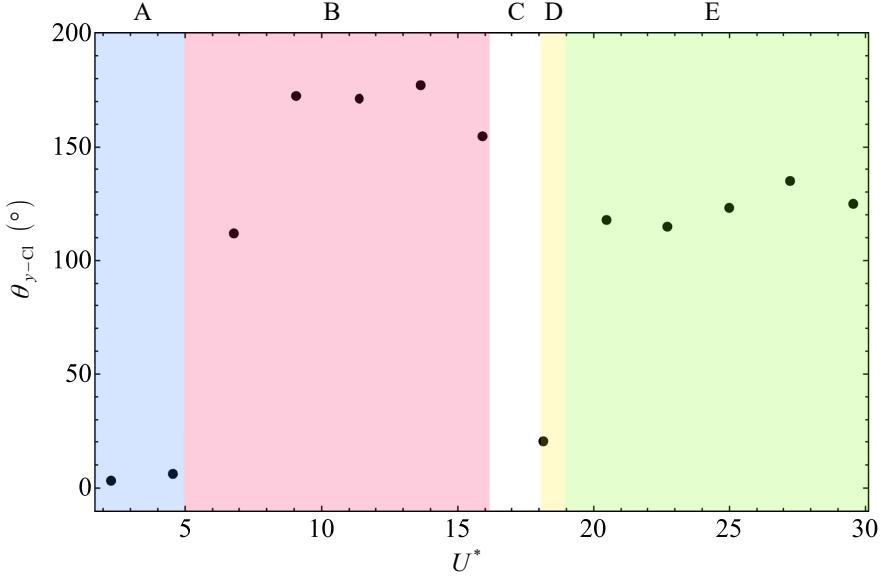


Figure 4.20 Variation of θ_{y-Cl} with respect to U^* for the pure cruciform.

Then, ϕ_{mean} experiences a slight drop from about one-sixth the value of ϕ_{mean} in region B as one enters region C, marking the start of the transition to the SVIV regime. Following this, the value of ϕ_{mean} drops to $\phi_{\text{mean}} \approx 20$ deg. at $U^* = 18.2$. Another jump is observed from $\phi_{\text{mean}} \approx 20$ deg. to approximately 120 deg. when $U^* \geq 20.5$. This region where the jump occurs is designated as region D. Finally, in region E, ϕ_{mean} maintains a value of approximately 120 deg. until the end of the observation range.

The discovery of these regimes of θ_{y-Cl} is only made possible through the use of HHT. The typical method of estimating θ_{y-Cl} from FFT is not applicable on complex lift signals such as those observed in this work. Results of this Section 4.3.3 in part answers thesis objective two.

4.3.4 Harnessable power

Figure 4.21 compares the power estimated from the experimental and numerical results with the experimental results of Nguyen *et al.* (2012) and the direct power measurement of Koide *et al.* (2013). Only the value for $P_{\text{Mech.,RMS}}$ is computed from the experimental results due to the absence of lift data. The numerical results have both lift and cylinder displacement data, from which both $P_{\text{Fluid,RMS}}$ and $P_{\text{Mech.,RMS}}$ are computed. The power is estimated from the experimental results of Nguyen *et al.* (2012)

by interpolating missing data points in both their amplitude and frequency responses to compute the value of $P_{\text{Mech.,RMS}}$ at a given value of U^* . The direct power measurement by Koide *et al.* (2013) connects the elastic support of the cylinder to a coil that moves with the cylinder. This setup enables a relative piston motion against a fixed magnet and produces an alternating current.

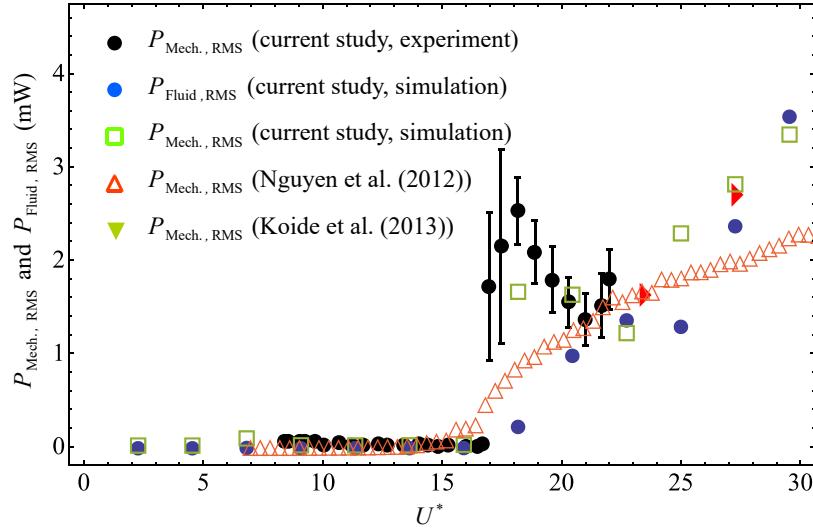


Figure 4.21 Estimation of $P_{\text{Mech.,RMS}}$ and $P_{\text{Fluid,RMS}}$ and comparison with available data.

The estimated power in the KVIV regime $U^* \leq 15.9$ produces power only in the order of μW , which is relatively insignificant in contrast to the magnitude of power produced in the SVIV regime (mW). In the region $18.2 \leq U^* \leq 22.7$, $P_{\text{Mech.,RMS}}$ for in the experimental and numerical work exhibits a similar trend where a sudden jump in power output is observed, followed by a gradual decrease. This gradual decrease can be attributed to the increased turbulence level right after the onset of SVIV that imposes a degree of intermittency to the normalised cylinder displacement signal, y^* . For $P_{\text{Fluid,RMS}}$, however, the quantity exhibits a gradual increase in the range $18.2 \leq U^* \leq 22.7$. A dip in $P_{\text{Fluid,RMS}}$ is only observed at $U^* = 25.0$, suggesting an increase in intermittency of C_{C_L,y^*} at this U^* . In the experimental work of Nguyen *et al.* (2012), $P_{\text{Mech.,RMS}}$ only experiences a gradual increase in the region $18.2 \leq U^* \leq 22.7$. This markedly different response of the system compared to this work possibly originate from the discrepancy in the cruciform used by Nguyen *et al.* (2012). They used two

circular cylinders of diameter 10 mm as their cruciform, whereas this study used a circular cylinder - strip plate in both the experiments and numerical work. There are no data from the direct power measurement of Koide *et al.* (2013) to compare with within $18.2 \leq U^* \leq 22.7$.

In the range $25.0 \leq U^* \leq 29.5$, a reasonably good agreement is found between the trend found in all data compared: they increase gradually against U^* . Although the value of $P_{\text{Fluid,RMS}}$ falls quite notably below the value of $P_{\text{Mech.,RMS}}$ of this study at $U^* = 25.0$, other values of $P_{\text{Fluid,RMS}}$, $P_{\text{Mech.,RMS}}$ from the numerical results of this study and the direct power measurements by Koide *et al.* (2013) agree well within $27.3 \leq U^* \leq 29.5$. The only set of power data that consistently falls short of the others is the $P_{\text{Mech.,RMS}}$ estimated from the experimental data of Nguyen *et al.* (2012), which again, is most probably due to the different cruciform used in their investigation.

4.3.5 Possibility for increasing fluid power

Recall in Fig. 4.21 that although $P_{\text{Fluid,RMS}}$ is computed according to Eq. 3.3, which uses $C_{C_L,\text{RMS}}$ instead of the actual root-mean-square amplitude of lift ($C_{L,\text{RMS}}$), the resulting power estimate does not result in a trend that is different from the trend found in the other datasets. In addition, the values of $P_{\text{Fluid,RMS}}$ are in reasonably good agreement with other benchmarked data at high U^* ($U^* = 27.3$ and 29.5), except for $P_{\text{Mech.,RMS}}$ estimated from the experimental data of Nguyen *et al.* (2012). This agreement is possibly an indication that the lift component selected for use in the computation of $P_{\text{Fluid,RMS}}$ is an arguably faithful representation of the force driving the motion of the cylinder. Hence, the motion of the cylinder, once it enters the SVIV regime, is driven only by one component and not the totality of the lift force. This component – that has a time-averaged frequency close to the system’s natural frequency, f_n – is the “streamwise component” of lift.

Another significant component of lift in the SVIV regime is the one whose mean frequency is close to the Karman frequency of vortex shedding, as explained in Section 4.3.3.2. This Karman component of lift is similar in amplitude to the streamwise component of lift, as evidenced in Fig. 4.22, thus registering it as a dominant component of lift. The Karman components are marked with a dashed, white

box, and the streamwise components are marked with a solid, white box, following the convention in Figs. 4.13, 4.14, 4.15, 4.17 and 4.18. However, the Karman component fails to affect the cylinder vibration like the streamwise component, most probably due to the significant difference between the mean frequency of the Karman component and the natural frequency of the system, f_n . The streamwise component has a mean frequency close to f_n and can synchronise with the vibration of the cylinder, producing a sizeable amplitude response.

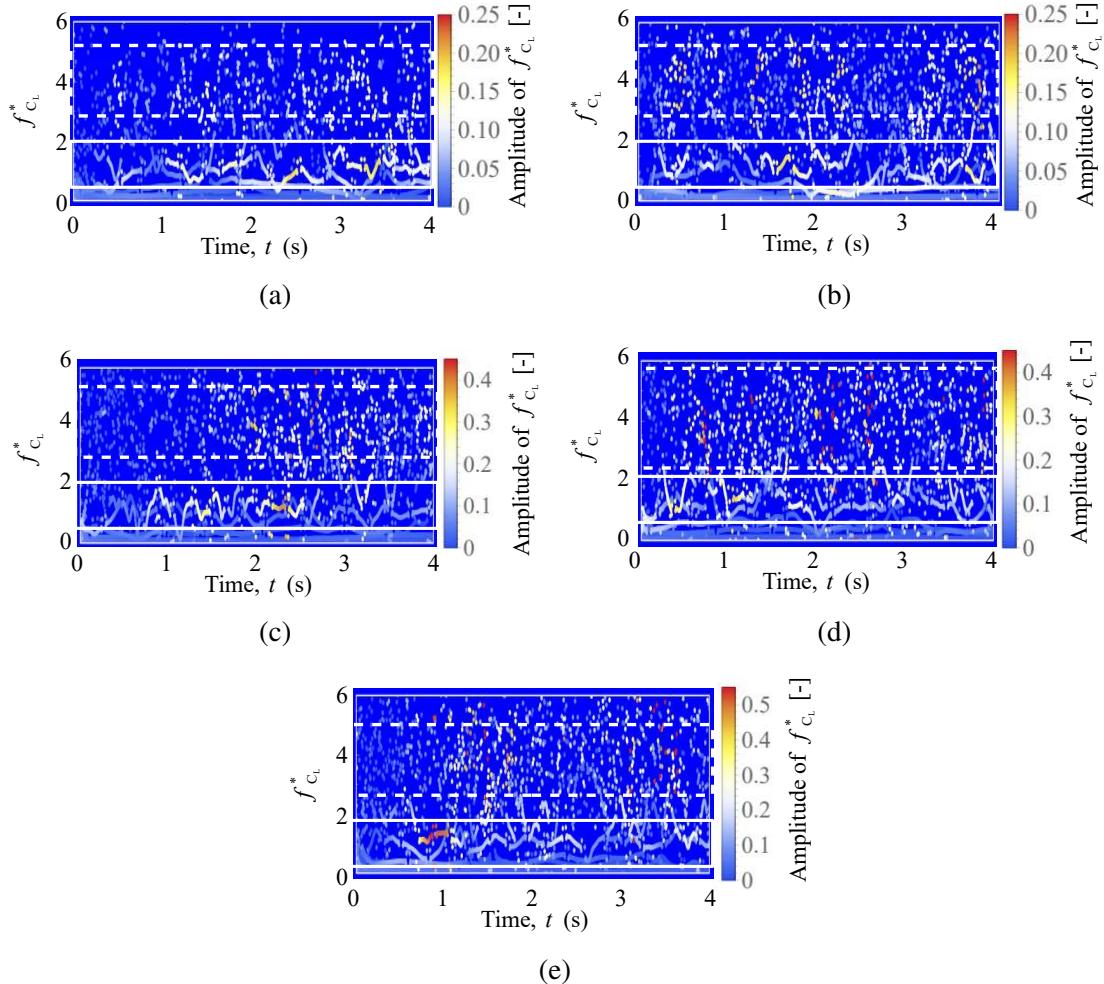


Figure 4.22 The HHT spectrogram of C_L between $20.5 \leq U^* \leq 29.5$. The solid and dashed line white boxes delineate the distribution of the streamwise and Karman components of lift, respectively.

Figure 4.23 shows the root-mean-square amplitude of the Karman and streamwise components of lift in the SVIV regime $U^* \geq 18.2$. Between $18.2 \leq$

$U^* \leq 22.7$, the magnitude of the Karman and streamwise components are nearly equal. However, once one exceeds $U^* = 22.7$, Fig. 4.23 shows that the contribution to the root-mean-square amplitude of total lift by the Karman component is on average twice the contribution of the streamwise component. Having such a significant contribution towards the root-mean-square amplitude of total lift implies a significant portion of energy from the free stream energising the Karman vortex in the flow. Consider a situation where one can redistribute the contribution by the Karman component to the streamwise component of lift. In other words, consider the situation where it is possible to redirect the energy from the Karman to the streamwise vortex. Then, the value for $C_{C_L,RMS}$ in Eq. 3.3 will increase close to a factor of 2 when $18.2 \leq U^* \leq 22.7$, and close to a factor of 3 when $25.0 \leq U^* \leq 29.5$. This increase in $C_{C_L,RMS}$ will lead to the scaling of $P_{Fluid,RMS}$ by the same factor, keeping the other parameters in Eq. 3.3 constant. This exercise demonstrates the room for improvement possible for $P_{Fluid,RMS}$ in future developments of cruciform energy harvesters.

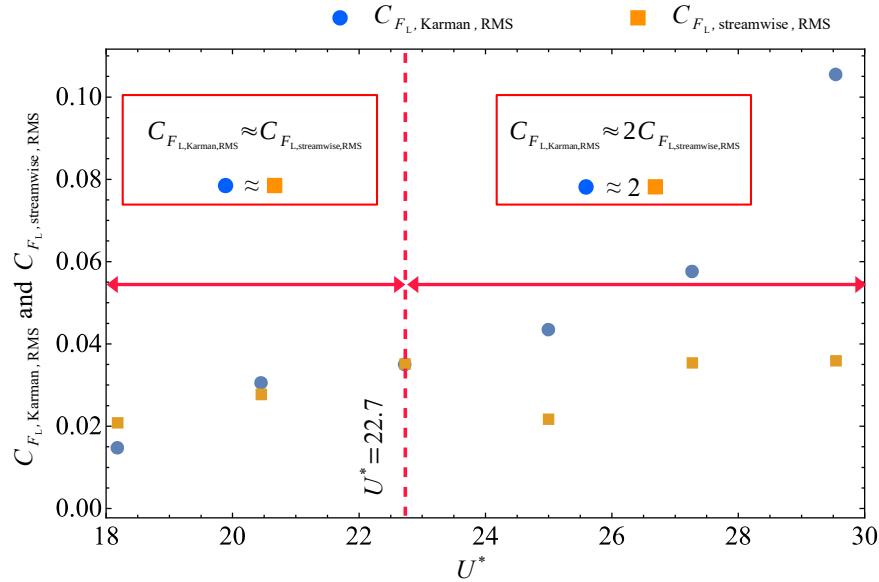


Figure 4.23 Evolution of $C_{F_L,\text{Karman},\text{RMS}}$ and $C_{F_L,\text{streamwise},\text{RMS}}$ with respect to U^* .

One possible method of improving $P_{Fluid,RMS}$ is by implementing a modified version of the cruciform that can guarantee the dominance of the vortical structure that can lock into f_n - which in Fig. 4.23 is the streamwise vortex - against the vortical structures that do not, i.e., the Karman vortices. This study explores one method –

namely the method of cruciform angle variation – to achieve said dominance in the following sections. Results of this Section 4.3.4 and the previous Section 4.3.5 answers thesis objective two.

4.4 Steep-angled cruciforms

The discovery made towards the end of Section 4.3 strongly supports the assertion that there is still plenty of room for improvement in terms of power output and efficiency for the cruciform energy harvester. The fact that in a pure cruciform, during SVIV, a significant portion of the freestream energy forked to sustain the formation of Karman vortices that does not contribute to energise the cylinder vibration seems to strongly suggest control of the vibration-driving vortical structures as the next logical step to break through the maximum effective lift, i.e., $C_{F_L,\text{streamwise,RMS}}$ observed in Section 4.3.5.

To achieve this, this study attempts to retard the formation of either one of the dominant vortical structures observed in the pure cruciform oscillator, preferably the Karman vortices since for the pure cruciform, the high-amplitude vibrations are driven by streamwise vortex shedding. In a manner similar to how the downstream strip plate was introduced to a single oscillator unit to suppress the Karman vortex shedding, perhaps a modified configuration of the downstream strip plate can potentially bring about an even more vigorous inhibition of Karman vortex shedding and thus direct a bigger portion of energy from the freestream towards the large-scale streamwise vortex. The modification chosen for this purpose is the rotation of the downstream strip plate and the resulting angle between the upstream circular cylinder and the strip plate.

This section investigates the amplitude/frequency responses of steep-angled cruciforms ($67.5 \leq \alpha(^{\circ}) \leq 45$), the vortical structures behind the amplitude/frequency responses, and how the vortical structures influence the lift acting on the cylinder and subsequently the phase lag between the C_L and y^* to locate branches that can be exploited for energy harvesting.

4.4.1 The amplitude and frequency response

As the cruciform angle is reduced to 67.5° and 45° , the SVIV branch observed in the pure cruciform case as $U^* \geq 15.9$ disappear, as one can inspect in Fig. 4.24. For the 45° cruciform, even y_{RMS}^* at the KVIV upper branch ($U^* = 4.5$) is lower than the corresponding values for both the 90° and 67.5° cruciforms.

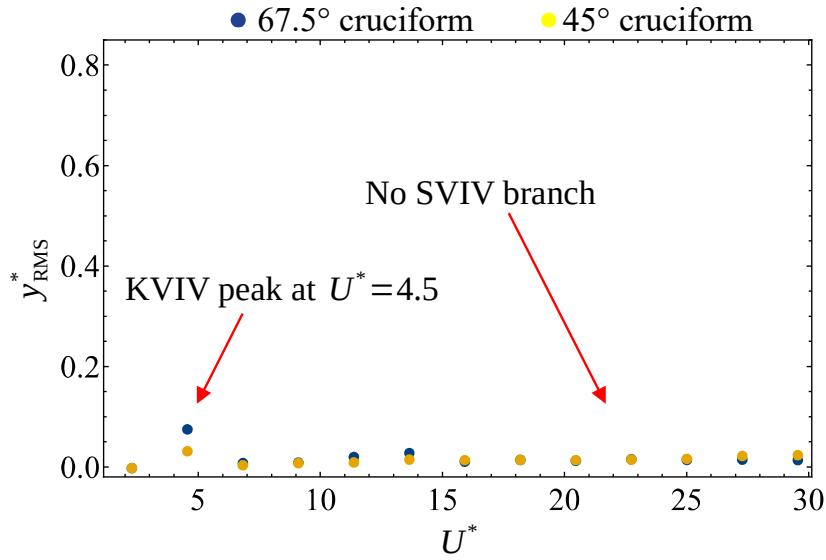


Figure 4.24 Evolution of the normalised vibration amplitude y_{RMS}^* , with respect to reduced velocity U^* , for the 67.5° and 45° cruciforms.

Another striking departure from the trend observed in the pure cruciform case, can be found in the evolution of f^* in Fig. 4.25. For the 67.5° cruciform in Fig. 4.25, f^* seems to fluctuate with respect to U^* - suggesting asymmetry in the vortical structures regulating the vibration as discussed previously in Section 4.3.1. This behaviour is perhaps due to the 45° cruciform being less similar to the 90° cruciform, in contrast to 67.5° . In other words, the 45° cruciform is less in transition from the response of the 90° cruciform and the flow around it is more evolved into its new configuration, unlike the 67.5° cruciform.

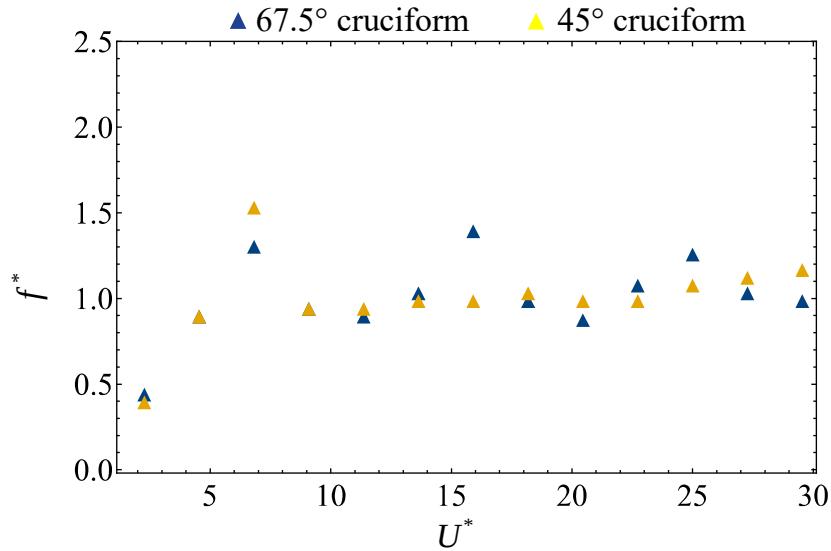


Figure 4.25 Evolution of the normalised cylinder displacement frequency, f^* , with respect to reduced velocity U^* , for the 67.5° and 45° cruciforms.

The root-mean-square lift coefficients $C_{L,RMS}$ of the 67.5° and 45° cruciforms are summarised in Fig. 4.26. The results showed that their evolution with respect to U^* in Fig. 4.26 approximates their corresponding y_{RMS}^* trend in Fig. 4.24. As for the variation of $f_{C_l}^*$ with respect to U^* , for both the 67.5° and 45° cruciforms, both exhibit outstanding similarity to $f_{v,Karman}$ of Eq. 2.6. This trait hints that vibrations resulting from the 67.5° and 45° cruciforms are primarily regulated by the shedding of Karman vortices.

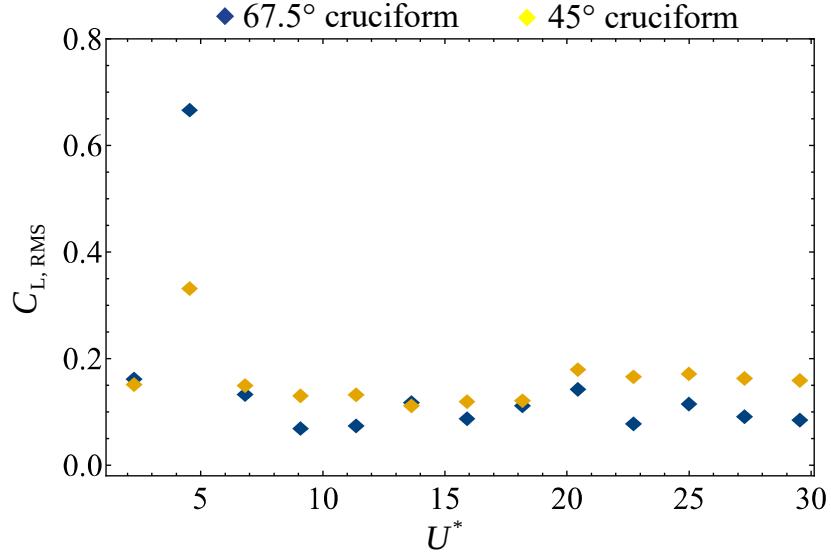


Figure 4.26 Evolution of the normalised C_L root-mean-square amplitude, $C_{L,RMS}$, with respect to reduced velocity U^* , for the 67.5° and 45° cruciforms.

The fact that the $f_{C_l}^*$ trends observed in Fig. 4.27 do not lead to similar trends in the evolution of f^* in Fig. 4.25 points to something more fundamental at play in developing the f^* patterns observed in Figs. 4.25. Hence the vortical structures present in the flow surrounding the 67.5° and 45° cruciforms are examined, the findings of which are discussed in Section 4.4.2.

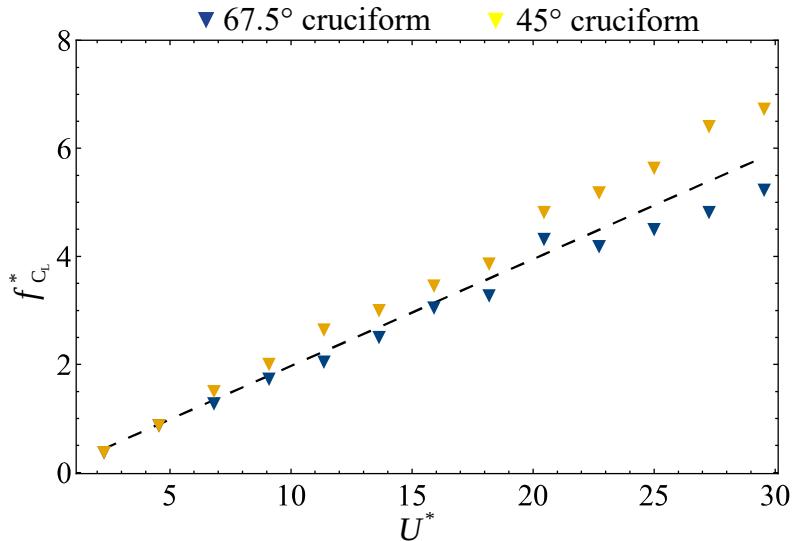


Figure 4.27 Evolution of the normalised C_L frequency, $f_{C_L}^*$, with respect to reduced velocity U^* , for the 67.5° and 45° cruciforms. The dashed lines outline $f_{v,\text{Karman}}$ from Eq. 2.6.

4.4.2 Main vibration-driving vortical structure

As the first step, the FFT of the y -component of velocity is computed similar to what was done in Fig. 4.9 for both the 67.5° and 45° cruciforms. Initial assessment of the $f_{v,\text{Karman}}^*$ distribution along the cylinder axis in Figs. 4.28a and 4.28b is that there is a strong representation of the Karman shedding frequency in both cases, which at $U^* = 22.7$ is $f_{v,\text{Karman}}^* = 4.49$. However, unlike Fig. 4.9, there is no frequency band close to 1 around the cruciform juncture.

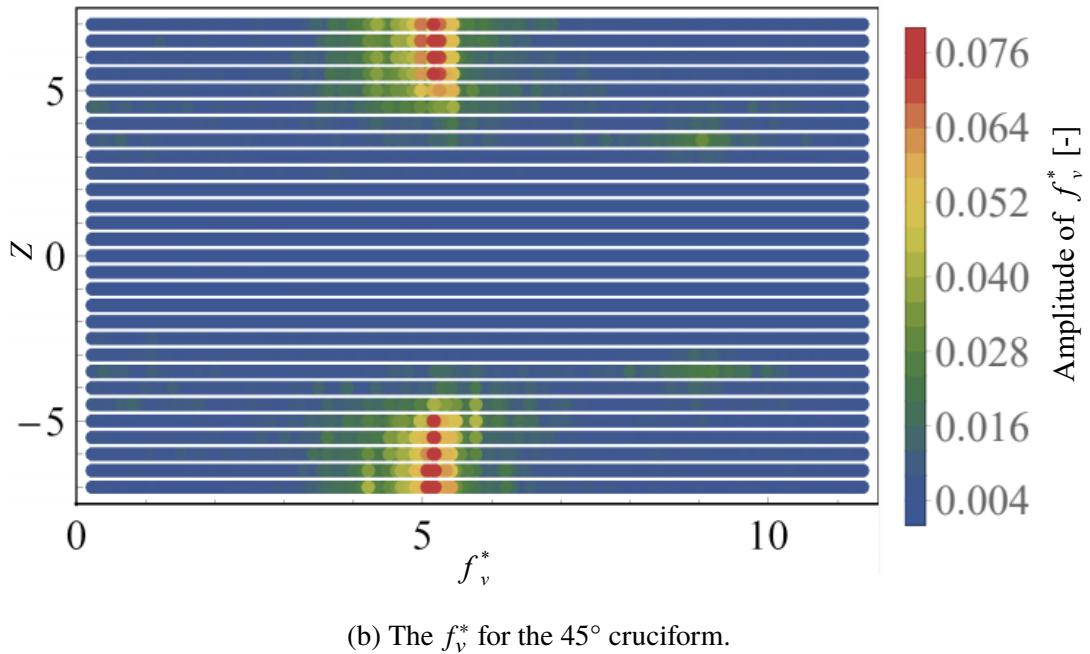
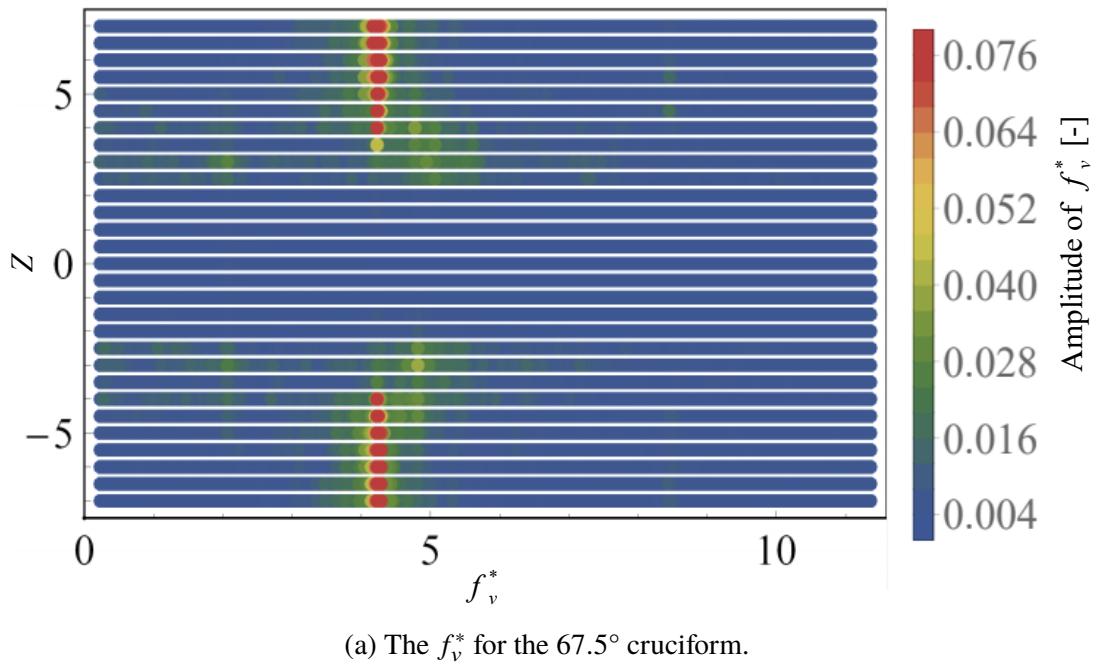


Figure 4.28 Distribution of normalised frequency of vortex shedding, along the span of the cylinder of the 67.5° and 45° cruciforms at $U^* = 22.7$.

The first guess is that streamwise vortices driving the vibration in the pure cruciform case do not get initiated once the cruciform angle deviates away from 90° .

However, x and z -component vorticity visualisations in Fig. 4.29 points out otherwise. These visualisations are produced under the same conditions as Fig. 4.10. Inspecting Figs. 4.29a and 4.29c, one can quite clearly make out the large-scale streamwise vortices close to the cruciform juncture. The cylinder vibration and streamwise vortices are thus expected to synchronise to each other, resulting in an $f^* \approx 1$ accross the values of U^* after the lower branch of KVIV which appears at $U^* = 6.8$. In addition, a large amplitude response is expected from the cylinder due to the formation and sustenance of the streamwise vortices close to the cruciform juncture. This was not the case.

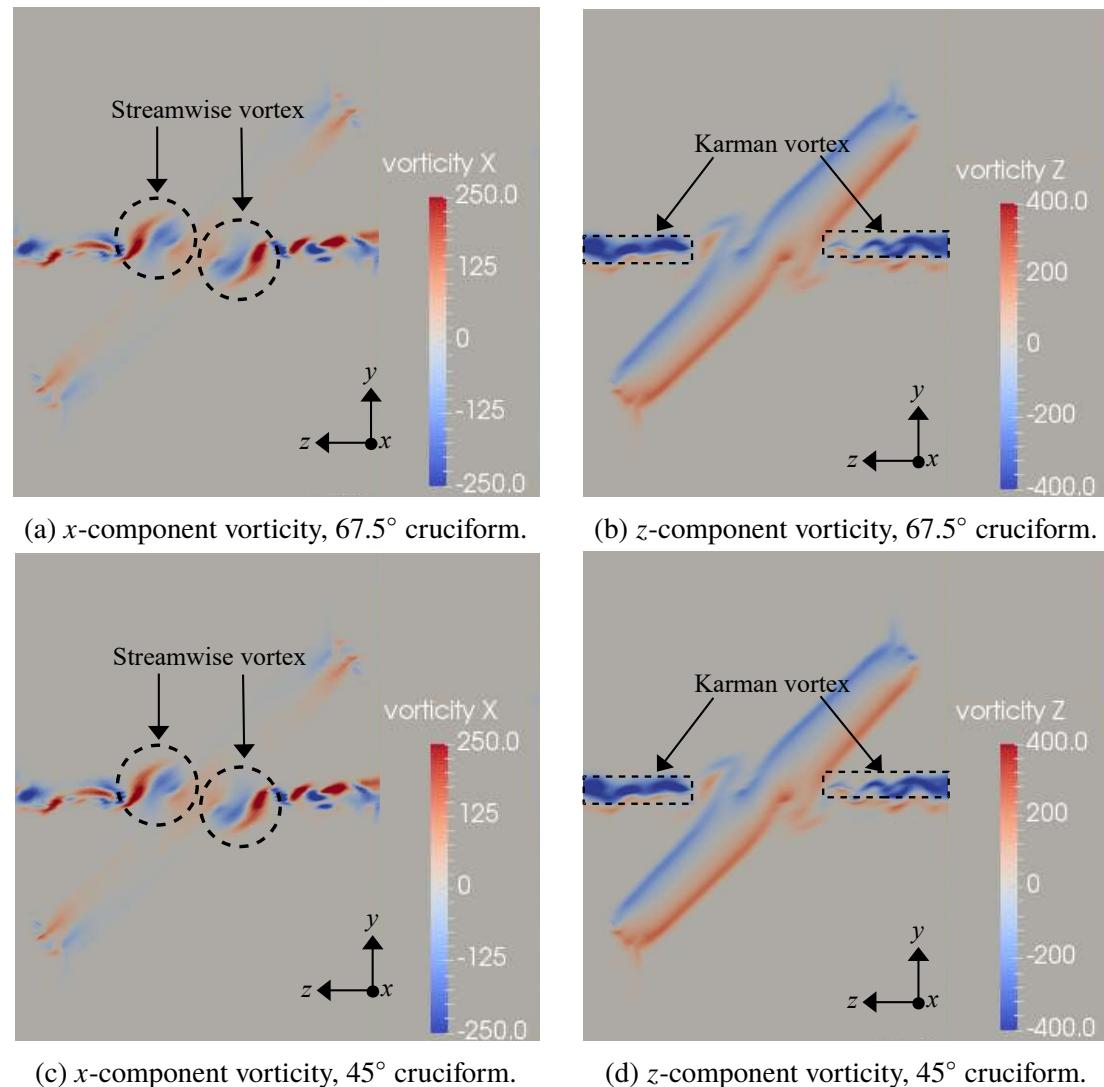


Figure 4.29 Dominant vortical structures at $U^* = 22.7$ observed in the 67.5° and 45° cases.

The reason behind this is thought to lie in the distribution of the streamwise vortex cells along the cylinder axis. As mentioned in Section 4.3.2, the streamwise vortex pair in the pure cruciform case lie on a plane parallel to the axis of the cylinder. The shared plane of formation parallel to cylinder axis is what seems to be the key to the large amplitude response observed in the pure cruciform case. A formation plane parallel to the cylinder axis ensures the resulting downward thrust to act perpendicular to the cylinder, securing a larger amplitude response. Also, the streamwise vortex cell on each side of the $Z = 0$ plane must be of opposing rotational direction for the production of thrust. These two aspects are found to be missing in the 67.5° and 45° cruciforms in Fig. 4.29.

What takes place in Figs. 4.29a and 4.29c is, two streamwise vortex cells of opposing poles form on each side of the $Z = 0$ plane. The result of this vortical arrangement is severe diminishing of useful thrust, and by extension, lift acting on the cylinder. This explains why the amplitude of f_v^* at and within the vicinity of 1 is extremely small in comparison to the dominant band close to $f_{v,\text{Karman}}^* = 4.49$, resulting in a low amplitude response for most of the U^* studied, even when $f^* \approx 1$.

The source of asymmetry in the vortical structure distribution around the cruciform is also found, which becomes apparent upon closer comparison of Fig. 4.29b and Fig. 4.29d. The Karman vortices of the 67.5° cruciform are shed at different phases depending on which side of the $Z = 0$ plane they are observed. For the particular case in Fig. 4.29b, Karman vortices are being shed from the top of the cylinder when $Z < 0$, and from the bottom of the cylinder when $Z > 0$. What suggested this interpretation is the observation of a strong expression of $-z$ vorticity when $Z < 0$ from the top of the cylinder, while on the $Z > 0$ half of the domain is a strong expression of $+z$ vorticity from the bottom of the cylinder. This does not seem to take place in Fig. 4.29d. On both sides of the $Z = 0$ plane, there exists a strong expression of $-z$ vorticity from the top of the cylinder. This asymmetry leads to competing vibration-driving mechanisms resulting in the oscillatory behaviour of f^* seen in Fig. 4.25.

Figure 4.30 presents the Q-criterion for the 67.5° cruciform at $U^* = 4.5$. It is apparent that Karman vortices dominated the shedding process at this U^* . The vortices

are coherent and orderly, which contributes to the peak in the amplitude response at this U^* .

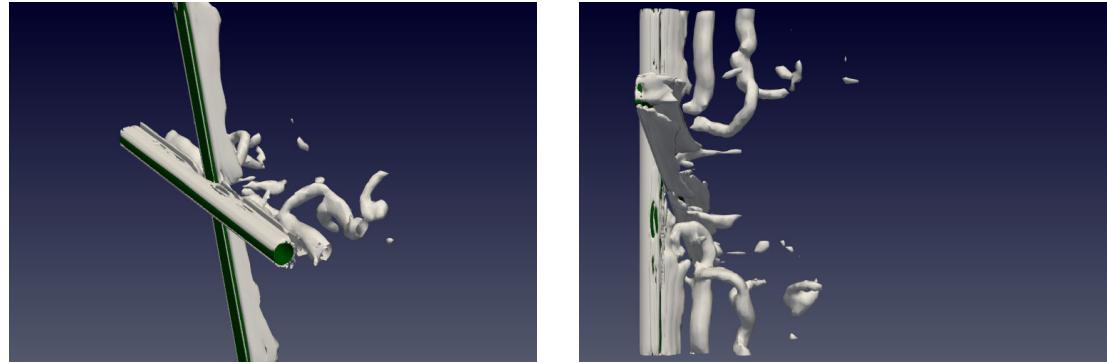


Figure 4.30 The Q-criterion for the 67.5° cruciform at $U^* = 4.5$: the isometric (4.30a) and plan view (4.30b).

On the other hand, at $U^* = 22.7$, the vortical structure in Fig. 4.31 lack coherence and are made up of many small vortices, instead of a few strong ones that can drive the vibration of the cylinder. This causes the vibration to be suppressed.

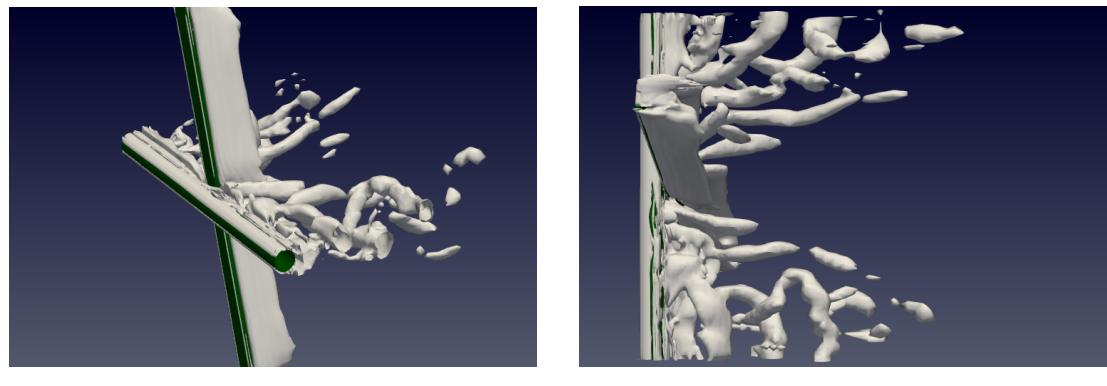
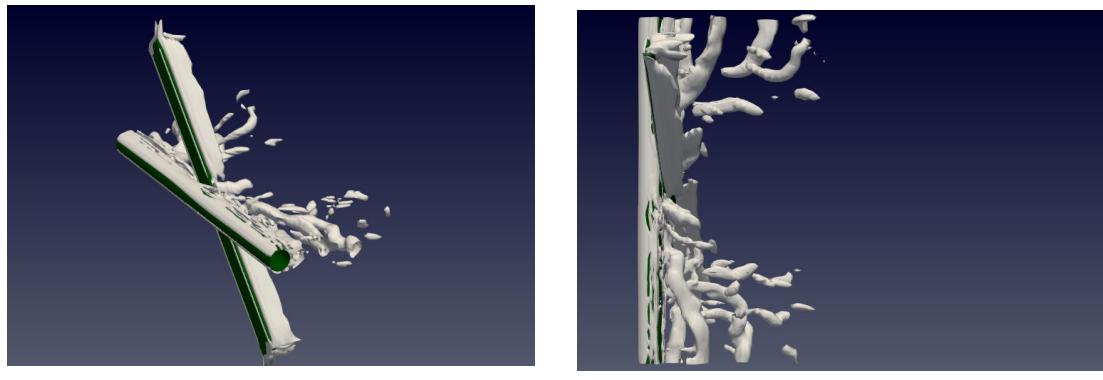


Figure 4.31 The Q-criterion for the 67.5° cruciform at $U^* = 22.7$: the isometric (4.31a) and plan view (4.31b).

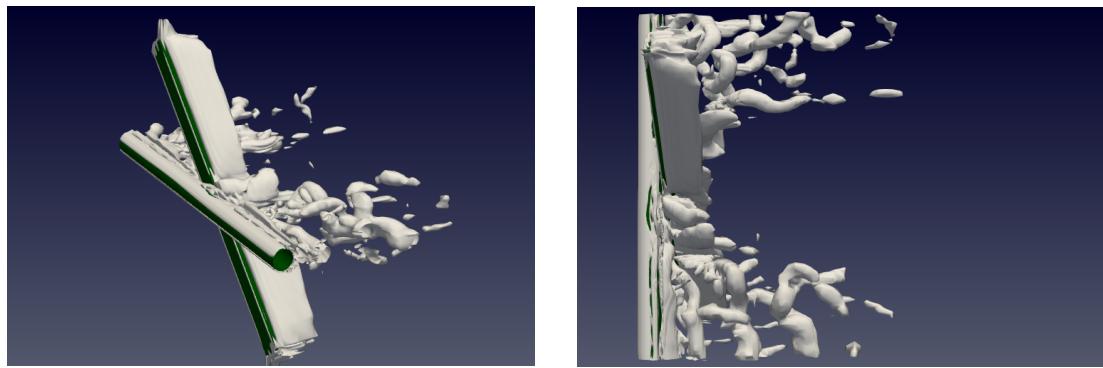
A similar result is observed for the 45° cruciform in Fig. 4.32. The Karman vortices being shed are too chaotic and small to match the amplitude response of the 67.5° cruciform at the same $U^* = 4.5$. Increasing the U^* to 22.7 does not solve this problem. As shown in Fig. 4.33, increasing U^* only increases the turbulence in the flow, not lift.



(a) Isometric view of the Q-criterion.

(b) Plan view of the Q-criterion.

Figure 4.32 The Q-criterion for the 45° cruciform at $U^* = 4.5$: the isometric (4.32a) and plan view (4.32b).



(a) Isometric view of the Q-criterion.

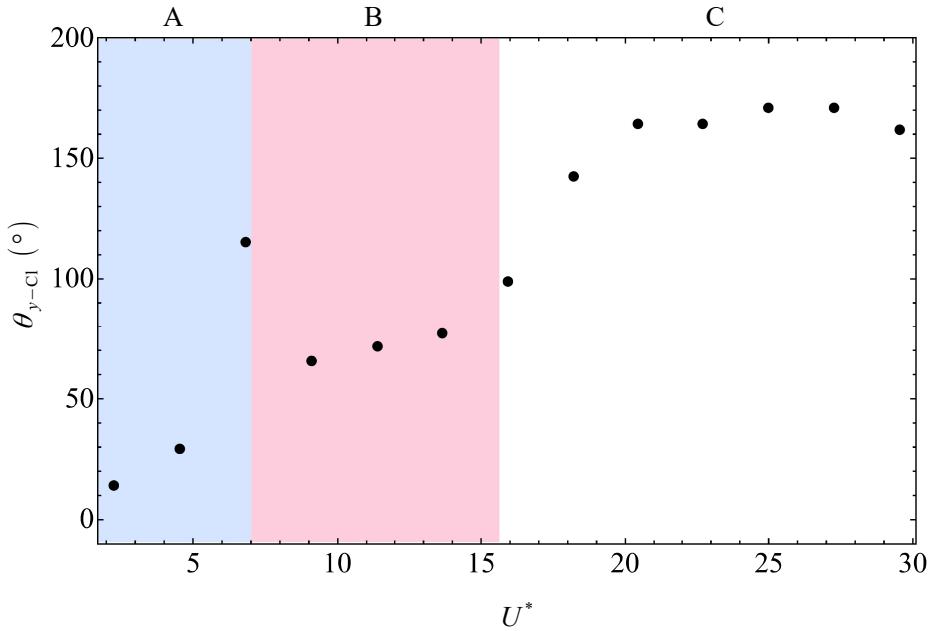
(b) Plan view of the Q-criterion.

Figure 4.33 The Q-criterion for the 45° cruciform at $U^* = 22.7$: the isometric (4.33a) and plan view (4.33b).

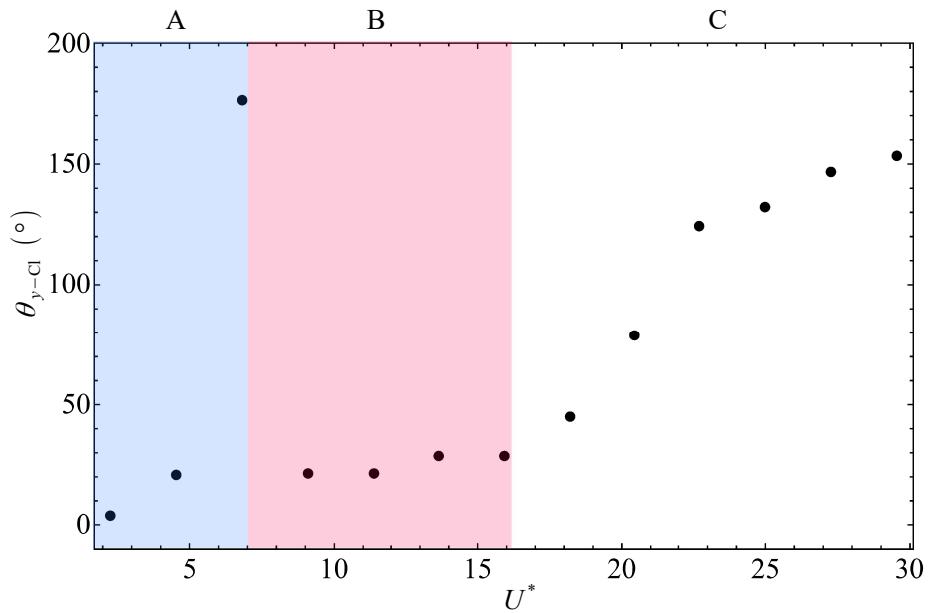
4.4.3 Phase lag between C_L and normalised cylinder displacement

Evolution of θ_{y-C_L} for the 67.5° and 45° cruciforms share a similar trend in the $2.3 \leq U^* \leq 6.8$ range. For the 67.5° cruciform, past $U^* = 6.8$, there seem to be two distinct VIV branches between $2.3 \leq U^* \leq 13.6$, and between $15.9 \leq U^* \leq 29.5$. In the first branch between $2.3 \leq U^* \leq 13.6$, θ_{y-C_L} seems to remain close to 70° , while in the second branch, close to 110° . In some sense, this is fairly similar to the θ_{y-C_L} vs. U^* pattern of the pure cruciform case, except for two features. First, the lower branch of KVIV – which in the pure cruciform case exhibits a $\theta_{y-C_L} \approx 180^\circ$ – does not extend beyond $U^* = 6.8$. Instead, the value for θ_{y-C_L} suddenly drops to $\approx 70^\circ$ before jumping back up to $\approx 110^\circ$ starting at $U^* = 15.9$. This value of 110° is curiously close to θ_{y-C_L} of the pure cruciform between $20.5 \leq U^* \leq 29.5$, equivalent to the upper branch of SVIV. Working backwards from $U^* = 20.5$ in the direction of decreasing U^* , and compare Fig. 4.34a and Fig. 4.20, one confronts the possibility that the $\theta_{y-C_L} = 70^\circ$ branch of the 67.5° cruciform is a *variant* of the SVIV initial branch. For the pure cruciform case, this occurs within a narrow window of $15.9 < U^* < 20.5$, with $\theta_{y-C_L} \approx 20^\circ$.

For the 45° cruciform in Fig. 4.34b, right after lower branch of KVIV at $U^* = 6.8$, θ_{y-C_L} transitioned to $\approx 65^\circ$ between $11.4 \leq U^* \leq 20.5$. The proximity between the values 65° and 70° for the 67.5° cruciform suggests the equivalence of the two branches. However, this study is inclined to a more cautious conclusion: the two are *variants* of the same branch that is only similar in limited respects as they originate from different angled cruciforms. In this respect, the 45° cruciform is much less similar to the pure cruciform case, as one might expect, simply because 45° is a much larger deviation from 90° compared to 67.5° . This larger deviation is in the opinion of this study, what causes θ_{y-C_L} in the 45° case to drop further to $\approx 35^\circ$ within $22.7 \leq U^* \leq 29.5$, instead of jumping up to some mean value between $100 \leq \theta_{y-C_L} (\circ) \leq 130$ similar to what is observed in the 90° and 67.5° cruciforms. Results from this Section 4.4.3 and the previous Sections 4.4.2 and 4.4.1 partially answers thesis objective one.



(a) Phase lag for the 67.5° cruciform.



(b) Phase lag for the 45° cruciform.

Figure 4.34 Phase lag θ_{y-Cl} (°) between C_L and y^* when 67.5° and 45° .

4.5 Shallow-angled Cruciforms

The previous Section 4.4 is an attempt to control the vortical structures dominating the flow around a cruciform oscillator to focus as much as possible energy from the freestream to the vortical structure driving the vibration of the cylinder. In

doing so, the steep-angled cruciforms seem to prefer the Karman vortex as the lift producing mechanism, as evidenced by the evolution of $f_{C_l}^*$ against U^* , which closely follow the shedding frequency of Karman vortex given in Eq. 2.5.

4.5.1 The amplitude and frequency response

As the cruciform angle is decreased even further to 22.5° , a significant change is observed in the amplitude and frequency response, compared to the transitional stage previously explored in Section 4.4. Consider Figs. 4.35 and 4.36. There is no apparent KVIV upper branch similar to what Fig. 4.24 has shown at $U^* = 4.5$. Then, there is no significant vibration elicited from the oscillator until $U^* = 20.5$. When $U^* = 20.5$, there is an abrupt jump in y_{RMS}^* from $y_{\text{RMS}}^* < 0.02$ to $y_{\text{RMS}}^* \approx 0.3$. The f^* vs. U^* trend demonstrated a bypassing of the KVIV lower branch - which occurred at $U^* = 6.8$ in the transitional stages of Section 4.4 - right into $f^* \approx 1$. Past $U^* = 20.5$, the value for y_{RMS}^* continues to increase and saturates at $U^* = 25.0$, and f^* continues to be close to 1 up to $U^* = 29.5$.

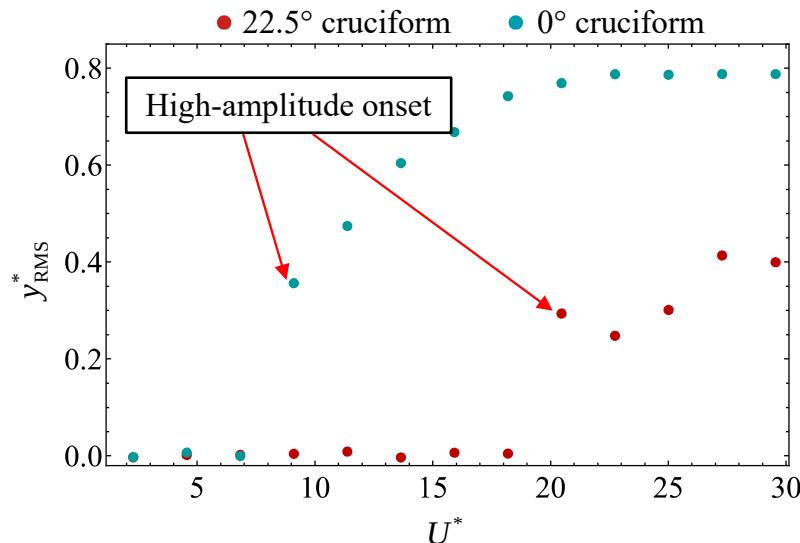


Figure 4.35 Evolution of the normalised vibration amplitude y_{RMS}^* , with respect to reduced velocity U^* , for the 22.5° and 0° cruciforms.

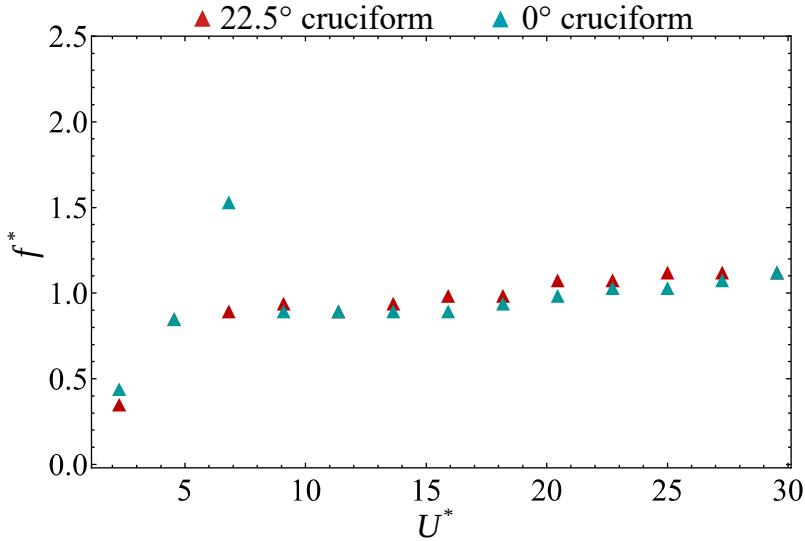


Figure 4.36 Evolution of the normalised cylinder displacement frequency, f^* , with respect to reduced velocity U^* , for the 22.5° and 0° cruciforms.

The 0° cruciform in essence exhibits a very similar trend in its y_{RMS}^* and f^* evolutions with respect to U^* . However, the jump – which for the 22.5° cruciform occurs at $U^* = 20.5$ – occurs at a much lower $U^* = 9.1$. Then, y_{RMS}^* continues to grow until $U^* = 20.5$, reaching a staggering $y_{\text{RMS}}^* \approx 0.8$, a value no other study on energy harvesting using cruciform oscillators has ever achieved. The value of y_{RMS}^* then saturates close to 0.8 up to $U^* = 29.5$. Also similar to the 22.5° cruciform, f^* falls close to 1 at same U^* the y_{RMS}^* jump occurs - hinting at synchronisation between vortex shedding and system natural frequency.

Apart from the amplitude/frequency response of the 22.5° cruciform, the evolution of $C_{L,\text{RMS}}$ against U^* showcases a similar trend to the evolution y_{RMS}^* , as shown in Fig. 4.37. The corresponding $f_{C_L}^*$ in Fig. 4.38 demonstrates the dominant frequency of C_L taking after Eq. 2.6 between $2.3 \leq U^* \leq 18.2$, before abruptly dropping close to 1 between $20.5 \leq U^* \leq 29.5$. This in part informs the investigation that the flow between $2.3 \leq U^* \leq 18.2$ is governed by flow physics that are similar to both 67.5° and 45° within the same U^* range.

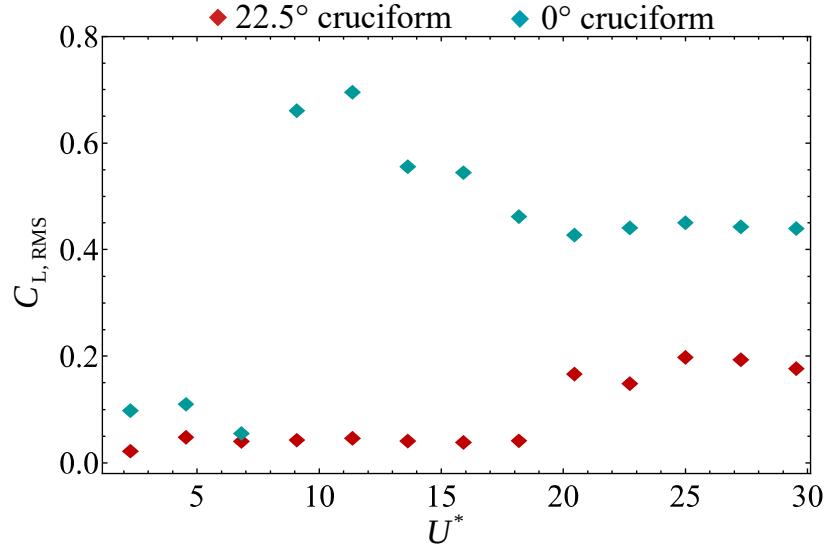


Figure 4.37 Evolution of the normalised C_L root-mean-square amplitude, $C_{L,RMS}$, with respect to reduced velocity U^* , for the 22.5° and 0° cruciforms.

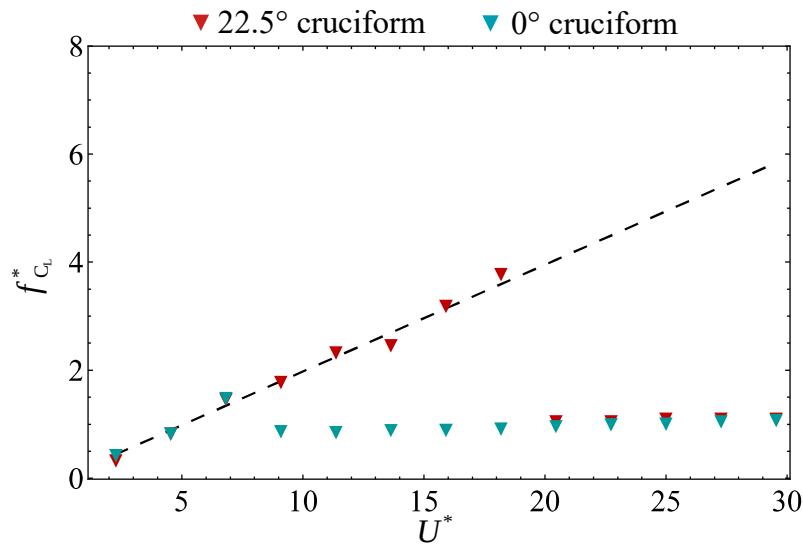


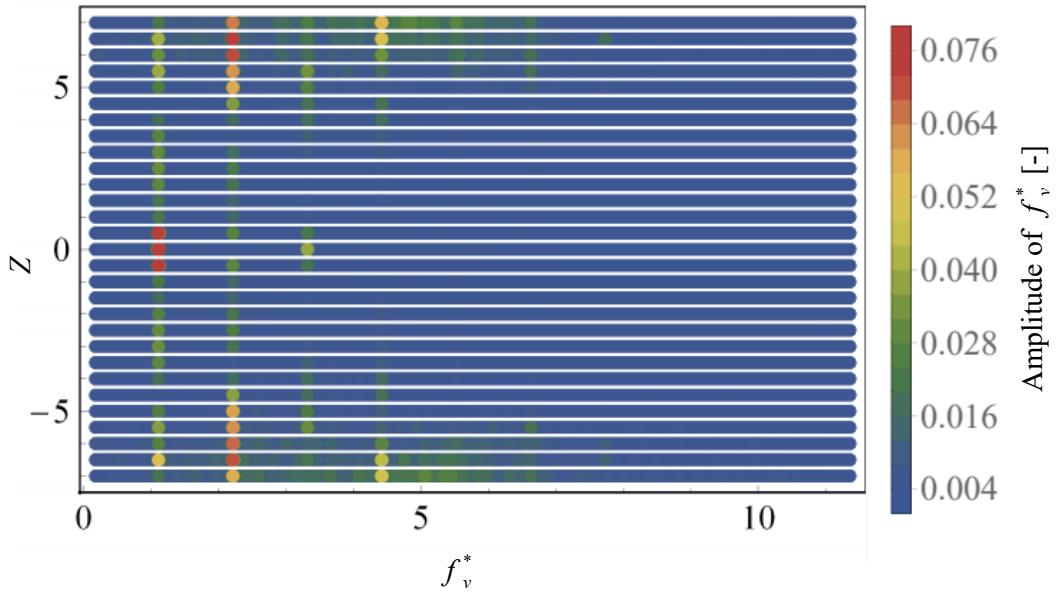
Figure 4.38 Evolution of the normalised C_L frequency, $f_{C_L}^*$, with respect to reduced velocity U^* , for the 22.5° and 0° cruciforms. The dashed lines outline $f_{v,\text{Karman}}$ from Eq. 2.6.

For the 0° cruciform, the jump in $C_{L,RMS}$ seems to occur at the same U^* as the jump in the corresponding y_{RMS}^* i.e., $U^* = 9.1$. After $U^* = 9.1$, the magnitude of

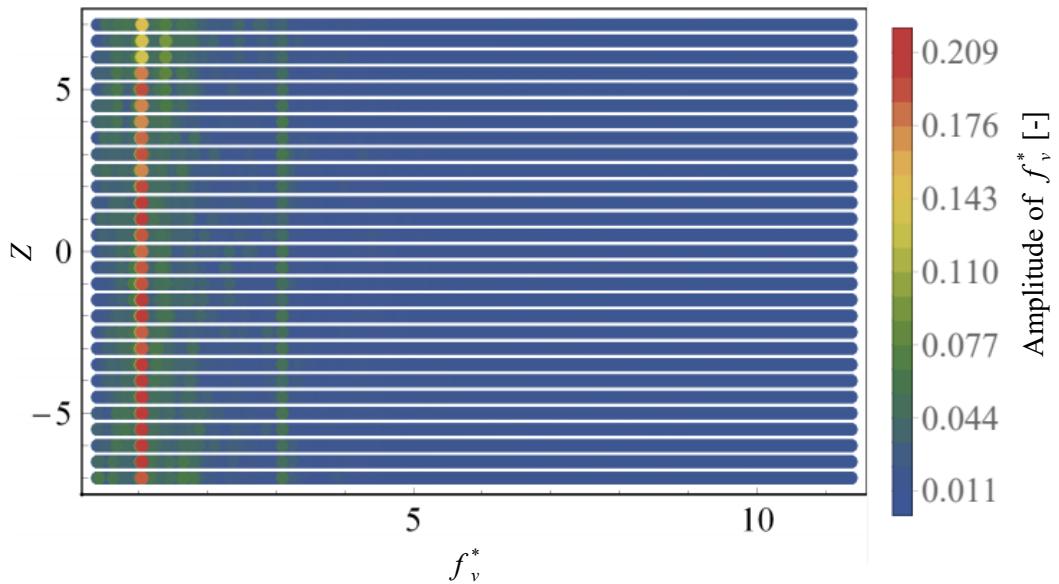
$C_{L,RMS}$ gradually drops to a final value of $C_{L,RMS} \approx 0.45$ at $U^* = 20.5$, and remains there up to $U^* = 29.5$. Similar to the 22.5° cruciform, $f_{C_l}^*$ grows linearly in accordance with, again, Eq. 2.6 until the jump in both $C_{L,RMS}$ and y_{RMS}^* , where $f_{C_l}^*$ drops close to 1 for the rest the U^* examined in this study.

4.5.2 Main vibration-driving vortical structure

To understand the cause behind the marked difference between the amplitude/frequency response in both 67.5° and 45° cruciforms, this study proceeds to deduce the type of vortical structures that form in the flows around the 22.5° and 0° cruciform. First, visualise f_v^* along the cylinder in Fig. 4.39a. Inspecting Fig. 4.39a, one notices that several frequency bands exist: $f_v^* \approx 1, 2, 3, 4.5$, the most visible of which is the $f_v^* \approx 1$ band. However, unlike the pure cruciform case in Fig. 4.9 – where the dominant frequency bands are localised to certain regions along the cylinder – the $f_v^* \approx 1$ band of the 22.5° cruciform seems to encompass the length of the cylinder. This also seems to be the case for the 0° cruciform, displaying a dominant f_v^* band at approximately 1 along the length of the cylinder.



(a) The f_v^* for the 22.5° cruciform.



(b) The f_v^* for the 0° cruciform.

Figure 4.39 Distribution of normalised frequency of vortex shedding, along the span of the cylinder of the 22.5° and 0° cruciforms at $U^* = 22.7$.

Then, the x and z -component vorticity contours of the 22.5° cruciform is queried for deeper insight, presented in Figs. 4.40a and 4.40b. In doing so, the large scale streamwise vortex pair near the cruciform juncture is found to be absent. Instead, streamwise vortex cells are found to be distributed on both sides of the $Z = 0$ plane, except within the immediate neighbourhood of the cruciform juncture. Note that these streamwise vortex cells are distributed at a slight angle relative to the z -axis, seemingly following the angle of the strip plate, i.e. 22.5° . Visualisation of the z -component vorticity in Fig. 4.40b intimates the nature of the tilted streamwise vortex cells: they are simply three-dimensional Karman vortex structures, akin to those observed in the experiments of Williamson (1996b), especially mode B. This is inferred from comparison of the same visual region delimited by dashed rectangles in Figs. 4.40a and 4.40b, showing the overlap between the streamwise vortex cells and the strong Karman vortex component.

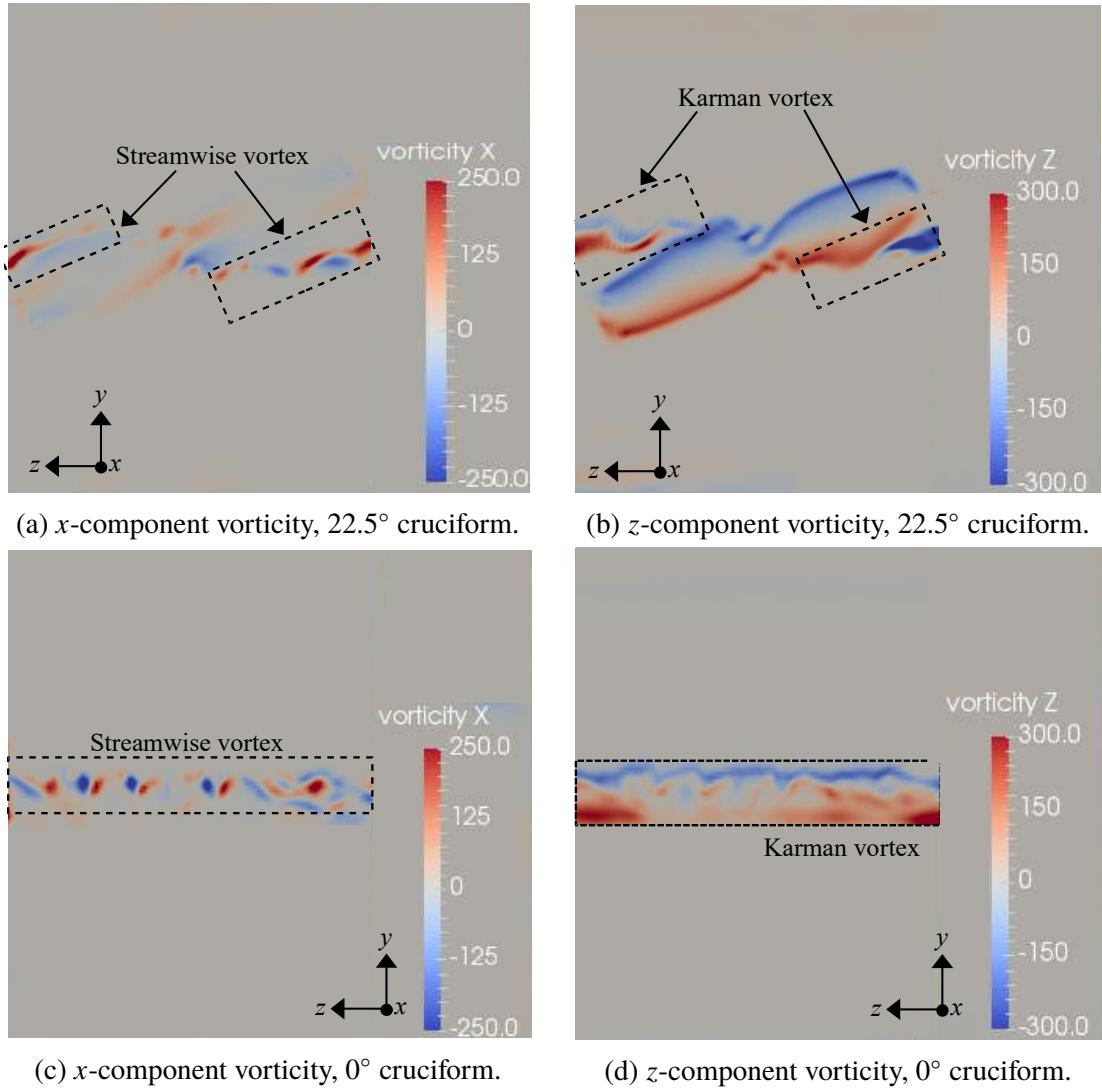
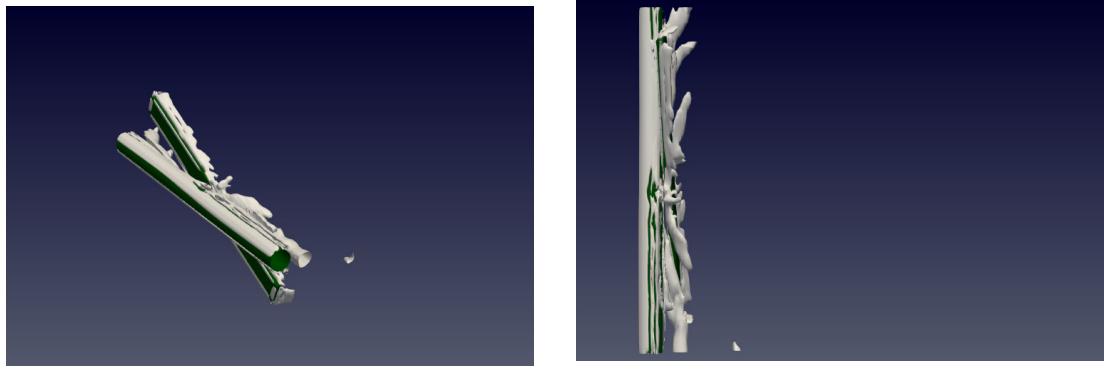


Figure 4.40 Dominant vortical structures at $U^* = 22.7$ observed in the 22.5° and 0° cases.

For the 0° cruciform in Figs. 4.40c and 4.40d, this overlap between the streamwise vortex cells and the distinct Karman vortex component is even more visually pronounced. This is interpreted as further evidence to the hypothesis that three-dimensional Karman vortical structures govern the vibration of the cylinder for shallow angled cruciforms, including the 0° cruciform, which perhaps is more aptly named in-tandem configuration. Notice that for the 0° layout, both the streamwise vortex cells and the Karman vortical structure are arranged parallel to the z -axis, or at 0° relative to the cylinder. This observation seems to demonstrate the role of the strip

plate in shallow angled cruciforms: it modifies the spatial distribution of the Karman vortical structure that is driving the vibration of the cylinder.

Figure 4.41 presents the Q-criterion for the 22.5° cruciform at $U^* = 4.5$. The visualisation shows that while vortices do form around the cruciform, they do not seem to be sufficiently energised by the surrounding flow. Hence, their effect on driving the vibration of the cylinder becomes negligible. Apart from that, the vortical structures do not seem to be shed in a periodic manner. Instead, the vortical structures seem bunched up in the near-wake region of the cruciform. It is possible that this also contributed to the suppression of the vibration.

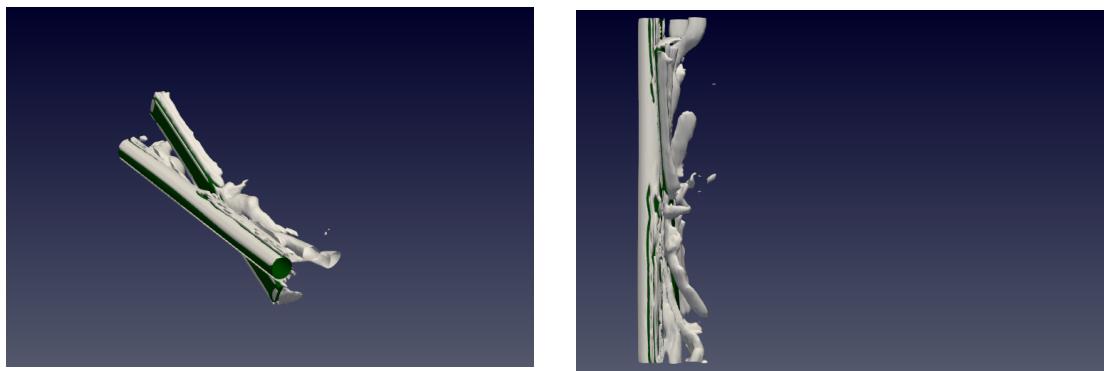


(a) Isometric view of the Q-criterion.

(b) Plan view of the Q-criterion.

Figure 4.41 The Q-criterion for the 22.5° cruciform at $U^* = 4.5$: the isometric (4.41a) and plan view (4.41b).

On the other hand, Fig. 4.42 presents the Q-criterion for the 22.5° cruciform at $U^* = 22.7$. This time, the vortices in the near-wake of the cruciform is larger than those in Fig. 4.41. When the vortices being shed are large enough and sufficiently energised, they can impose a periodic lift capable to drive the vibration of the cylinder. This results in the jump in onset of high-amplitude vibrations shown previously in Fig. 4.35.

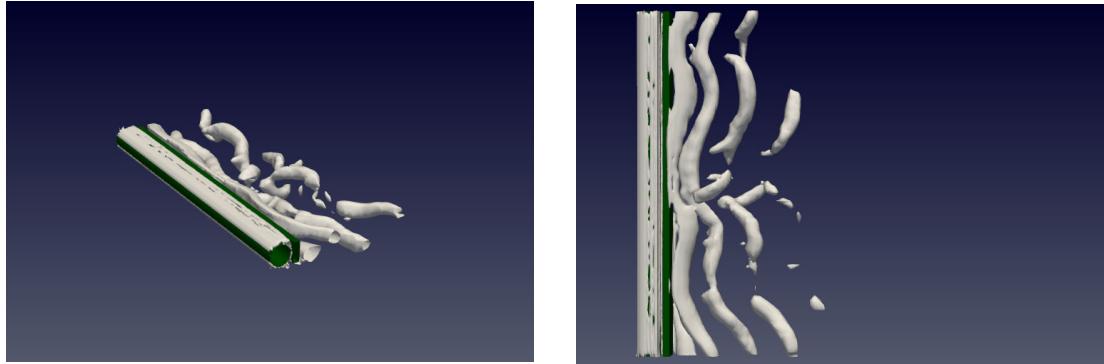


(a) Isometric view of the Q-criterion.

(b) Plan view of the Q-criterion.

Figure 4.42 The Q-criterion for the 22.5° cruciform at $U^* = 22.7$: the isometric (4.42a) and plan view (4.42b).

In contrast, the Q-criterion of the 0° cruciform at $U^* = 4.5$ show that periodic shedding of Karman vortices do occur. The Karman vortices are coherent and they span the length of the cylinder. The reason behind the small vibration amplitude observed in Fig. 4.35 is thus due to insufficient energising of the vortical structures.

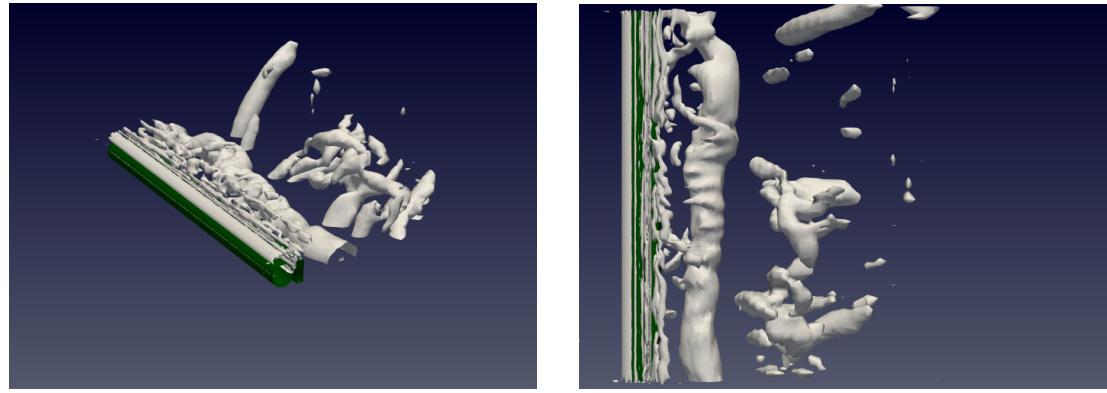


(a) Isometric view of the Q-criterion.

(b) Plan view of the Q-criterion.

Figure 4.43 The Q-criterion for the 0° cruciform at $U^* = 4.5$: the isometric (4.43a) and plan view (4.43b).

However, because the vortices in the 0° cruciform are highly coherent and periodic, even a slight increase in U^* triggered the onset of high-amplitude vibrations, visible in Fig. 4.35. The onset takes place at $U^* = 9.1$, which is a mere $9.1 - 4.5 = 4.6$ from $U^* = 4.5$ in Fig. 4.43. An example vortical structure shed during the high-amplitude vibrations of the 0° cruciform is shown in Fig. 4.44. It is apparent especially from Fig. 4.43b that the diameter of the vortex is significantly bigger compared to that visualised in Fig. 4.43b. This increase in diameter, or size, is an indication of increased strength of the vortex. As a result, the cylinder produces the highest amplitude vibration among all cruciforms studied in this thesis.



(a) Isometric view of the Q-criterion.

(b) Plan view of the Q-criterion.

Figure 4.44 The Q-criterion for the 45° cruciform at $U^* = 22.7$: the isometric (4.44a) and plan view (4.44b).

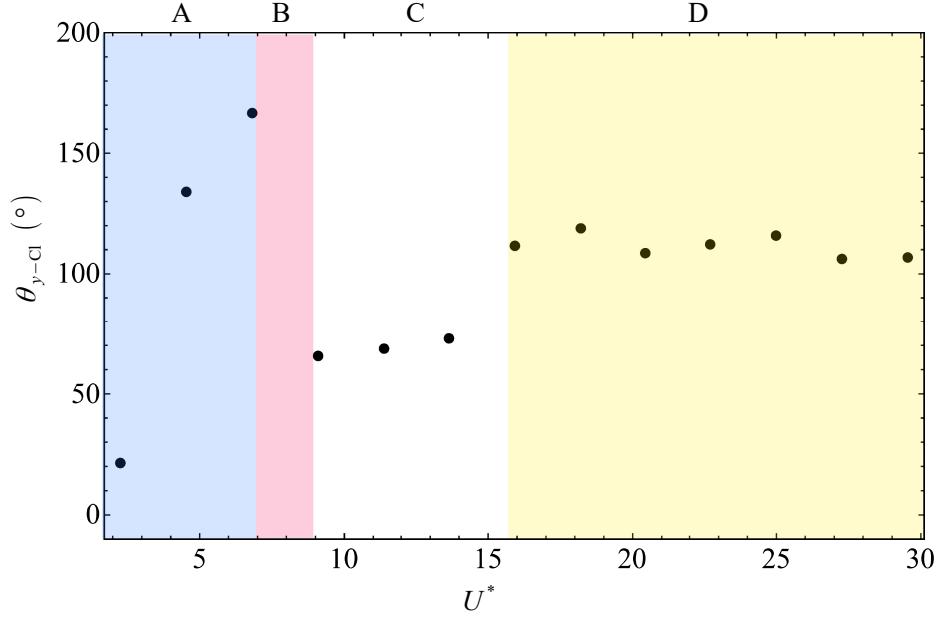
As demonstrated in Section 4.3 and 4.4, eliciting a significant vibration amplitude Karman vortex shedding is limited to a narrow U^* range containing the upper branch of KVIV. Beyond that, Karman vortex shedding fails to lock into the natural frequency of the system to produce meaningful vibrations. The fact that shallow angled cruciforms in this Section 4.5.2 are able to produce very large vibration amplitudes intimate the crucial role played by the strip plate in forcing the shedding of vortical structures and cylinder vibration to lock into the natural frequency of the system f_n . The mechanics of this forced lock-in is thought to be as follows.

1. Shallow angled cruciforms have a larger overlap area between the cylinder and strip plate. This permits a more perceptible interaction among vortices shed from the cylinder and the strip plate.
2. Upon exceeding a critical U^* , vortical structures shed from both the cylinder and the strip plate becomes sufficiently energised, and they start to behave as one.
3. This vortical synchronisation locks into the natural frequency of the elastic structure in its immediate vicinity - the circular cylinder.

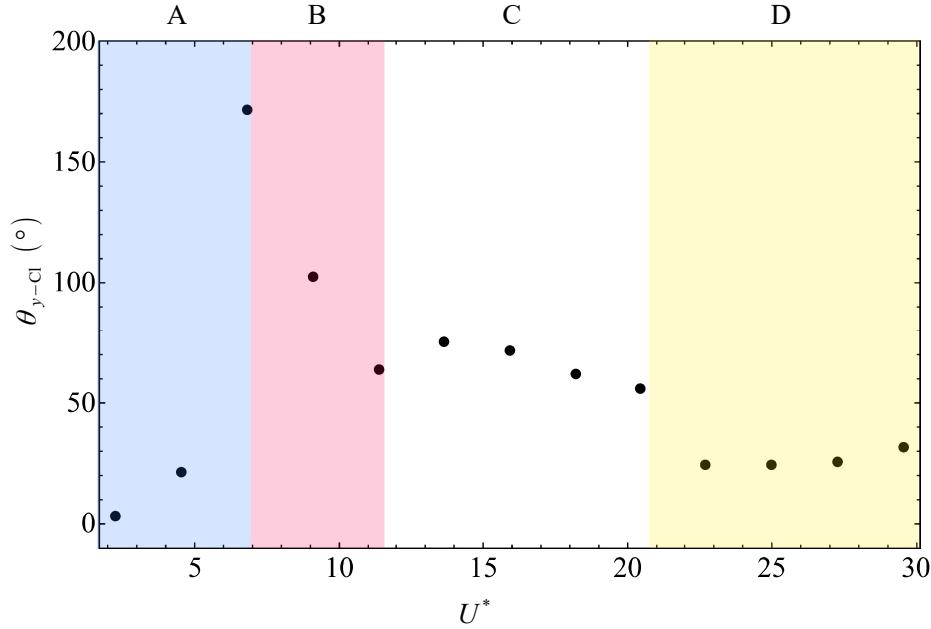
The results also suggest the total cylinder-strip plate area overlap as a factor influencing the exact U^* at which the vortical synchronisation occurs. The U^* at which the synchronisation – and the jump to large y_{RMS}^* amplitude – occurs at a lower value when the overlap area is bigger. Nevertheless, there seems to be a limit to this lowering of U^* , which in this work is determined to be $U^* = 9.1$. Recall that this is the value where the synchronisation begins for the 0° layout; the layout where the totality of the cylinder and strip plate projections onto the $y - z$ plane coincides with each other.

4.5.3 Phase lag between C_L and normalised cylinder displacement

In Fig. 4.45a, the evolution of θ_{y-C_L} is summarised according to U^* for the 22.5° cruciform. It is observed that $\theta_{y-C_L} \approx 115^\circ$ at $U^* = 6.8$. The significance of $U^* = 6.8$ for the 22.5° cruciform is that it is where a jump in θ_{y-C_L} occurs from $\approx 30^\circ$ to $\approx 115^\circ$. This abrupt jump usually demarcates transition to the KVIV lower branch, as stated in the discussion accompanying Figs. 4.20 and 4.34, with a value that is very close to 180° . The θ_{y-C_L} for the 22.5° cruciform however, is about 36% smaller than the expected $\approx 180^\circ$. The fact that $\theta_{y-C_L} < 180^\circ$, may be the cause of absence of the KVIV lower branch in the f^* vs. U^* plot of the 22.5° cruciform in Fig. 4.36.



(a) Phase lag for the 22.5° cruciform.



(b) Phase lag for the 0° cruciform.

Figure 4.45 Phase lag θ_{y-C_L} ($^\circ$) between C_L and y^* when 22.5° and 0° .

The 0° arrangement produces a similar trend to Fig. 4.45a, as one can see in Fig. 4.45b. However, the θ_{y-C_L} jump at $U^* = 29.5$ is more pronounced and achieves a value very close to 180° . Following the sudden jump, is the sudden drop at $U^* = 9.1$. This brings θ_{y-C_L} to approximately 25° . This trend continues up to $U^* = 15.9$, after

which θ_{y-C_L} is found to gradually increase up to $U^* = 29.5$. Results from this Section 4.5.3, and previous Sections 4.5.1 and 4.5.2 answers thesis objective one.

4.6 Power characteristic in cruciform angle - reduced velocity parameter space

Table 4.2 summarises the key values observed in this study. In the table, key values such as the maximum y_{RMS}^* , high-amplitude vibration onset (U^*), maximum $P_{\text{Mech.,RMS}}$ (mW) and maximum $\eta_{\text{Mech.}}$ (%) are presented. These values serve as the basis to create the map for y_{RMS}^* , $P_{\text{Mech.,RMS}}$ and $\eta_{\text{Mech.}}$ in α ($^\circ$) – U^* parameter space.

Table 4.2 Summary of main findings.

Parameter / Cruciform Angle, α ($^\circ$)	0	22.5	45	67.5	90
Maximum y_{RMS}^*	0.79	0.41	0.03	0.08	0.49
High-amplitude onset (U^*)	9.1	20.5	4.5	4.5	22.7
Maximum $P_{\text{Mech.,RMS}}$ (mW)	11.3	2.9	0.01	0.07	3.6
Maximum $\eta_{\text{Mech.}}$ (%)	1.8	0.17	0.22	1.01	0.27

In this study, the mechanical power is computed for each cruciform through the application of the formula in Eq. 3.4. To understand how mechanical power $P_{\text{Mech.,RMS}}$ is influenced not only by U^* , but also by the cruciform angle α ($^\circ$), $P_{\text{Mech.,RMS}}$ is visualised as contour plots, where the abscissa and ordinate are U^* and α , respectively, and the colour of the contours denote the magnitude of $P_{\text{Mech.,RMS}}$. As an example, the values of y_{RMS}^* against U^* and α are plotted in Fig. 4.46.

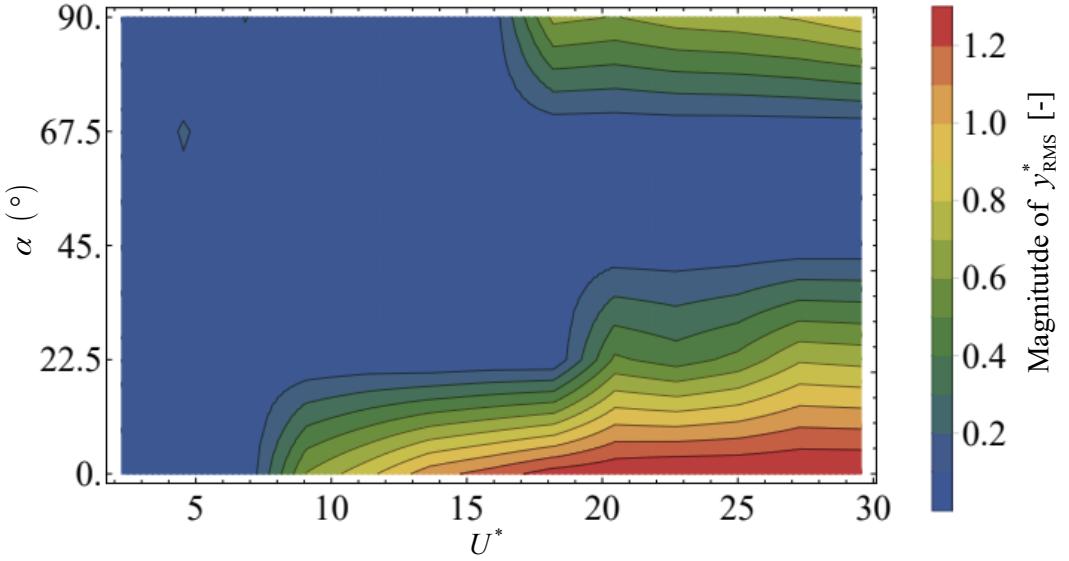


Figure 4.46 Isocontours describing the map of the normalised RMS amplitude of cylinder displacement, y_{RMS}^* in the cruciform angle - reduced velocity ($\alpha-U^*$) parameter space.

The data used to produce Fig. 4.46 are those from Figs. 4.4, 4.24 and 4.35. Then, linear interpolations are performed on the y_{RMS}^* data along both U^* and α axes to populate the $\alpha-U^*$ parameter space. The result of this two-dimensional interpolation is Fig. 4.46. The snapshot of y_{RMS}^* evolution in the $\alpha-U^*$ parameter space summarises the observations made previously in Figs. 4.4, 4.24 and 4.35.

Then, the same two-dimensional interpolation is performed on the results of $P_{\text{Mech.,RMS}}$ and then summarised Fig. 4.47. Two regions of significant power generation exist: first, in the $18.2 \leq U^* \leq 29.5$ range as α approaches 90° , and second, starting as low as $U^* = 9.1$ up to $U^* = 29.5$ as α approaches 0° . The estimated power in the region approaching $\alpha = 90^\circ$ agrees well in magnitude with previous experimental works such as Koide *et al.* (2013). Also, even though no power data was measured in pure cruciform oscillator studies of Koide *et al.* (2009); Nguyen *et al.* (2012), their y_{RMS}^* data agrees well in trend and in magnitude with Fig. 4.46, along the 90° line. The $P_{\text{Mech.,RMS}}$ contour of Fig. 4.47 visualises the high power region as α approaches

0° and U^* approaches 29.5. The highest $P_{\text{Mech.,RMS}}$ estimated from the simulation reaches $O(10^1)$ mW, which is one order of magnitude larger than any cruciform energy harvester of this scale have ever recorded in the literature.

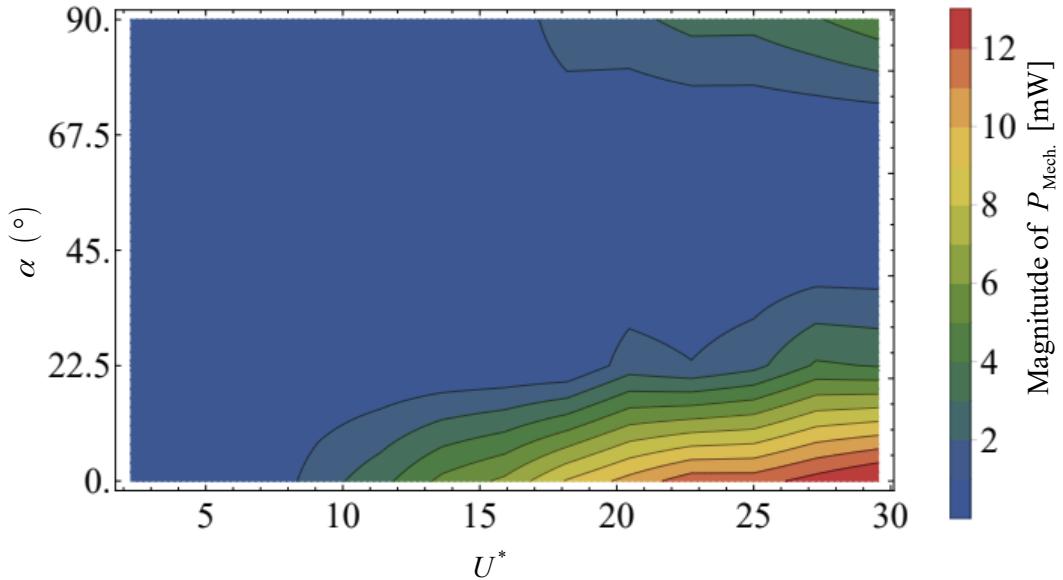


Figure 4.47 Isocontours describing the map of the estimated mechanical power in the cruciform angle - reduced velocity ($\alpha-U^*$) parameter space.

The $P_{\text{Mech.,RMS}}$ contour also elucidated the feasibility of cruciform angle variation as a means to control the range of U^* within which substantive quantity of power can be harnessed. For a given operating range of U^* , one can choose for substantive power generation to take place in the high U^* region ($U^* \geq 18.2$), or across a larger range starting from a minimum of $U^* = 9.1$, by manipulating the cruciform angle. For power generation in the high U^* region, one simply sets the cruciform angle to 90° , and for power generation starting from the lowest possible U^* , one should opt for a shallow-angled cruciform, with increasing magnitude of power generated as $\alpha \rightarrow 0^\circ$.

Unlike Fig. 4.47, the efficiency contour in Fig. 4.48 does not display a trend similar to the contour of y_{RMS}^* in Fig. 4.46. The pure cruciform achieves maximum $\eta_{\text{Mech.}}$ close to $U^* = 18.2$, steep-angled cruciforms (67.5° and 45° cruciforms) attain

maximum $\eta_{\text{Mech.}}$ within the vicinity of $(U^*, \alpha) = (4.5, 67.5^\circ)$, and shallow-angled cruciforms (22.5° and 0° layouts) strikes maximum $\eta_{\text{Mech.}}$ in the neighbourhood of $(U^*, \alpha) = (9.1, 0^\circ)$. These high-efficiency regions is consistent with the assertion that different flow dynamics govern the vibration resulting from either the pure, steep-angled or shallow-angled cruciforms. This Section 4.6 answers objective three.

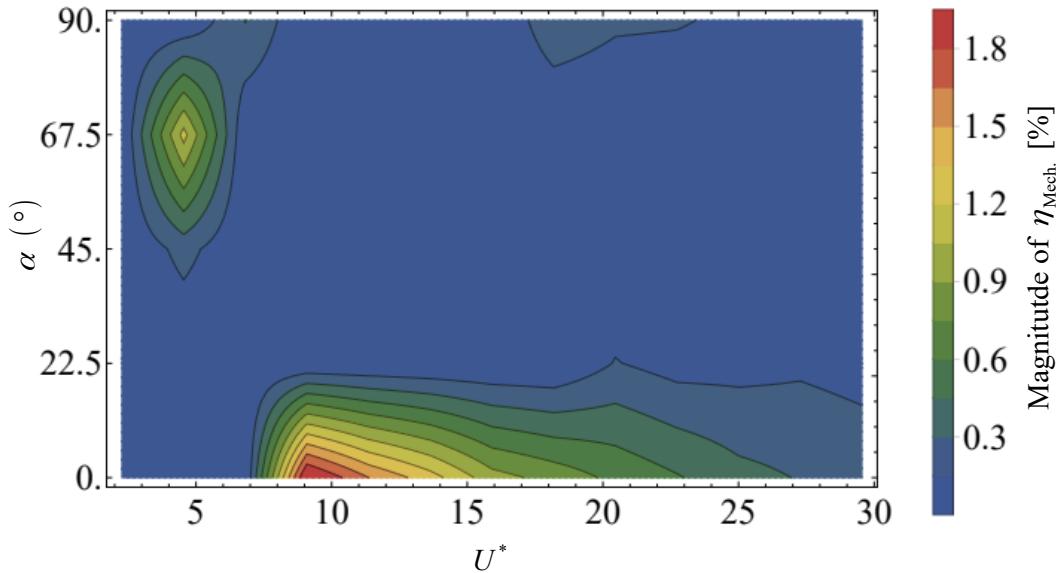


Figure 4.48 Isocontours describing the map of the estimated mechanical efficiency in the cruciform angle - reduced velocity ($\alpha-U^*$) parameter space.

4.7 Chapter Summary

The chapter begins with the study of amplitude/frequency responses of the pure cruciform. Then, these results are validated against experiment done in the open flow channel, and with experimental works of others in the literature. In doing so, this work found good agreement between the amplitude responses and observed fair agreement between the frequency responses. Then, the chapter proceeds with the demonstration of grid independency of the numerical solution. Through the GCI study, the fine mesh used for numerical data collection has been demonstrated to produce convergent results for y_{RMS}^* , f^* and C_L .

Next, as part of fulfilling objective one, this chapter demonstrated the vortical structures present in the flow during the high-amplitude vibrations of the pure cruciform. This is found to be due to the alternate shedding of large-scale streamwise vortices. Karman vortices continue to be shed in the region away from the juncture of the cruciform, but the region close to the juncture is dominated by streamwise vortex shedding.

For the steep-angled cruciforms, a different amplitude/frequency response as the pure cruciform was observed. This time, there only exists a narrow region of meaningful vibration in the KVIV regime. The SVIV regime seems to be non-existent in this steep-angled layout. Flow visualisations confirm the existence of large-scale streamwise vortices near the cruciform juncture, but the absence of a counter-rotating pair in the same plane as either the top or bottom of the upstream cylinder results in a severely diminished vibration-driving lift acting on the cylinder. Furthermore, the unstable evolution of f^* with respect to U^* led this study to discover an inherent asymmetry in the distribution of vortices along the length of the cylinder, most apparent of which are the Karman vortex cells. This non-uniform distribution of force along the length of the cylinder is what probably induces the instability in the evolution of f^* with respect to U^* .

For the shallow-angled cruciforms, increased symmetry in the vortical structures was found to improve y_{RMS}^* , compared to the pure cruciform. In addition, the high-amplitude vibrations are observed to start at a very low 9.1, compared to 20.5 for the pure cruciform case. The magnitude of $C_{L,\text{RMS}}$ is also found to improve by one order of magnitude for the 0° cruciform. The main vibration-driving vortical structure in the shallow angled cruciforms seems to be Karman vortices, as suggested by the flow visualisations. They are symmetrically distributed relative to the $Z = 0$ plane, and this seems to be the key to the onset of high-amplitude vibrations for both the 22.5° and 0° cruciforms.

In answering objective two, the lift signal of the pure cruciform is decomposed via EEMD. In doing so, this study discovers that during the early stages of the onset of SVIV, there is an increase in the level of intermittency of the signal, causing a dip in the

amplitude response. The results also demonstrate that there exists two main parts to the lift signal, namely the contribution due to the shedding of streamwise vortex and the contribution due to the shedding of Karman vortex. The presence of these two dominant components in the lift signal of the pure cruciform explains the saturation of y_{RMS}^* in the amplitude response curve, wherein a significant amount energy from the freestream is lost due to the production of Karman vortices. If the loss can be eliminated, this thesis found that for the pure cruciform, the power output can potentially be improved by a factor of two to a factor of three depending on U^* . Computation of θ_{y-C_L} using HHT suggests the existence of five regimes of vibration of the pure cruciform, four for the steep angled-cruciforms, and three for the shallow-angled cruciforms.

In answering objective three, y^* , $P_{\text{Mech.,RMS}}$ and $\eta_{\text{Mech.}}$ have been mapped out in the α ($^\circ$) – U^* parameter space. Through the isocontours of mechanical power, there exists two bands suitable for energy harvesting, first as the oscillator approaches a pure cruciform configuration and second as the oscillator approaches the in-tandem configuration (0°). However, the isocontours of the mechanical efficiency does not coincide with the isocontours of mechanical power. Instead, maximum efficiency is found at the onset of SVIV for the pure cruciform, at the onset of KVIV for the steep-angled cruciforms, and at the onset of high-amplitude KVIV for the shallow-angled cruciforms.

CHAPTER 5

CONCLUSION

This thesis studies an energy harvesting technology based on a cruciform oscillator. Three objectives were outlined at the beginning of the study. The three objectives are as follows.

1. To identify the causes of the difference in amplitude and frequency response of the lift and vibration signals when the dominant vortical structure changes from Karman to streamwise vortex, in a pure cruciform.
2. To distinguish the dominant components of the lift signal and how the components interact to modify the amplitude and frequency response of cylinder vibration, in a pure cruciform.
3. To synthesise a map for each of the amplitude, power, and efficiency, summarised in the cruciform angle α ($^{\circ}$) - reduced velocity U^* parameter space.

The main findings of this thesis are summarised below.

1. The high-amplitude vibration of the pure cruciform is governed by the shedding of large-scale streamwise vortices, whose effects become visible when $U^* > 18.2$. Karman vortex shedding govern the flow when $2.3 \leq U^* \leq 15.9$.
2. The pure cruciform in SVIV has two dominant lift components: lift due to the shedding of streamwise vortices and lift due to the shedding of Karman vortices. The application of EEMD has been a key factor in the detection of these two dominant components of lift. This is thus one of the novelties of the current study.
3. The vibration amplitude of the pure cruciform in SVIV can be improved between two to three times if Karman vortex shedding is suppressed. This is also a result

that follows directly from the application of EEMD and is another novelty of this study.

4. Asymmetries in the vortical structure distribution in the steep-angled cruciform prevents the streamwise vortex from driving the vibration of the cylinder at high U^* . The KVIV still dominates at low U^* . Varying the cruciform angle and measuring the system response has never been proposed before and is another novelty of this study.
5. Vortical structures become more symmetrical in shallow-angled cruciforms. The vibrations are governed by the shedding of Karman vortices and they produce high-amplitude vibrations.
6. Vibration regimes have been identified for all cruciforms through the computation of θ_{y-C_L} ($^\circ$). This is a novel result that is the consequence of the application of HHT in the computation of instantaneous phase ϕ ($^\circ$).
7. A map of y_{RMS}^* , $P_{\text{Mech.,RMS}}$ and $\eta_{\text{Mech.}}$ has been synthesised from the numerical results. The map allows for the identification of vibration regimes, and optimisation of $P_{\text{Mech.,RMS}}$ and $\eta_{\text{Mech.}}$.

Following the findings listed above, this study has demonstrated the identification of the dominant vibration-driving vortical structure in a pure cruciform oscillator and gave an explanation to the observed system response. This corresponds to the achievement of thesis objective one. Furthermore, this study has demonstrated the identification of the main lift component acting on the cylinder and explained why the system responses behave the way they do for both steep-angled and shallow-angled cruciforms. This corresponds to the achievement of thesis objective two. Finally, this study has demonstrated the synthesis of the system responses from all cruciform studied and mapped how the mechanical power and efficiency of a generalised cruciform with varying angle evolves against reduced velocity. This demonstrates the achievement of thesis objective three.

5.1 Recommendation of Future Works

The current study focusses on a generalised form of cruciform with a fixed gap of $G = 0.16$ between the upstream cylinder and downstream strip plate. The Reynolds

numbers studied fall at the boundary between TrSL1 and TrSL2. The mechanical system of the oscillator consists of a linear spring with a linear damper. Here are a few recommendation to further this study in the future.

- It may possibly be beneficial for the generalised cruciform oscillator to include, for example, nonlinear springs to improve energy harvesting in the sub-mW power output regime, or even simply increase the amount of damping. This is because the damping coefficient is proportional to harnessed energy and therefore, useful to know beforehand, how the system responds under increased damping.
- In addition, the Reynolds number range studied lies square in the TrSI2 regime. This Reynolds number range of $1.1 \times 10^3 \leq \text{Re} \leq 14.6 \times 10^6$ lies in the transition regime of Reynolds number that does not bring about maximum lift from the shedding of Karman vortices from a circular cylinder. In the future, studies should be made in the TrSL3 regime of Reynolds number to exploit this feature. In fact, apart from the higher computational power required to compute numerical solutions in the region $8 \times 10^3 \leq \text{Re} \leq 1.5 \times 10^5$ (TrSL3), research in this regime can be easily done by enlarging the diameter of the cylinder and collecting data under similar conditions as presented in this thesis.
- Finally, the implementation of a more efficient procedure in the numerical loop to simplify the computation of cylinder displacement. In this work, ACMI is implemented to allow transport of scalar and vector quantities across non-adjointing patches. However, during motion of the cylinder, the whole computational domain upstream the strip plate moves along with the cylinder, causing a large number of nodes to be translated at each time step. It can be more efficient for the computation to pre-emptively limit the region of motion to include only the circular cylinder and nothing else.

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Appendix A Temporal Evolution of Lift in a Pure Cruciform System for Energy

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Temporal evolution of lift in a pure cruciform system for energy harvesting

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ABSTRACT

We investigated the displacement and lift time series of a circular cylinder - strip plate cruciform system for energy harvesting in the Reynolds number range $1.1 \times 10^3 \leq Re \leq 14.6 \times 10^3$, numerically using the open source C++ library: OpenFOAM. The Karman vortex-induced vibration (KVIV) regime was identified between reduced velocity, U^* , 2.3 and 13.6, while the streamwise vortex-induced vibration (SVIV) regime was identified between $18.2 \leq U^* \leq 29.5$. We analysed the cylinder displacement and lift time series using the Hilbert-Huang transform (HHT). Within this range of U^* , Karman vortex shedding contributes nearly as much as streamwise vortex shedding to the root-mean-square amplitude of total lift, while between $25.0 \leq U^* \leq 29.5$, the Karman component contribution is on average twice that of the streamwise component. These findings hint at the possibility to improve the power output of the harvester by a factor of two between $18.2 \leq U^* \leq 22.7$ and by a factor of three between $25.0 \leq U^* \leq 29.5$, if we can unite the contribution to the root-mean-square amplitude of the total lift under a single vibration-driving mechanism: the shedding of streamwise vortex.

1. Introduction

Streamwise vortex-induced vibration (SVIV) is a type of vortex-induced vibration (VIV) driven by vortical structures whose vorticity vector points in the direction of the free stream. In recent decades, there have been efforts to exploit the SVIV phenomenon from cruciform structures for energy harvesting, an example of which is given in Fig. 1. The literature on this subject can be broadly categorised into two groups: how the mechanical properties of the oscillator (e.g., mass ratio, damping, etc.) affects the amplitude/frequency response of SVIV (Koide et al., 2009, 2013; Nguyen et al., 2012) and how the minutiae of the flow field affect the force driving the vibration of the cylinder, i.e. the fluid mechanical aspect of the system (Deng et al., 2007; Koide et al., 2017; Zhao and Lu, 2018).

In the first focus area, researchers studied some permutation of the following method to convert the vibration into electrical power. The method consists of a coil and magnet. The coil, which moves with the vibrating cylinder, creates relative motion against the magnet, which is placed in the hollow of the coil (Koide et al., 2009). While investigating the system at a Reynolds number in the order of $Re \sim O(10^4)$, Koide et al. (2009) showed that increased damping due to energy harvesting reduces the maximum vibration amplitude close to a factor of 4. Amplitude reduction due to increased total damping was also mentioned in

Bernitsas et al. (2008); Bernitsas and Raghavan (2008); Bernitsas et al. (2009). Further investigation in Nguyen et al. (2012) revealed that damping not only affects the amplitude response of the cylinder but also narrows the synchronisation region between vortex shedding and cylinder vibration. Moreover, Nguyen et al. (2012) demonstrated a strong coupling between mass ratio and damping in determining both the width of the synchronisation region and the maximum amplitude response of the cylinder.

In the second focus area, investigators turned their attention to the details of the flow where streamwise vortex shedding occurs. One such study carefully shot motion pictures of the dye-injected flow (Koide et al., 2017) at Reynolds number in the order of $Re \sim O(10^3)$. A lower Reynolds number (Re) reduces the amount of turbulence in the flow, allowing a clearer shot of the vortex structures. Their study also highlights the higher level of turbulence produced by the circular cylinder-strip plate cruciform in contrast to the twin circular cylinder cruciform, which diminishes the periodicity of vortex shedding. Although visually enlightening, this and other more qualitative studies contribute little towards improving our understanding of the relationship between vortex shedding and the resulting lift. Deng et al. (2007) demonstrated a way to overcome such a shortcoming.

In their study, Deng et al. (2007) examined the flow field of a twin circular cylinder cruciform using computational fluid dynamics (CFD).

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Appendix B OpenFOAM Implementation for The Study of Streamwise Vortex-Induced Vibration-Based Energy Harvester for Sensor Networks

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OpenFOAM Implementation for The Study of Streamwise Vortex-Induced Vibration-Based Energy Harvester for Sensor Networks

Open Access

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ABSTRACT

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The study of streamwise vortex induced vibration has reached a level of maturity that allows it to be harnessed to generate power. However, studies have primarily concentrated on the variables that measured through point-based instruments. This severely limits our understanding of the fluid forcing mechanism that results in the vibration of the elastically supported bluff body. We proposed the usage of computational fluid dynamics: the open source C++ libraries of OpenFOAM. To implement this successfully to the streamwise vortex-induced vibration problem, which involves near-wall fluid-structure interaction, we explored the method of dynamic mesh handling in OpenFOAM for six degrees of freedom motion of a rigid body fully submerged in fluid. Finally, we argued for the usage of arbitrarily coupled mesh interface to overcome the problem of severely distorted mesh in tight gaps between two walls. We run a short simulation to test this setup and found that the case runs uninterrupted, unlike its former counterpart that relies solely on cell displacement diffusion, suggesting the potential success of a further converged solution of the setup when running on a more powerful machine.

Keywords:

OpenFOAM, vortex shedding, vortex induced-vibration, streamwise vortices

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1. Introduction

1.1 Off-Grid Operation of Sensor Networks

The growing demand for real-time monitoring and management of agriculture [29], civil structures [44], machinery [9], and hydrological systems [5] led towards widespread adoption of sensors networks in these disciplines. Under the desired operating conditions, most of the application of the sensors are at sites where power from the national grid is either difficult to source, or non-existent. Sometimes, the issue is not so much on the fact that power lines from the national grid are out of reach, as it is related to the involvedness of the means to distribute the power, e.g.,

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LIST OF PUBLICATIONS

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