



# Dual-pol microstrip patch antenna



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## Abstract:

A dual Polarized Patch antenna edge-feeding with stable radiation pattern centered @ 17GHz with total Bandwidth of 10%, XPD of -26dB can be enhanced to -30dB, With isolation between the two ports of -26dB.

## Introduction:

The capacity and variety of wireless communication channels can be significantly increased by installing dual-polarized antennas at the transmitter and/or receiver, as recent findings in communication theory [1] have shown. Using dual-polarized transmit and receive antennas can increase capacity threefold over a comparable system with single antennas at the transmitter and receiver. For instance, in the richly scattering environments considered in [1], a dual-polarized transmitter antenna can increase capacity by more than 50% over a single transmit antenna.

Also, in radar systems Dual polarization can achieve improvements such:

Enhanced Target Discrimination: Dual polarization facilitates the differentiation of various target kinds. Radar systems can improve the capacity to distinguish between different objects by providing further details on the size, shape, and composition of the targets through the transmission and reception of signals in both horizontal and vertical polarizations.

## Problem definition:

For achieving a dual polarized patch antenna, it's required to have two orthogonal ports to feed the patch but to achieve this it is also required to have a square patch to have the same characteristics and specifications in both ports otherwise the width and length of the patch in aspect of each port would be reversed so the radiation characteristics will differ, another challenging design parameter is to achieve the highest XPD without affecting other parameters such as scattering parameters, input impedance and also the gain of the antenna, the feeding lines are also challenging that a 50ohm microstrip lines' width is about 3mm whereas the width of the patch is about 3.5 mm so this was not physically or in terms of matching applicable to have achieve matching between ports and the antenna and having input impedance of 50ohm in a relatively wideband with minimum imaginary part to be in resonance mode which is preferable for the antenna to be radiative in as it has pure real impedance, It is also required to achieve high isolation between the two ports to increase the XPD.

# Design Procedure

## Design Procedure

We started with initial design of a single polarized patch antenna radiating at 17GHz, we calculated the dimensions of the patch using patch antenna calculator on internet that estimated  $W = 5.37 \text{ mm}$ ,  $L=3.37\text{mm}$

But the patch is required to be square as illustrated in the problem definition section that each port will see the reversed dimensions of the other ..so we changed the Width of the patch to be equal to the length and we didn't change the length cause we found that the length of the patch corresponds to the frequency of radiation while the width of the patch corresponds to the matching (determines the S parameters values at certain frequency) so in the design  $W = 3.155\text{mm}$  ,  $L=3.155 \text{ mm}$ .

We obtained these values through a parametric sweep that achieves best results , the matching is done by  $\lambda/4$  section of  $W=0.65\text{mm}$  the input impedance seen from the ports is almost 50ohm as intended , the isolation between the ports is achieved by widening the feeding lines , but this affects the value of XPD which found that it depends on the width of the feeding lines and contribute in the radiation so we choose to decrease the radiation of the transmission lines by decreasing its width to eliminate the fringing field out of transmission lines , but changing the width of the transmission line will change its impedance and the matching will be affected so we solve this problem by changing the thickness of the substrate instead of  $\lambda/4$  we found in many papers that we could make the substrate thickness to be  $\lambda/10$  so the new substrate thickness  $t=0.84\text{mm}$  , so we managed to decrease the width of the transmission line to be  $W=0.3\text{mm}$  and decreasing the substrate thickness also reduced the radiation of the feeding lines bur also affected other parameters of the antenna such the gain , bandwidth and the efficiency .

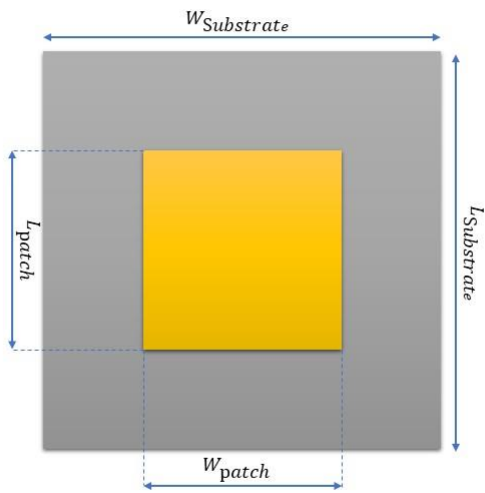


Figure 2 Antenna

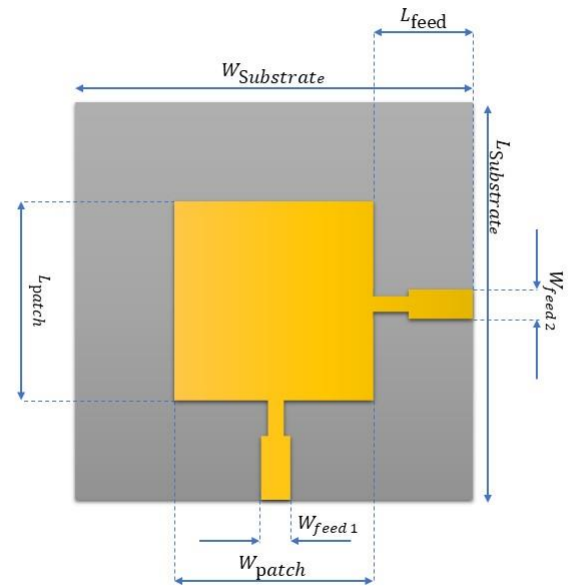


Figure 1 TOP view

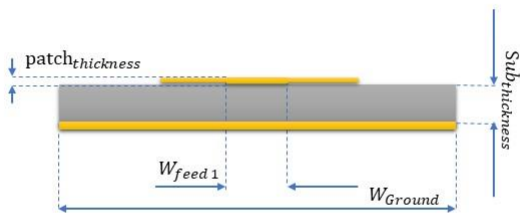


Figure 3 Front View

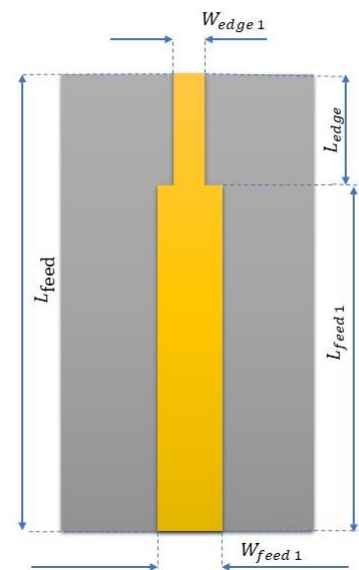


Figure 4 Feeding

Antenna Dimensions	
$W_{\text{Substrate}}$	8
$L_{\text{Substrate}}$	8
$W_{\text{patch}}$	3.155
$L_{\text{patch}}$	3.155
$W_{\text{feed } 1}$	0.65
$L_{\text{feed}}$	2.4225
$W_{\text{edge } 1}$	0.3
$L_{\text{edge}}$	0.335
$L_{\text{feed } 1}$	2.0875
patch <sub>thickness</sub>	0.035
Sub <sub>thickness</sub>	1.6
$W_{\text{Ground}}$	8

All dimensions in this table are in millimetres (mm).



# Results & Discussion

## Results

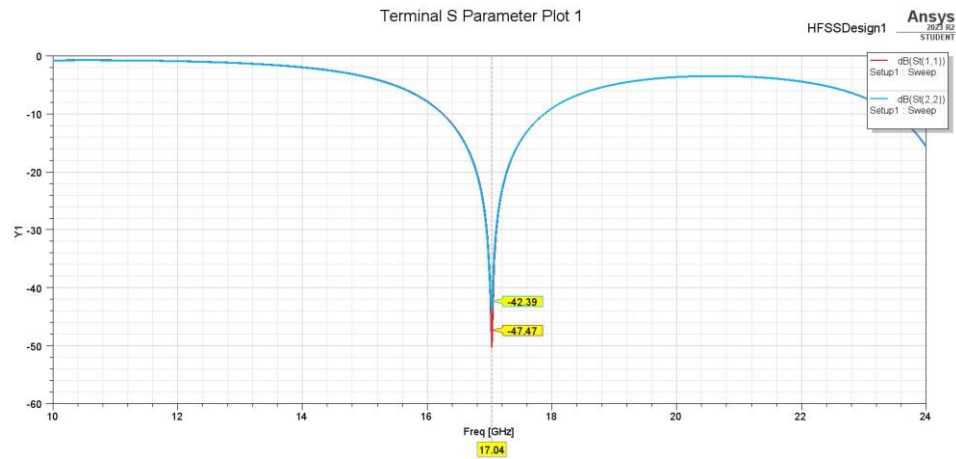


Figure 5 RETURN LOSS

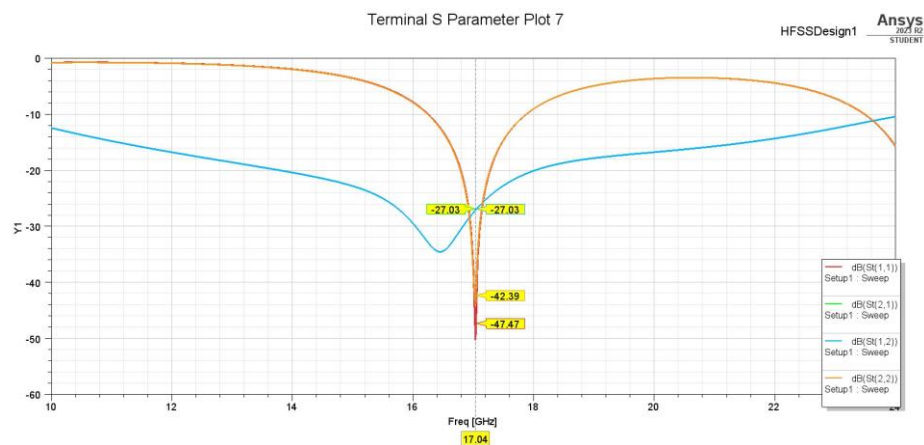


Figure 6 S PARAMETERS

Name	Freq [GHz]	Ang	Mag	RX
m1	17	-1.4711	49.7348	-1.0410 - 0.0011j

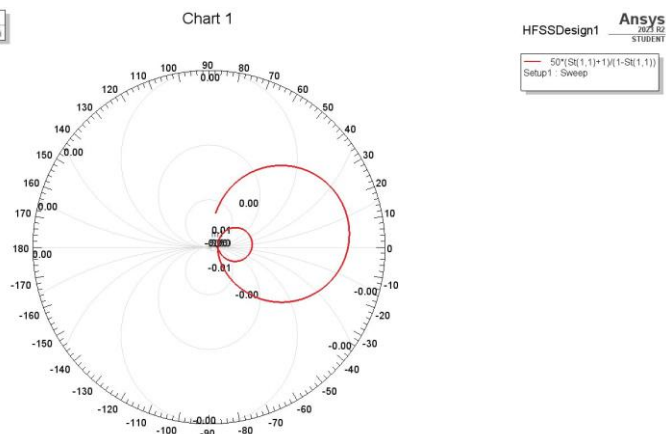
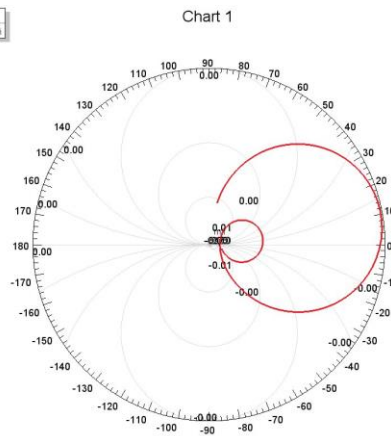


Figure 7 Input Impedance 1

# Results & Discussion

## Results

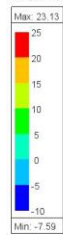
Name	Freq [GHz]	Ang	Mag	RX
m1	17	-1.2019	49.5289	-1.0412 - 0.0009i



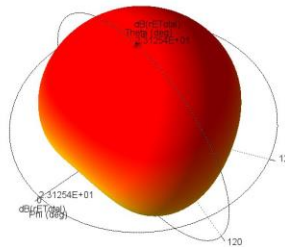
HFSSDesign1 Ansys  
2023 R2  
STUDENT  
50\*(S(2,2)+1)\*(1-S(2,2))  
Setup1: Sweep

Figure 8 Input Impedance 2

Ansys Inc.



rE Plot 5



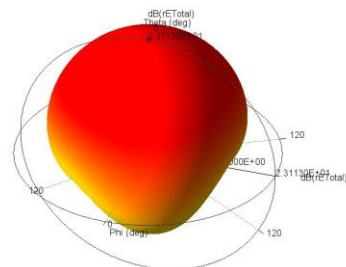
Ansys  
2023 R2  
STUDENT

Figure 9 Radiation pattern of port 1

Ansys Inc.



rE Plot 2



Ansys  
2023 R2  
STUDENT

Figure 10 Radiation pattern of port 2

## Results

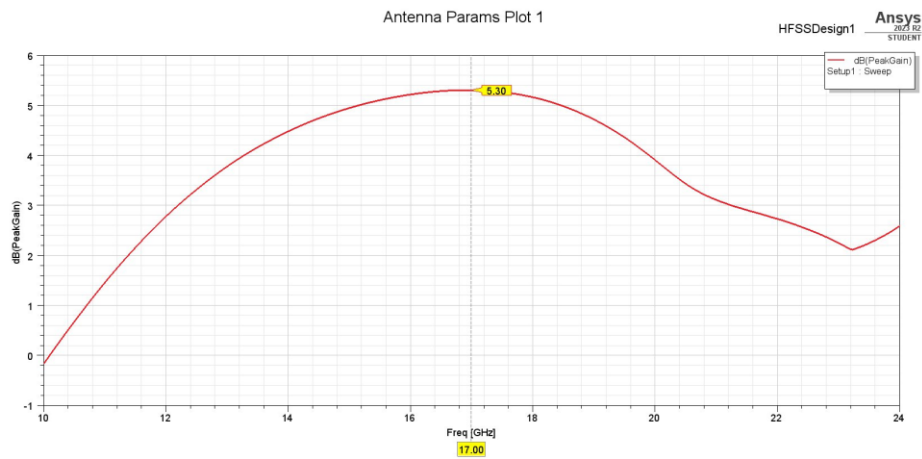


Figure 11 GAIN (dB) VS Frequency

Gain = 5.3

This gain is acceptable.

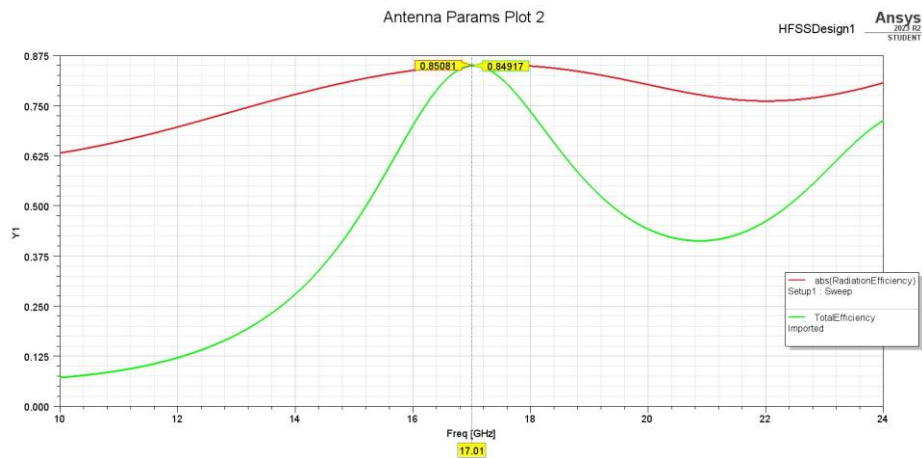


Figure 12 Radiation efficiency vs frequency

Radiation efficiency = 85%

## Results

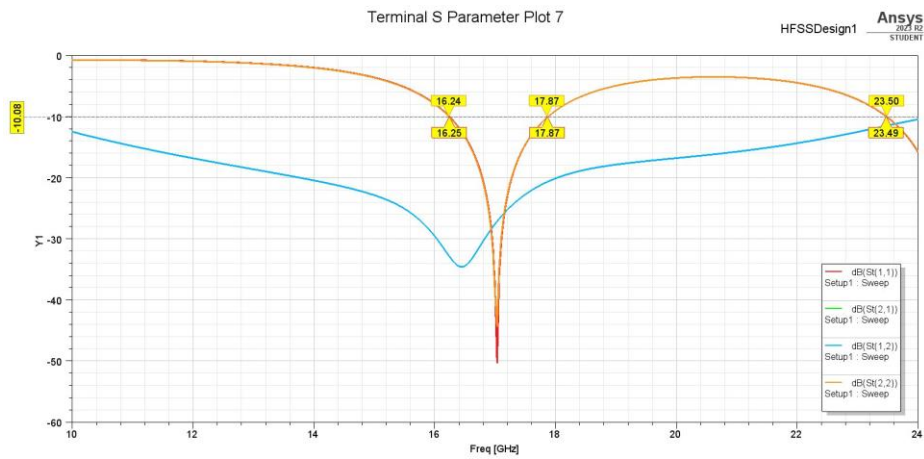


Figure 13 Bandwidth

$$\text{Bandwidth} = \frac{(17.87 - 16.24)}{17} = 10\%$$

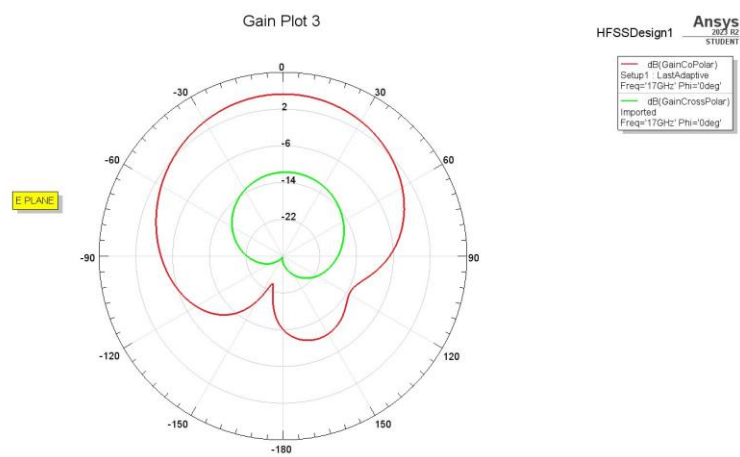


Figure 14 Co & Cross on E plane of port 1

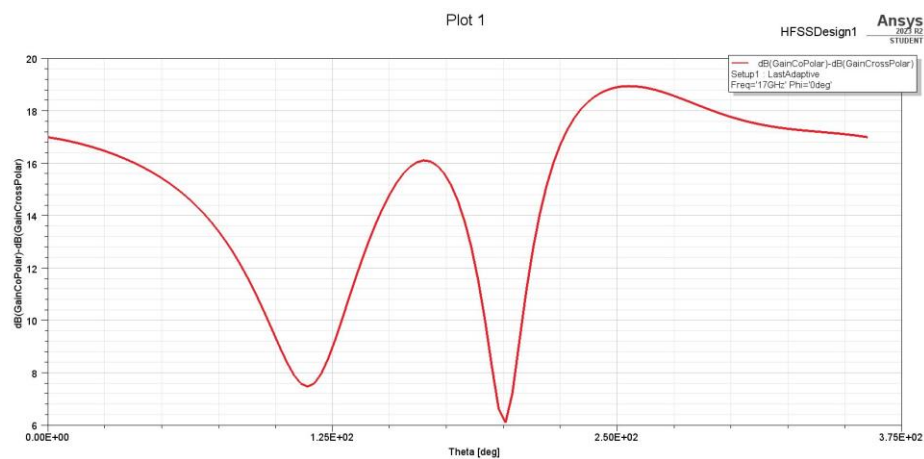


Figure 15 XPD on E plane (port 1)

## Results

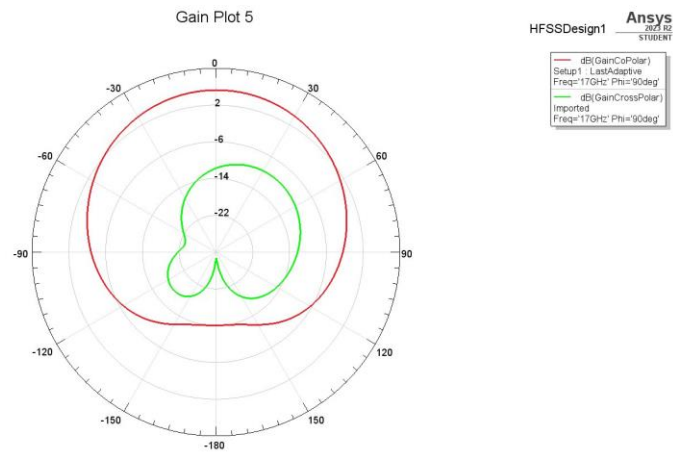


Figure 16 Co & Cross on H plane of port 1

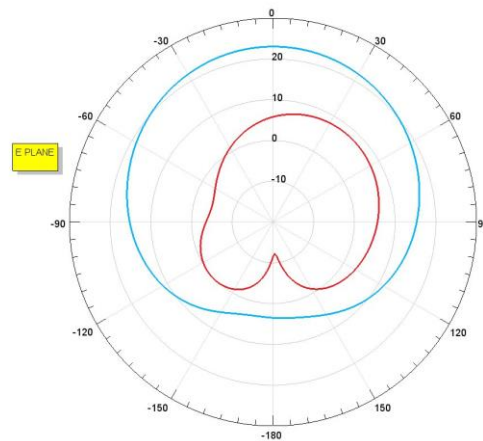


Figure 17 Co & Cross on E plane of port 2

## Results

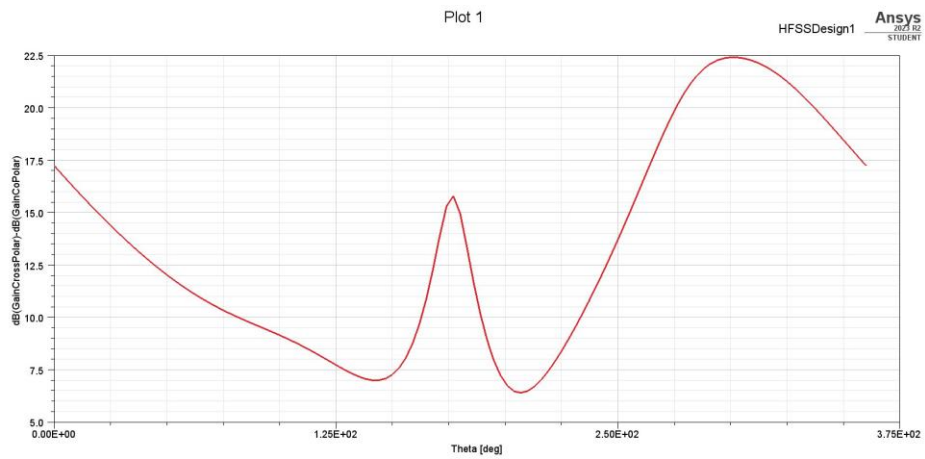


Figure 18 XPd on E plane (port 2)

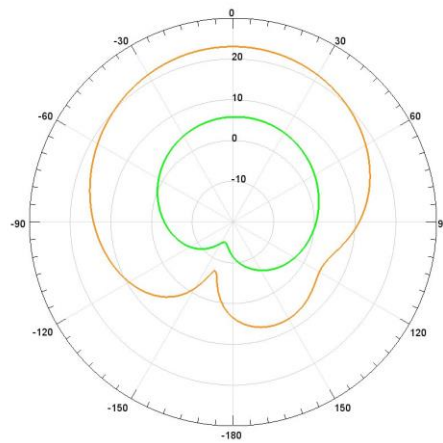


Figure 19 Co & Cross on H plane of port 2

# Results & Discussion

## Discussion

Figure 6: It Shows the scattering parameters  $S_{11} = -47\text{dB}$  that corresponds to the reflection coefficient of port 1 and the same for  $S_{22} = -42\text{dB}$  but for port 2 at  $f = 17\text{GHz}$ , which are very acceptable values, and  $S_{12} = -27\text{dB}$  that corresponds to the interaction between ports, assigns how much power from port 1 transmitted to port 2 and  $S_{21}$  for reverse how much power transmitted from port 2 to port 1.

Figure 7&8: Show the input impedance on smith chart, which is  $49.7\ \Omega$  at  $17\text{GHz}$  for port 1, and  $49.5\ \Omega$  for port 2 and these are very good values and close to  $50\ \Omega$ .

Figure 9&10: Show the 3-D radiation pattern which is stable along frequency with maximum gain in the bore side ( $\theta = 0$ ) of  $5.3\ \text{dB}$ , the gain bandwidth is wide  $G > 4\text{dB}$  [ $13\text{GHz}:20\text{GHz}$ ]

Figure 12: shows the radiation efficiency along the frequency at  $17\ \text{GHz}$  the radiation efficiency =  $85\%$  which is a good percentage.

Figure 13: shows the Bandwidth of the  $S_{11}$  &  $S_{22}$  almost  $10\%$  which is relatively acceptable at this high frequency a bandwidth of  $1.63\text{GHz}$  and it is the total Bandwidth as it is the smallest bandwidth of all other parameters

$$\text{Bandwidth} = \frac{(17.87 - 16.24)}{17} = 10\%$$

Figure 14:20 : Show the Co-polarization & Cross-polarization gain along  $\theta$ , the electric field(10&11) and the magnetic field(12&13) that shows XPD (Cross Polarization Discrimination) which indicates the intended polarization to the orthogonal one which is  $17\text{dB}$  for electric field and  $17.5\text{dB}$  for magnetic field in Port 1, and XPD of  $17.5\text{dB}$  for both electric field and magnetic field for port 2 all calculated at bore side ( $\theta = 0^\circ$ ).

Results Adjusted XPD

Name	Theta [degmin]	Ang	Mag
m1	21600	-5.1159E-13	-15.7612
m2	21600	-5.1159E-13	5.3348

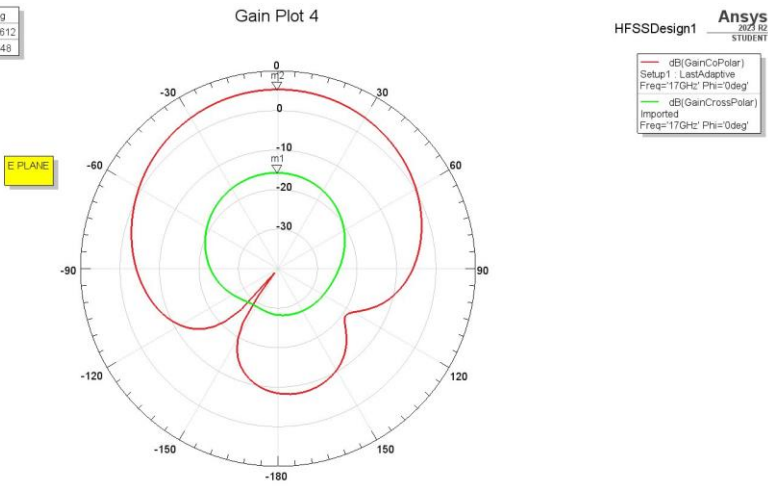


Figure 20 XPD of port 1 = 21dB

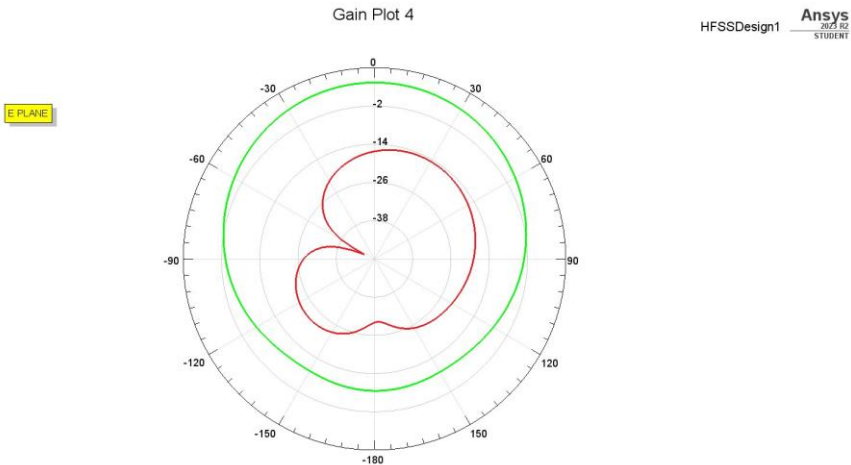


Figure 21 XPD of Port 2 = 22.5dB

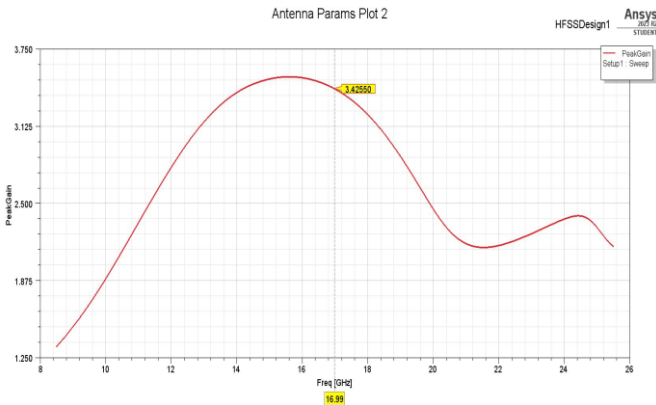


Figure 23 Gain of the second Design = 3.4dB

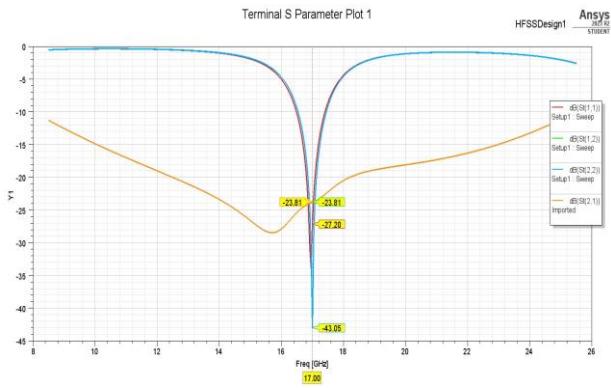


Figure 22 : S Parameters of design 2



# Results & Discussion

## Results Adjusted XPD

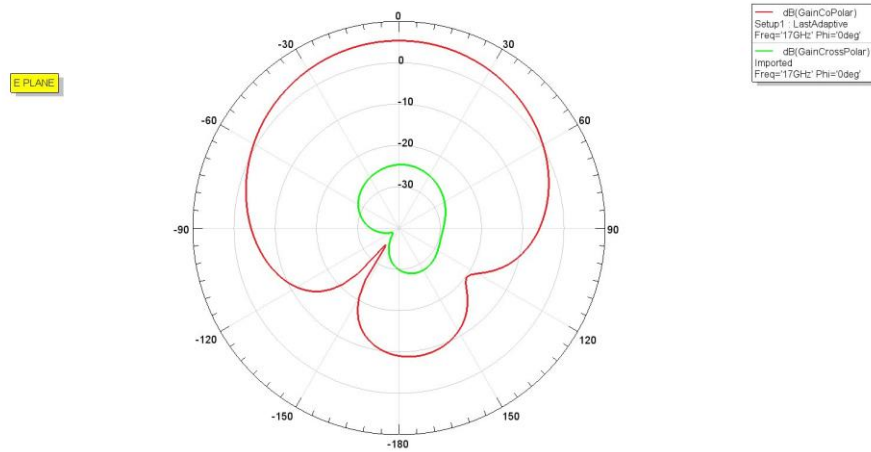


Figure 24 Co/Cross when exciting the two ports Simultaneously.

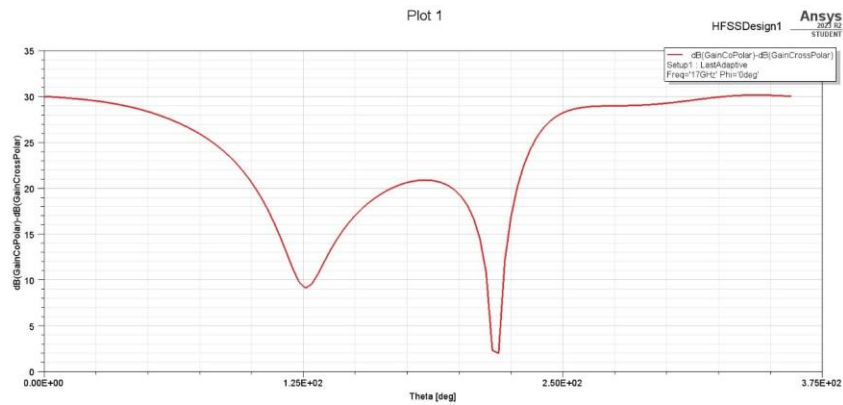


Figure 25 XPD = 30 in broad side when exciting the two ports simultaneously

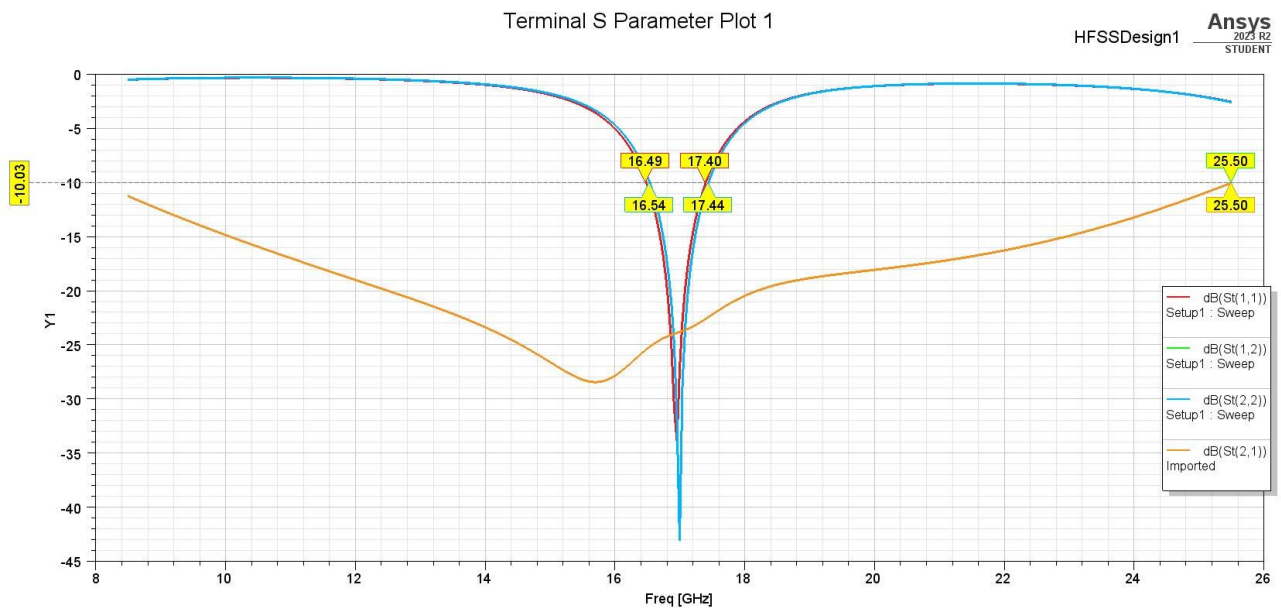


Figure 26 BW

# Results & Discussion

## Discussion Adjusted XPD

### Adjusted XPD Design results

This Design results provide higher XPD as in fig(21:27) but less gain(fig 11), less Bandwidth, more deformed radiation pattern, less efficiency, less isolation and less S11, S22 due to reducing the thickness of the substrate and the Width of feeding lines when each port is excited separately.

When the two ports are excited simultaneously the characteristics improve and XPD get even higher to reach 30dB fig(25&26) and the other parameter also improved like(fig 27).

### Adjusted XPD Design Layout

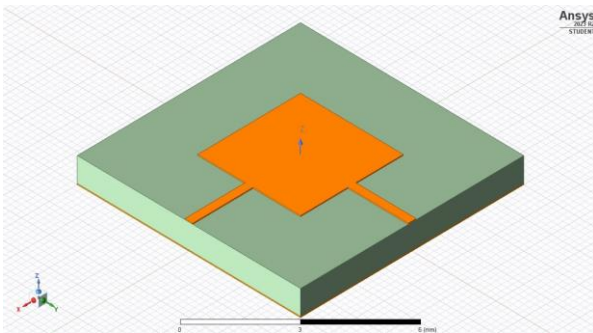


Figure 27 Adjusted XPD Design

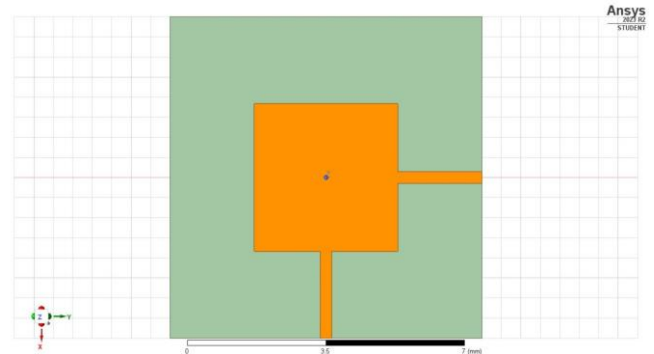


Figure 28 Top View

# Circuit model

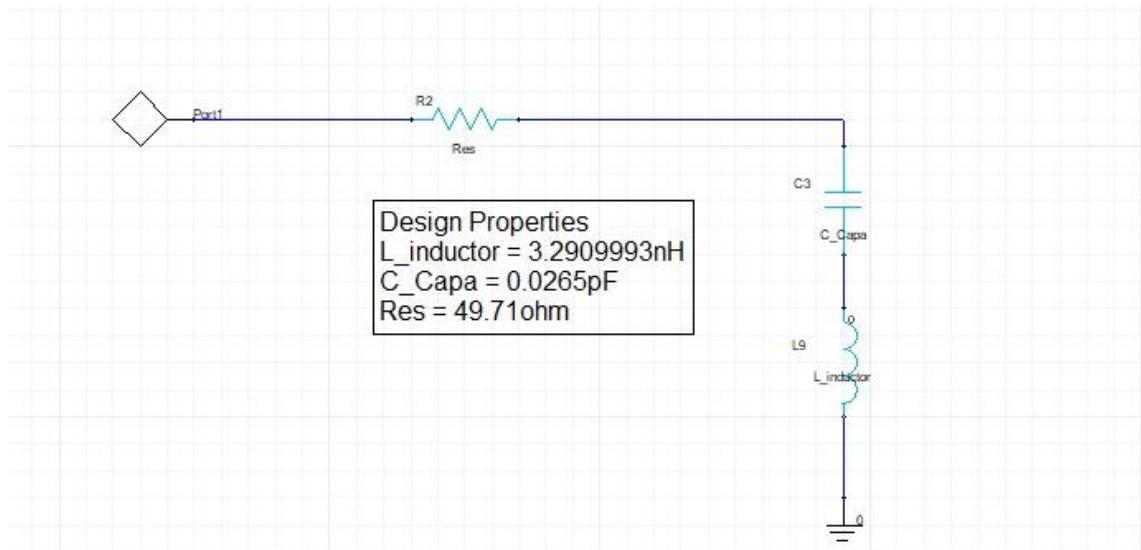


Figure 29 Circuit Model

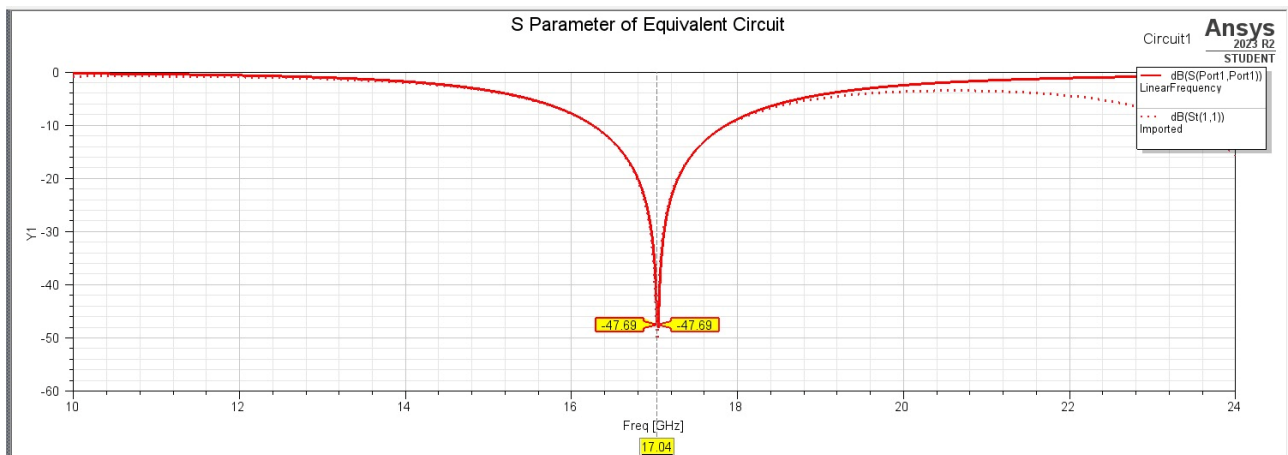


Figure 30 S11 of Circuit Model (line) & antenna design (dotted)

Figure 30 shows that S11 of the Circuit Model follows S11 of the antenna design.

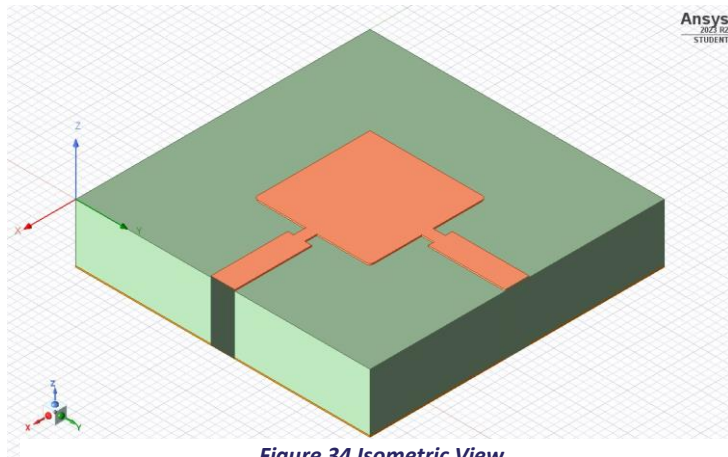


Figure 34 Isometric View

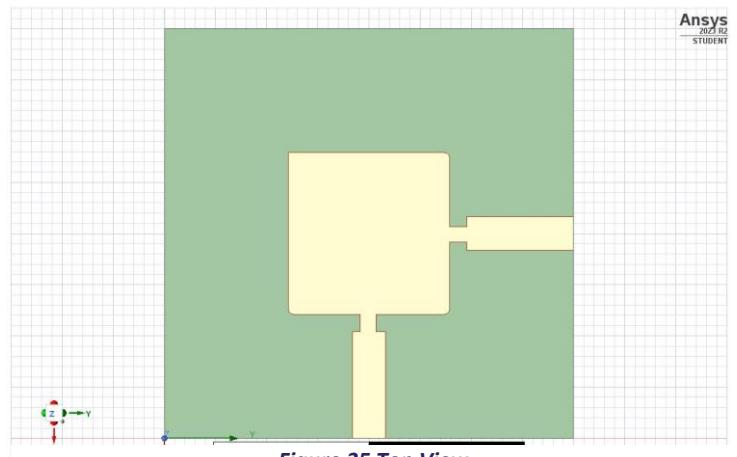


Figure 35 Top View

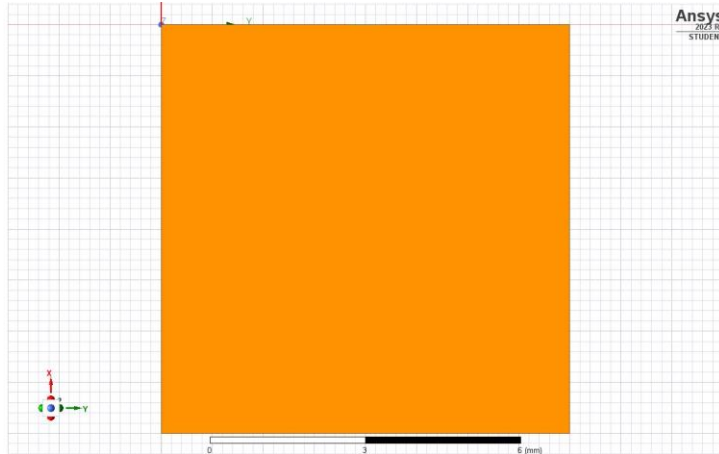


Figure 32 Bottom View

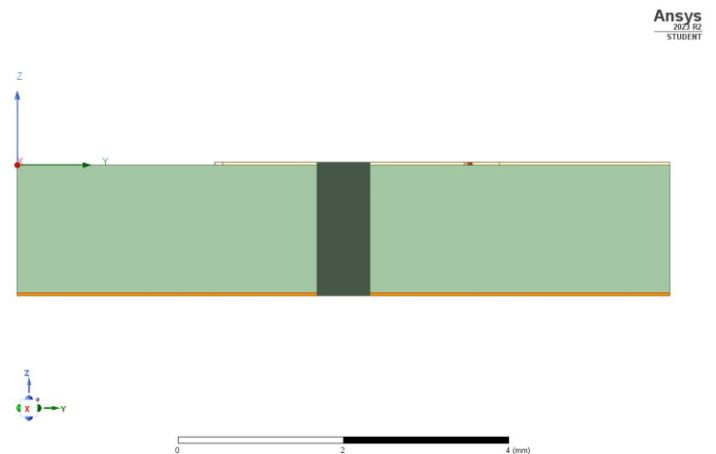


Figure 33 Front View

# Verification of tool

simple Dipole antenna achieves parameters near to that in the same design in the paper and verified by this paper [\[3\]](#)

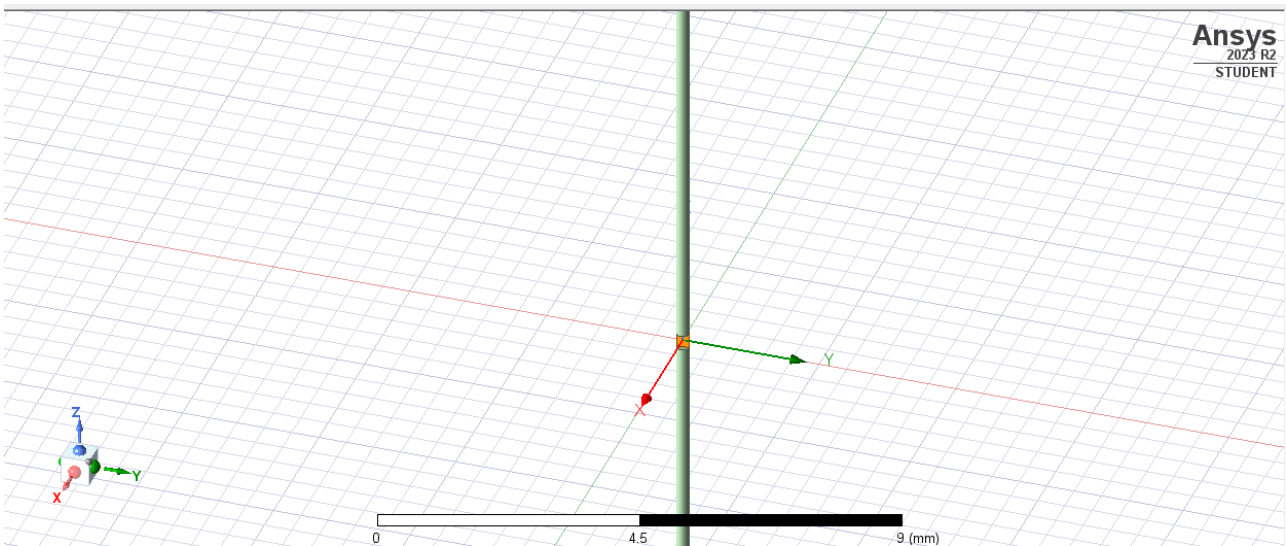


Figure 36 Schematic of the dipole for verification

**L = 55 mm**

**R=0.115 mm**

**gap=0.275 mm**

## Dipole results:

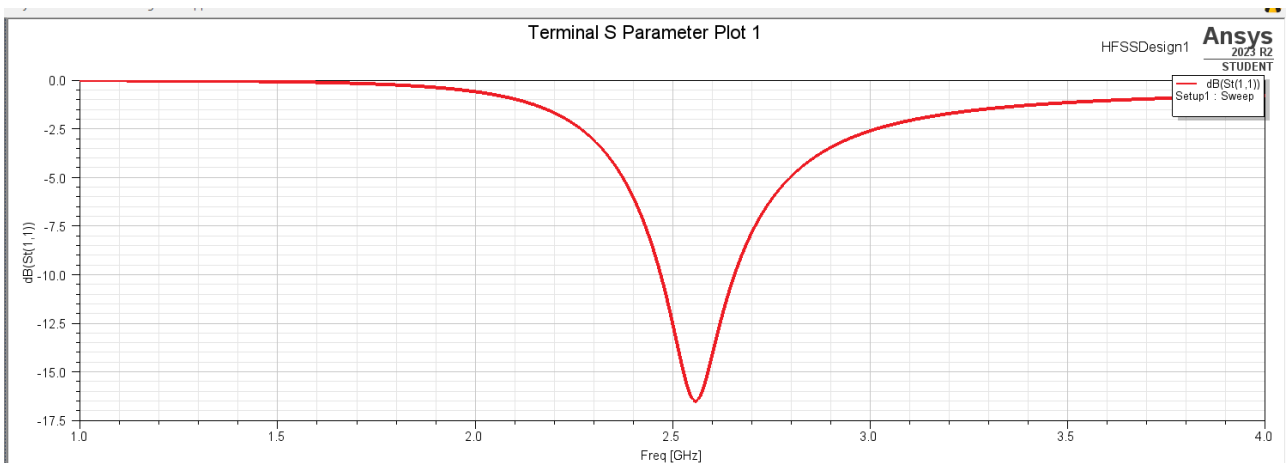


Figure 37 s11 for the dipole.

# Verification of tool

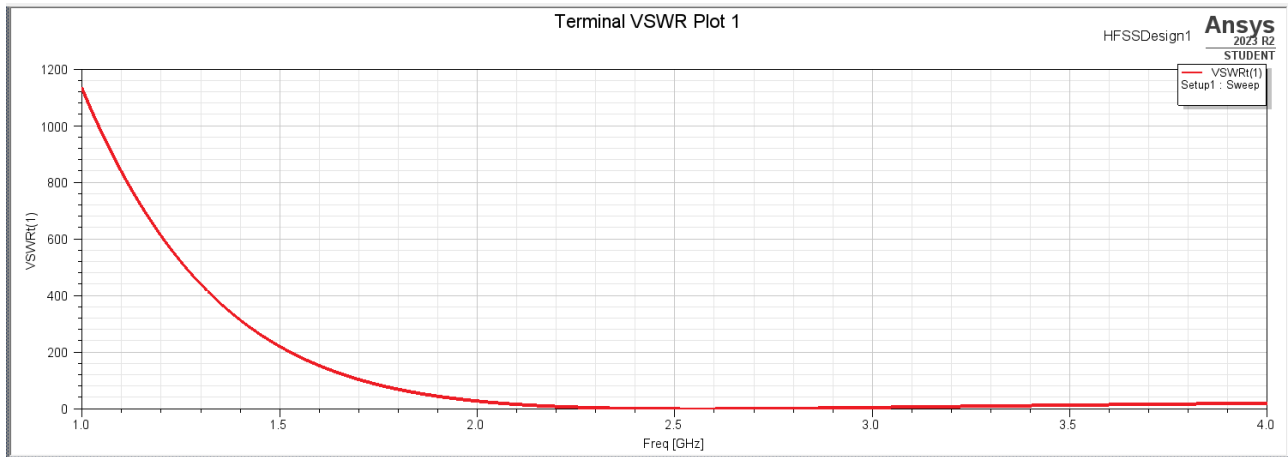


Figure 38 VSWR of the dipole.

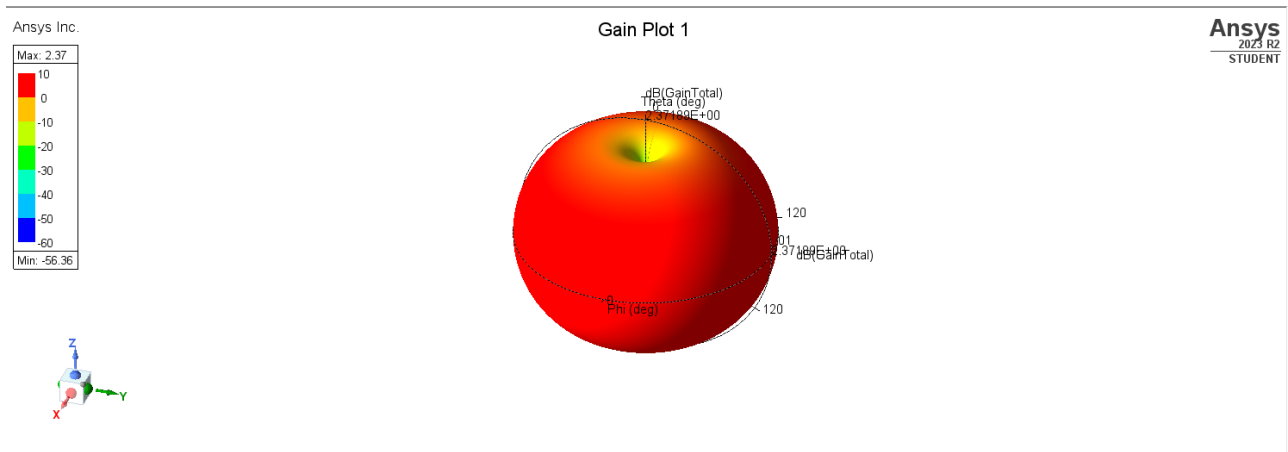


Figure 39 Gain of dipole on 3\_D

as shown of the previous figures the results are very near to that in intended paper.

## Conclusion

In this report, The Dual Polarized microstrip patch antenna has been designed and analysed at operating frequency 17GHz using HFSS Tool. The specifications required for the cross polarization (XPD) and isolation between the 2 ports have been achieved as shown in the above graphs in details.

## References:

- [1] [G. J. Foschini and M. J. Gans, "On limits of wireless communications in a fading environment when using multiple antennas," Wireless Personal Communications, vol. 6, no. 3, pp. 311–335, March 1998.](#)
- [2] [Singh, S. P., Singh, A., Upadhyay, D., Pal, S., & Munde, M. \(2021, May\). Design and Fabrication of Microstrip Patch Antenna at 2.4 GHz for WLAN Application using HFSS. IOSR Journal of Electronics and Communication Engineering, Special Issue - AETM'16, 1, e-ISSN: 2278-2834, p-ISSN: 2278-8735.](#)
- [3] [Onu, I. P., & Orakwue, S. I. \(2020\). Design Analysis for A Half-Wave Dipole Antenna For 2.4ghz Wireless Application using CST Microwave Studio. ResearchGate.](#)