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# Wave-DNA

(Wave Doppler effects in Nonlinear Acoustics)

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# Chapter 1

## About Wave-DNA

**Wave-DNA** is a simulation tool for one-dimensional and spherically-symmetric nonlinear acoustic waves in transient and spatially variable background flow fields. The motion of the background medium is accounted for by considering a convective form of the lossless Kuznetsov wave equation [10], derived from first principles based on perturbations of the continuity equation and the transient Bernoulli equation. The background flow field in which the acoustic waves propagate is treated as an input to the wave solver, and in principle, may be obtained from analytical considerations, numerical simulations, or experimental measurements. **Wave-DNA** offers a tailored numerical framework to study nonlinear Doppler phenomena in acoustic wave propagation.

The moving boundary may represent a moving wave emitter or scatterer, and it may move relative to the fluid or displace the surrounding fluid. This allows the user to study nonlinear Doppler effects associated with moving wave emitters/scatterers and/or non-uniform background flow fields. The motion of the domain boundary is conveniently taken into account by a generic coordinate transformation of the governing wave equation, where the transformed wave equation is solved in a fixed computational domain. This technique enables accurate numerical solutions of the combined wave-flow problem without the necessity to interpolate data between the moving grid points in the physical domain. The numerical technique is based on an explicit finite-difference time-domain (FDTD) method and equipped with a predictor-corrector method to counteract the onset and growth of dispersive numerical noise due to broad frequency bands or shock waves [9]. Furthermore, absorbing boundary conditions can be imposed in order to let the acoustic waves pass the domain boundaries without reflection.

A particularly well-suited example to demonstrate the capability of the simulation framework is the acoustic black/white hole analogue as presented in [8, 10]. The present documentation provides detailed instructions on how to conduct acoustic black and white hole simulations using **Wave-DNA**, as well as other examples to demonstrate its capabilities and functionalities.

The **Wave-DNA** repository is located at <https://github.com/polycfd/Wave-DNA>, is under the copyright of its developers and made available as open-source software under the terms of the [MIT License](#). Details about the theory and numerical methods of **Wave-DNA**, as well as examples of its scientific applications, can be found in these papers: [2, 8, 9, 10].

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# Chapter 2

## Using Wave-DNA

### 2.1 Installation

It is convenient to compile the source code in a build directory separate from the source directory by executing the `cleanbuild_release.sh` script to compile in optimized release mode, or by executing the `cleanbuild_debug.sh` script to compile in debug mode. The program runs significantly faster in release mode.

By running the build scripts (`cleanbuild_release.sh` or `cleanbuild_debug.sh`), all files in the build directory that were previously generated by `cmake` are removed. Subsequently, a `cmake` run is performed on the `CMakeLists.txt` file. In the `CMakeLists.txt` file, the `gcc` compiler must be set as `CMAKE_C_COMPILER`, providing the path to the `gcc` executable. For instance:

```
set(CMAKE_C_COMPILER /usr/bin/gcc)
```

Furthermore, the environmental variable `$mylibdirs` must be set in `CMakeLists.txt`. For instance:

```
set(mylibdirs $mylibdirs /usr/lib64/)
```

Finally, the Wave-DNA source directory must be specified. This is done by either directly setting the path to the source directory as

```
FILE (GLOB_RECURSE MYFILES ABSOLUTE /path/to/wavedna/src/*.c)
```

or by setting:

```
FILE (GLOB_RECURSE MYFILES ABSOLUTE $ENV{WaveDNA_DIR}/src/*.c)
```

The latter option requires to set the environmental variable `$WaveDNA_DIR` to `/path/to/wavedna` in the configuration file of the Unix shell, as for instance `/path/to/home/.bashrc`. With the default settings in the provided `CMakeLists.txt` file, the executable `WaveDNA` is created in the build directory upon successful compilation. See the following lines in `CMakeLists.txt`:

```
add_executable(WaveDNA ${MYFILES})
target_link_libraries(WaveDNA ${mylibs})
```

## 2.2 Running a simulation

The simulation case directory needs to have an options file, called `run.DNA` by default, which contains the user options<sup>1</sup>, and a `results` directory is generated upon executing `Wave-DNA`, into which the output files are written. The simulation is run in the case directory by executing the following command:

```
/path/to/some/arbitrary/build/directory/WaveDNA
```

The options file may also take another name different from `run.DNA`. In that case, the simulation must be executed with the following command line option:

```
/path/to/some/arbitrary/build/directory/WaveDNA -options optionsFileName
```

## 2.3 Run options and fluid properties

The basic run options and fluid properties are set in the sections `RUNOPTIONS` and `FLUID`, respectively. Next to the background density and speed of sound,  $\rho_0$  and  $c_0$ , respectively, one can specify the nonlinearity coefficient  $\beta$  to admit cumulative nonlinearities. Independent of this option, one can further indicate, whether local nonlinearities (a non-zero Lagrangian density  $\mathcal{L}$ ) are taken into account. By this means, one can effectively solve

- the linear wave equation ( $\beta = 0$ ,  $\mathcal{L} = 0$ ),
- the lossless Westervelt equation ( $\beta \neq 0$ ,  $\mathcal{L} = 0$ ) [9],
- or the lossless Kuznetsov equation ( $\beta \neq 0$ ,  $\mathcal{L} \neq 0$ ) [10].

The following table provides a detailed overview of the run and fluid property options.

Command	Description
Section <code>RUNOPTIONS</code>	
<code>TimeStart &lt;float&gt;</code>	Physical start time of the simulation.
<code>TimeEnd &lt;float&gt;</code>	Physical end time of the simulation.
<code>WriteFrequency &lt;float&gt;</code>	Number of time steps between successive write to disc occurrences. This determines the time instances at which the field data is written to disc ( <code>fields.dat</code> ). The data recorded at sample points is stored in buffer and written to disc ( <code>probes.dat</code> ) at this occasion as well.
<code>SamplePoints &lt;int&gt; &lt;float&gt; ...</code>	Number of sample points ( <code>&lt;int&gt;</code> ) followed by the coordinates ( <code>&lt;float&gt;</code> ) of the sample points. The nearest neighbor grid points to the target locations and their IDs is identified, and the sample is taken at those grid points throughout the entire simulation. This means that the probe is moving with the grid. If the indicated number of sample points is larger than zero and does not match the number of given points, the simulation aborts with the error message "An unknown option ...".
Section <code>FLUID</code>	
<code>SoundSpeed &lt;float&gt;</code>	Background speed of sound $c_0$ of the fluid.
<code>Density &lt;float&gt;</code>	Background density $\rho_0$ of the fluid.

<sup>1</sup>If the file is empty, a default run is performed based on the default options as indicated in Section 2.7 (also see `src/io/iodefaultoptions.c`)

<code>FluidNonLinearity &lt;float&gt;</code>	Nonlinearity coefficient $\beta$ of the fluid.
<code>LocalNonlinearity &lt;string&gt;</code>	If set to <b>True</b> , the second-order acoustic terms giving rise to local nonlinear wave propagation are active. The option <b>False</b> (default) in combination with a non-zero value for $\beta$ effectively means that the Westervelt equation is solved.

---

## 2.4 Wave excitation

Several options are available to excite an acoustic pressure wave at a specific emission node. The present modeling framework is particularly designed to solve boundary value problems, where the domain boundaries act as wave-emitting boundaries. Before explaining the different types of excitation functions, there are some important things to keep in mind:

- The moving boundary is always associated with the grid node 0, regardless of whether its coordinate  $R(t)$  takes a larger or smaller value than the coordinate  $R_{\text{stat}}$  of the fixed boundary. This means that the grid node  $N_{\text{points}} - 1$  is always associated with the fixed boundary  $R_{\text{stat}}$ .
- Only one single excitation node can currently be specified.
- The user is free to specify any node between 0 and  $N_{\text{points}} - 1$ . However, as the present modeling framework is specifically designed to solve boundary value problems, the source pressure is not a volumetric source.
- The emission of the acoustic pressure as specified by the excitation function is always strictly enforced as per the applied boundary condition, regardless of whether the wave-emitting boundary is in relative motion to the background medium or not. Consequently, the effect of convective amplification/attenuation, which relies on the Doppler-factor of the relative motion between emitter and background medium [7], must be taken into account in the specification of the emitted acoustic pressure amplitude.

The sinusoidal excitation function for the acoustic pressure  $p_1$  at the emission node is given by

$$p_1(t)|_{\text{emission node}} = G(t) \Delta p_a [\sin(2\pi f_a t - \Delta\varphi)]^n, \quad (2.1)$$

where  $\Delta p_a$ ,  $f_a$ , and  $\Delta\varphi$  are the emitted acoustic pressure amplitude, the excitation frequency and a fixed phase shift, respectively. The sine function can be raised to a power  $n$ , to admit nonlinearities in the excitation signal. The factor  $G(t)$  is a Gauss function given by

$$G(t)|_{\text{emission node}} = q^{4(f_a t - N + 1/2)^2}, \quad (2.2)$$

which has a peak value of unity and where  $q$  is a shape coefficient that specifies the width of the Gaussian. Eq. (2.2) can be used in conjunction with Eq. (2.1) to define a Gauss-enveloped sinusoidal excitation signal, for which the Gaussian peaks at the center of the  $N^{\text{th}}$  period. Alternatively, it can be used to emit a Gaussian pulse  $\Delta p_a G(t)$ , where  $f_a$  and  $N$  as well  $\Delta p_a$  must be specified to indicate the center time and the amplitude of the pulse, respectively. The parameters of Eqs. (2.1) and (2.2) are set in the section **EXCITATION** of the options file.

Command	Description
Section <b>EXCITATION</b>	
<code>ExcitationStart &lt;float&gt;</code>	Physical start time of the wave excitation. By default, equal to the simulation start time <b>TimeStart</b> (see <b>RUNOPTIONS</b> ).
<code>ExcitationEnd &lt;float&gt;</code>	Physical end time of the wave excitation. By default, equal to the simulation end time <b>TimeEnd</b> (see <b>RUNOPTIONS</b> ).

ExcitationNode <int>	Node (ID of the grid point) at which the wave is excited (0 is default).
ExcitationFunctionType <string>	Type of the excitation function. Options are <b>sine</b> (Eq. (2.1)) and <b>GaussPulse</b> . The latter is given by Eq. (2.2) times the pressure amplitude specified below.
PressureAmplitude <float>	Excitation amplitude $\Delta p_a$ of the acoustic pressure signal $p_1$ . This applies to both the options <b>sine</b> and <b>GaussPulse</b> .
ExcitationFrequency <float>	Unmodulated frequency $f_a$ of the excitation signal if <b>ExcitationFunctionType</b> is set to <b>sine</b> .
PhaseShiftAngle <float>	Phase shift angle $\Delta\varphi$ in the argument of the excitation signal, if <b>ExcitationFunctionType</b> is set to <b>sine</b> .
PowerCoeff <float>	Exponent $n$ of the sinusoidal excitation function (1.0 is default), if applicable.
GaussEnvelope <string>	The excitation function can be enveloped by the Gauss function $G(t)$ with peak value 1.0 by setting this option to <b>True</b> ( <b>False</b> is default). If <b>ExcitationFunctionType</b> is set to <b>GaussPulse</b> , the corresponding pointer is set to a function that returns the amplitude of the excitation signal ( <b>PressureAmplitude</b> ), which is then convoluted by the Gauss function, irrespective of the option for <b>GaussEnvelope</b> <string>.
EnvelopedPeriod <float>	Period number $N$ of the sinusoidal excitation function that is Gauss-enveloped by Eq. (2.2) (not necessarily an integer). This setting can also be used to specify the center of the peak in the time domain if <b>ExcitationFunctionType</b> is set to <b>GaussPulse</b> .
GaussShapeCoeff <float>	Coefficient $q$ in Eq. (2.2) that determines the width of the Gauss pulse in the time domain.

---

## 2.5 Boundary, grid, and background flow motion

The present simulation framework for moving domain boundaries and background flow fields admits the following configurations, where one boundary is always fixed, whereas the other can be either fixed or moving:

- **Moving emitter/scatterer in a quiescent medium:** One of the domain boundaries is in motion whereas the background medium is at rest. This configuration gives rise to the classical Doppler effect. If the moving boundary is the wave emitting boundary, it acts like a moving wave emitter. If the non-moving boundary is the wave emitting boundary, the moving boundary acts like a moving wave scatterer, given that the corresponding boundary condition is not an absorbing one.
- **Moving flow-inducing boundary:** The moving boundary induces a background flow field by mimicking a solid boundary that displaces the surrounding fluid. The wave may be emitted by the moving boundary itself, so that the emitter does not move relative to the background flow field. Alternatively, the wave may be excited at the fixed boundary (or any node between the left and the right boundary), so that emitter and background medium are in relative motion.
- **Stationary acoustic black/white hole:** A special case of the previous configuration is the acoustic black or white hole. In principle, any of the options to specify the boundary and fluid motion can mimic a background flow field with sonic transition. However, **Wave-DNA** specifically allows simulating stationary spherical acoustic black holes and white holes with a pre-defined radius of the sonic horizon.

All the above options can be combined with the assumption of linear acoustics ( $\beta = 0$ ,  $\mathcal{L} = 0$ ) or with nonlinear acoustics as specified in Section 2.3.

The distribution of the background flow velocity is either spatially uniform in the case of a one-dimensional Cartesian geometry (it may still be time-dependent if one of the boundaries is moving), or it follows from the relation

$$u_0(r, t) = \dot{R}(t) \left( \frac{R(t)}{r} \right)^n, \quad (2.3)$$

if a variable cross-sectional area or a spherically-symmetric configuration is considered. In the present implementation, the parameter  $n$  is a constant equal to 2 by default, such that Eq. (2.3) represents the spherically-symmetric velocity field obeying the continuity equation for an incompressible fluid. The value of  $n$  may be changed in the options file, and with some minor modifications of the source, even time- and space-dependent distributions of  $n$  can be realized.

If Mach numbers of considerable magnitude are involved, it should be noted that according to the theory underpinning the present modeling framework, the background density and speed of sound are assumed to be constant. This means, for instance, that the background fluid state of the acoustic black hole scenario represents a so-called slab geometry rather than a fully physical configuration.

It follows from the linear coordinate transformation

$$\xi(r, t) = \mathcal{X}_\infty + (r - R_{\text{stat}}) \frac{\mathcal{X}_\infty - \mathcal{X}_R}{R_{\text{stat}} - R(t)} \quad (2.4)$$

that

$$\frac{\partial \xi}{\partial r} = \frac{\mathcal{X}_\infty - \mathcal{X}_R}{R_{\text{stat}} - R(t)}, \quad (2.5)$$

$$\frac{\partial \xi}{\partial t} = -\frac{\mathcal{X}_\infty - \xi}{R_{\text{stat}} - R(t)} \dot{R}(t), \quad (2.6)$$

$$\frac{\partial^2 \xi}{\partial t \partial \xi} = \frac{\dot{R}(t)}{R_{\text{stat}} - R(t)}, \quad (2.7)$$

$$\frac{\partial^2 \xi}{\partial r \partial \xi} = 0, \quad (2.8)$$

$$\frac{\partial^2 \xi}{\partial t^2} = 2 \frac{\partial \xi}{\partial t} \frac{\partial^2 \xi}{\partial t \partial \xi} - \ddot{R} \frac{\partial \xi}{\partial r} \frac{\mathcal{X}_\infty - \xi}{\mathcal{X}_\infty - \mathcal{X}_R}. \quad (2.9)$$

The motion of the grid-points is then fully described by the instantaneous position  $R$  of the moving domain boundary, as well as the velocity  $\dot{R}$  and acceleration  $\ddot{R}$  thereof.

An oscillatory boundary motion is described by the function

$$R(t) = R_0 + \frac{\Delta v_{\text{b,a}}}{2\pi f_{\text{b}}} \sin(2\pi f_{\text{b}} t), \quad (2.10)$$

$$\dot{R}(t) = \Delta v_{\text{b,a}} \cos(2\pi f_{\text{b}} t), \quad (2.11)$$

$$\ddot{R}(t) = -2\pi f_{\text{b}} \Delta v_{\text{b,a}} \sin(2\pi f_{\text{b}} t), \quad (2.12)$$

where  $f_{\text{b}}$  and  $\Delta v_{\text{b,a}}$  are the frequency and the velocity amplitude of the oscillating boundary, respectively.

For the acoustic black and white hole analogues, with  $r_{\text{h}}$  being the steady-state sonic horizon radius



in a flow field obeying Eq. (2.3), the functions describing the boundary motion are given by

$$R(t) = [R_0^{n+1} - (n+1)c_0 r_h^n t]^{\frac{1}{n+1}}, \quad (2.13)$$

$$\dot{R}(t) = -c_0 r_h^n [R_0^{n+1} - (n+1)c_0 r_h^n t]^{-\frac{n}{n+1}}, \quad (2.14)$$

$$\ddot{R}(t) = -nc_0^2 r_h^{2n} [R_0^{n+1} - (n+1)c_0 r_h^n t]^{-\frac{2n+1}{n+1}} \quad (2.15)$$

for the acoustic black hole scenario, and by

$$R(t) = [R_0^{n+1} + (n+1)c_0 r_h^n t]^{\frac{1}{n+1}}, \quad (2.16)$$

$$\dot{R}(t) = c_0 r_h^n [R_0^{n+1} + (n+1)c_0 r_h^n t]^{-\frac{n}{n+1}}, \quad (2.17)$$

$$\ddot{R}(t) = -nc_0^2 r_h^{2n} [R_0^{n+1} + (n+1)c_0 r_h^n t]^{-\frac{2n+1}{n+1}} \quad (2.18)$$

for the acoustic white hole scenario.

Command	Description
<b>Section BOUNDARYMOTION</b>	
BoundaryMotionType <string>	Function type describing the motion of the moving domain boundary. Options are <linear> for a constant velocity, <oscillating> for an oscillatory motion around the initial position, described by a sine function (see Eq. (2.10)), and <stationaryBlackHole> or <stationaryWhiteHole> for the simulation of an acoustic black or white hole configuration (see Eq. (2.13)).
BoundaryMotionStartTime <float>	Physical time at which the moving boundary starts to move from its initial position. The function describing the boundary motion depends on the time interval that has passed relative to this start time.
BoundaryMotionEndTime <float>	Physical time at which the boundary motion ends. The boundary position will remain constant for the remaining simulation time.
InitialMovingBoundaryPosition <float>	Initial position of the moving domain boundary (0 is the default).
FixedBoundaryPosition <float>	Position of the fixed domain boundary. The default setting is a domain that comprises 10 emitted wavelengths, $\lambda_0 = c_0/f_a$ .
MovingBoundaryVelocityAmplitude <float>	Velocity amplitude $\Delta v_{b,a}$ of the moving domain boundary, if BoundaryMotionType is set to <oscillating>. If BoundaryMotionType is set to <linear>, $\lambda_0 = c_0/f_a$ represents the constant boundary velocity.
MovingBoundaryFrequency <float>	Frequency $f_b$ of the moving domain boundary, if BoundaryMotionType is <oscillating> (default: $f_b = 0.1f_a$ ).
<b>Section BACKGROUNDFLOW</b>	
BackgroundMotionMode <string>	Specifies whether the background flow field is quiescent (option <quiescent>), regardless of the motion of the moving domain boundary, or whether the background flow field is coupled to the moving domain boundary (option <coupledToMovingBoundary>).

Geometry <string>	Specifies whether the flow field is spatially uniform (option <1dCartesian>) or whether it satisfies the continuity equation of a spherically symmetric flow (option <3dSphericallySymmetric>).
HorizonRadius <float>	Point of sonic transition if BoundaryMotionType is set to <stationaryBlackHole> or <stationaryWhiteHole>.
BackgroundVelocityScalingFactor <float>	Exponent $n$ in Eq. (2.3), defining the parametrization of the spatially non-uniform background flow.
GravitationalPotential <string>	If set to True and if BackgroundMotionMode is set to <stationaryBlackHole> or <stationaryWhiteHole>, a gravitational potential is included to mimic a simplified Bondi-Parker-type flow (see [8]).

---

## 2.6 Finite-difference discretization

To be compatible with the predictor-corrector method and the wave-absorbing boundary conditions as explained further below, we use first-order finite differences in time. For the spatial discretization, second-order central differences are used. The Laplacian and the mixed spatial-temporal derivatives only have to be evaluated in the inner field, whereas the gradient also has to be evaluated at the boundary, to impose the wave-absorbing boundary condition. At the boundaries, a first-order finite difference stencil is used to compute the gradient.

Next to the time step size  $\Delta t$  and the total number of grid points, one can specify the parameter  $\gamma$  of a predictor-corrector method [3, 6], where the interim solution  $\tilde{\Phi}_1$ , predicted by the explicit finite-difference integration, is weighted by  $(1 - \gamma)$ , whereas the corrected solution is weighted by  $\gamma$ . With  $i$  and  $j$  indicating the grid point and the time step, respectively, the spatial and temporal finite-difference approximations are given by

$$\left(\frac{\partial^k \Phi_1}{\partial t^k}\right)_i = \frac{a_0^{(k)}}{\Delta t^k} \Phi_{1,i}^{j+1} + \underbrace{\frac{1}{\Delta t^k} \sum_{n=1}^{N-1} a_n^{(k)} \Phi_{1,i}^{j+1-n}}_{b_i^{(k,j)}}, \quad (2.19)$$

$$\left(\frac{\partial^k \Phi_1}{\partial \xi^k}\right)_i = \frac{a_0^{(k)} \Phi_{1,i}^j + \sum_{n=1}^{(N-1)/2} \left(a_n^{(k)} \Phi_{1,i+n}^j + a_n^{(k)} \Phi_{1,i-n}^j\right)}{\Delta \xi^k}. \quad (2.20)$$

The predicted solution  $\tilde{\Phi}_{1,i}$  is obtained as

$$\tilde{\Phi}_{1,i} \underbrace{\sum_{k=1}^2 \mathcal{A}_{k,i}^j \frac{a_0^{(k)}}{\Delta t^k}}_{\mathcal{H}_i^j} + \underbrace{\mathcal{R}_i^j + \sum_{k=1}^2 \mathcal{A}_{k,i}^j \frac{b_i^{(k,j)}}{\Delta t^k}}_{\mathcal{S}_i^j} = -\mathcal{A}_{L,i}^j \left(\frac{\partial^2 \Phi_1}{\partial \xi^2}\right)_i^j + \left(\frac{c_0^2}{A} \frac{\partial A}{\partial r} \frac{\partial \xi}{\partial r}\right)_i^j \left(\frac{\partial \Phi_1}{\partial \xi}\right)_i^j, \quad (2.21)$$

where the term  $\mathcal{R}_i^j$  involves the finite-difference approximations of the gradient and mixed-derivative terms. The new solution  $\Phi_{1,i}^{j+1}$  is then obtained as

$$\Phi_{1,i}^{j+1} = (1 - \gamma) \tilde{\Phi}_{1,i} + \frac{\gamma}{\mathcal{H}_i^j \left(\Phi_{1,i}^j\right)} \left[ \underbrace{\mathcal{A}_{L,i}^j \left(\Phi_{1,i}^j\right) \left(\frac{\partial^2 \tilde{\Phi}_1}{\partial \xi^2}\right)_i^j - \left(\frac{c_0^2}{A} \frac{\partial A}{\partial r} \frac{\partial \xi}{\partial r}\right)_i^j \left(\frac{\partial \tilde{\Phi}_1}{\partial \xi}\right)_i^j}_{\text{spherical Laplacian}} + \mathcal{S}_i^j \left(\Phi_{1,i}^j\right) \right], \quad (2.22)$$

where the spherical Laplacian is updated based on the predicted solution  $\tilde{\Phi}_1$ , whereas all remaining terms, summarized in the terms  $\mathcal{H}$  and  $\mathcal{S}$ , and the time- and space-dependent coefficient  $\mathcal{A}_L$ , remain unchanged in the corrector step. The corrector step may be performed multiple times in a corrector loop. However, a single corrector step should serve the purpose of counteracting dispersive noise. In fact, the value of  $\gamma$  is more important. For  $\gamma = 0$ , a standard explicit finite-difference time integration scheme is obtained. With increasing  $\gamma$ , the predictor-corrector method becomes increasingly diffusive. The resolution of the simulation must be increased at constant Courant-Friedrichs-Lewy (CFL) number to avoid excessive diffusion, while preserving the stabilizing effect of the predictor-corrector scheme. To this end, the CFL number is given by

$$\text{CFL} = \frac{c_0 \Delta t}{\Delta x} = \frac{c_0 \Delta t (N_{\text{points}} - 1)}{L_{\text{domain}}}, \quad (2.23)$$

where  $\Delta t$  and  $\Delta x$  are the time-step size and the spatial-step size, respectively, and  $N_{\text{points}}$  and  $L_{\text{domain}}$  are the total number of grid points in the domain, including the boundaries, and the length of the physical domain, respectively. In other words, the increase in numerical stability comes at the expense of an increased computational effort to preserve the accuracy of the numerical solution. Rather than representing a blended solution, the predictor-corrector method effectively generates a  $\Delta x$ - and  $\Delta t$ -dependent attenuation term that predominantly acts on the higher frequencies [6]. Therefore, values of  $0 \leq \gamma \leq 1$  are possible and  $\gamma > 0$  may even be required, in particular if shocks are involved.

The boundary conditions can either be *scattering*, where the incoming wave is fully reflected at the domain boundary, or *absorbing*, where the incoming wave passes the domain boundary without reflection. The absorbing boundary condition is based on Mur's first-order absorbing boundary condition, given by [5]

$$\Phi_{1,0}^{j+1} = \Phi_{1,1}^j + \frac{\text{CFL} - 1}{\text{CFL} + 1} (\Phi_{1,1}^{j+1} - \Phi_{1,0}^j) + 2u_{1,1}^j \frac{\Phi_{1,0}^j - \Phi_{1,N}^j}{\Delta x}, \quad (2.24)$$

$$\Phi_{1,N}^{j+1} = \Phi_{1,N-1}^j + \frac{\text{CFL} - 1}{\text{CFL} + 1} (\Phi_{1,N-1}^{j+1} - \Phi_{1,N}^j) + 2u_{1,N}^j \frac{\Phi_{1,N-1}^j - \Phi_{1,N}^j}{\Delta x} \quad (2.25)$$

for the *west* and the *east* boundary, respectively, and where the advective terms are added in order to allow the waves to pass the domain boundaries in the presence of a non-zero background flow field.

The following table provides an overview of the options for the finite-difference discretization.

Command	Description
<hr/> Section FINITEDIFFERENCE <hr/>	
TimeStepSize <float>	Constant time-step size $\Delta t$ , where the acoustic CFL number takes the value 0.1 by default.
NPoints <int>	Total number of grid points in the computational domain, including the domain boundaries, where the default setting is 100 points per emitted wavelength $\lambda_0 = c_0/f_a$ .
nCorrectors <int>	Number of corrector steps applied in the predictor-corrector method (1 by default).
correctorWeight <float>	Corrector weight $\gamma$ of the predictor-corrector method ( $\gamma = 0.1$ by default).
BoundaryConditionWest <string>	Boundary condition at the <i>west</i> domain boundary, which can be <absorbing> (default) or <scattering>.
BoundaryConditionEast <string>	Boundary condition at the <i>east</i> domain boundary, which can be <absorbing> (default) or <scattering>.

## 2.7 Default settings

These are the default settings for the Wave-DNA options file `run.DNA`, indicating the dependencies between certain default settings (see the source file `src/io/iodefaultoptions.c`). The default settings are used if the corresponding option is not included in `run.DNA`.

### FLUID

```
SoundSpeed 1500.0
Density 1000.0
FluidNonLinearity 0.0
LocalNonlinearity False
END
```

### RUNOPTIONS

```
TimeStart 0.0
TimeEnd 10.0/<ExcitationFrequency>
WriteFrequency (<TimeEnd> - <TimeStart>)/<TimeStepSize>
SamplePoints 0
END
```

### BOUNDARYMOTION

```
BoundaryMotionType linear
BoundaryMotionStartTime <TimeStart>
BoundaryMotionEndTime <TimeEnd>
InitialMovingBoundaryPosition 0.0
FixedBoundaryPosition 10.0*<SoundSpeed>/<ExcitationFrequency>
MovingBoundaryVelocityAmplitude 0.0
MovingBoundaryFrequency 0.1*<ExcitationFrequency>
END
```

### BACKGROUNDFLOW

```
Geometry 1dCartesian
BackgroundMotionMode quiescent
HorizonRadius 0.9*<InitialMovingBoundaryPosition>
BackgroundVelocityScalingFactor 2.0
GravitationalPotential False
END
```

### EXCITATION

```
ExcitationStart <TimeStart>
ExcitationEnd <TimeEnd>
ExcitationNode
ExcitationFunctionType sine
PressureAmplitude 1.0e3
ExcitationFrequency 1.0e5
PhaseShiftAngle 0
PowerCoeff 1
GaussEnvelope False
EnvelopedPeriod 1
GaussShapeCoeff 1.0
END
```

### FINITEDIFFERENCE

```
TimeStepSize (<FixedBoundaryPosition> - <InitialMovingBoundaryPosition>)/...
...(<NPoints> - 1)*0.1/<SoundSpeed>
```

```

NPoints 100*(<FixedBoundaryPosition> - <InitialMovingBoundaryPosition>)/...
      ...(<SoundSpeed>/<ExcitationFrequency>)) + 1
nCorrectors 1
correctorWeight 0.1 BoundaryConditionEast absorbing
BoundaryConditionWest absorbing
END

```

## 2.8 Results

Three different result files may be written to the `results` sub-directory:

- `fields.dat`,
- `probes.dat`,
- `horizon.dat`.

The output file `fields.dat` is always written to disk and contains the field data (data at the grid points). The data is written at time instances specified by `WriteFrequency` in the options file. The output columns represent the data for

Grid point ID  $[-]$ ,  $x$  [m],  $p_1$  [Pa],  $\phi_1$  [ $\text{m}^2\text{s}^{-1}$ ],  $u_0$  [ $\text{ms}^{-1}$ ].

Each output section starts with indicating the physical time, the corresponding time-step number, the instantaneous position  $R$  of the (possibly) moving boundary as well as its instantaneous velocity  $\dot{R}$ . The output section concludes with the key word `EOS`.

The output file `probes.dat` is only written if a non-zero number  $N_{\text{sample points}}$  of `SamplePoints` is given. The sample points represent grid nodes for which time signals of the acoustic pressure are written to disk. The output columns represent

Time step  $[-]$ ,  $t$  [s],  $p_1$  (sample points 1) [Pa], ...,  $p_1$  (sample points  $N_{\text{sample points}}$ ) [Pa].

The grid nodes may be moving if one of the domain boundaries is in motion.

The output file `horizon.dat` is only written if `BoundaryMotionType` is set to `stationaryBlackHole` or `stationaryWhiteHole`, as described in Section 2.5. The output file contains time signals recorded at the sonic horizon of the acoustic black hole, representing

Time step  $[-]$ ,  $t$  [s],  $R$  [m],  $\dot{R}$  [ $\text{ms}^{-1}$ ],  $r_h$  [m],  $p_1$  [Pa],  $\phi_1$  [ $\text{m}^2\text{s}^{-1}$ ].

Note that the sonic horizon radius  $r_h$  is constant over time in the case of a stationary acoustic black or white hole.

# Chapter 3

## Source code guide

### 3.1 Header files

The header files (\*.h) are located in `src/include`. In `DNA-functions.h`, the function prototypes are defined. The file `DNA-constants.h` contains macros of constants (such as  $\pi$ ) and mathematical operators (such as trigonometric functions or min/max operators). In the `DNA.h` file, all structures used throughout the program are declared. There are four main structures, the instances of which are created in `main.c`:

- **struct DNA\_RunOptions**: Structure containing variables and function pointers associated with the run options. Nested structures:
  - **struct DNA\_NumericsFD**: Structure containing variables used for the temporal and spatial discretization (e.g.  $\Delta t$ ,  $\Delta x$ , etc.) and function pointers associated with the boundary conditions. Nested structure:
  - **struct DNA\_FDCoeffs**: Finite-difference coefficients.
  - **struct DNA\_WaveExcitation**: Variables of the wave excitation functions (see Eqs. (2.1) and (2.2)).
  - **struct DNA\_Probes**: Variables specifying the acoustic pressure probes (see Section 2.3).
- **struct DNA\_FluidProperties**: Fluid properties such as the background density and speed of sound, as well as the fluid nonlinearity.
- **struct DNA\_Fields**: Structure comprising all scalar fields. Nested structures:
  - **struct DNA\_Grid**: Scalars and scalar fields, represented by pointers, representing the dependent coordinates  $x(\xi, t)$  of the time-dependent physical domain  $\Omega(t)$ , the fixed computational domain  $\Theta$ , and the metrics of the coordinate transformation according to Eqs. (2.5) to (2.9).
  - **struct DNA\_BackgroundFlowField**: Scalar fields, represented by pointers, involving the background flow velocity field as well as spatial and temporal derivatives thereof.
  - **struct DNA\_PhiField**: Scalar fields, represented by pointers, involving the acoustic (velocity) potential field (the primary solution) as well as spatial and temporal derivatives thereof. The acoustic pressure is included in this structure as well.
  - **struct DNA\_OldPhiField**: Similar to the previous, but containing the data from the two preceding time steps. This information is required for the time integration.
- **struct DNA\_MovingBoundary**: Variables associated with the moving boundary of the physical domain  $\Omega(t)$ .

## 3.2 Source files

The core of the computational method evolves around solving the lossless convective Kuznetsov equation [10] in the coordinates of the fixed computational domain. The following table provides an overview and brief description of the source files.

Source file	Description
<b>Directory backgroundflow</b>	
<code>backgroundflowgravitation.c</code>	Function to compute the gravitational potential if applicable.
<code>backgroundflowmotion.c</code>	Functions to compute the background flow velocity field $u_0$ and its spatial and temporal derivatives.
<b>Directory boundary</b>	
<code>boundaryconditions.c</code>	Calling the functions to set the boundary conditions.
<code>boundarymotion.c</code>	Functions to describe the motion of the moving domain boundary.
<b>Directory fd</b>	
<code>fdboundaryconditions.c</code>	Functions to apply the boundary conditions. The functions for the West and East boundaries are called by reference. The corresponding pointers are <code>int (*FDBC_West)(...)</code> and <code>int (*FDBC_East)(...)</code> , respectively.
<code>fdcoeffs.c</code>	Finite difference coefficients for the spatial and temporal discretization.
<code>fddt.c</code>	Functions to construct the explicit finite difference approximations of the time derivatives.
<code>fd dx.c</code>	Functions to construct the explicit finite difference approximations of the spatial derivatives.
<code>fdsumaphi.c</code>	Functions to compute the sums over previous time-steps needed for the finite difference discretization, see Eq. (2.19).
<b>Directory grid</b>	
<code>gridmakegrid.c</code>	Functions to create the time-dependent grid for the physical domain $\Omega(t)$ and the fixed grid for the computational domain $\Theta$ .
<code>gridmotion.c</code>	Updating the derivatives of the dependent coordinate $\xi(r, t)$ as given by Eqs. (2.5) to (2.9).
<b>Directory include</b>	
<code>DNA.h</code>	See Section 3.1.
<code>DNA-constants.h</code>	See Section 3.1.
<code>DNA-functions.h</code>	See Section 3.1.
<b>Directory initialize</b>	
<code>initializefield.c</code>	Routines to initialize single fields of the type <code>struct DNA.Fields</code> .
<code>initializeprocessoptions.c</code>	Setting all function pointers based on the specifications in the Wave-DNA options file or the default options.

<code>initializesimulation.c</code>	Routine that allocates memory for all scalar fields and results vectors by calling functions in <code>memoryallocfields.c</code> (see below). Initial values are set and the grid point IDs corresponding to the coordinates of the probe sample locations (IDs of the nearest neighbours are taken) specified in the Wave-DNA options file are identified.
<hr/> Directory <code>io</code> <hr/>	
<code>iodefaultoptions.c</code>	Defaults for the options that can be set in the Wave-DNA options file. A simulation is performed even with an empty options file (see Section 4.1).
<code>ioonscreen.c</code>	Functions for output on screen during the run time of the simulation.
<code>ioreadcommandlineoptions.c</code>	Function to read command line options.
<code>ioreadoption.c</code>	Called in <code>ioreadoptionsfile.c</code> to read a single option the Wave-DNA options file.
<code>ioreadoptionsfile.c</code>	Function that reads the Wave-DNA options file.
<code>ioresults.c</code>	Functions to write output data to disk.
<hr/> Directory <code>memory</code> <hr/>	
<code>memoryalloc.c</code>	Function to allocate memory for fields of the type <code>struct DNAField</code> and the probe sample points and vectors.
<code>memoryallocfields.c</code>	Routine calling <code>memoryalloc.c</code> to allocate all fields.
<code>memoryfreefields.c</code>	Routine called in <code>main.c</code> to free all fields upon termination of the programme.
<hr/> Directory <code>solve</code> <hr/>	
<code>solveexplicitderivatives.c</code>	Routine calling the functions in <code>fddx.c</code> and <code>fddt.c</code> to construct the finite difference approximations explicit temporal, spatial, and mixed derivatives.
<code>solveloop.c</code>	This file contains the function <code>SolveTimeLoop</code> , representing the time loop of the simulation, and the function <code>Solve</code> , which is called in <code>SolveTimeLoop</code> at each time step and which calls the functions relevant to the numerical algorithm.
<code>solvepredictorcorrector.c</code>	Routines to apply the predictor (see Eq. (2.21)) and the corrector steps (see Eq. (2.22)). Additional routines are to update the Laplacian prior to the corrector step and to store the initial guess $\widetilde{\Phi}_{1,i}$ computed based on Eq. (2.21) and required in Eq. (2.22).
<code>solvesumaphi.c</code>	Routine calling the functions in <code>fdsumaphi.c</code> to compute the sums over the previous time steps required for the explicit finite difference approximations of the time-derivatives.
<code>solveupdatefields.c</code>	Contains the function that updates the old fields.
<hr/> Directory <code>transform</code> <hr/>	



<code>transformeqn.c</code>	Functions to compute the space- and time-dependent coefficients of the transformed wave equation, and to assemble the terms of the discretized equation. The file contains the function <code>TransformEqn_Predictor</code> to assemble the terms for the predictor step of the predictor-corrector method (see Eq. (2.21)), and the function <code>TransformEqn_Corrector</code> , which only updates the coefficients and terms that are relevant for the corrector step, see Eq. (2.22).
<code>transformgeometricaldecay.c</code>	Function to account for the change of the cross-sectional area $A$ in the Laplacian in the case of spherical symmetry.
<code>transformpotential.c</code>	Routines to convert the acoustic pressure $p_1$ into the perturbation potential $\Phi_1$ (required at the excitation node) and vice versa (required to reconstruct the acoustic pressure field from the solution for $\Phi_1$ ).
<hr/>	
Directory <code>waveexcitation</code>	
<code>waveexcitation.c</code>	Functions to excite the acoustic pressure wave at the specified excitation node.

# Chapter 4

## Examples

The following examples are found in the Wave-DNA source directory `</path/to/wavedna/examples/>`. The case folder must contain the following files and directorie

### 4.1 Default run

This example is found in `examples/DefaultRun`.

If the `run.DNA` options file is empty, the simulation is exclusively based on the default options. The result is a sinusoidal wave comprising ten emitted wave periods in a domain that comprises ten wavelengths. The is excited at the left (West) boundary and travels from left to right. The CFL number is equal to 0.1 and the spatial resolution is  $N_{\text{ppw}} = 100$  points per wavelength. `fields.dat` is the only output file as no probes are specified. The instantaneous obtained at a physical time of ten wave periods is shown in Fig. 4.1. See Sec. 2.7 and/or the source file `src/io/iodefualtoptions.c` for the default settings.

### 4.2 Absorbing vs reflecting boundary conditions

This example is found in `examples/ScatteringAbsorbing`.

This test case illustrates the options for the boundary conditions. A Gaussian pulse is emitted as indicated by the red lines in Fig. 4.2 (see the `run.DNA` file). The pulse is emitted at  $x = 0$  and travels from left to right. In Fig. 4.2 (a), the settings are:

`BoundaryConditionEast scattering`

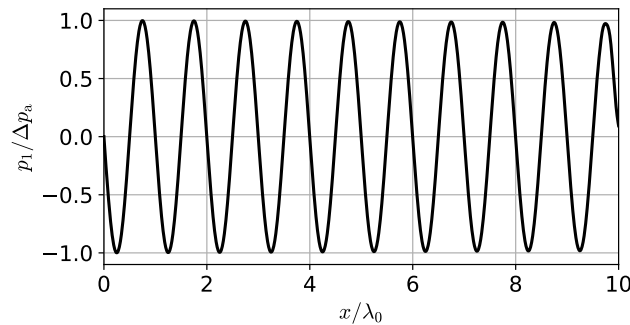


Figure 4.1: Instantaneous wave profile obtained for the default settings (empty `run.DNA` file).

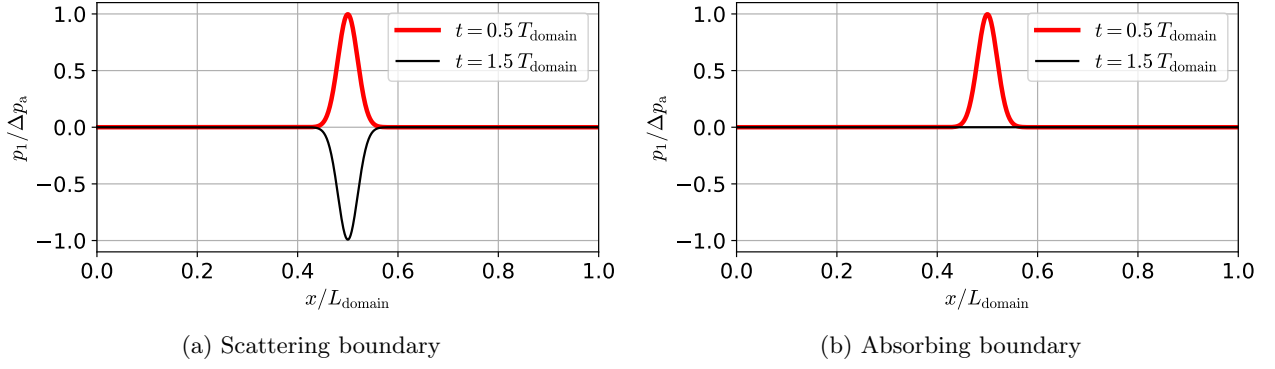


Figure 4.2: Illustration of the **scattering** (a) and the **absorbing** (b) boundary condition. A pulse travels from left to right (red lines). In (a), the pulse is reflected at the East domain boundary and travels back to the left (black line). In (b), the pulse passes the domain so that no reflection is visible (black line).

`BoundaryConditionWest scattering`

With the **scattering** condition at the East boundary, the pulse is reflected at the boundary as indicated by the black line in Fig. 4.2 (a). In Fig. 4.2 (b), the settings are:

`BoundaryConditionEast absorbing`  
`BoundaryConditionWest scattering`

With the **absorbing** condition at the East boundary, the pulse leaves the domain without reflection as shown by the black line in Fig. 4.2 (b). The settings for the West boundary are arbitrary as this boundary is the emission node in this case.

### 4.3 Shock-driven attenuation

This example is found in `examples/ShockDrivenAttenuation`.

This test case is concerned with the progressive deformation, shock formation, and shock-driven attenuation of an initially sinusoidal wave. The background medium is quiescent and the computational domain is at rest throughout the entire simulation. The CFL number is 0.05 with a spatial resolution of  $N_{\text{ppw}} = 400$  points per wavelength  $\lambda_0$  and a corrector weight of  $\gamma = 1.5$ , set as follows:

`FluidNonLinearity 3.5`

This rather high resolution is needed in order avoid excessive numerical dissipation due to the presence of the steep wavefront. The wave is emitted at the left boundary and travels to the right. The excitation amplitude and the nonlinearity coefficient  $\beta$  are set in such a way that the nominal shock formation distance, given by [1]

$$x_{\text{sh}} = \frac{\rho_0 c_0^3}{2\pi\beta f_a \Delta p_a}, \quad (4.1)$$

takes the value  $x_{\text{sh}} = 10$ . At the shock formation distance, the progressively steepening wavefront first starts to develop a discontinuity. The red dashed line in Fig. 4.3 represents the envelope  $\hat{p}_1$  owing to the Fay solution [4], given by [1]

$$\frac{\hat{p}_1}{\Delta p_a} = \frac{\pi}{1 + x/x_{\text{sh}}}. \quad (4.2)$$

The Fay solution is not applicable to the close vicinity of the emitter, but asymptotically approaches the wave profile decay at distances larger than approximately  $3x_{\text{sh}}$ , where the initially sinusoidal has

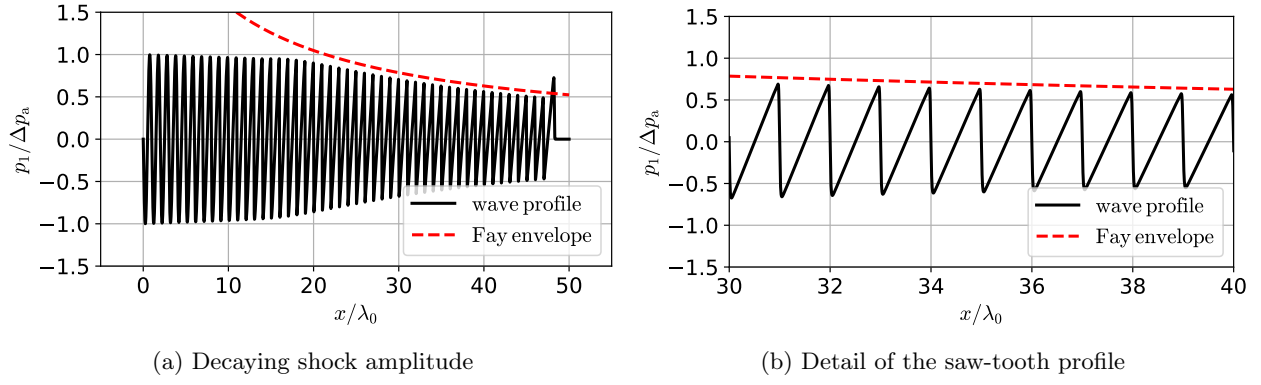


Figure 4.3: Initially sinusoidal and progressively steepening and shock-forming wave. As the wave has traveled past the shock formation distance  $x_{\text{sh}} = 10\lambda_0$  (see Eq. (4.1)) in subfigure (a), its amplitude starts to decay rapidly, asymptotically approaching the envelope of Fay solution [4] as given by Eq. (4.2) [1]. Subfigure (b) depicts a detail of the fully developed saw-tooth profile.

fully evolved into a saw-tooth shape. Fig. 4.3 (a) shows that the wave profile exhibits only a minor decay prior to the shock formation distance, after which starts to approach the Fay envelope. Fig. 4.3 (b) shows a detail of the fully developed saw-tooth pattern. It is noted that the predictor-corrector method drives the attenuation associated with the dissipation across the shock front. See Schenke *et al.* [9] for further discussions of this effect.

## 4.4 Moving emitter, boundary and flow

The following examples are found in `examples/MovingBoundary`.

### 4.4.1 Moving emitter

This example is found in `examples/MovingBoundary/RelativeEmitterMotion`.

This example illustrates how the Doppler shift due to the motion of an emitter relative to a quiescent medium can be reproduced with **Wave-DNA**. A sine wave is excited at the left (West) domain boundary and travels from left to right. The background flow field is quiescent:

```
BackgroundMotionMode quiescent
```

The speed of sound is:

```
SoundSpeed 1500.0
```

The moving boundary moves at a constant velocity magnitude of  $500 \text{ m/s} = c_0/3$ , where the setting

```
BoundaryMotionType linear
```

is used to indicate a constant velocity of the boundary. The excitation location at the left boundary (default) is specified by:

```
ExcitationNode 0
```

The initial position of the moving boundary is  $x = 0$  (default) and the fixed boundary is located at  $x = 0.18 \text{ m}$  (12 times the unmodulated wavelength  $\lambda_0$ ), specified as follows:

```
InitialMovingBoundaryPosition 0.0
```

```
FixedBoundaryPosition 0.18
```

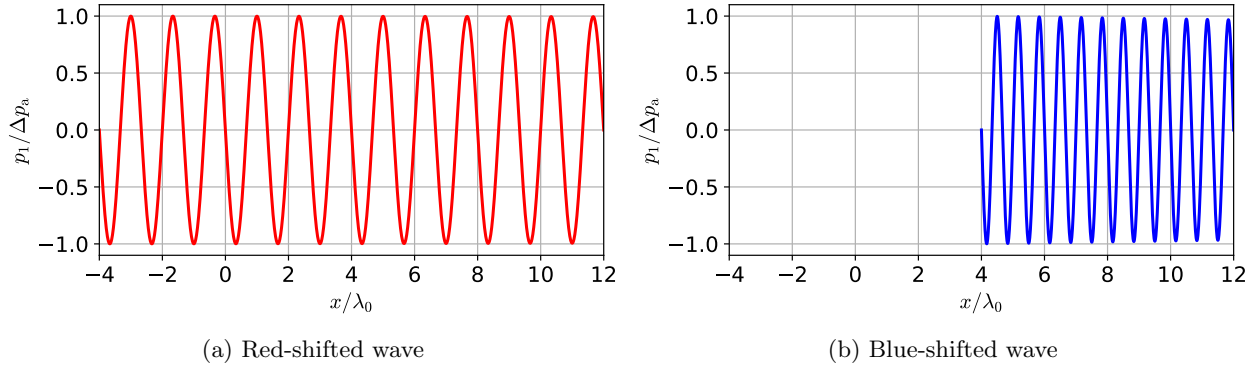


Figure 4.4: Doppler-shift induced by an emitter moving relative to a quiescent medium: the wave is excited at the moving boundary. The wave emitting boundary starts at  $x = 0$  and moves in negative  $x$ -direction in (a), thereby red-shifting the emitted wave, and in positive  $x$ -direction in (b), thereby blue-shifting the emitted wave. The magnitude of the boundary velocity is  $c_0/3$ .

Hence, the moving boundary acts as a wave emitting boundary so that the acoustic wave is Doppler-shifted upon emission. In Fig. 4.4 (a), the wave emitting boundary moves from right to left, hence against the direction of wave propagation, by setting:

```
MovingBoundaryVelocityAmplitude -500
```

This causes a red-shift (frequency decrease) of the emitted wave. In Fig. 4.4 (b), the wave emitting boundary moves from left to right, hence in the direction of wave propagation, by setting:

```
MovingBoundaryVelocityAmplitude 500
```

This causes a blue-shift (frequency increase) of the emitted wave.

#### 4.4.2 Induced flow field

This example is found in `examples/MovingBoundary/InducedFlow`.

Fig. 4.5 shows how an acoustic wave is Doppler-shifted by a temporarily constant and spatially uniform background flow field in one-dimensional Cartesian coordinates. In both Figs. 4.5 (a) and (b), the left domain boundary moves to the right with a velocity of  $c_0/3$ , and in both cases it induces a background flow field of the same velocity and direction by setting:

```
BackgroundMotionMode coupledToMovingBoundary
```

In Fig. 4.5 (a), the wave is excited at the moving boundary, which is initially at  $x = 0$  by setting:

```
ExcitationNode 0
```

As a result, the wave travels from left to right and there is no relative motion between the wave emitter and the background flow field and the emitted wavelength  $\lambda_0$  is not modulated. The instantaneous wave profile in Fig. 4.5 is shown at two time instances in order to illustrate the variable position of the wave emitting boundary. In Fig. 4.5 (b), the wave is excited at the fixed right boundary by setting:

```
ExcitationNode 4800
```

Hence, the wave travels from right to left and the fixed wave emitting boundary is in relative motion to the encountered background flow field. This causes a blue-shift of the emitted wavelength.

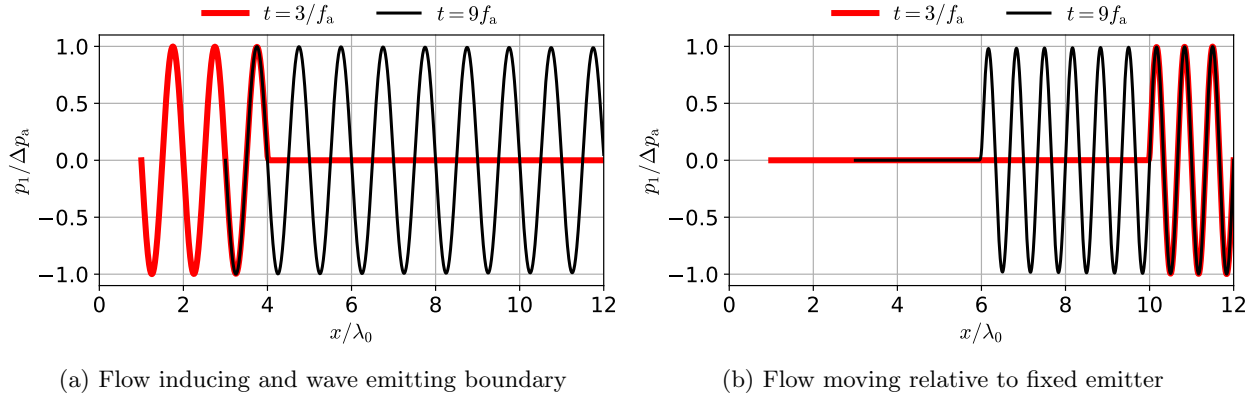


Figure 4.5: Illustration of a flow-induced Doppler shift. The left domain boundary is initially at  $x = 0$  and moves from left to right with a velocity of  $c_0/3$ . At the same time, the moving boundary induces a temporarily and spatially constant background flow field. In (a), the wave is excited at the moving boundary and travels from left to right. As there is no relative motion between background medium in (a), the emitted wavelength is not modulated. In (b), the wave is excited at the right boundary and travels from right to left, so that the wave emitting boundary is in relative motion to the encountered background flow. This causes a blue-shift of the emitted wave.

## 4.5 Possible combinations of moving boundaries, flow fields and emitters

In `examples/MovingBoundary/PossibleCombinations`, the possible combinations of setting up moving boundaries wave-emitting or non-emitting boundaries and quiescent or induced moving flow fields are demonstrated. Table 4.1 illustrates the hierarchy of possible configurations.

The initial positions of the moving and the fixed boundary determines, which of them is identified as the West and the East boundary, where the boundary further to the left is the West boundary. The boundary condition (either `scattering` or `absorbing`) is assigned to the West and East boundaries, respectively (`BoundaryConditionWest` or `BoundaryConditionEast`). Irrespective of which of the two domain boundaries is the moving one, any of the two boundaries can be the wave-emitting boundary. It is recalled from Sec. 2.4 that the wave-emitting boundary with instantaneous position  $R(t)$  is always associated with grid node 0, whereas the fixed boundary with position  $R_{\text{stat}}$  is always associated with grid node  $N_{\text{points}} - 1$ . Finally, for each of the four configurations of moving vs fixed and emitting vs non-emitting boundaries, the moving boundary can be a flow inducing one or move relative to a quiescent background flow field. This gives the eight different configurations as listed in Table 4.1.

Each of the test cases in this example directory is set up in such a way that waves move past the domain domain boundary. Hence, the test cases also illustrate how the wave-absorbing boundary condition is applied in these configurations.

## 4.6 Slowly oscillating emitter and flow field

The example of a slowly oscillating emitter is concerned with a slowly oscillating domain boundary, where “slow” means that the frequency  $f_b$  of the sinusoidal motion of the domain boundary is smaller than the emitted wave frequency  $f_a$ . In this example, a spherically symmetric wave is considered, where the settings for the background flow field are:

```
Geometry 3dSphericallySymmetric
BackgroundMotionMode quiescent
```

Moving West boundary	Emitting West boundary ( <code>ExcitationNode 0</code> )	Quiescent flow
		Induced flow
	Emitting East boundary ( <code>ExcitationNode <math>N_{\text{points}} - 1</math></code> )	Quiescent flow
		Induced flow
Moving East boundary	Emitting West boundary ( <code>ExcitationNode <math>N_{\text{points}} - 1</math></code> )	Quiescent flow
		Induced flow
	Emitting East boundary ( <code>ExcitationNode 0</code> )	Quiescent flow
		Induced flow

Table 4.1: Eight possible configurations of moving vs fixed, emitting vs non-emitting, and flow inducing vs relatively moving (quiescent flow) boundaries.

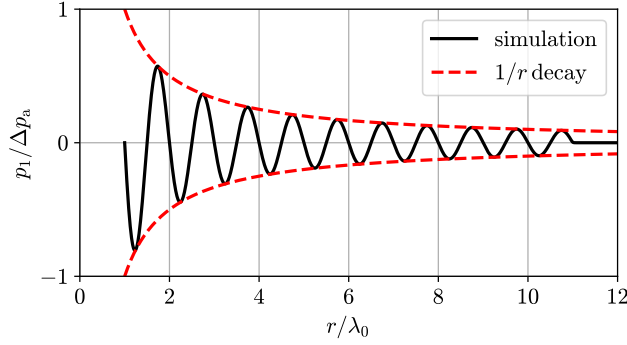


Figure 4.6: spherically symmetric wave decaying like  $1/r$ .

`BackgroundVelocityScalingFactor 2.0`

for a quiescent background medium to which the wave-emitting boundary is in relative motion or

`BackgroundMotionMode coupledToMovingBoundary`

for the case where the moving boundary displaces the fluid. The settings for the oscillatory boundary motion are:

```
BoundaryMotionType oscillating
BoundaryMotionStartTime 0.0e-0
BoundaryMotionEndTime 2.3e10
InitialMovingBoundaryPosition 0.015
FixedBoundaryPosition 0.195
MovingBoundaryVelocityAmplitude 375
MovingBoundaryFrequency 1e4
```

Hence, the boundary oscillates around an initial radius of  $R_0 = 0.015$  m, which corresponds to one wavelength with an emitted wave frequency of  $f_a = 100$  kHz (ten times larger than the frequency the boundary motion) and a speed of sound of  $c_0 = 1500$  m/s. With a velocity amplitude of 375 m/s of the boundary motion, the maximum Mach number is 0.25.

For reference, Fig. 4.6 shows the instantaneous wave profile for a resting wave-emitting boundary (`MovingBoundaryVelocityAmplitude 0`), where the wave decays like  $1/r$  as indicated by the red dashed line. Figs. 4.7 (a), (b), and (c) show the space-time diagrams for the resting, the relatively moving, and the flow-inducing moving boundaries, respectively. In the latter case, the characteristics possess a slight curvature due to the variable background flow field in which the acoustic wave propagates.

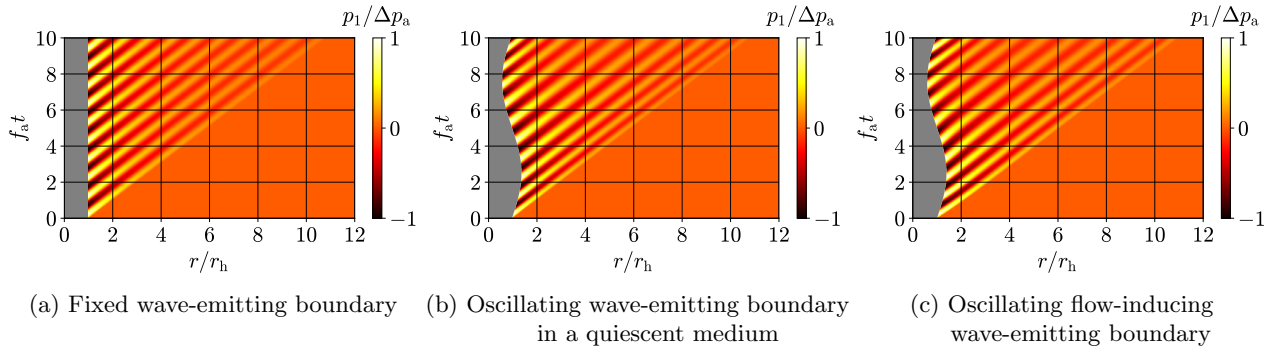


Figure 4.7: Space-time diagrams of an oscillating wave-emitting boundary, where ten acoustic wave periods are emitted during one oscillation cycle of the moving boundary.

## 4.7 Acoustic black and white holes

The following examples show how Wave-DNA can be used to simulate the acoustic wave propagation in acoustic black and white hole configurations [8]. The individual test case folders, containing illustrative acoustic black and white hole examples, include python postprocessing scripts in order to produce space-time diagrams, the plots of the instantaneous wave profiles, and the acoustic pressure evolution at the sonic horizon.

It is important to note that rather than representing compressible background flow fields with variable  $\rho_0$  and  $c_0$ , the acoustic black/white hole configurations are model systems for acoustic waves propagating in accelerating flow fields of any (also subsonic) velocity magnitude. The reason for the acoustic black/white hole being such a convenient system for the computational study of acoustic waves in accelerating flow fields lies in the fact that they allow to trap a wave characteristic at the point of sonic transition, the sonic horizon, where it is subject to both a constant background flow velocity and a constant background flow acceleration. Due to the non-zero acceleration, the neighbouring characteristics are either converging towards or diverging away from the sonic horizon.

In the acoustic black hole example shown here, nonlinearities are neglected ( $\beta = 0$  and  $\mathcal{L} = 0$ ). Fig. 4.8 exemplarily shows (a) the space-time diagram and (b) the instantaneous acoustic pressure profiles for an acoustic black hole. The entire physical domain in Fig. 4.8 is initially located outside the acoustic black hole. Subsequently, the moving wave emitting boundary collapses and eventually passes the sonic horizon while emitting outgoing characteristics. The example in Fig. 4.8 is realized by the following boundary settings:

```
BoundaryMotionType stationaryBlackHole
InitialMovingBoundaryPosition 1.60175
FixedBoundaryPosition 1.75175
```

The stationary sonic horizon radius and the geometry settings are:

```
Geometry 3dSphericallySymmetric
BackgroundMotionMode coupledToMovingBoundary
HorizonRadius 1.5
```

With these settings, the wave emitting boundary radiates a wavetrain that propagates in positive  $r$ -direction. At the same time, the spherical moving boundary collapses and induces an inward-directed spherically symmetric background fluid flow that satisfies Eq. (2.3). The boundary satisfies Eq. (2.13) so that a stationary flow field is obtained. The data at the stationary sonic horizon is written to the output file `horizon.dat`. This file can be consulted to examine the evolution of the acoustic pressure and the acoustic (velocity) potential at the sonic horizon.



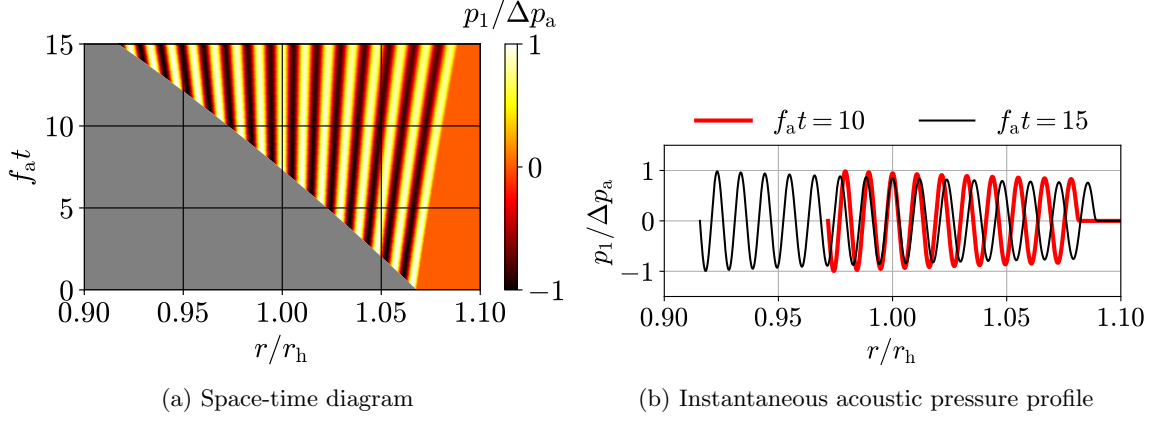


Figure 4.8: Example of an acoustic black hole.

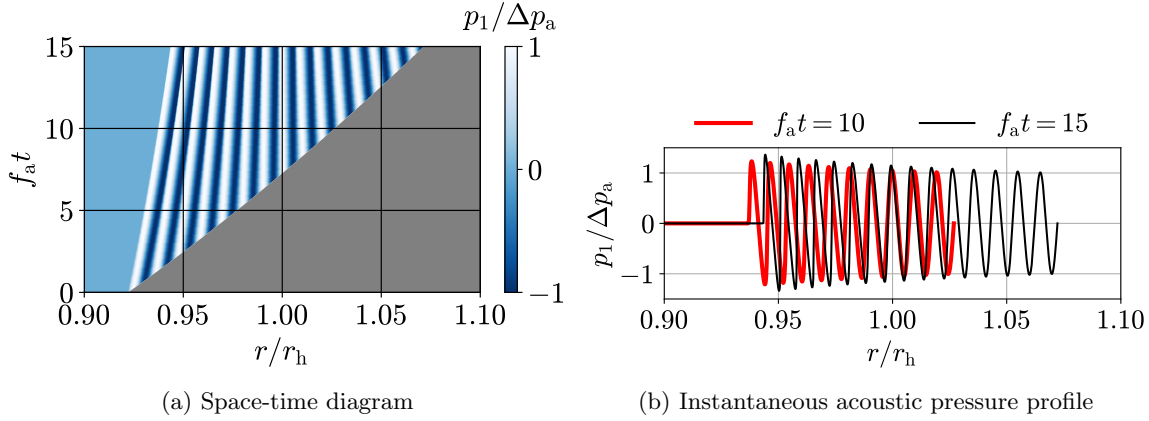


Figure 4.9: Example of an acoustic white hole.

Fig. 4.9 exemplarily shows (a) the space-time diagram and (b) the instantaneous acoustic pressure profiles for an acoustic white hole, which can be seen as the inverse problem of the acoustic black hole. This time, the entire physical domain is initially located inside the acoustic white hole. Subsequently, the wave emitting boundary expands and eventually passes the sonic horizon while emitting ingoing characteristics. The sonic horizon radius, the speed of sound, and the emitted wave frequency are the same as in Fig. 4.8. The settings to trap the same emitted wave period at the sonic horizon as in the acoustic black hole configuration are as follows:

```
BOUNDARYMOTION
BoundaryMotionType stationaryWhiteHole
InitialMovingBoundaryPosition 1.3824
FixedBoundaryPosition 1.2359
```

Furthermore, Fig. 4.9 shows the results for the nonlinear wave, which exhibits the well-known nonlinear wave-steepening. The settings to achieve the nonlinear wave propagation behavior, in this particular case dominated by the constitutive nonlinearity represented by the nonlinearity coefficient  $\beta$  (FluidNonLinearity), are:

```
FluidNonLinearity 3.5
LocalNonlinearity True
```

In the acoustic white hole in Fig. 4.9, the characteristics converge towards the sonic horizon so that the acoustic wave is progressively blue-shifted while the acoustic wave amplitude increases over time.

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