

# Week 9\_Francesca Aiuti

## Task 1

Use a weather forecast website utilizing the psychrometric chart and the formula we went through in class to determine the absolute humidity, the wet-bulb temperature and the mass of water vapour in the air in classroom A of Piacenza campus at the moment you are solving the exercise (providing the inputs you utilized).

Umidità: Relative humidity; Pressione atmosferica: Air total pressure (1 hPa: 0.1 kPa); Temperatura effettiva: Temperature to be utilized.

Il tempo oggi in Piacenza Lunedì, 02 Dicembre 2019						
	13:00	14:00	16:00	18:00	20:00	21:00
Temperatura effettiva	10°C	10°C	9°C	6°C	7°C	7°C
Temperatura percepita	10°C	10°C	8°C	5°C	7°C	6°C
Precipitazioni	0 mm	0 mm	0 mm	0 mm	0 mm	0 mm
Umidità	79 %	77 %	89 %	90 %	90 %	91 %
Pressione atmosferica	1016 hPa	1015 hPa	1016 hPa	1017 hPa	1019 hPa	1019 hPa

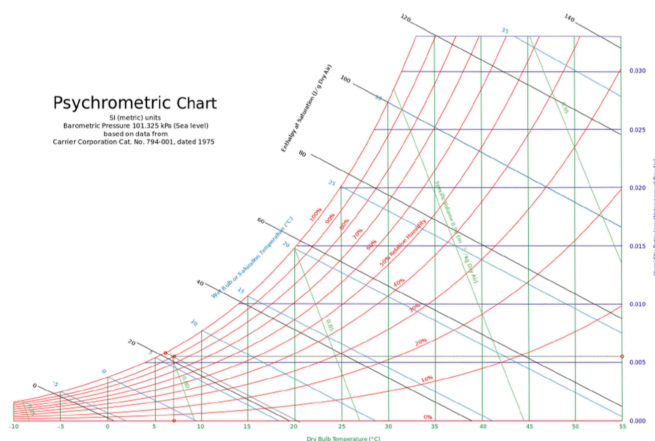
The time is 20.24, from the data given in the website

<https://www.meteo-oggi.it/italia/regione-emilia-romagna/tempo-piacenza/>

Umidità: 90%; Relative humidity:  $\phi = 90\%$ .

Pressione atmosferica: 1019 hPa; Air total pressure:  $P = 101.9 \text{ kPa}$ .

Temperatura effettiva: 7°C; Temperature:  $T = 230 \text{ K}$ .



Starting from the psychrometric chart, it is possible to see that the humidity ratio is  $\omega = 0.0055$ ;  
The web-bulb temperature is  $T_{wb} = 6^\circ\text{C}$ .

$$\omega = \frac{0.622Pv}{Pa} = \frac{0.622Pv}{P-Pv} = 0.0055, \text{ introducing } P = 101.9 \text{ kPa in the equation, } Pv = 0.893 \text{ kPa, } \phi = \frac{mv}{mg} = 90\%$$

Since for any ideal gas  $m =$

$\frac{PV}{RspT}$  and that during the class we were told for water vapor

$Rsp = 0.4615$ , we introduce the pressure of water vapour ( $Pv = 0.893$  kPa and we define the volume ( $V$ ) of aula A:

$$mv = 0.893 \frac{V}{0.4615 \cdot 230} = 8.41 \times 10^{-3} V$$

Then, we calculate the maximum water vapour  $mg$ :

$$mg = \frac{mv}{90\%} = 9.34 \times 10^{-3} V$$

## Task 2

Utilize the same methodology we went through in class and determine the sensible and latent load corresponding to internal gains, the ventilation and the infiltration in a house, with a good construction quality, and with the same geometry (height of 2.5 m, considering two occupants and one bed room, a conditioned floor area of 200 m<sup>2</sup> and a wall area of 144 m<sup>2</sup>, calculate the internal gains, infiltration and ventilation loads), as for the example located in Brindisi, Italy.

BRINDISI, Italy														WMO#: 163200				
Lat: 40.65N		Long: 17.95E		Elev: 10		StdP: 101.2		Time Zone: 1.00 (EUW)		Period: 86-10		WBAN: 99999						
Annual Heating and Humidification Design Conditions																		
Coldest Month	Heating DB		Humidification DPMCD and HR						Coldest month WSMCD				MCWS/PCWD to 99.6% DB					
	99.6%		99%		DP		HR		MCDB		WS		MCDB		MCWS		PCWD	
	(a)	(b)	(c)	(d)	(e)	(f)	(g)	(h)	(i)	(j)	(k)	(l)	(m)	(n)	(o)	(p)	(q)	
(1)	2	2.9	4.1	-5.1	2.5	7.2	-3.0	3.0	7.4	13.4	10.2	12.4	10.6	3.4	250			
Annual Cooling, Dehumidification, and Enthalpy Design Conditions																		
Hottest Month	Cooling DB/MCWB		Evaporation WBMCD						Evaporation WBMCD				MCWS/PCWD to 0.4% DB					
	0.4%		1%		2%		3%		4%		5%		6%		7%		8%	
	(a)	(b)	(c)	(d)	(e)	(f)	(g)	(h)	(i)	(j)	(k)	(l)	(m)	(n)	(o)	(p)	(q)	
(2)	8	7.1	32.8	23.6	31.1	24.3	29.9	24.3	27.2	29.7	26.3	29.0	25.6	28.3	4.2	180		
Dehumidification DPMCD and HR																		
Coldest Month	Cooling DB/MCWB		Evaporation WBMCD						Evaporation WBMCD				MCWS/PCWD to 0.4% DB					
	0.4%		1%		2%		3%		4%		5%		6%		7%		8%	
	(a)	(b)	(c)	(d)	(e)	(f)	(g)	(h)	(i)	(j)	(k)	(l)	(m)	(n)	(o)	(p)	(q)	
(3)	26.3	21.8	29.2	25.4	20.7	28.5	24.7	19.7	27.9	86.0	30.1	82.2	29.1	78.5	28.3	1236		
Extreme Annual Design Conditions																		
Extreme Annual WS			Extreme Annual DB			n-Year Return Period Values of Extreme DB												
			Max	Min	Mean	Standard deviation	Mean		Standard deviation		n=5 years		n=10 years		n=20 years		n=50 years	
			1%	2.5%	5%	WB	Min	Max	Min	Max	Min	Max	Min	Max	Min	Max	Min	Max
(4)			11.3	9.9	8.7	31.4	0.4	37.3	1.4	3.0	-0.6	39.4	-1.4	41.1	-2.2	42.8	-3.2	44.9

### 1) Internal gains

Calculating the sensible cooling load from internal gains:

$$q_{ig,s} = 136 + 2.2Acf + 22Noc = 136 + 2.2 \cdot 200 \cdot 22 \cdot 2 = 620 W$$

Calculating the latent cooling load from internal gains:

$$q_{ig,l} = 20 + 0.22Acf + 12Noc = 20 + 0.22 \cdot 200 + 12 \cdot 2 = 88 W$$

## 2) Infiltration

For a house with a good construction quality, we have the unit leakage area  $Aul = 1.4 \frac{cm^2}{m^2}$  and the exposed surface  $Aes = A_{wall} +$

$$A_{roof} = 200 + 144 = 344 m^2$$

Therefore, we have  $AL = Aes * Aul = 344 * 1.4 = 481.6 cm^2$

Defining the cooling temperature ( $T_{cooling} = 24^\circ C$ ) and the heating temperature ( $T_{heating} = 20^\circ C$ ) in Brindisi:

$$\Delta T_{cooling} = 31.1^\circ C - 24^\circ C = 7.1^\circ C = 7.1 K$$

$$\Delta T_{heating} = 20^\circ C - (-4.1^\circ C) = 24.1^\circ C = 24.1 K$$

$$DR = 7.1^\circ C = 7.1 K$$

Given the  $IDF_{heating} = 0.073 \frac{L}{s * cm^2}$  and  $IDF_{cooling} = 0.033 \frac{L}{s * cm^2}$ , we calculate the infiltration airflow rate:

$$Q_{i, heating} = AL * IDF_{heating} = 481.6 * 0.073 = 35.157 \frac{L}{s}$$

$$Q_{i, cooling} = AL * IDF_{cooling} = 481.6 * 0.033 = 15.893 \frac{L}{s}$$

The required minimum whole-building ventilation rate is:

$$Q_v = 0.05 A_{cf} + 3.5 (N_{br} + 1) = 0.05 * 200 + 3.5 * (1 + 1) = 17 \frac{L}{s}$$

$$\text{Therefore, } Q_{i-v, heating} = Q_{i, heating} + Q_v = 35.157 + 17 = 52.157 \frac{L}{s}$$

$$Q_{i-v, cooling} = Q_{i, cooling} + Q_v = 15.893 + 17 = 32.893 \frac{L}{s}$$

Given that  $C_{sensible} = 1.23$ ,  $C_{latent} = 3010$ ,  $\Delta \omega_{cooling} = 0.0039$ :

$$q_{inf-ventilationcoolingsensible} = C_{sensible} Q_{i-v, cooling} \Delta T_{cooling} = 1.23 * 32.893 * 7.1 = 287.25 W$$

$$q_{inf-ventilationcoolinglatent} = C_{latent} Q_{i-v, cooling} \Delta \omega_{cooling} = 3010 * 32.893 * 0.0039 = 386.13 W$$

$$q_{inf-ventilationheatingsensible} = C_{sensible} Q_{i-v, heating} \Delta T_{heating} = 1.23 * 52.157 * 24.1 = 1546.09 W$$