

Week 7_Francesca Aiuti

Sunday, 8 December 2019

16:32

Task 1

Use a weather forecast website utilizing the psychrometric chart and the formula we went through in class to determine the absolute humidity, the wet-bulb temperature and the mass of water vapour in the air in classroom A of Piacenza campus at the moment you are solving the exercise (providing the inputs you utilized).

Umidità: Relative humidity; Pressione atmosferica: Air total pressure (1 hPa: 0.1 kPa); Temperatura effettiva: Temperature to be utilized.

Il tempo oggi in Piacenza Lunedì, 02 Dicembre 2019						
	13:00	14:00	16:00	18:00	20:00	21:00
Temperatura effettiva	10°C	10°C	9°C	6°C	7°C	7°C
Temperatura percepita	10°C	10°C	8°C	5°C	7°C	6°C
Precipitazioni	0 mm	0 mm	0 mm	0 mm	0 mm	0 mm
Umidità	79 %	77 %	89 %	90 %	90 %	91 %
Pressione atmosferica	1016 hPa	1015 hPa	1016 hPa	1017 hPa	1019 hPa	1019 hPa

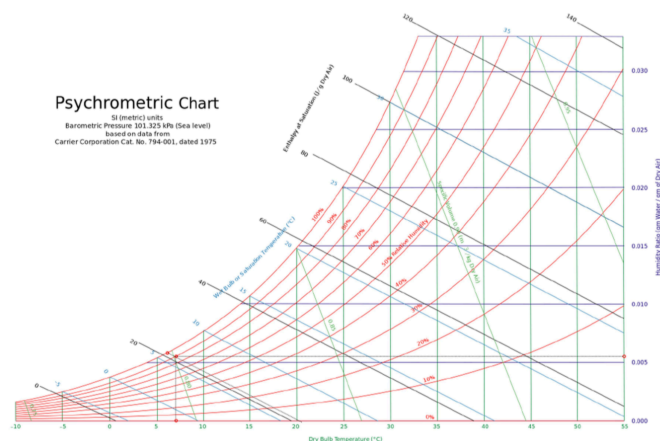
The time is 20.24, from the data given in the website

<https://www.meteo-oggi.it/italia/regione-emilia-romagna/tempo-piacenza/>

Umidità: 90%; Relative humidity: $\phi = 90\%$.

Pressione atmosferica: 1019 hPa; Air total pressure: $P = 101.9 \text{ kPa}$.

Temperatura effettiva: 7°C; Temperature: $T = 230 \text{ K}$.



Starting from the psychrometric chart, it is possible to see that the humidity ratio is $\omega = 0.0055$;
The wet-bulb temperature is $T_{wb} = 6^\circ\text{C}$.

$$\omega = \frac{0.622P_v}{P_a} = \frac{0.622P_v}{P - P_v} = 0.0055, \text{ introducing } P = 101.9 \text{ kPa in the equation, } P_v = 0.893 \text{ kPa, } \phi = \frac{mv}{mg} = 90\%$$

Since for any ideal gas $m = \frac{PV}{RspT}$ and that during the class we were told for water vapor $Rsp = 0.4615$, we introduce the pressure of water vapour ($P_v = 0.893$ kPa) and we define the volume (V) of aula A:

$$mv = 0.893 \frac{V}{0.4615 \cdot 273} = 8.41 \times 10^{-3} V$$

Then, we calculate the maximum water vapour mg :

$$mg = \frac{mv}{90\%} = 9.34 \times 10^{-3} V$$

Task 2

Utilize the same methodology we went through in class and determine the sensible and latent load corresponding to internal gains, the ventilation and the infiltration in a house, with a good construction quality, and with the same geometry (height of 2.5 m, considering two occupants and one bed room, a conditioned floor area of 200 m² and a wall area of 144 m², calculate the internal gains, infiltration and ventilation loads), as for the example located in Brindisi, Italy.

BRINDISI, Italy														WMO#: 163200		
Lat: 40.65N		Long: 17.95E		Elev: 10		StdP: 101.2		Time Zone: 1.00 (EUW)		Period: 86-10		WBAN: 99999				
Annual Heating and Humidification Design Conditions																
Coldest Month	Heating DB		Humidification DPMCD and HR						Coldest month WSMCD				MCWS/PCWD to 99.6% DB			
	99.6%	99%	DP	HR	MCDB	DP	HR	MCDB	WS	MCDB	WS	MCDB	MCWS	PCWD		
	(a)	(b)	(c)	(d)	(e)	(f)	(g)	(h)	(i)	(j)	(k)	(l)	(m)	(n)		
(1)	2	2.9	4.1	-5.1	2.5	7.2	-3.0	3.0	7.4	13.4	10.2	12.4	10.6	3.4	250	
Annual Cooling, Dehumidification, and Enthalpy Design Conditions																
Hottest Month	Cooling DB/MCWB		Evaporation WSMCD						Evaporation WSMCD				MCWS/PCWD to 0.4% DB			
	0.4%	1%	2%	0.4%	1%	2%	0.4%	1%	2%	0.4%	1%	2%	0.4%	1%		
	(a)	(b)	(c)	(d)	(e)	(f)	(g)	(h)	(i)	(j)	(k)	(l)	(m)	(n)		
(2)	8	7.1	32.8	23.6	31.1	24.3	29.9	24.3	27.2	29.7	26.3	29.0	25.6	28.3	4.2	180
Dehumidification DPMCD and HR																
Coldest Month	Heating DB		Humidification DPMCD and HR						Enthalpy/MCDB				Hours 8 to 6 & 12 to 6			
	0.4%	1%	2%	0.4%	1%	2%	0.4%	1%	2%	0.4%	1%	2%	0.4%	1%		
	(a)	(b)	(c)	(d)	(e)	(f)	(g)	(h)	(i)	(j)	(k)	(l)	(m)	(n)		
(3)	26.3	21.8	29.2	25.4	20.7	28.5	24.7	19.7	27.9	86.0	30.1	82.2	29.1	78.5	28.3	1236
Extreme Annual Design Conditions																
Extreme Annual WS			Extreme Annual DB				n-Year Return Period Values of Extreme DB									
	1%	2.5%	5%	Mean	Standard deviation	min	max	min	max	min	max	min	max	min	max	
(4)	(a)	(b)	(c)	(d)	(e)	(f)	(g)	(h)	(i)	(j)	(k)	(l)	(m)	(n)	(o)	
	11.3	9.9	8.7	31.4	0.4	37.3	1.4	3.0	-0.6	39.4	-1.4	41.1	-2.2	42.8	-3.2	44.9

1) Internal gains

Calculating the sensible cooling load from internal gains:

$$q_{ig,s} = 136 + 2.2Acf + 22Noc = 136 + 2.2 \cdot 200 \cdot 22 \cdot 2 = 620 \text{ W}$$

Calculating the latent cooling load from internal gains:

$$q_{ig,l} = 20 + 0.22Acf + 12Noc = 20 + 0.22 \cdot 200 + 12 \cdot 2 = 88 \text{ W}$$

2) Infiltration

For a house with a good construction quality, we have the unit leakage area $Aul = 1.4 \frac{cm^2}{m^2}$ and the exposed surface $Aes = Awall +$

$$Aroof = 200 + 144 = 344 m^2$$

$$\text{Therefore, we have } AL = Aes * Aul = 344 * 1.4 = 481.6 cm^2$$

Defining the cooling temperature ($T_{cooling} = 24^\circ C$) and the heating temperature ($T_{heating} = 20^\circ C$) in Brindisi:

$$\Delta T_{cooling} = 31.1^\circ C - 24^\circ C = 7.1^\circ C = 7.1 K$$

$$\Delta T_{heating} = 20^\circ C - (-4.1^\circ C) = 24.1^\circ C = 24.1 K$$

$$DR = 7.1^\circ C = 7.1 K$$

$$\text{Given the } IDF_{heating} = 0.073 \frac{L}{s * cm^2} \text{ and } IDF_{cooling} = 0.033$$

$\frac{L}{s * cm^2}$, we calculate the infiltration airflow rate:

$$Q_{i, heating} = AL * IDF_{heating} = 481.6 * 0.073 = 35.157 \frac{L}{s}$$

$$Q_{i, cooling} = AL * IDF_{cooling} = 481.6 * 0.033 = 15.893 \frac{L}{s}$$

The required minimum whole-building ventilation rate is:

$$Qv = 0.05Acf + 3.5 (Nbr + 1) = 0.05 * 200 + 3.5 * (1 + 1) = 17 \frac{L}{s}$$

$$\text{Therefore, } Q_{i - v, heating} = Q_{i, heating} + Qv = 35.157 + 17 = 52.157 \frac{L}{s}$$

$$Q_{i - v, cooling} = Q_{i, cooling} + Qv = 15.893 + 17 = 32.893 \frac{L}{s}$$

Given that $C_{sensible} = 1.23$, $Clatent = 3010$, $\Delta \omega_{cooling} = 0.0039$:

$$q_{inf - ventilationcoolingsensible} = C_{sensible} Q_{i - v, cooling} \Delta T_{cooling} = 1.23 * 32.893 * 7.1 = 287.25 W$$

$$q_{inf - ventilationcoolinglatent} = Clatent Q_{i - v, cooling} \Delta \omega_{cooling} = 3010 * 32.893 * 0.0039 = 386.13 W$$

$$q_{inf - ventilationheatingsensible} = C_{sensible} Q_{i - v, heating} \Delta T_{heating} = 1.23 * 52.157 * 24.1 = 1546.09 W$$