

Week 9_Francesca Aiuti

Sunday, 8 December 2019

16:32

Task 1

Use a weather forecast website utilizing the psychrometric chart and the formula we went through in class to determine the absolute humidity, the wet-bulb temperature and the mass of water vapour in the air in classroom A of Piacenza campus at the moment you are solving the exercise (providing the inputs you utilized).

Umidità: Relative humidity; Pressione atmosferica: Air total pressure (1 hPa: 0.1 kPa); Temperatura effettiva: Temperature to be utilized.

| Il tempo oggi in Piacenza Lunedì, 02 Dicembre 2019 | | | | | | |
|---|----------|----------|----------|----------|----------|----------|
| | 13:00 | 14:00 | 16:00 | 18:00 | 20:00 | 21:00 |
| | | | | | | |
| Temperatura effettiva | 10°C | 10°C | 9°C | 6°C | 7°C | 7°C |
| Temperatura percepita | 10°C | 10°C | 8°C | 5°C | 7°C | 6°C |
| Precipitazioni | 0 mm | 0 mm | 0 mm | 0 mm | 0 mm | 0 mm |
| Umidità | 79 % | 77 % | 89 % | 90 % | 90 % | 91 % |
| Pressione atmosferica | 1016 hPa | 1015 hPa | 1016 hPa | 1017 hPa | 1019 hPa | 1019 hPa |

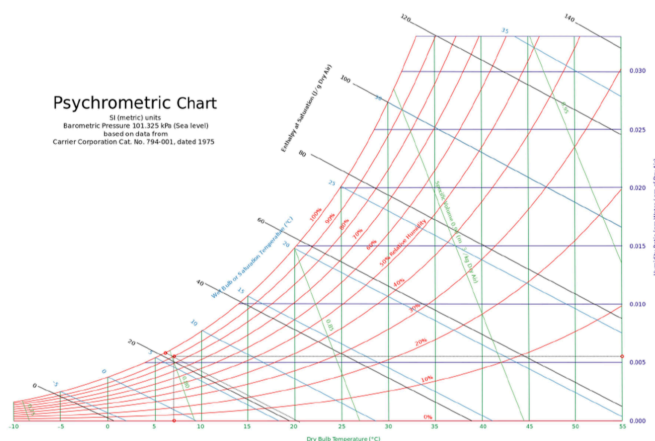
The time is 20.24, from the data given in the website

<https://www.meteo-oggi.it/italia/regione-emilia-romagna/tempo-piacenza/>

Umidità: 90%; Relative humidity: $\phi = 90\%$.

Pressione atmosferica: 1019 hPa; Air total pressure: $P = 101.9 \text{ kPa}$.

Temperatura effettiva: 7°C; Temperature: $T = 230 \text{ K}$.



Starting from the psychrometric chart, it is possible to see that the humidity ratio is $\omega = 0.0055$;
The web-bulb temperature is $T_{wb} = 6^\circ\text{C}$.

$$\omega = \frac{0.622Pv}{Pa} = \frac{0.622Pv}{P-Pv} = 0.0055, \text{ introducing } P = 101.9 \text{ kPa in the equation, } Pv = 0.893 \text{ kPa, } \phi = \frac{mv}{mg} = 90\%$$

Since for any ideal gas $m = \frac{PV}{RspT}$ and that during the class we were told for water vapor $Rsp = 0.4615$, we introduce the pressure of water vapour ($Pv = 0.893$ kPa and we define the volume (V) of aula A:

$$mv = 0.893 \frac{V}{0.4615 \cdot 230} = 8.41 \times 10^{-3} V$$

Then, we calculate the maximum water vapour mg:

$$mg = \frac{mv}{90\%} = 9.34 \times 10^{-3} V$$

Task 2

Utilize the same methodology we went through in class and determine the sensible and latent load corresponding to internal gains, the ventilation and the infiltration in a house, with a good construction quality, and with the same geometry (height of 2.5 m, considering two occupants and one bed room, a conditioned floor area of 200 m² and a wall area of 144 m², calculate the internal gains, infiltration and ventilation loads), as for the example located in Brindisi, Italy.

| BRINDISI, Italy | | | | | | | | | | | | | | | WMO#: 163200 | |
|--|-------------------|-------------------------------|------|-----------------------------|--------------------|-------------|------|---|------|---------------------|------|-------------|------|-----------------------------|--------------|------|
| Lat: 40.65N | | Long: 17.95E | | Elev: 10 | | StdP: 101.2 | | Time Zone: 1.00 (EUV) | | Period: 86-10 | | WBAN: 99999 | | | | |
| Annual Heating and Humidification Design Conditions | | | | | | | | | | | | | | | | |
| (1) | Coldest Month | Heating DB | | Humidification DPMCD and HR | | | | | | Coldest month WSMCD | | | | MCWS/PCWD to 99.6% DB | | |
| | | 99.6% | 99% | DP | HR | MCDB | DP | HR | MCDB | WS | MCDB | WS | MCDB | MCWS | PCWD | |
| | | (a) | (b) | (c) | (d) | (e) | (f) | (g) | (h) | (i) | (j) | (k) | (l) | (m) | (n) | (o) |
| | 2 | 2.9 | 4.1 | -5.1 | 2.5 | 7.2 | -3.0 | 3.0 | 7.4 | 13.4 | 10.2 | 12.4 | 10.6 | 3.4 | 250 | |
| Annual Cooling, Dehumidification, and Enthalpy Design Conditions | | | | | | | | | | | | | | | | |
| (2) | Hottest Month | Cooling DB/MCWB | | Evaporation WBMCD | | | | | | Evaporation WBMCD | | | | MCWS/PCWD to 0.4% DB | | |
| | | 0.4% | 1% | 2% | DB | MCWB | DB | MCWB | WB | MCDB | WB | MCDB | WB | MCDB | MCWS | PCWD |
| | | (a) | (b) | (c) | (d) | (e) | (f) | (g) | (h) | (i) | (j) | (k) | (l) | (m) | (n) | (o) |
| | 8 | 7.1 | 32.8 | 23.6 | 31.1 | 24.3 | 29.9 | 24.3 | 27.2 | 29.7 | 26.3 | 29.0 | 25.6 | 28.3 | 4.2 | 180 |
| (3) | | Dehumidification DPMCD and HR | | | | | | Enthalpy MCD | | | | | | Hours 8 to 4 & 12 to 8/20.6 | | |
| | | 0.4% | 1% | 2% | DP | HR | MCDB | DP | HR | MCDB | Enth | MCDB | Enth | MCDB | Enth | |
| | | (a) | (b) | (c) | (d) | (e) | (f) | (g) | (h) | (i) | (j) | (k) | (l) | (m) | (n) | (o) |
| | 26.3 | 21.8 | 29.2 | 25.4 | 20.7 | 28.5 | 24.7 | 19.7 | 27.9 | 86.0 | 30.1 | 82.2 | 29.1 | 78.5 | 28.3 | 1236 |
| Extreme Annual Design Conditions | | | | | | | | | | | | | | | | |
| (4) | Extreme Annual WS | | | Extreme Annual DB | | | | n-Year Return Period Values of Extreme DB | | | | | | | | |
| | | | | Mean | Standard deviation | | | n=5 years | | n=10 years | | n=20 years | | n=50 years | | |
| | 1% | 2.5% | 5% | Min | Max | Min | Max | Min | Max | Min | Max | Min | Max | Min | Max | |
| | (a) | (b) | (c) | (d) | (e) | (f) | (g) | (h) | (i) | (j) | (k) | (l) | (m) | (n) | (o) | (p) |
| | 11.3 | 9.9 | 8.7 | 31.4 | 0.4 | 37.3 | 1.4 | 3.0 | -0.6 | 39.4 | -1.4 | 41.1 | -2.2 | 42.8 | -3.2 | 44.9 |

1) Internal gains

Calculating the sensible cooling load from internal gains:

$$q_{ig,s} = 136 + 2.2Acf + 22Noc = 136 + 2.2 \cdot 200 \cdot 22 \cdot 2 = 620 \text{ W}$$

Calculating the latent cooling load from internal gains:

$$q_{ig,l} = 20 + 0.22Acf + 12Noc = 20 + 0.22 \cdot 200 + 12 \cdot 2 = 88 \text{ W}$$

2) Infiltration

For a house with a good construction quality, we have the unit leakage area $Aul = 1.4 \frac{cm^2}{m^2}$ and the exposed surface $Aes = A_{wall} +$

$$A_{roof} = 200 + 144 = 344 m^2$$

$$\text{Therefore, we have } AL = Aes * Aul = 344 * 1.4 = 481.6 cm^2$$

Defining the cooling temperature ($T_{cooling} = 24^\circ C$) and the heating temperature ($T_{heating} = 20^\circ C$) in Brindisi:

$$\Delta T_{cooling} = 31.1^\circ C - 24^\circ C = 7.1^\circ C = 7.1 K$$

$$\Delta T_{heating} = 20^\circ C - (-4.1^\circ C) = 24.1^\circ C = 24.1 K$$

$$DR = 7.1^\circ C = 7.1 K$$

$$\text{Given the } IDF_{heating} = 0.073 \frac{L}{s * cm^2} \text{ and } IDF_{cooling} = 0.033$$

$\frac{L}{s * cm^2}$, we calculate the infiltration airflow rate:

$$Q_{i, heating} = AL * IDF_{heating} = 481.6 * 0.073 = 35.157 \frac{L}{s}$$

$$Q_{i, cooling} = AL * IDF_{cooling} = 481.6 * 0.033 = 15.893 \frac{L}{s}$$

The required minimum whole-building ventilation rate is:

$$Q_v = 0.05 A_{cf} + 3.5 (N_{br} + 1) = 0.05 * 200 + 3.5 * (1 + 1) = 17 \frac{L}{s}$$

$$\text{Therefore, } Q_{i-v, heating} = Q_{i, heating} + Q_v = 35.157 + 17 = 52.157 \frac{L}{s}$$

$$Q_{i-v, cooling} = Q_{i, cooling} + Q_v = 15.893 + 17 = 32.893 \frac{L}{s}$$

Given that $C_{sensible} = 1.23$, $C_{latent} = 3010$, $\Delta \omega_{cooling} = 0.0039$:

$$q_{inf-ventilationcoolingsensible} = C_{sensible} Q_{i-v, cooling} \Delta T_{cooling} = 1.23 * 32.893 * 7.1 = 287.25 W$$

$$q_{inf-ventilationcoolinglatent} = C_{latent} Q_{i-v, cooling} \Delta \omega_{cooling} = 3010 * 32.893 * 0.0039 = 386.13 W$$

$$q_{inf-ventilationheatingsensible} = C_{sensible} Q_{i-v, heating} \Delta T_{heating} = 1.23 * 52.157 * 24.1 = 1546.09 W$$