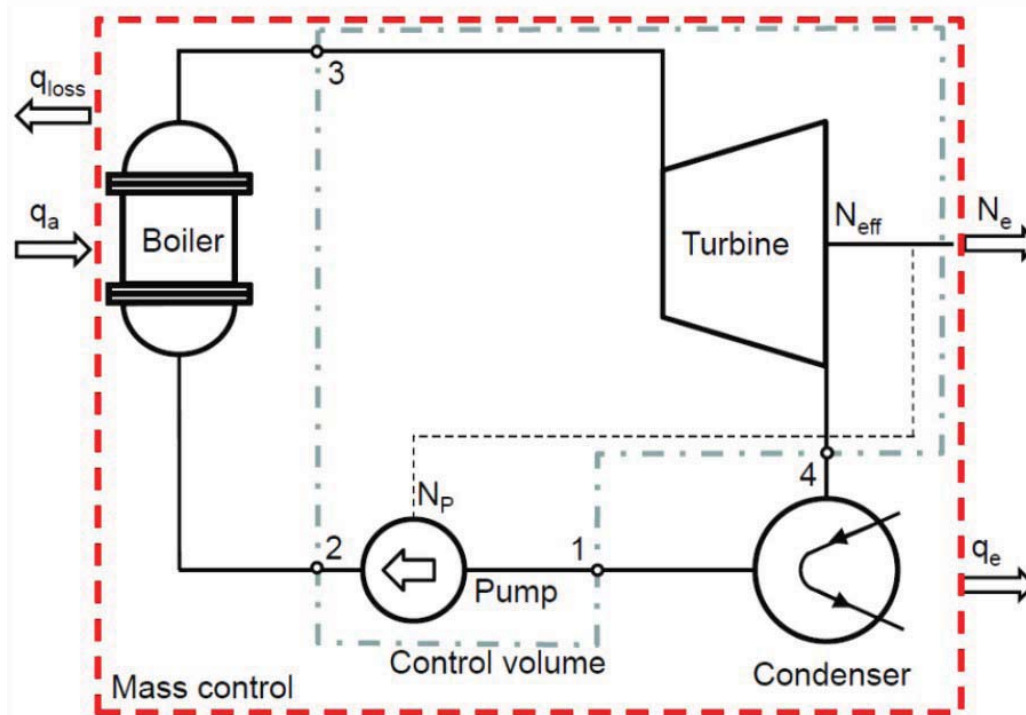


SH2706  
Sustainable Energy Transformation Technologies  
Exercise Session 01

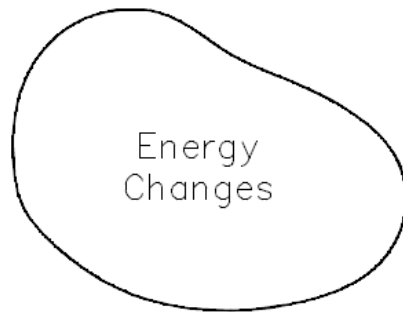
## E01\_P01

- Applying the control mass system as shown in the figure, calculate the added thermal power  $q_a$ .
  - The net shaft power extracted from the system is  $N_e = 1$  MW.
  - The thermal power extracted in the condenser is equal to 65% of  $q_a$ .
  - Assume thermal losses  $q_{\text{loss}} = 1.5\%$  of  $q_a$ .

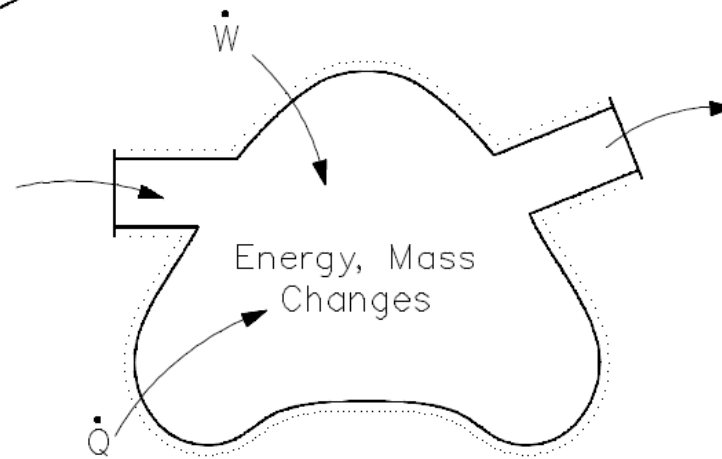
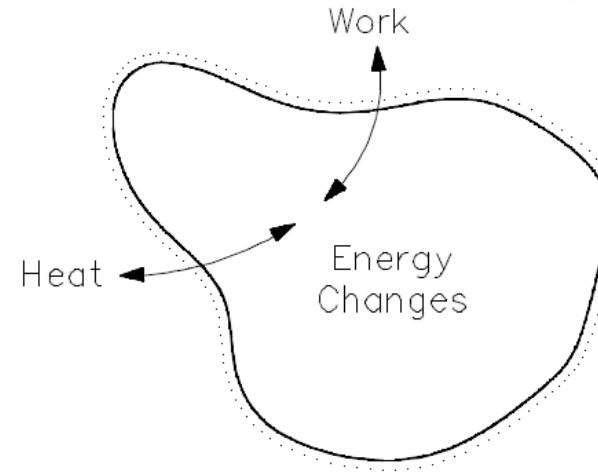


# Thermodynamic systems

Isolated system



Control mass (closed system)



Control Volume (open system)

# Control Mass Formulation (7)

- Frequently the energy equation is expressed in terms of the specific total energy, that is the total energy per unit mass,  $e_T = E_T/m$ , where  $e_T = e_I + e_K + e_P$ :

$$\frac{dE_T}{dt} = \frac{d}{dt} \left[ m(e_I + e_K + e_P) \right] = q - N_{shaft} - N_{normal} - N_{shear}$$

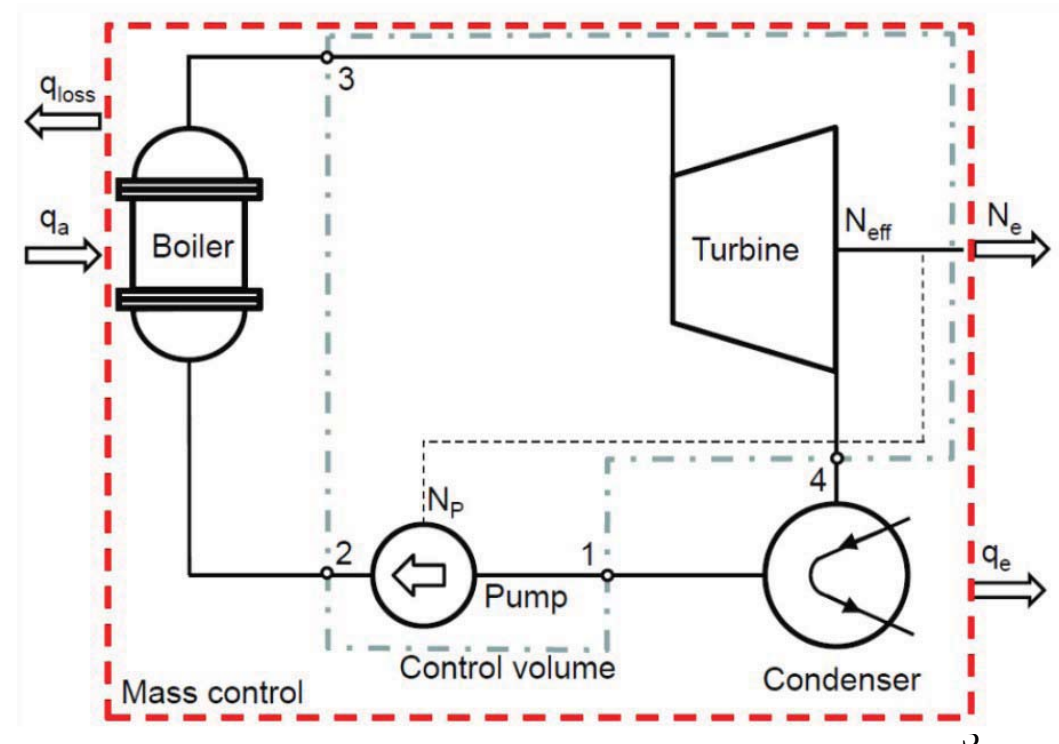
- we should note that  $e_I$  is the specific internal energy,  $e_K = U^2/2$  – is the specific kinetic energy and  $e_P = gh$  – is the specific potential energy

## E01\_P01

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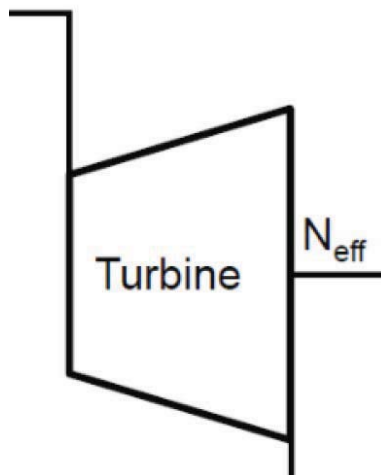
Solution

- First law:  $dE = Q - L$
- $0 = (q_a - q_e - q_{\text{loss}}) - N_e \quad (1)$
- $q_e = 0.65 \cdot q_a \quad (2)$
- $q_{\text{loss}} = 0.015 \cdot q_a \quad (3)$
- $q_a = 2.985 \text{ MW}$



## E01\_P02

- A steam turbine operates at steady-state conditions and delivers effective (shaft) power  $N_{\text{eff}} = 423 \text{ MW}$ .
- Steam mass flow rate through the turbine is  $\dot{W} = 500 \text{ kg/s}$ .
- The inlet specific enthalpy and the mean velocity of the steam are  $i_{\text{in}} = 2770 \text{ kJ/kg}$  and  $U_{\text{in}} = 90 \text{ m/s}$ , respectively.
- The corresponding parameters for steam at the outlet are  $i_{\text{out}} = 1900 \text{ kJ/kg}$  and  $U_{\text{out}} = 230 \text{ m/s}$ .
- Neglect potential energy of the steam streams.
- Calculate the turbine heat losses to the surroundings.



# Control Volume Formulation (4)

- Thus the total energy change of the system is

$$\frac{dE_T}{dt} = e_T W - (-pW / \rho) = (e_T + p/\rho) W = W (e_I + p/\rho + e_K + e_P)$$

- since the specific enthalpy is  $i = e_I + p/\rho$  we can write

$$\frac{dE_T}{dt} = W (i + e_K + e_P)$$

- and the energy conservation equation becomes

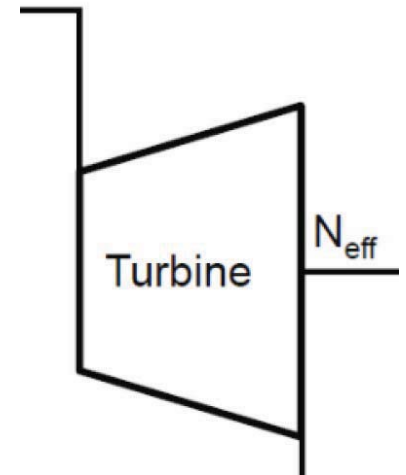
$$\frac{dE_T}{dt} = q - N_{shaft} - N_{normal} - N_{shear} + \sum_{j \in in} (i + e_P + e_K)_j W_j - \sum_{k \in out} (i + e_P + e_K)_k W_k$$

## E01\_P02

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Solution

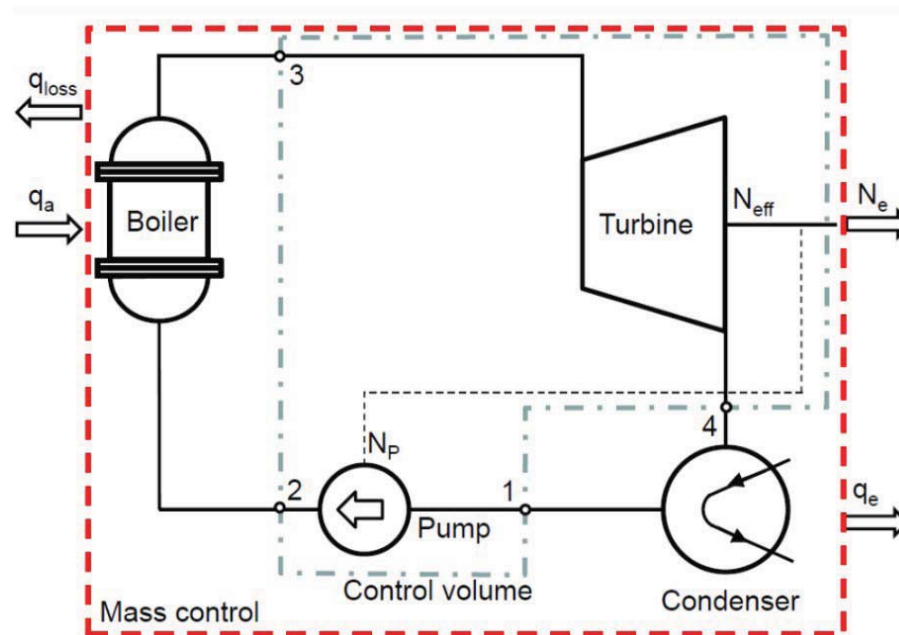
- $de = q - N + W \cdot d(i + k_e + p_e)$
- $0 = 0 - q_{\text{loss}} - N_{\text{eff}} + W \cdot (i_{\text{in}} + U_{\text{in}}^2/2 - i_{\text{out}} - U_{\text{out}}^2/2)$
- $q_{\text{loss}} = 800 \text{ kW}$





## E01\_P03

- A thermodynamic system is shown in the figure. Calculate the thermal power that is extracted in a condenser  $q_e$ .
  - The specific enthalpy of steam at the inlet to the turbine is  $i_3=3130$  kJ/kg and its mass flow rate is  $W_3 = 10$  kg/s.
  - Specific enthalpy after isentropic expansion in the turbine is  $i_{4s}=2710$  kJ/kg .
  - The turbine internal efficiency is  $\eta_i = 0.75$  and its mechanical efficiency is  $\eta_m = 0.95$ . The system energy efficiency is  $\eta_E = 0.38$ .
  - Assume  $q_{\text{loss}} = 0.01 q_a$  and pumping power  $N_p = q_{\text{loss}}$ .



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  - Assume  $q_{loss} = 0.01 q_a$  and pumping power  $N_p = q_{loss}$ .

– Solution

–  $dE = Q - L$

–  $0 = q_a - q_{loss} - q_e - N_e \quad (1)$

–  $N_{th} = W_3^*(i_3 - i_{4s}) \quad (2)$

–  $N_{eff} = N_{th} * \eta_i * \eta_m \quad (3)$

–  $N_e = N_{eff} - N_p \quad (4)$

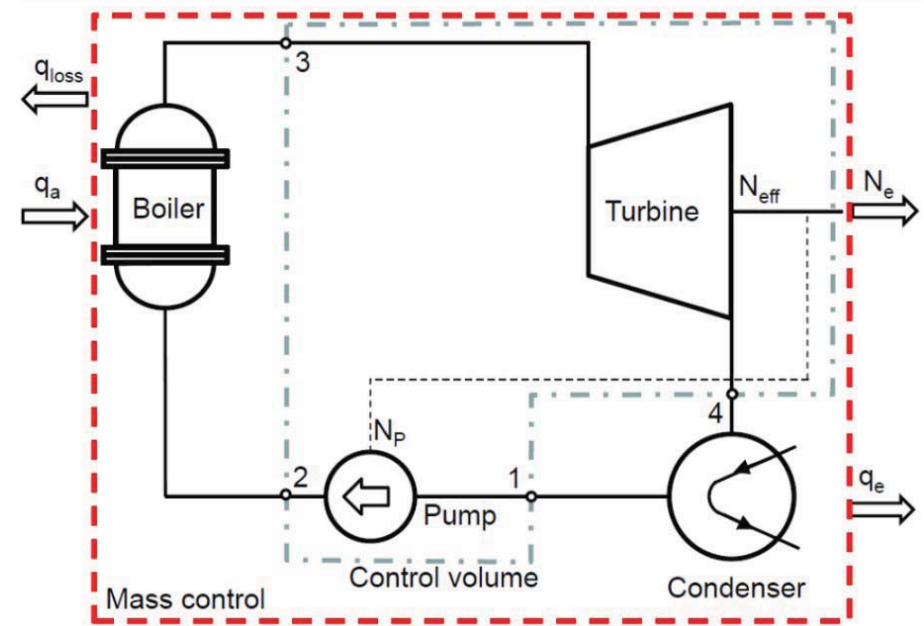
–  $q_{loss} = 0.01 * q_a \quad (5)$

–  $N_p = q_{loss} \quad (6)$

–  $N_e / q_a = \eta_E \quad (7)$

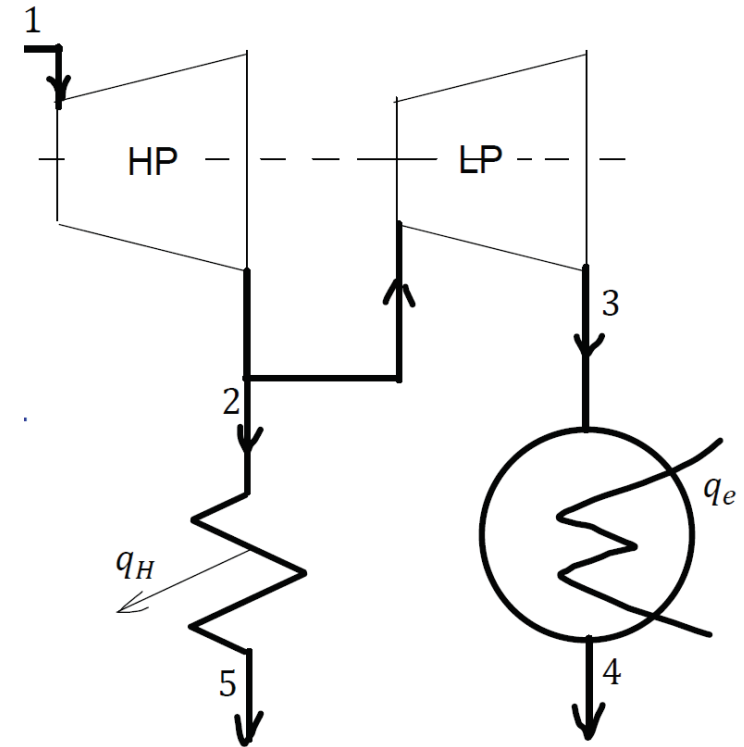
$q_e = 4.68$  MW

(7 unknowns:  $q_a, q_{loss}, q_e, N_e, N_{th}, N_{eff}, N_p$ )



## E01\_P04

- Superheated steam with specific enthalpy  $i_1$  flows into high-pressure turbine which has internal efficiency  $\eta_{iHP}$ . The isentropic expansion enthalpy is  $i_{2s}$ .
- After leaving the turbine, the steam is partly used for heating with thermal power  $q_H$  at temperature  $T_H$ , and the rest is feeding the low pressure turbine, which has internal efficiency  $\eta_{iLP}$ . The isentropic expansion enthalpy is  $i_{3s}$ .
- The exit specific enthalpy and entropy of bleeding steam are  $i_5$  and  $s_5$ .
- Condensate leaving the condenser has a specific enthalpy  $i_4$  and the specific entropy  $s_4$ .
- The total internal power of turbines is  $N_i$ .
- Heat is extracted in the condenser at temperature  $T_{amb}$ .
- Ambient steam specific enthalpy and entropy are  $i_{amb}$  and  $s_{amb}$ .
- Calculate the total exergy loss in the system.



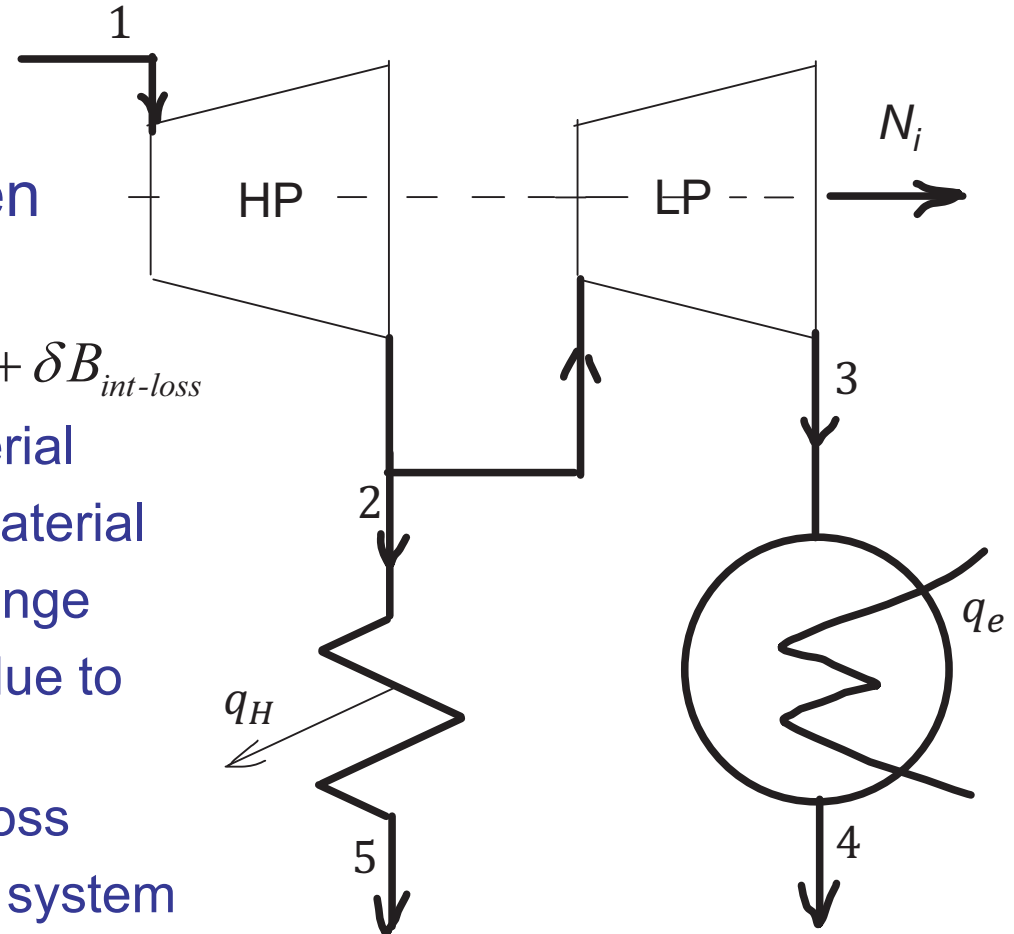
- $i_{amb} = 62.3 \text{ kJ/kg}$ ;  $s_{amb} = 0.222 \text{ kJ/kg/K}$ ;  $T_{amb} = 288\text{K}$ ;
- $i_1 = 3130 \text{ kJ/kg}$ ;  $s_1 = 7.125 \text{ kJ/kg/K}$ ;
- $i_4 = 116.6 \text{ kJ/kg}$ ;  $s_4 = 0.406 \text{ kJ/kg/K}$ ;
- $i_5 = 292.4 \text{ kJ/kg}$ ;  $s_5 = 0.953 \text{ kJ/kg/K}$ ;
- $i_{2s} = 2710 \text{ kJ/kg}$ ;
- $i_{3s} = 2245 \text{ kJ/kg}$ ;
- $N_i = 5 \text{ MW}$ ;
- $\eta_{iHP} = 0.76$ ;  $\eta_{iLP} = 0.79$ ;
- $q_H = 1.4 \text{ MW}$ ;  $T_H = 333\text{K}$ ;

# Exergy (10)

- The general rule for the exergy balance in an open system is as follows

$$B_a = \Delta B_{sys} + B_e + L + \Delta B_{sources} + \delta B_{int-loss}$$

- $B_a$  – exergy of added material
- $B_e$  – exergy of extracted material
- $\Delta B_{sys}$  – system exergy change
- $\Delta B_{source}$  – exergy change due to heat sources/sinks
- $\delta B_{int-loss}$  – internal exergy loss
- $L$  – work performed by the system

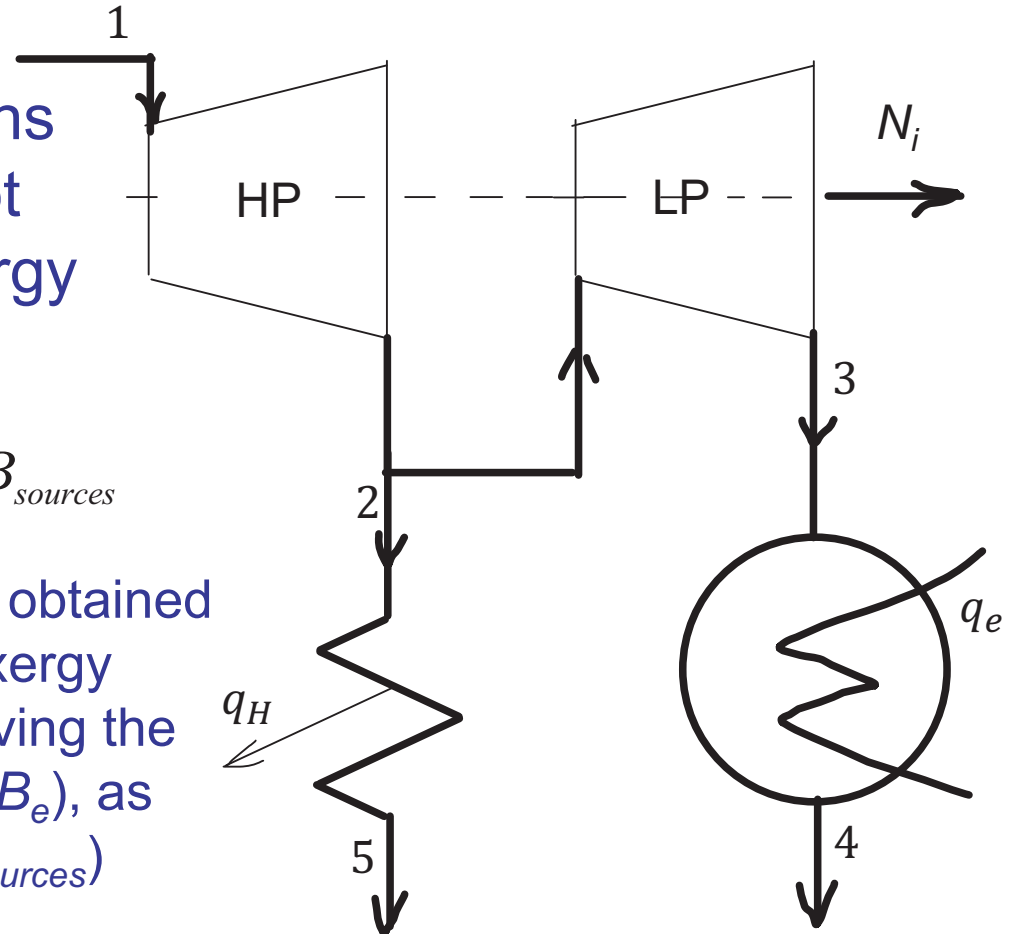


# Exergy (11)

- For steady-state conditions the system exergy will not change, and internal exergy losses can be found as

$$\delta B_{int-loss} = B_a - B_e - L - \Delta B_{sources}$$

- thus the exergy losses are obtained as a difference between exergy added ( $B_a$ ) and exergy leaving the system with working fluid ( $B_e$ ), as work ( $L$ ) and as heat ( $\Delta B_{sources}$ )



# Exergy (12)

- Expressed as time-rate loss of exergy, we have

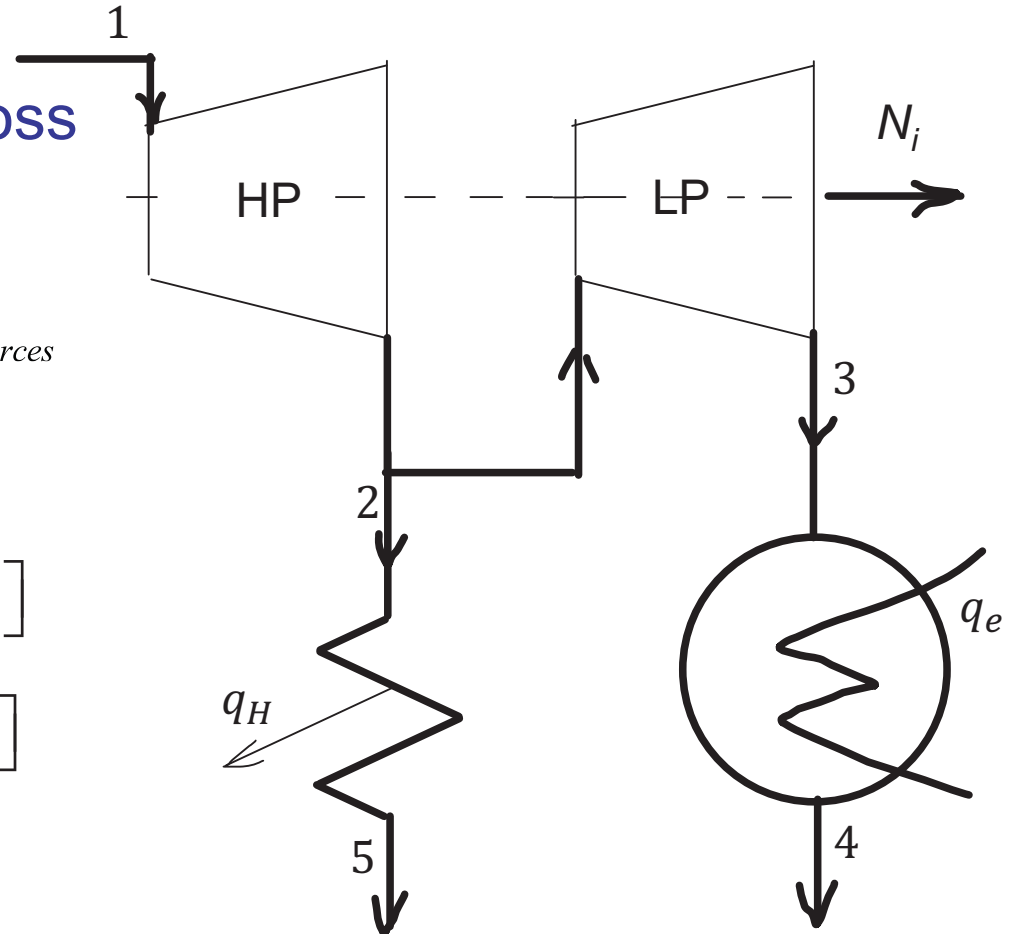
$$\delta \dot{B}_{int-loss} = \dot{B}_a - \dot{B}_e - N - \Delta \dot{B}_{sources}$$

- where

$$\dot{B}_a = W_a \left[ i_a - i_0 - T_0 (s_a - s_0) \right]$$

$$\dot{B}_e = W_e \left[ i_e - i_0 - T_0 (s_e - s_0) \right]$$

$$\Delta \dot{B}_{sources} = q_{sources} \frac{T_{sources} - T_0}{T_{sources}}$$



# E01\_P04

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- The total internal power of turbines is  $N_i$ .
- Heat is extracted in the condenser at temperature  $T_{amb}$ .
- Ambient steam specific enthalpy and entropy are  $i_{amb}$  and  $s_{amb}$ .
- Calculate the total exergy loss in the system.

## Solution

- $B_{loss} = B_a - B_e - N - dB_{sources}$
- $B = W \cdot (i - i_{amb} - T_{amb} \cdot (s - s_{amb}))$  for point 1, 4, 5
- $dB_{sources} = q \cdot (T - T_{amb}) / T$  for  $q_H$  and  $q_e$

- $W_1 = W_2 + W_3$  (1)
  - $q_H = W_2 \cdot (i_2 - i_5)$  (2)
  - $\eta_{iHP} = (i_1 - i_2) / (i_1 - i_{2s})$  (3)
  - $\eta_{iLP} = (i_2 - i_3) / (i_2 - i_{3s})$  (4)
  - $N_i = W_1 \cdot (i_1 - i_2) + W_3 \cdot (i_2 - i_3)$  (5)
- (5 unknowns:  $W_1, W_2, W_3, i_2, i_3$ )

- $W_1 = 6.85 \text{ kg/s}$   $W_2 = 0.556 \text{ kg/s}$

- $B_{loss} = 2.187 \text{ MW}$

