

4CM00: Control Engineering

FeedForward control

Dr.ir. Gert Witvoet



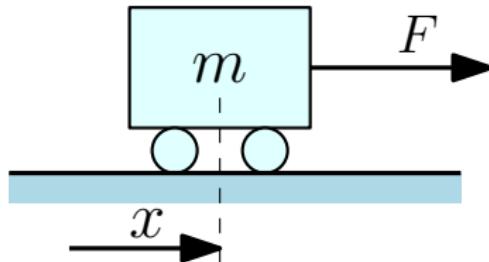
TU/e

Technische Universiteit
Eindhoven
University of Technology

September 2020

Where innovation starts

Consider a simple motion system



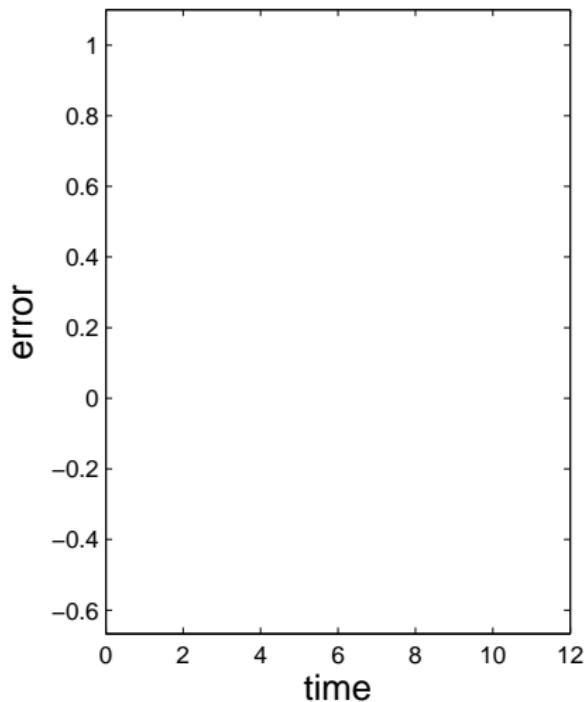
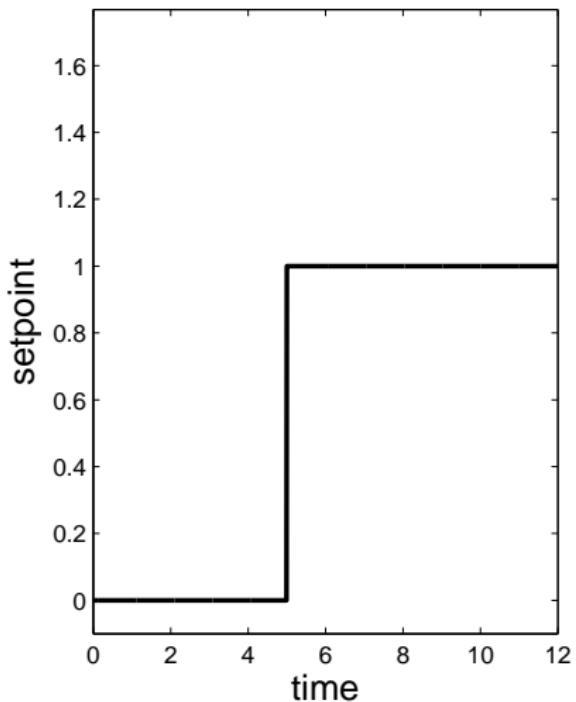
Objective: Move the mass move from position 0 to 1

Question 1: How does the error depend on the setpoint trajectory x_s ?
I.e. how do we get from 0 to 1?

Question 2: Can we obtain (nearly) perfect tracking using just a simple PD-controller?

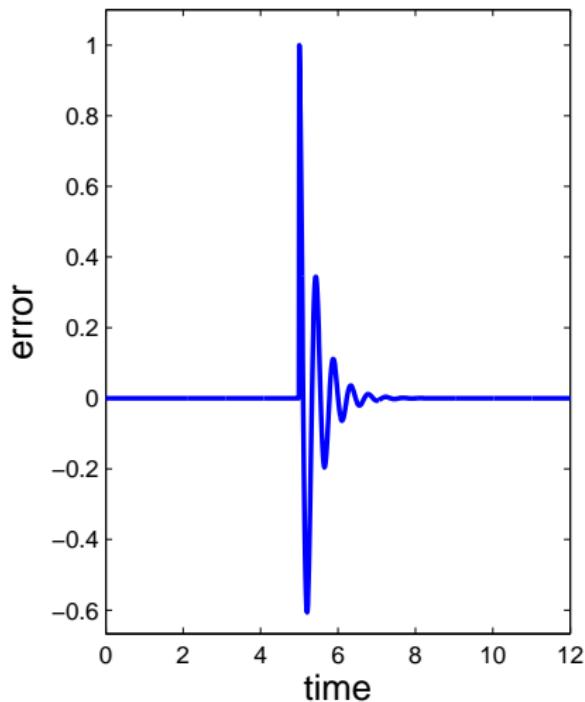
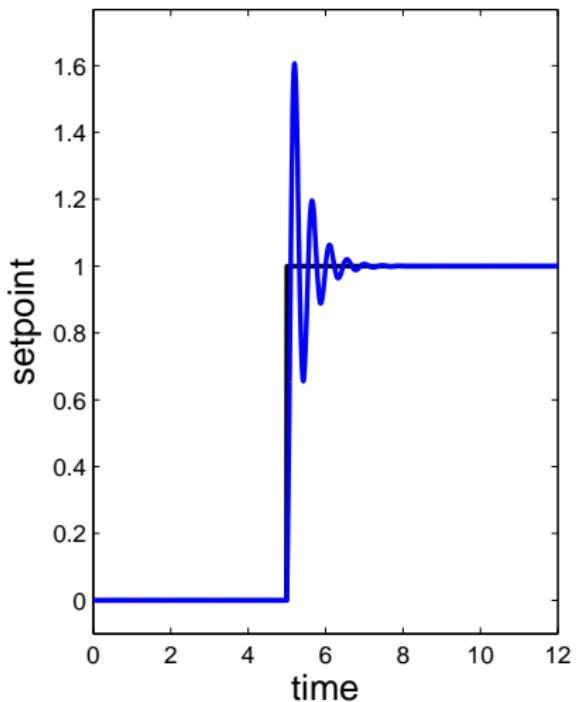
Closed loop response: 0th order setpoint

3/36



Closed loop response: 0th order setpoint

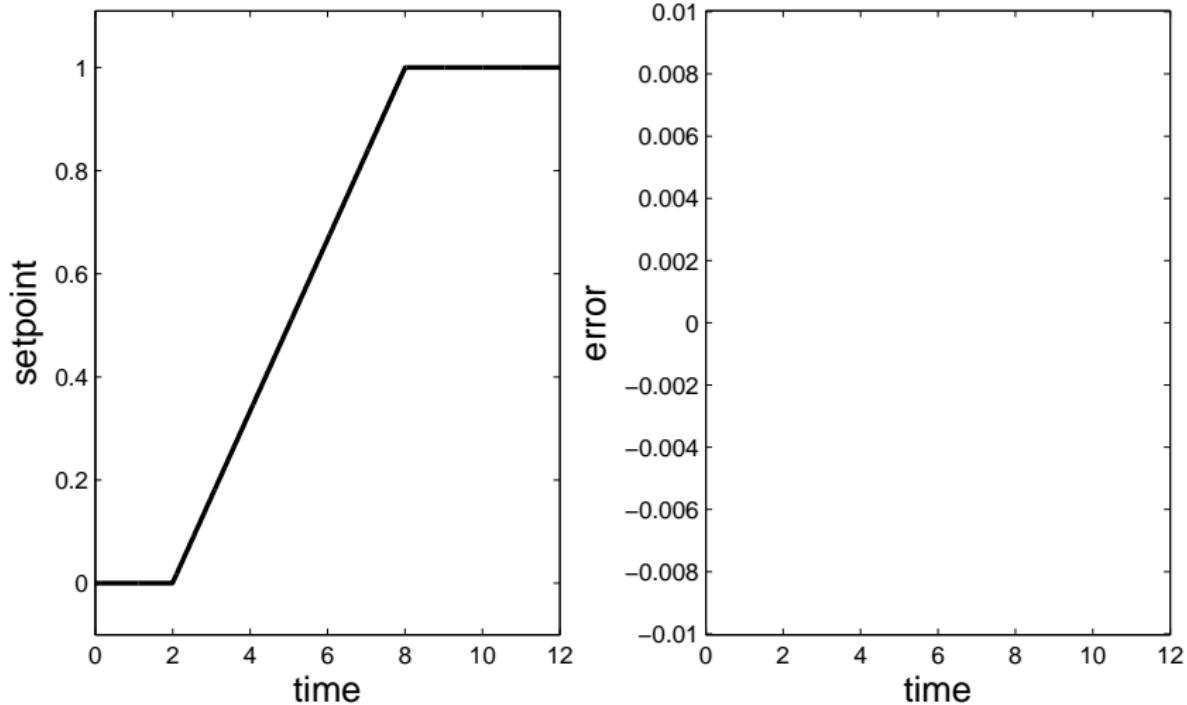
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Maximal error / overshoot: 0.6

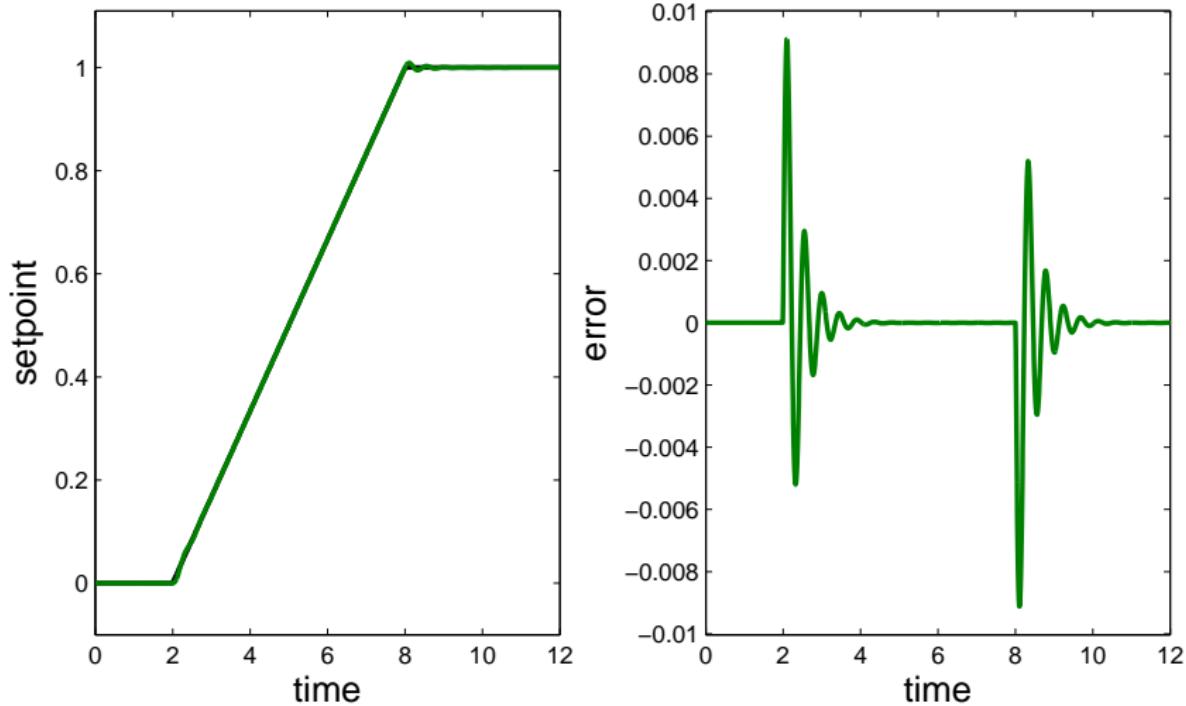
Closed loop response: 1st order setpoint

4/36



Closed loop response: 1st order setpoint

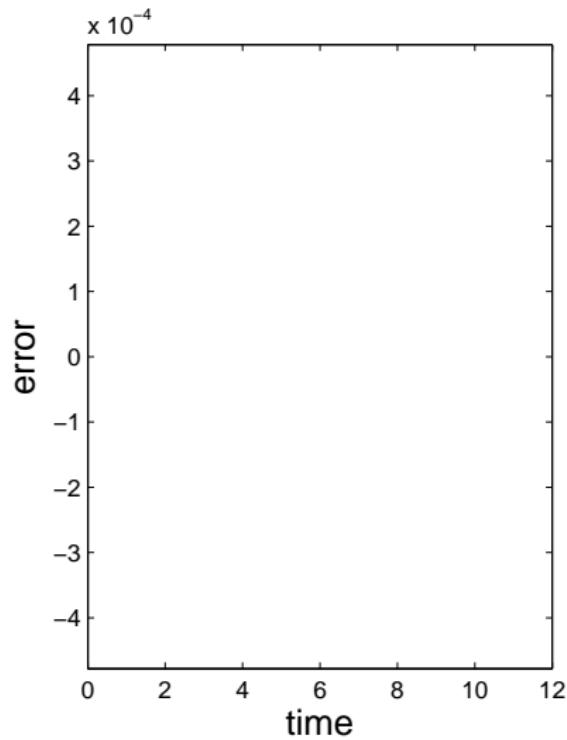
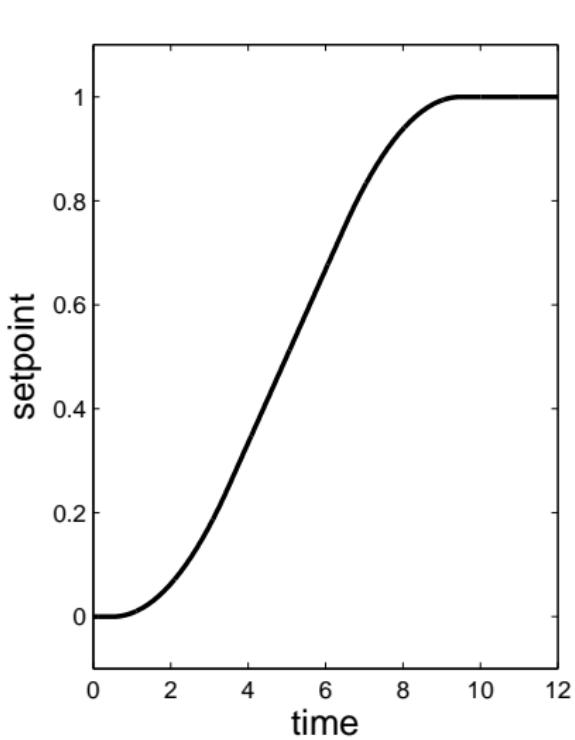
4/36



Maximal error / overshoot: 0.009

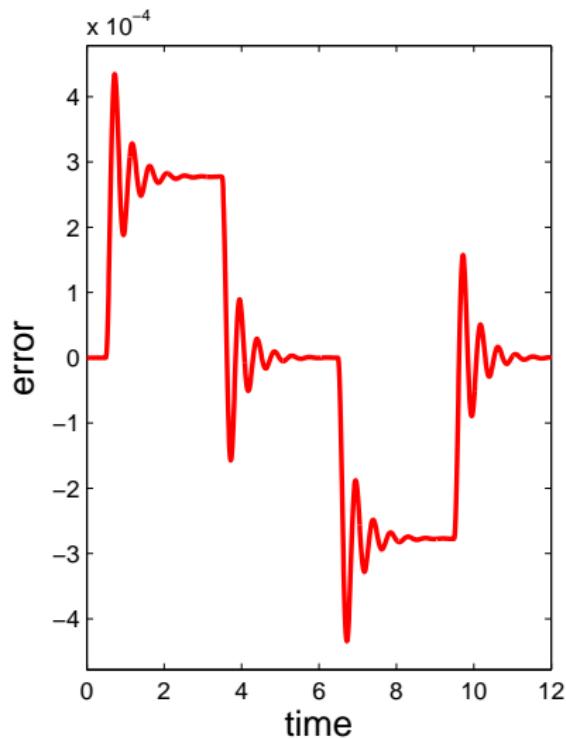
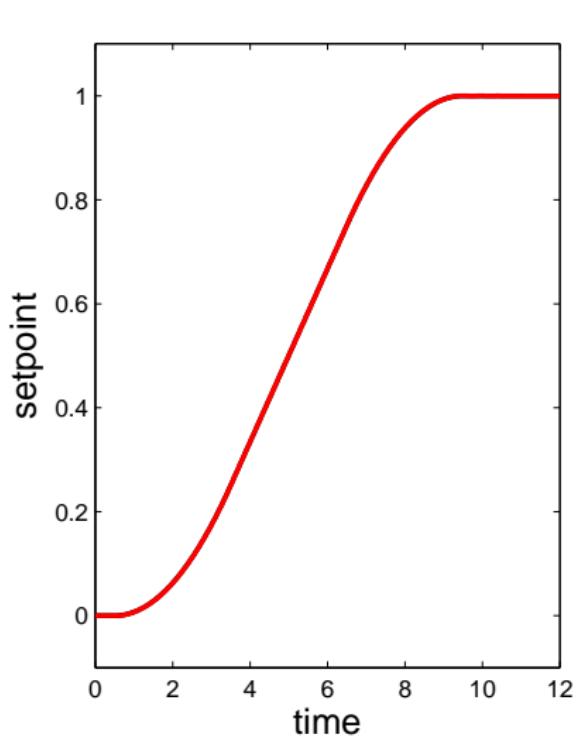
Closed loop response: 2nd order setpoint

5/36



Closed loop response: 2nd order setpoint

5/36



Maximal error / overshoot: 0.0004

Very good tracking results can be obtained

- ▶ using a simple (low bandwidth) controller
- ▶ using a ‘smart’ trajectory for x_s
- ▶ basic idea: shape trajectory → restrict \dot{x}_s , \ddot{x}_s , etc

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Advantages of trajectory planning:

- ▶ less oscillations
- ▶ possibly faster settling times
- ▶ smaller control signals (less saturation issues)

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One can wonder...

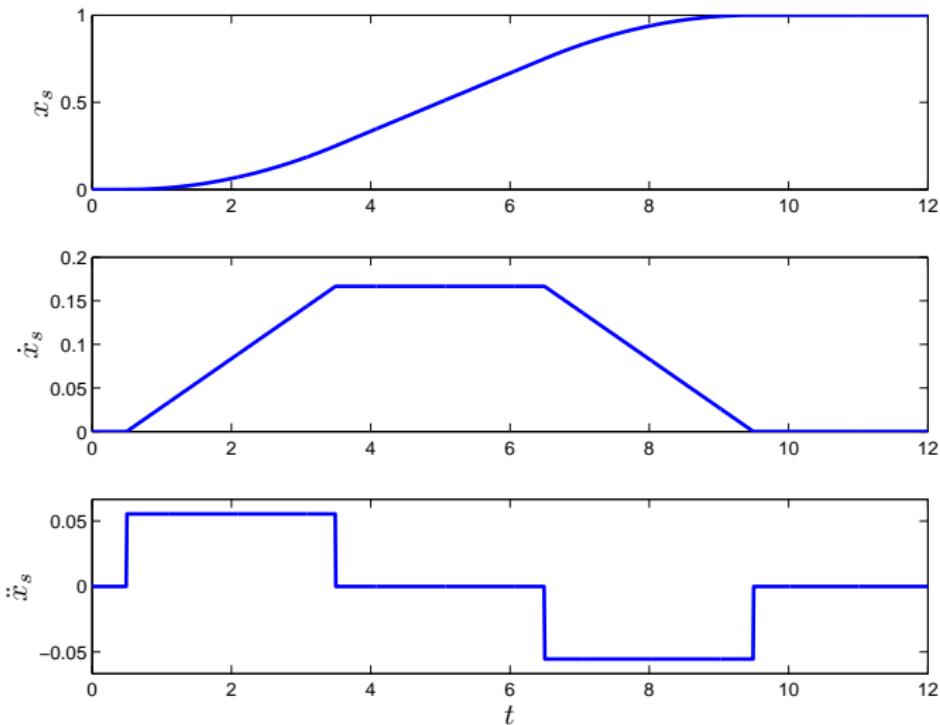
- ▶ Can we quantify the tracking error?
- ▶ Is there a way to further reduce this tracking error?

Understanding the servo error

2nd order trajectory

8/36

For now, assume only x_s , \dot{x}_s and \ddot{x}_s are restricted

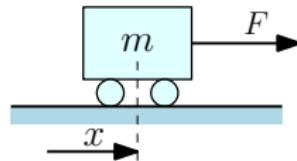


Tracking example 1: error dynamics

9/36

Equation of motion:

$$m\ddot{x} = F$$



PD-controller:

$$\begin{aligned} F &= K_p e + K_v \dot{e} \\ &= K_p (x_s - x) + K_v (\dot{x}_s - \dot{x}) \end{aligned}$$

Hence

$$\begin{aligned} m\ddot{x} + K_v (\dot{x} - \dot{x}_s) + K_p (x - x_s) &= 0 \\ m(\ddot{x}_s - \ddot{x}) + K_v (\dot{x}_s - \dot{x}) + K_p (x_s - x) &= m\ddot{x}_s \end{aligned}$$

Using $e = x_s - x$, the tracking error dynamics becomes

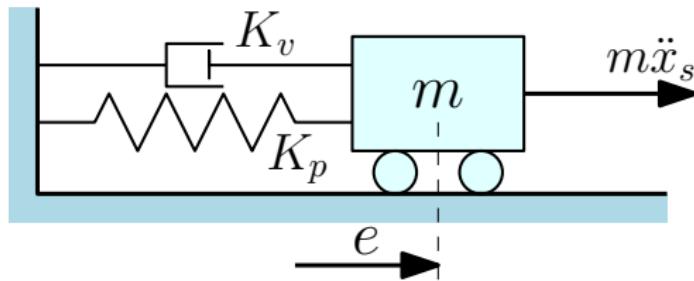
$$m\ddot{e} + K_v \dot{e} + K_p e = m\ddot{x}_s$$

Tracking example 1: error dynamics

10/36

$$\underbrace{m\ddot{e} + K_v \dot{e} + K_p e}_{\text{mass - spring - damper}} = \underbrace{m\ddot{x}_s}_{\text{force on mass}}$$

Does e go to zero?

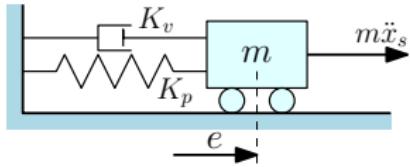


- Iff $\ddot{x}_s = 0$ then $e \rightarrow 0$
- Tracking error whenever $\ddot{x}_s \neq 0$

Whenever the mass needs to be accelerated, there is a tracking error!

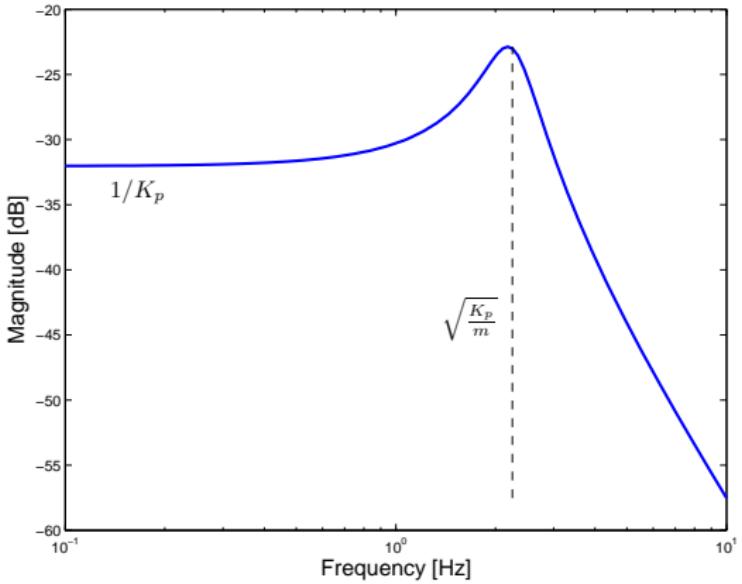
Tracking example 1: error dynamics

11/36



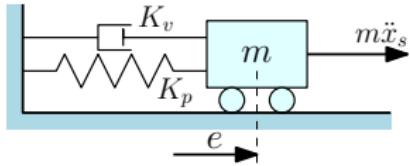
$$m\ddot{e} + K_v\dot{e} + K_p e = u$$

- ▶ DC-gain: $\frac{1}{K_p}$
- ▶ Eigenfrequency: $\sqrt{\frac{K_p}{m}}$
- ▶ $u = m\ddot{x}_s$



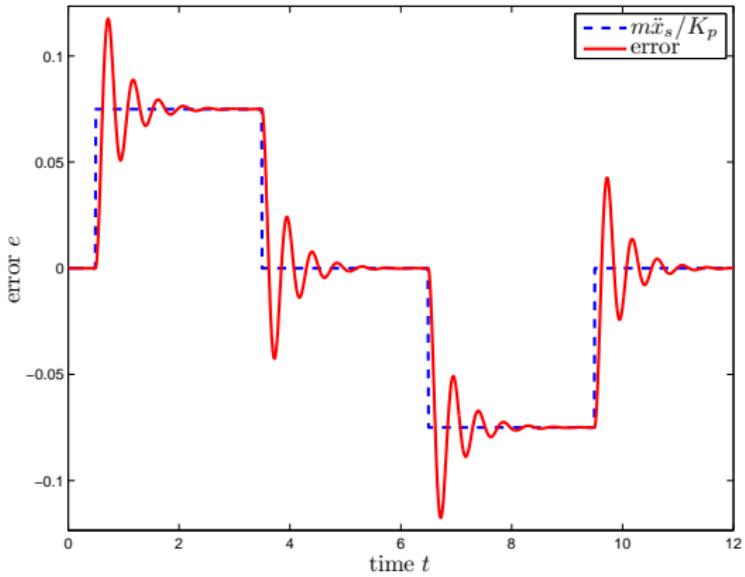
Tracking example 1: error dynamics

11/36



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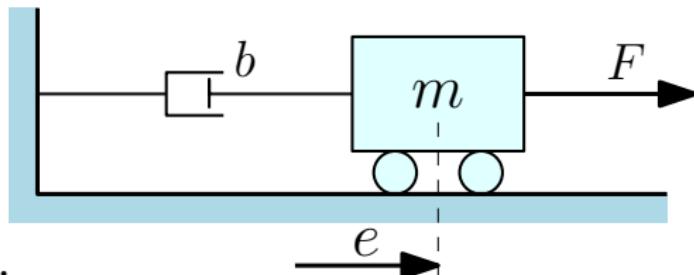
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- ▶ $u = m\ddot{x}_s$



Tracking example 2: error dynamics

12/36

Suppose the mass encounters friction:



Equation of motion:

$$m\ddot{x} + b\dot{x} = \underbrace{K_p(x_s - x) + K_v(\dot{x}_s - \dot{x})}_{\text{PD-controller}}$$

Hence, the error dynamics becomes

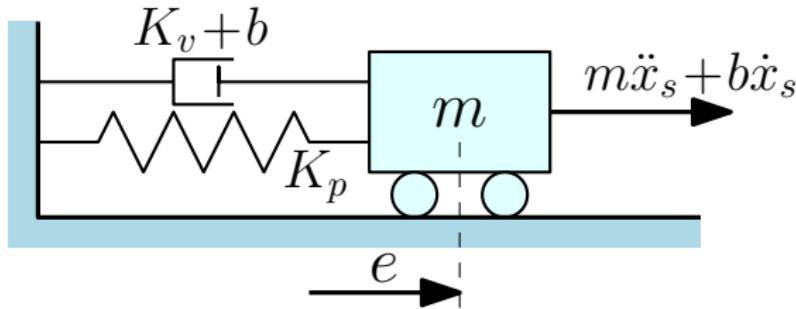
$$\begin{aligned} m(\ddot{x}_s - \ddot{x}) + (K_v + b)(\dot{x}_s - \dot{x}) + K_p(x_s - x) &= m\ddot{x}_s + b\dot{x}_s \\ m\ddot{e} + (K_v + b)\dot{e} + K_p e &= m\ddot{x}_s + b\dot{x}_s \end{aligned}$$

Tracking example 2: error dynamics

13/36

$$\underbrace{m\ddot{e} + (K_v + b)\dot{e} + K_p e}_{\text{mass - spring - damper}} = \underbrace{m\ddot{x}_s + b\dot{x}_s}_{\text{force on mass}}$$

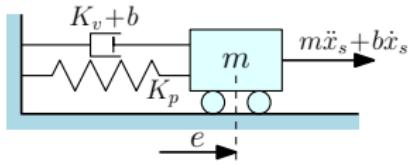
Does e go to zero?



- If $\ddot{x}_s = 0$ and $\dot{x}_s = 0$, then $e \rightarrow 0$
- Tracking error whenever $\ddot{x}_s \neq 0$ and/or $\dot{x}_s \neq 0$

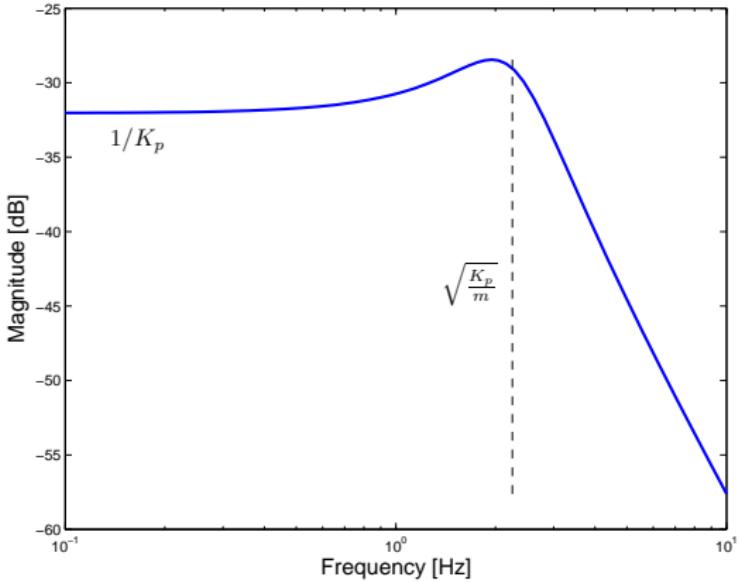
Tracking example 2: error dynamics

14/36



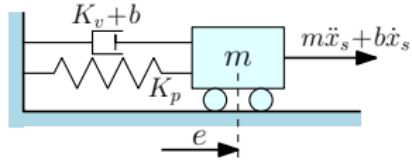
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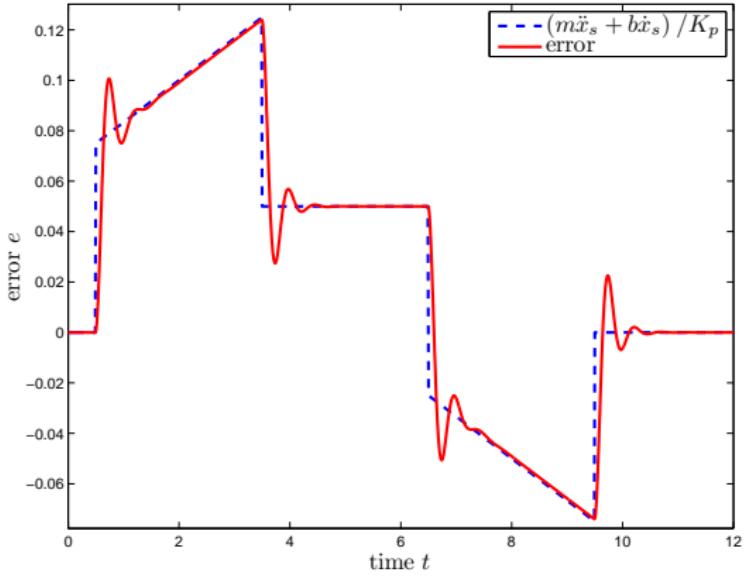
Tracking example 2: error dynamics

14/36



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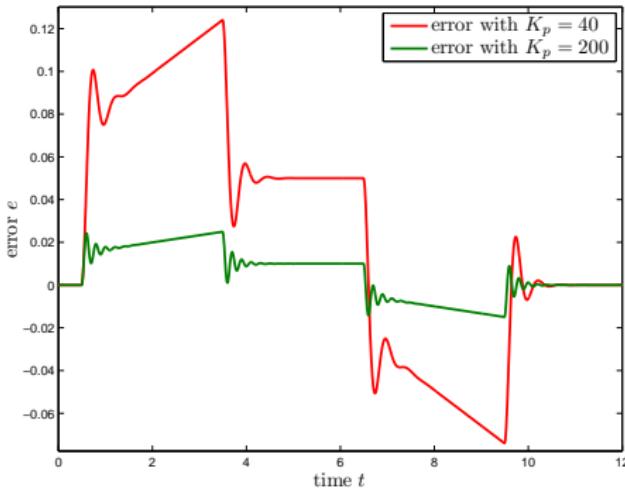
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- ▶ Using feedback
 - increase K_p

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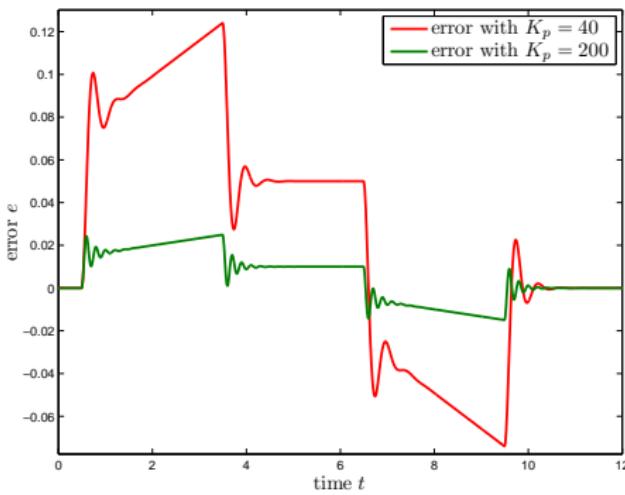
- ▶ Using feedback
 - increase K_p



There is still a (steady-state) error...

How can we decrease this error?

- ▶ Using feedback
 - increase K_p



- ▶ Using feedforward

$$m\ddot{e} + K_v \dot{e} + K_p e = \underbrace{m\ddot{x}_s}_{\text{is known!}}$$

- ▶ Given x_s , can we compensate the error *beforehand*?

There is still a (steady-state) error...

Feedback:

- ▶ Controller responds to an error
- ▶ Error thus already exists
- ▶ Feedback = looking back
 - you're always lagging behind

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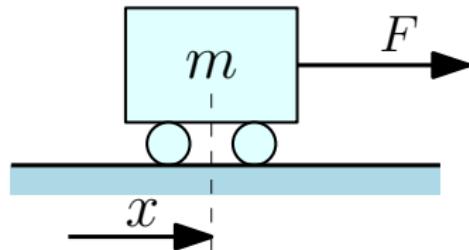


Feedforward:

- ▶ Use knowledge about the input
- ▶ Correct *before* the error can occur
- ▶ Feedforward = looking ahead
 - anticipate what happens or what is needed

Feedforward for motion systems

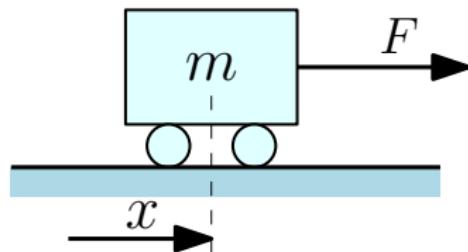
How does feedforward work?



- ▶ Goal: zero error for $t \rightarrow \infty$ for all x_s :

$$m\ddot{e} + K_v\dot{e} + K_p e = 0$$

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- ▶ Goal: zero error for $t \rightarrow \infty$ for all x_s :

$$m\ddot{e} + K_v\dot{e} + K_p e = 0$$

- ▶ Since $m\ddot{x} = F$, we can obtain this when

$$F = \underbrace{m\ddot{x}_s}_{\text{feedforward}} + \underbrace{-K_v\dot{e} - K_p e}_{\text{PD-controller}}$$

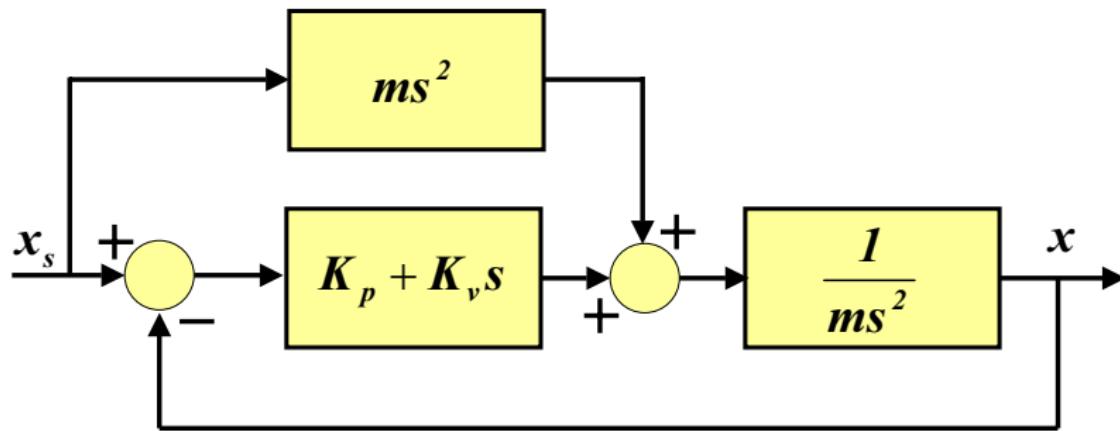
Note that x_s is known and

$$\mathcal{L}\{m\ddot{x}_s\} = ms^2 \mathcal{L}\{x_s\}$$

Feedforward in the loop (1)

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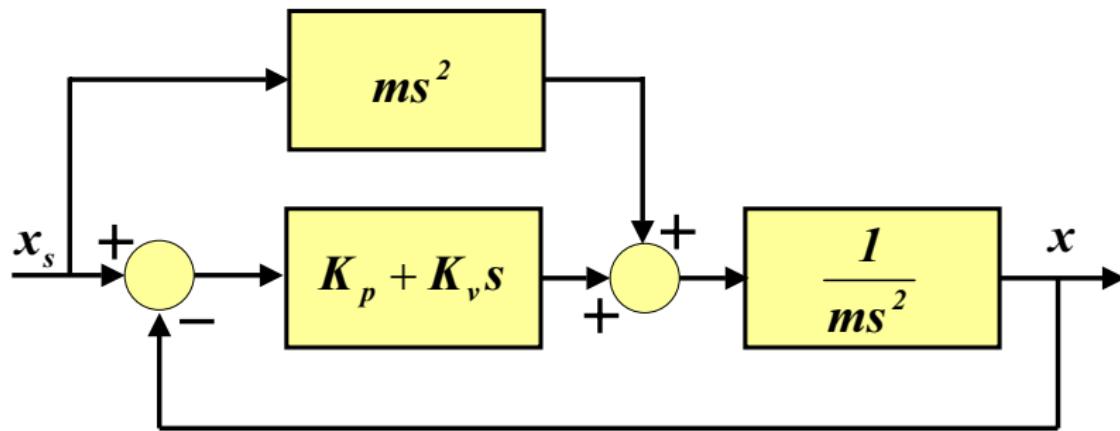


Feedforward in the loop (1)

19/36

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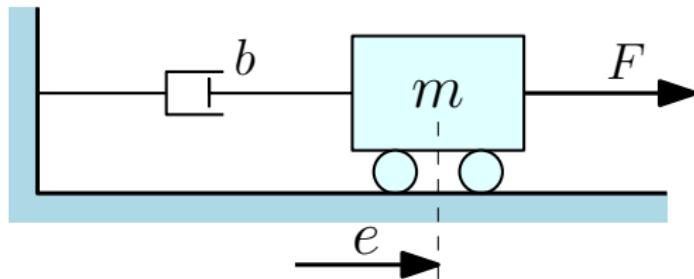
$$\mathcal{L}\{m\ddot{x}_s\} = ms^2 \mathcal{L}\{x_s\}$$



Forward feed / prescribe in advance ...

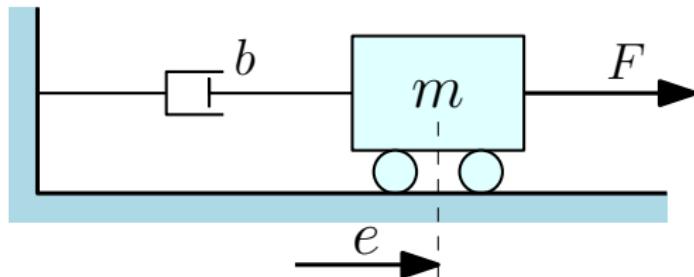
- ...the force necessary to accelerate the rigid mass.

The inverse problem (2)



- ▶ Goal: zero error for $t \rightarrow \infty$ for all x_s :

$$m\ddot{e} + K_v \dot{e} + K_p e = 0$$



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$$F = \underbrace{m\ddot{x}_s + b\dot{x}_s}_{\text{feedforward}} \quad \underbrace{-K_v \dot{e} - K_p e}_{\text{PD-controller}}$$

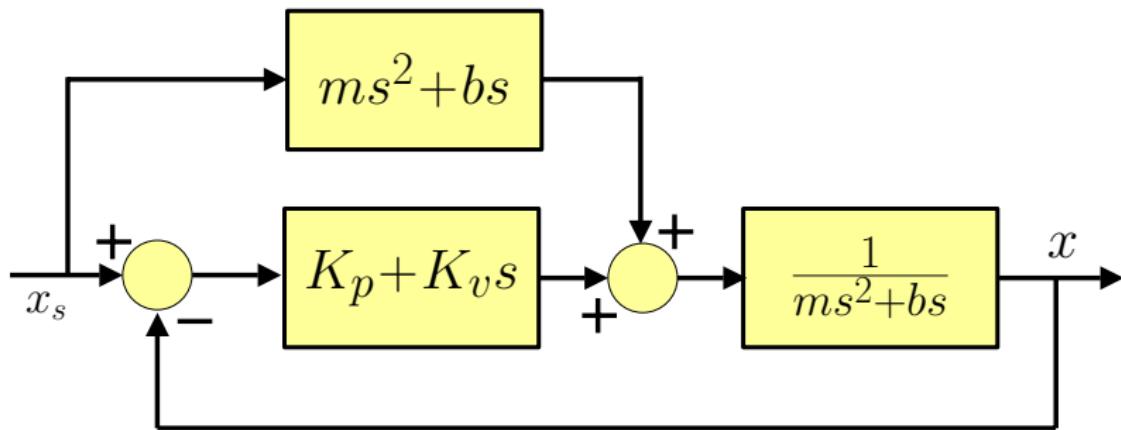
Note that x_s is known and

$$\mathcal{L}\{m\ddot{x}_s + b\dot{x}_s\} = (ms^2 + bs)\mathcal{L}\{x_s\}$$

Feedforward in the loop (2)

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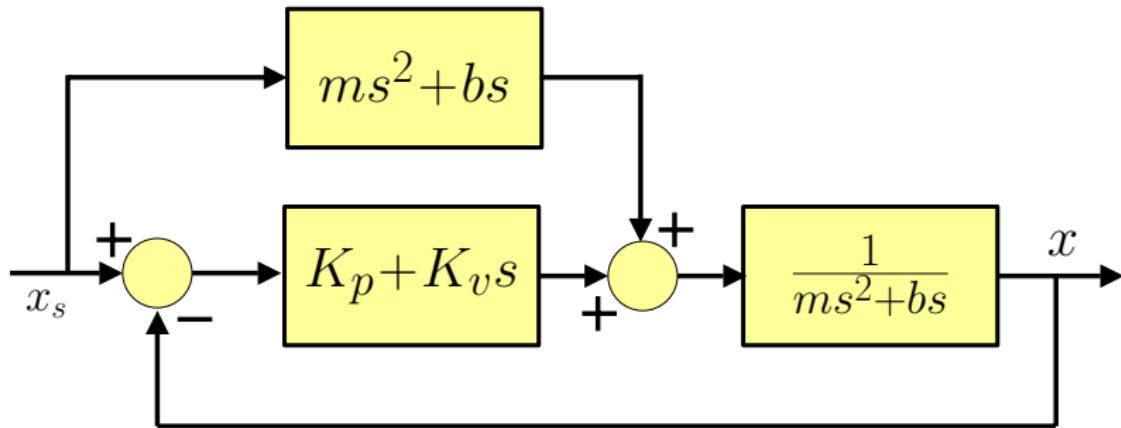


Feedforward in the loop (2)

21/36

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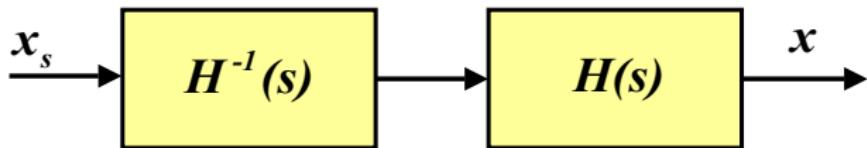
$$\mathcal{L}\{m\ddot{x}_s + b\dot{x}_s\} = (ms^2 + bs)\mathcal{L}\{x_s\}$$



Forward feed / prescribe in advance ...

- ... the force necessary to accelerate the rigid mass,
- ... the force required to overcome the friction.

In theory, a feedback controller is not necessary:



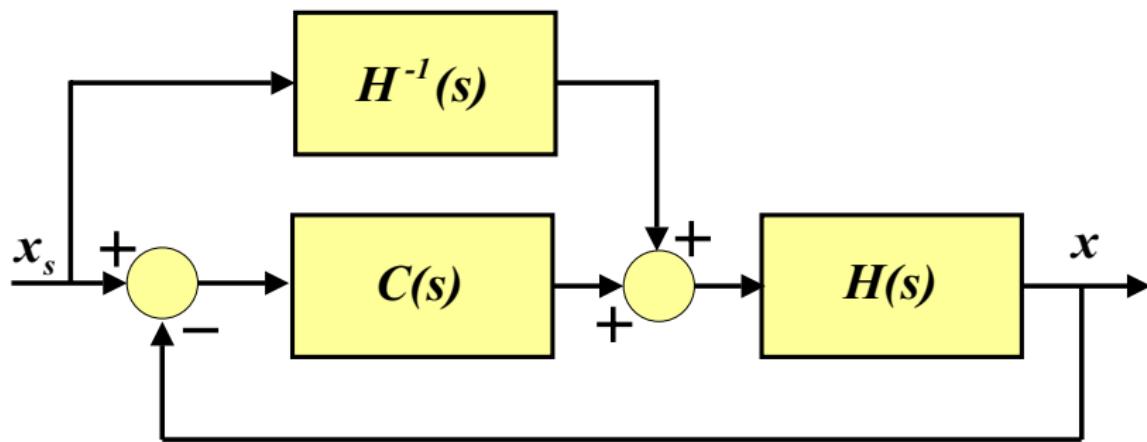
Ideal feedforward:

- ▶ $C_{ff}(s) = H^{-1}(s)$
- ▶ $x = H(s)H^{-1}(s)x_s = x_s$
- ▶ use the plant inverse to compute the plant input *in advance*

Combination feedback and feedforward

23/36

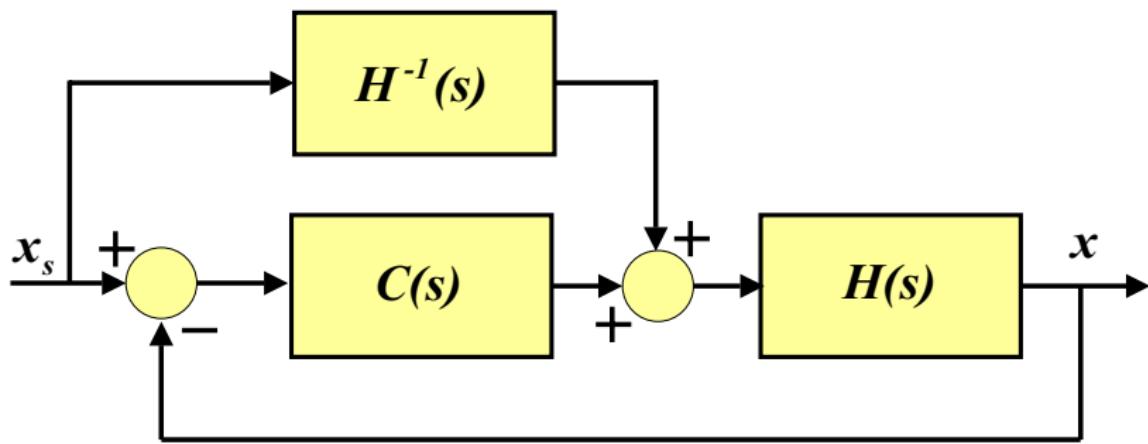
In practice, feedback is needed to compensate disturbances around x_s :



Combination feedback and feedforward

23/36

In practice, feedback is needed to compensate disturbances around x_s :



However,

- ▶ what if $H^{-1}(s)$ is unstable?
- ▶ what if $H(s)$ is unknown?

Then we try to approximate $H^{-1}(s)$ in time domain.

Forward feeding the force required to...

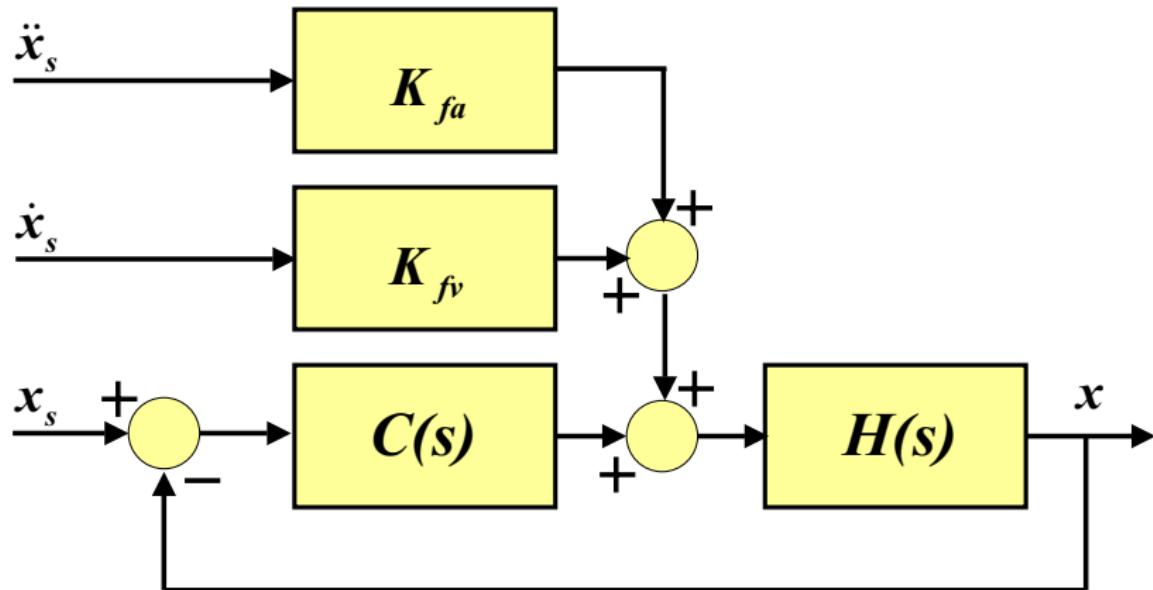
- ▶ ...accelerate the rigid body mode of the plant: $F_a = K_{fa} \ddot{x}_s$
- ▶ ...overcome the viscous friction with the fixed world: $F_v = K_{fv} \dot{x}_s$

General feedforward (1)

24/36

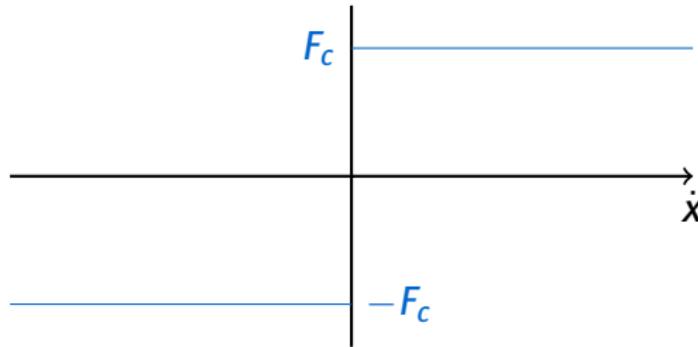
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What if Coulomb friction (dry friction) is present?

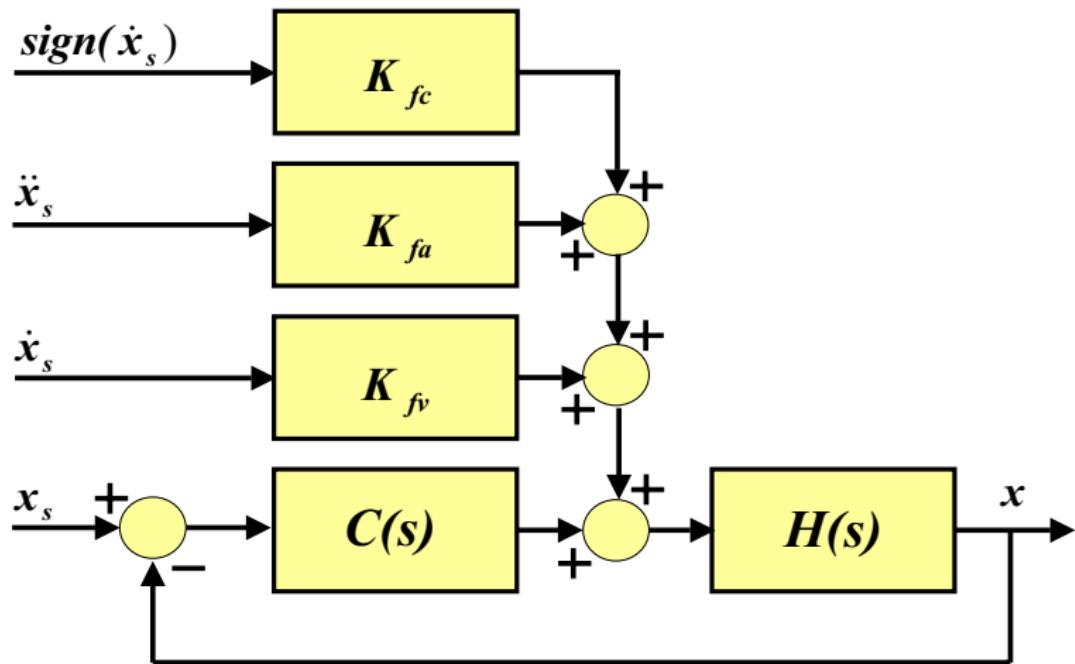
- ▶ constant force, opposing direction of motion
- ▶ direction dependent



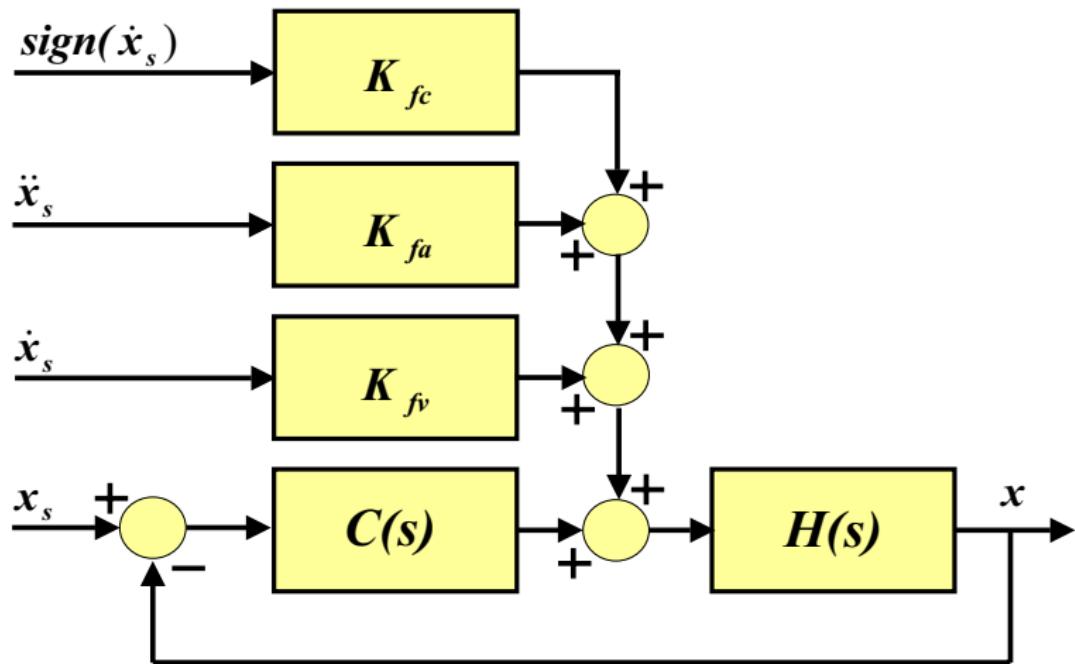
Hence, to overcome this force in advance, we need a feedforward

$$F_c = K_{fc} \cdot \text{sign}(\dot{x}_s)$$

General feedforward (2)



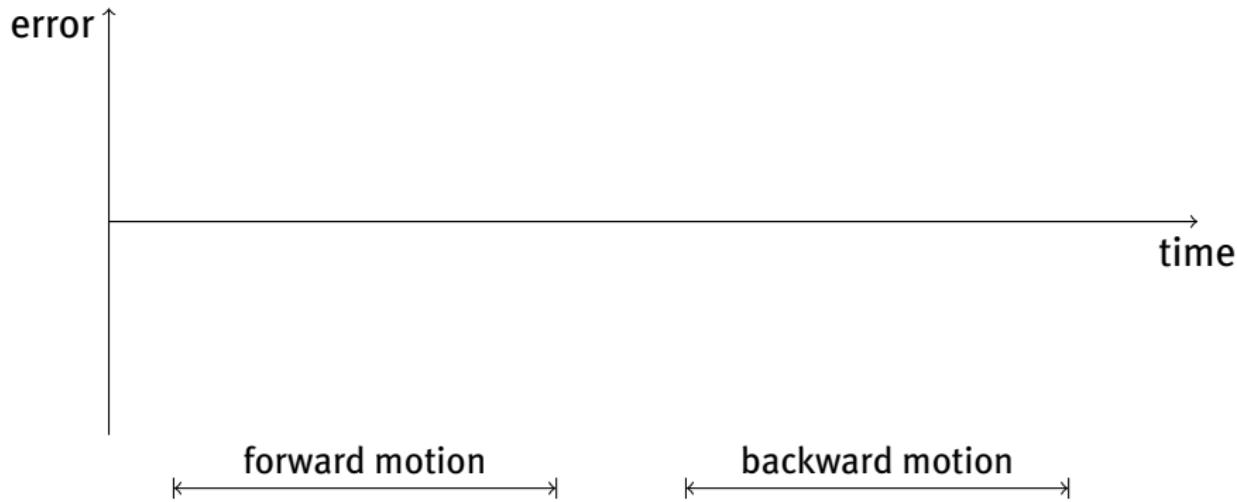
General feedforward (2)



$$F_{ff} = K_{fa}\ddot{x}_s + K_{fv}\dot{x}_s + K_{fc}\text{sign}(\dot{x}_s)$$

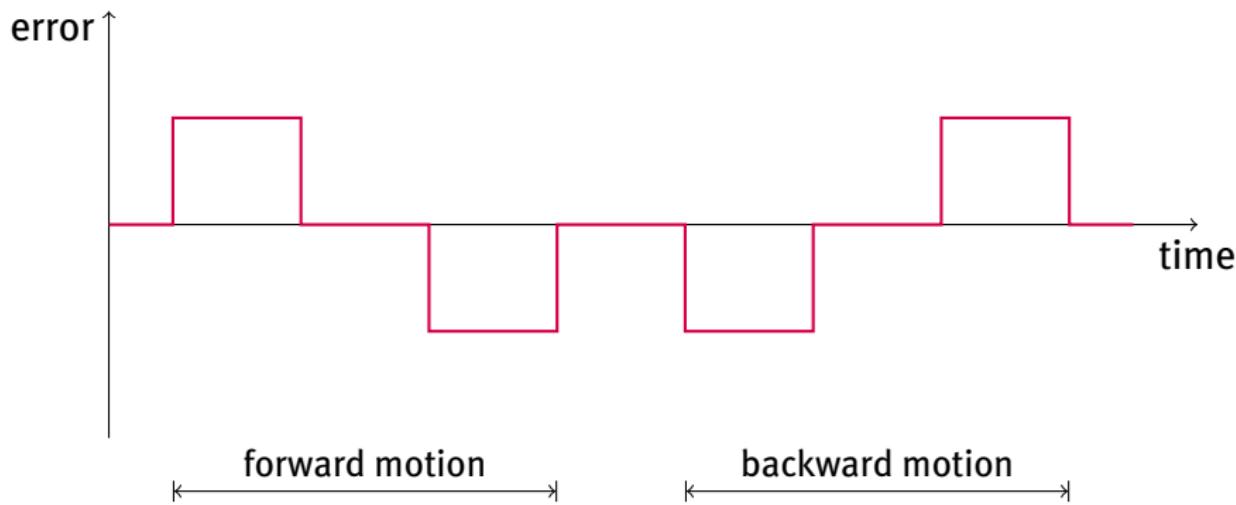
Tuning feedforward parameters

Feedforward tuning is based on error profile in time domain



There is an error due to:

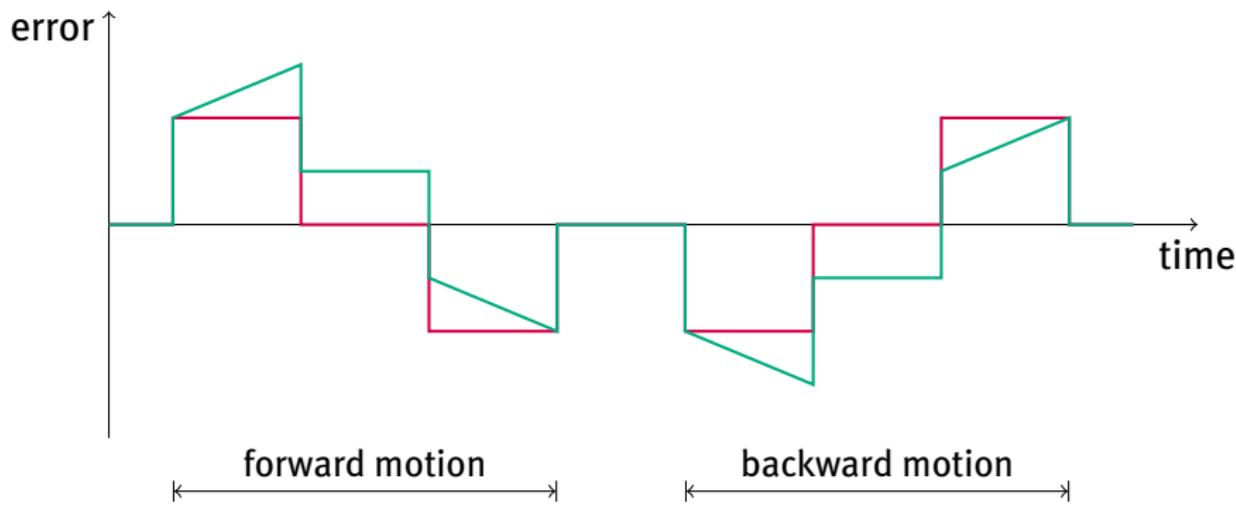
Feedforward tuning is based on error profile in time domain



There is an error due to:

- ▶ lack of force to accelerate (K_{fa})

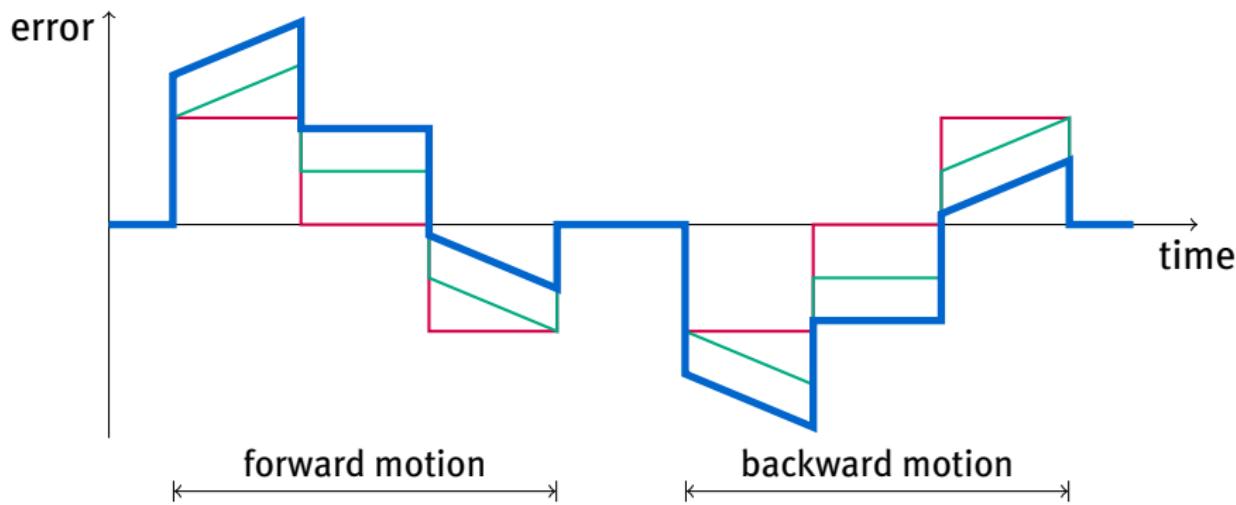
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There is an error due to:

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Feedforward tuning is based on error profile in time domain



There is an error due to:

- ▶ lack of force to accelerate (K_{fa})
- ▶ lack of force to compensate viscous friction (K_{fv})
- ▶ lack of force to compensate Coulomb friction (K_{fc})

- ▶ Define a suitable (2nd or higher order) setpoint trajectory
 - both forward and backward movement (with a small pause)
 - rather ‘challenging’ (it must generate some error profile)
 - approx 1/3 acceleration, 1/3 constant velocity, 1/3 deceleration

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 - the error should be large enough
 - each feedforward component should be recognizable
 - maybe feedback bandwidth should be lowered?

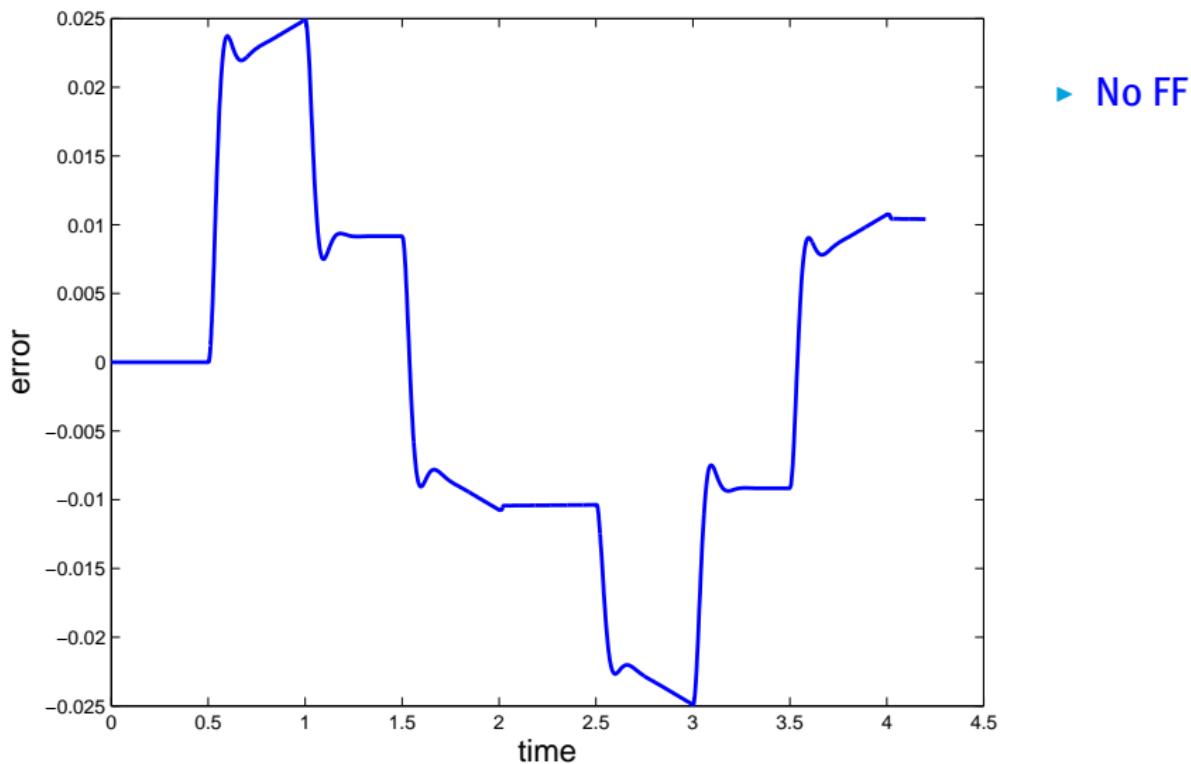
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 - remove slopes during acceleration and deceleration
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- ▶ Tune K_{fa}
 - minimize error during acceleration and deceleration

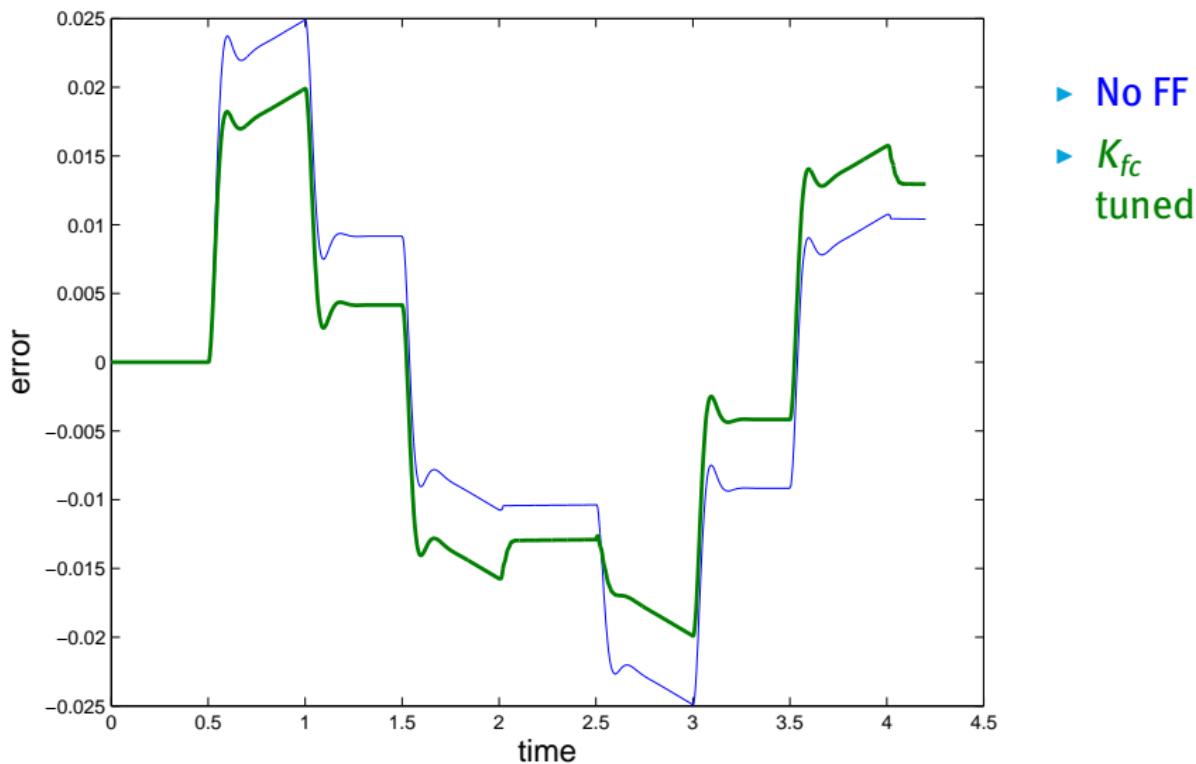
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- ▶ Monitor the error
 - the error should be large enough
 - each feedforward component should be recognizable
 - maybe feedback bandwidth should be lowered?
- ▶ Tune K_{fc}
 - deceleration forward movement and acceleration backward movement should have same error
- ▶ Tune K_{fv}
 - remove slopes during acceleration and deceleration
 - no error during constant velocity phase when K_{fc} and K_{fv} are correct
- ▶ Tune K_{fa}
 - minimize error during acceleration and deceleration
- ▶ If desired, tune up the feedback controller

Feedforward tuning



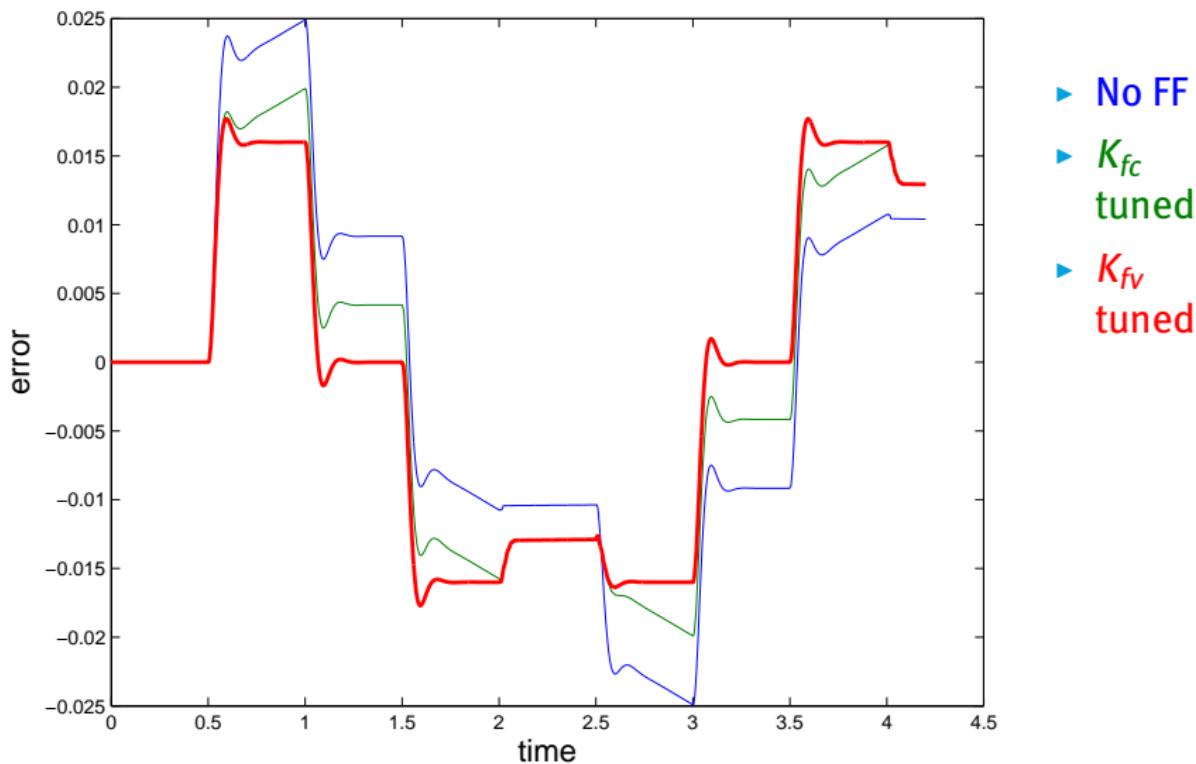
Feedforward tuning

30/36



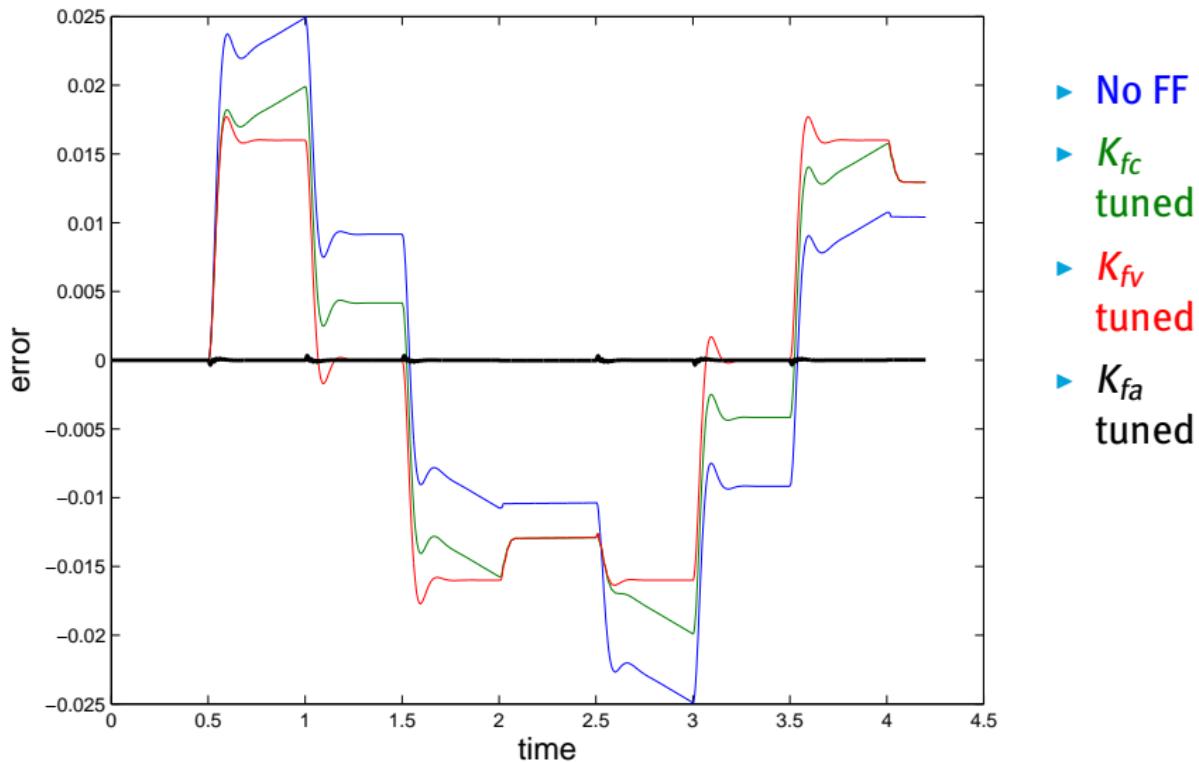
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30/36

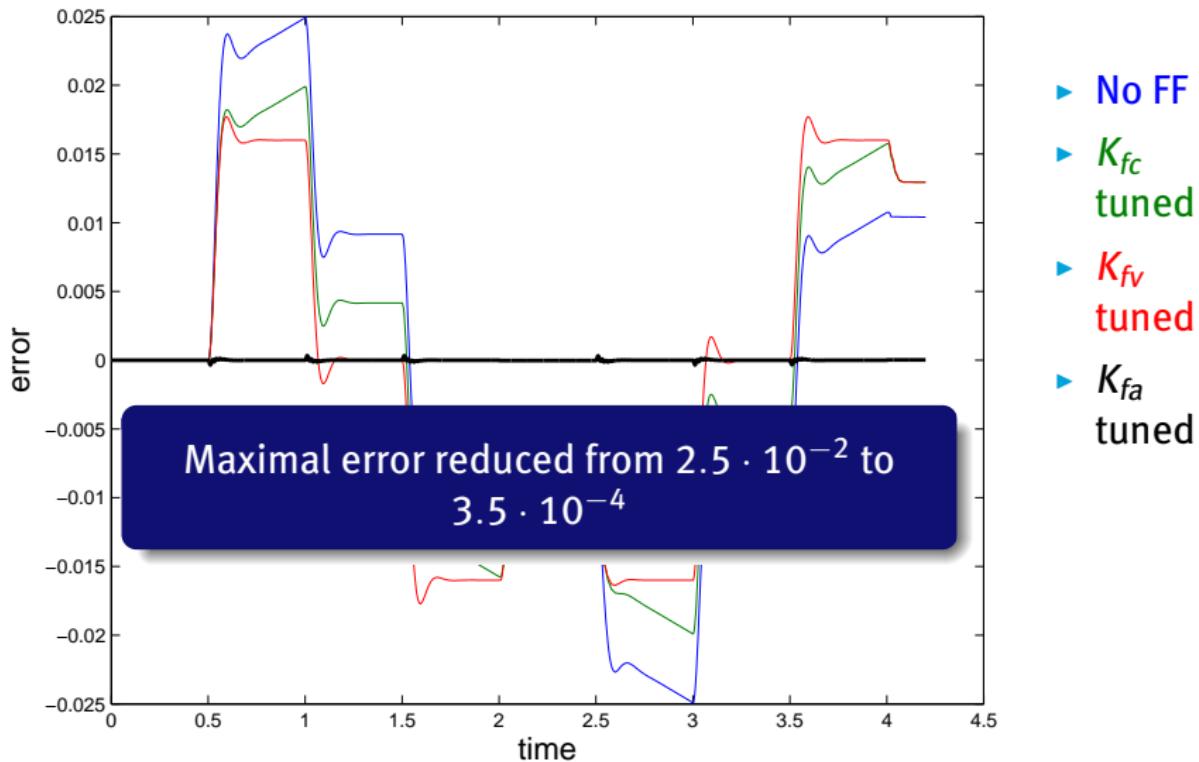


Feedforward tuning

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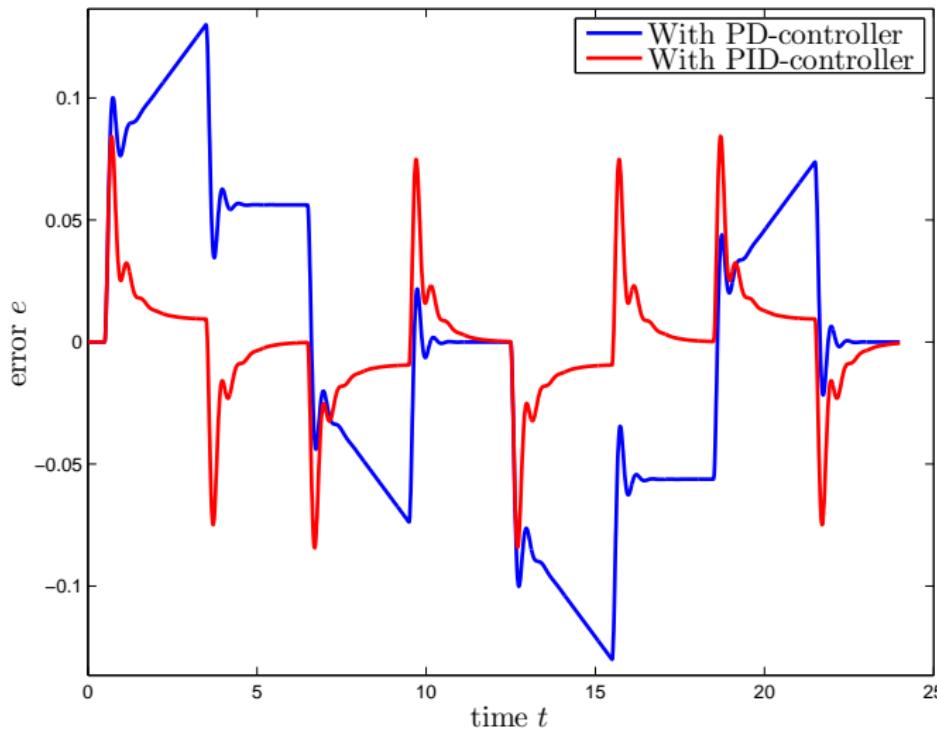


Feedforward tuning



Integral controller action

To tune feedforward, don't use a high performance feedback controller!



Feedforward issues to be aware of

32/36

Feedforward tuning is time domain trial and error.

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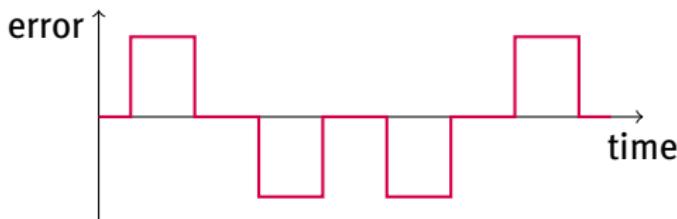
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- What happens if we over-tune feedforward parameters?



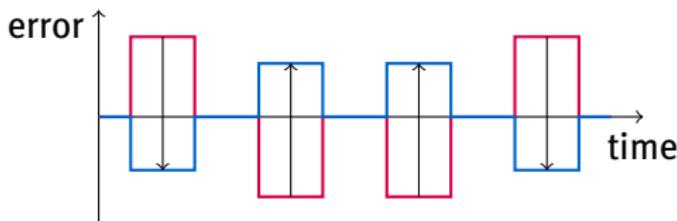
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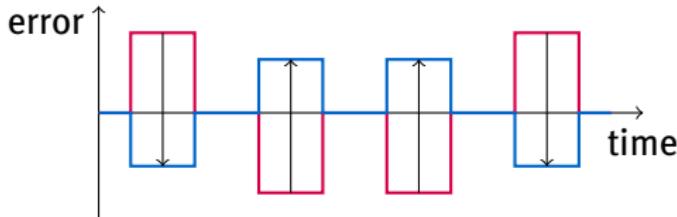
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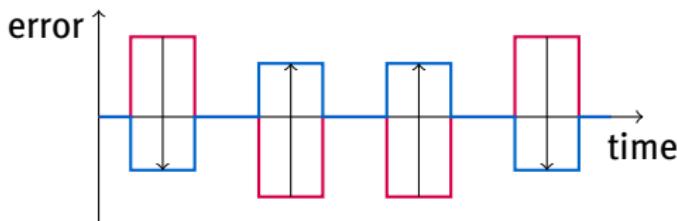
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- ▶ Trajectory dependence

- Do the feedforward terms change when the trajectory changes? **No.**
- ⇒ Terms represent system parameters, which do not change

Second order trajectory may not be sufficient

- ▶ jump in $\ddot{x}_s \Rightarrow$ jump in feedforward force
- ▶ can excite parasitic (higher order) dynamics
- ▶ can introduce oscillations
- ▶ can cause actuator saturation

Second order trajectory may not be sufficient

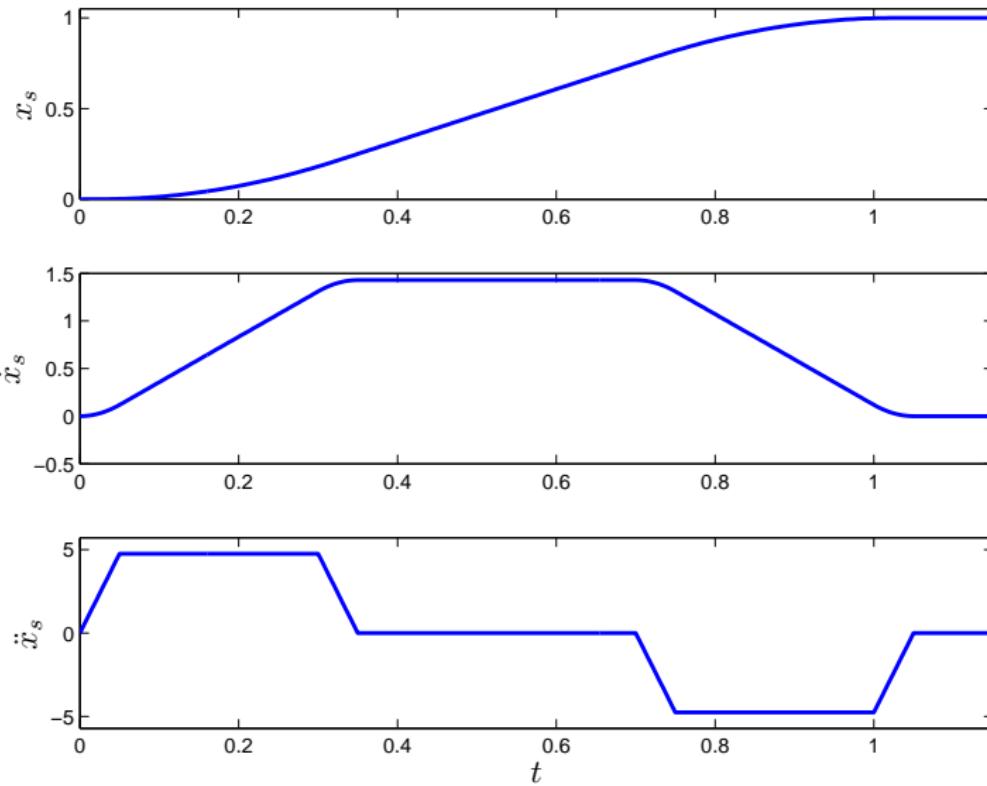
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How to solve this?

- ▶ Higher order setpoints
 - gradual increase of feedforward forces (smoothing)
 - by limiting higher derivatives (e.g. jerk)
- ▶ Here: using 3rd order setpoints

3rd order setpoint

34/36



Higher order setpoints

Momentum = *mass* × *velocity*

Force = *mass* × *acceleration*

Yank = *mass* × *jerk*

Tug = *mass* × *snap*

Snatch = *mass* × *crackle*

Shake = *mass* × *pop*



Other more advanced techniques:

- ▶ Model-based input shaping
- ▶ Learning input shaping
 - adapt the trajectory after each trial
- ▶ Iterative Learning Control (ILC)
 - adapt the feedforward signal after each trial
 - frequency domain, lifted domain, or using basis functions

See other courses (4SC070: Learning Control) and current research.