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## Fundamentals

If you want a nice discussion of SPH, with some interesting background see Joe Monaghan's introduction on youtube (<https://youtu.be/tAXHCAEgSuE>). We wish to evaluate the equations of motion of a barotropic fluid (in Lagrangian form, i.e. dealing with material derivatives):

$$\begin{cases} \frac{D\rho}{Dt} = -\rho \nabla \cdot \mathbf{u} \\ \frac{D\mathbf{u}}{Dt} = -\frac{1}{\rho} \nabla P + \frac{\nu}{\rho} \nabla^2 \mathbf{u} + \mathbf{g} \\ P = F(\rho) \end{cases} \quad (1)$$

These PDE's are continuum equations, we wish to discretise these onto a set of particles that we follow through time and space. Kernel interpolation theory begins by considering the integral representation of an arbitrary field function  $f$  through a volume  $\Omega$  in the form

$$f(\mathbf{x}) = \int_{\Omega} f(\mathbf{x}') \delta(\mathbf{x} - \mathbf{x}') d\mathbf{x}', \quad (2)$$

where  $\delta$  is the Dirac-delta function and  $d\mathbf{x}$  a volume element. Equation 2 is an exact interpolation, but cannot be integrated, hence the delta function is replaced with a smoothing function  $W(\mathbf{x} - \mathbf{x}', h)$  such that

$$\langle f(\mathbf{x}) \rangle = \int_{\Omega} f(\mathbf{x}') W(\mathbf{x} - \mathbf{x}', h) d\mathbf{x}'. \quad (3)$$

The smoothing or kernel function  $W$  has a radius of influence proportional to a length scale  $h$ , termed the 'smoothing length'. As the kernel function is only an approximation of the delta function, equation 3 cannot be exact, but is second order accurate if  $W$  is symmetric and meets the normalisation condition  $\int_{\mathbf{x}} W d\mathbf{x} = 1$  [1]. Hence, this step is defined by the kernel approximation operator  $\langle \rangle$ . Similarly, the spatial derivative can be approximated by replacing  $A(\mathbf{x})$  with  $\nabla A(\mathbf{x})$ ,

$$\langle \nabla f(\mathbf{x}) \rangle = \int_{\Omega} [\nabla f(\mathbf{x}')] W(\mathbf{x} - \mathbf{x}', h) d\mathbf{x}' \quad (4)$$

With the spatial derivative likely unknown, the identity

$$\nabla[f(\mathbf{x}') W(\mathbf{x} - \mathbf{x}', h)] = [\nabla f(\mathbf{x}')] W(\mathbf{x} - \mathbf{x}', h) + f(\mathbf{x}') [\nabla W(\mathbf{x} - \mathbf{x}', h)] \quad (5)$$

is applied. Resulting in

$$\langle \nabla f(\mathbf{x}) \rangle = \int_{\Omega} \nabla[f(\mathbf{x}') W(\mathbf{x} - \mathbf{x}', h)] d\mathbf{x}' - \int_{\Omega} f(\mathbf{x}') [\nabla W(\mathbf{x} - \mathbf{x}', h)] d\mathbf{x}' \quad (6)$$

Through the divergence theorem, the first term of Equation 6 can be replaced with a surface integral

$$\langle \nabla f(\mathbf{x}) \rangle = \int_S f(\mathbf{x}') W(\mathbf{x} - \mathbf{x}', h) \cdot \vec{n} dS - \int_{\Omega} f(\mathbf{x}') [\nabla W(\mathbf{x} - \mathbf{x}', h)] d\mathbf{x}' \quad (7)$$

where  $\vec{n}$  is a unit normal to the surface  $S$ . With the surface integral being evaluated over the kernel support radius ( $\kappa h$ ), if the chosen kernel has compact support ( $W(\kappa h, h) = 0$ ) this term will disappear and equation 7 reduces to

$$\langle \nabla f(\mathbf{x}) \rangle = - \int_{\Omega} f(\mathbf{x}') [\nabla W(\mathbf{x} - \mathbf{x}', h)] d\mathbf{x}', \quad (8)$$

With the continuous fluid being discretised by a finite number of particles, the integral in equations 3 and 8 can be approximated by a summation over  $N$  neighbouring particles, which are assigned mass and density, taking the form

$$\langle f(\mathbf{x}_i) \rangle \approx \sum_j f(\mathbf{x}_j) W(\mathbf{x}_i - \mathbf{x}_j, h) \frac{m_j}{\rho_j}, \quad (9)$$

$$\langle \nabla f(\mathbf{x}_i) \rangle \approx - \sum_j f(\mathbf{x}_j) \nabla W(\mathbf{x}_i - \mathbf{x}_j, h) \frac{m_j}{\rho_j}. \quad (10)$$

Equation 9 represents the SPH particle approximation of a variable or function. A fundamental application of SPH is to set  $A(\mathbf{x})$  equal to  $\rho(\mathbf{x})$ , deriving the SPH density estimator

$$\langle \rho(\mathbf{x}_i) \rangle \approx \sum_j m_j W(\mathbf{x}_i - \mathbf{x}_j, h). \quad (11)$$

With the particle approximation, the equations governing particle motion for fluid flow can now be formulated; initially consider the inviscid momentum equation from the Lagrangian perspective such that

$$\frac{D\mathbf{u}}{Dt} = -\frac{\nabla P}{\rho} + g. \quad (12)$$

The kernel approximation operator is subsequently dropped for clarity. Equation 12 can be directly evaluated using the particle approximation, but results in a term that does not conserve linear nor angular momentum [2]. Thus, to symmetrise the pressure gradient the identity

$$\frac{\nabla P}{\rho} = \nabla \frac{P}{\rho} + \frac{P}{\rho^2} \nabla \rho \quad (13)$$

is applied, leading to

$$\frac{\nabla P}{\rho} = -\sum_j \frac{m_j}{\rho_j} \left[ \frac{P_j}{\rho_j} \right] \nabla_i W_{ij} - \left[ \frac{P_i}{\rho_i^2} \right] \sum_j \frac{m_j}{\rho_j} \rho_j \nabla_i W_{ij} \quad (14)$$

$$\frac{\nabla P}{\rho} = -\sum_j m_j \left[ \frac{P_j}{\rho_j^2} + \frac{P_i}{\rho_i^2} \right] \nabla_i W_{ij}. \quad (15)$$

#### Momentum

$$\frac{D\mathbf{u}_i}{Dt} = -\sum_j m_j \left[ \frac{P_j}{\rho_j^2} + \frac{P_i}{\rho_i^2} + \Pi_{ij} \right] \nabla W_{ij} + \sum_j m_j \nu \frac{\rho_i + \rho_j}{\rho_i \rho_j} \frac{\mathbf{x}_{ij} \cdot \nabla W_{ij}}{|\mathbf{x}_{ij}|^2 + 0.001h^2} \mathbf{u}_{ij} + \mathbf{a}_{ST,i} + \mathbf{g} \quad (16)$$

$$\Pi_{ij} = \begin{cases} \frac{-\alpha \bar{c}_{ij} \mu_{ij} + \beta \mu_{nk}^2}{\rho_{ij}} & : \mathbf{u}_{ij} \cdot \mathbf{x}_{ij} < 0 \\ 0 & : \mathbf{u}_{ij} \cdot \mathbf{x}_{ij} > 0 \end{cases}, \quad \mu_{ij} = \frac{h \mathbf{u}_{ij} \cdot \mathbf{x}_{ij}}{\mathbf{x}_{ij}^2 + 0.001h^2}, \quad \beta = 0. \quad (17)$$

#### Continuity

$$\frac{D\rho_i}{Dt} = \sum_j m_j \mathbf{u}_{ij} \cdot \nabla W_{ij} + \delta h c_0 \mathcal{D}_i \quad (18)$$

$$\mathcal{D}_i = 2 \sum_j \psi_{ij} \frac{\mathbf{x}_{ij} \cdot \nabla W_{ij}}{|\mathbf{x}_{ij}|} V_j \quad (19)$$

$$\psi_{ij} = \left\{ (\rho_i - \rho_j) - \frac{1}{2} (\langle \nabla \rho \rangle_i^L + \langle \nabla \rho \rangle_j^L) \cdot \mathbf{x}_{ij} \right\} \quad (20)$$

$$\langle \nabla \rho \rangle_i^L = \sum_j (\rho_i - \rho_j) \mathbf{L}_i \nabla W_{ij} V_j, \quad \mathbf{L}_i = \left[ -\sum_j \mathbf{x}_{ij} \otimes \nabla W_{ij} V_j \right]^{-1} \quad (21)$$

#### Tait equation of state and C2 Kernel

$$P = \frac{\rho_0 c_0^2}{\gamma} \left[ \left( \frac{\rho}{\rho_0} \right)^\gamma - 1 \right] \quad (22)$$

$$W_{ij} = \alpha_d \left( 1 - \frac{|\mathbf{x}_{ij}|}{2h} \right)_+^4 \left( \frac{2|\mathbf{x}_{ij}|}{h} + 1 \right) \quad (23)$$

$$\alpha_w = \frac{7}{4\pi h^2}, \quad \text{for dim} = 2$$

$$\alpha_w = \frac{21}{16\pi h^3}, \quad \text{for dim} = 3 \quad (24)$$

#### Surface tension

Renormalised surface normal:

$$\mathbf{n}_i = -\mathbf{L}_i \sum_j \nabla W_{ij} V_j \quad (25)$$

Shepard interpolant over normals:

$$\tilde{\mathbf{n}}_i = \frac{\sum_j \mathbf{n}_i W_{ij} V_j}{\sum_j W_{ij} V_j} \quad (26)$$

Obtain boundary normal:

$$\mathbf{n}_i^{b\perp} = \sum_{j \in \text{boundary}} \nabla W_{ij} V_j \quad (27)$$

Giving boundary tangent (using unit vectors for these following rotations):

$$\hat{\mathbf{n}}_i^{b\parallel} = \hat{\mathbf{n}}_i - (\hat{\mathbf{n}}_i^{b\perp} \cdot \hat{\mathbf{n}}_i) \hat{\mathbf{n}}_i^{b\perp} \quad (28)$$

Prescribed normal's at wall, contact angle  $\theta$ :

$$\mathbf{n}_i^\theta = \hat{\mathbf{n}}_i^{b\perp} \cos(\theta) + \hat{\mathbf{n}}_i^{b\parallel} \sin(\theta) \quad (29)$$

Smoothed normal prescription over distance  $y^+$ :

$$\mathbf{n}_i^\alpha = \alpha^+ \hat{\mathbf{n}}_i^\theta + (1 - \alpha^+) \tilde{\mathbf{n}}_i \quad (30)$$

$$\alpha^+ = \begin{cases} 1 & \text{for } y^+ \leq \Delta r \\ 1 + (\Delta r - y^+)/2h & \text{for } \Delta r < y^+ \leq 2h + \Delta r \\ 0 & \text{for } y^+ > 2h + \Delta r \end{cases} \quad (31)$$

Final surface normal with smoothed contact angle prescription, length is set to original fluid magnitude:

$$\mathbf{n}_i^{mod} = \hat{\mathbf{n}}_i^\alpha |\tilde{\mathbf{n}}_i| \quad (32)$$

Curvature calculations are only performed over particles (i) and their neighbours (j) that are identified to lie on the surface. For this we use the minimum eigenvalue ( $\lambda$ ) of the renormalisation matrix ( $\mathbf{L}_i$ ), if  $\lambda_i \leq 0.75$ , we say this particle lies on/near the surface and it is included in calculation and summations. A less binary surface identification would aid the stiffness of the ST method and improve convergence.

$$\kappa_i = \sum_j V_j (\hat{\mathbf{n}}_j^{mod} - \hat{\mathbf{n}}_i^{mod}) \cdot \nabla W_{ij} \quad (33)$$

Corrected curvature,  $\kappa^* = \kappa/\mathcal{L}$ , due to limited particle support from only using surface particles:

$$\mathcal{L}_i = \sum_j V_j W_{ij} \quad (34)$$

Surface tension body acceleration:

$$\mathbf{a}_{ST,i} = \frac{\sigma}{\rho_i} \kappa_i^* \mathbf{n}_i^{mod} \quad (35)$$

This first equation is incorrect. Modified normals should only influence effective curvature to set energy at boundaries, use smoothed normal as direction of surface tension acceleration:

$$\mathbf{a}_{ST,i} = \frac{\sigma}{\rho_i} \kappa_i^* \tilde{\mathbf{n}}_i \quad (36)$$

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Newmark integration

$$\dot{\mathbf{x}}^{n+1} = \dot{\mathbf{x}}^n + (1 - \gamma) \Delta t \ddot{\mathbf{x}}^n + \gamma \Delta t \ddot{\mathbf{x}}^{n+1} \quad (37)$$

$$\mathbf{x}^{n+1} = \mathbf{x}^n + \Delta t \dot{\mathbf{x}}^n + (0.5 - \beta) \Delta t^2 \ddot{\mathbf{x}}^n + \beta \Delta t^2 \ddot{\mathbf{x}}^{n+1} \quad (38)$$

## References

- [1] D. J. Price, “Smoothed particle hydrodynamics and magnetohydrodynamics,” *Journal of Computational Physics*, vol. 231, no. 3, pp. 759 – 794, 2012, special Issue: Computational Plasma Physics.
- [2] J. J. Monaghan, “Smoothed particle hydrodynamics,” *Annual review of astronomy and astrophysics*, vol. 30, 1992.

$$\begin{aligned}\frac{D\mathbf{u}_i}{Dt} = & -\sum_j m_j \left[ \frac{P_j}{\rho_j^2} + \frac{P_i}{\rho_i^2} + \Pi_{ij} \right] \nabla W_{ij} \\ & + \sum_j m_j \nu \frac{\rho_i + \rho_j}{\rho_i \rho_j} \frac{\mathbf{x}_{ij} \cdot \nabla W_{ij}}{|\mathbf{x}_{ij}|^2 + 0.001 h^2} \mathbf{u}_{ij} \\ & + \mathbf{a}_{ST,i} + \mathbf{g}\end{aligned}$$

$$\frac{D\rho_i}{Dt} = \sum_j m_j \mathbf{u}_{ij} \cdot \nabla W_{ij} + \delta h c_0 \mathcal{D}_i$$

$$P = \frac{\rho_0 c_0^2}{\gamma} \left[ \left( \frac{\rho}{\rho_0} \right)^\gamma - 1 \right]$$

$$M\ddot{x} + C_1\dot{x} + C_2|\dot{x}|\dot{x} + Kx = F_{sph}$$

$m_{eq}$	0.275	kg
$k$	1.1	N/mm
$f$	10.05	Hz
$\zeta$	0.23 - 0.34	%

$$\mathbf{n}_i = -\mathbf{L}_i \sum_j \nabla W_{ij} V_j$$

$$\tilde{\mathbf{n}}_i = \frac{\sum_j \mathbf{n}_i W_{ij} V_j}{\sum_j W_{ij} V_j}$$

$$\mathbf{n}_i^{mod} = f(\tilde{\mathbf{n}}_i, \theta, y^+)$$

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$$\mathbf{n}_i^\theta = \mathbf{n}_i^{b\perp} \cos(\theta) + \mathbf{n}_i^{b\parallel} \sin(\theta)$$

$$\mathbf{n}_i^\alpha = \alpha^+ \mathbf{n}_i^\theta + (1 - \alpha^+) \tilde{\mathbf{n}}_i$$

$$\alpha^+ = \begin{cases} 1 & \text{for } y^+ \leq \Delta r \\ 1 + (\Delta r - y^+)/2h & \text{for } \Delta r < y^+ \leq 2h + \Delta r \\ 0 & \text{for } y^+ > 2h + \Delta r \end{cases}$$


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$$\kappa_i = \sum_j V_j \left( \hat{\mathbf{n}}_j^{mod} - \hat{\mathbf{n}}_i^{mod} \right) \cdot \nabla W_{ij} \quad i, j : \lambda < 0.75$$

$$\mathcal{L}_i = \sum_j V_j W_{ij}$$

$$\kappa_i^* = \kappa_i / \mathcal{L}_i$$

$$\mathbf{a}_{ST,i} = \frac{\sigma}{\rho_i} \kappa_i^* \tilde{\mathbf{n}}_i$$

$$\mathbf{F}_{ij} = s_{ij} \cos\left(\frac{1.5\pi}{3h}|\mathbf{x}_{ij}|\right) \frac{\mathbf{x}_{ij}}{|\mathbf{x}_{ij}|}, \quad |\mathbf{x}_{ij}| \leq h \quad (39)$$

$$(\mathbf{a}_{ST})_i = -\frac{\sigma}{\rho_i} (\nabla \cdot \hat{\mathbf{n}})_i \mathbf{n}_i \quad (40)$$