

Assignment 4

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a) First,

$$\mathbf{C}_{ba} = \mathbf{C}_3(\theta) = \begin{bmatrix} \cos(\theta) & \sin(\theta) & 0 \\ -\sin(\theta) & \cos(\theta) & 0 \\ 0 & 0 & 1 \end{bmatrix}.$$

The position of p relative to w is given by:

$$\underline{r}^{pw} = \underline{\mathcal{F}}_b^T \mathbf{r}_b^{pw} = \underline{\mathcal{F}}_a^T \mathbf{C}_{ba}^T \mathbf{r}_b^{pw} = \underline{\mathcal{F}}_a^T \begin{bmatrix} \cos(\theta) & \sin(\theta) & 0 \\ -\sin(\theta) & \cos(\theta) & 0 \\ 0 & 0 & 1 \end{bmatrix}^T \begin{bmatrix} x_b \\ 0 \\ 0 \end{bmatrix} = \underline{\mathcal{F}}_a^T \underbrace{\begin{bmatrix} x_b \cos(\theta) \\ x_b \sin(\theta) \\ 0 \end{bmatrix}}_{\mathbf{r}_a^{pw}}$$

Thus, the velocity of p relative to w w.r.t. \mathcal{F}_a is:

$$\underline{v}^{pw/a} = \underline{r}^{pw \cdot a} = \left(\underline{\mathcal{F}}_a^T \mathbf{r}_a^{pw} \right)^{\cdot a} = \underline{\mathcal{F}}_a^T \dot{\mathbf{r}}_a^{pw} = \underline{\mathcal{F}}_a^T \underbrace{\begin{bmatrix} \dot{x}_b \cos(\theta) - x_b \sin(\theta) \dot{\theta} \\ \dot{x}_b \sin(\theta) + x_b \cos(\theta) \dot{\theta} \\ 0 \end{bmatrix}}_{\mathbf{v}_a^{pw/a}}$$

Finally, the acceleration of p relative to w w.r.t. \mathcal{F}_a is:

$$\begin{aligned} \underline{a}^{pw/a} &= \underline{v}^{pw/a \cdot a} = \left(\underline{\mathcal{F}}_a^T \mathbf{v}_a^{pw/a} \right)^{\cdot a} = \underline{\mathcal{F}}_a^T \dot{\mathbf{v}}_a^{pw/a} \\ &= \underline{\mathcal{F}}_a^T \underbrace{\begin{bmatrix} \ddot{x}_b \cos(\theta) - 2\dot{x}_b \sin(\theta) \dot{\theta} - x_b \cos(\theta) \dot{\theta}^2 - x_b \sin(\theta) \ddot{\theta} \\ \ddot{x}_b \sin(\theta) + 2\dot{x}_b \cos(\theta) \dot{\theta} - x_b \sin(\theta) \dot{\theta}^2 + x_b \cos(\theta) \ddot{\theta} \\ 0 \end{bmatrix}}_{\mathbf{a}_a^{pw/a}} \\ &= \underline{\mathcal{F}}_b^T \mathbf{C}_{ba} \mathbf{a}_a^{pw/a} = \underline{\mathcal{F}}_b^T \underbrace{\begin{bmatrix} \ddot{x}_b - x_b \dot{\theta}^2 \\ 2\dot{x}_b \dot{\theta} + x_b \ddot{\theta} \\ 0 \end{bmatrix}}_{\mathbf{a}_b^{pw/a}} \end{aligned}$$

Let $\underline{f}^{pt} = \begin{bmatrix} f_{b1}^{pt} & f_{b2}^{pt} & f_{b3}^{pt} \end{bmatrix} \underline{\mathcal{F}}_b$ be the reaction force of the table, $\underline{f}^{pg} = \begin{bmatrix} 0 & 0 & -mg \end{bmatrix} \underline{\mathcal{F}}_b$ the gravitational force applied on p and $\underline{f}^{ps} = \begin{bmatrix} -kx_b & 0 & 0 \end{bmatrix} \underline{\mathcal{F}}_b$ the spring force. Using the fact that the cut in the table is frictionless, i.e. $f_{b1}^{pt} = 0$, the total force acting on p becomes:

$$\underline{f}^p = \underline{f}^{pt} + \underline{f}^{pg} + \underline{f}^{ps} = \underline{\mathcal{F}}_b^T \underbrace{\begin{bmatrix} -kx_b \\ f_{b2}^{pt} \\ f_{b3}^{pt} - mg \end{bmatrix}}_{\mathbf{f}_b^p}$$

Since \mathcal{F}_a is an inertial frame and w is unforced, we can use Newton's Second Law to derive the differential equation that describes the motion of p :

$$\begin{aligned} m \underline{a}^{pw/a} &= \underline{f}^p \\ m \underline{\mathcal{F}}_b^T \underline{a}_b^{pw/a} &= \underline{\mathcal{F}}_b^T \mathbf{f}_b^p \\ m \underline{a}_b^{pw/a} &= \mathbf{f}_b^p \\ m \begin{bmatrix} \ddot{x}_b - x_b \dot{\theta}^2 \\ 2\dot{x}_b \dot{\theta} + x_b \ddot{\theta} \\ 0 \end{bmatrix} &= \begin{bmatrix} -kx_b \\ f_{b2}^{pt} \\ f_{b3}^{pt} - mg \end{bmatrix} \end{aligned} \quad (1)$$

We can see straight away that $f_{b3}^{pt} = mg$.

b) Using the fact that $\dot{\theta}$ is constant (i.e. $\ddot{\theta} = 0$) and rearranging, (1) can be rewritten as follows:

$$\ddot{x}_b + \left(\frac{k}{m} - \dot{\theta}^2\right)x_b = 0 \quad (2)$$

$$2\dot{x}_b \dot{\theta} - \frac{f_{b2}^{pt}}{m} = 0 \quad (3)$$

The general solution to (2), knowing that $\frac{k}{m} > \dot{\theta}^2$, is given by:

$$x_b(t) = A \cos(\omega t) + B \sin(\omega t), \quad A, B \in \mathbb{R}, \quad \omega = \sqrt{\frac{k}{m} - \dot{\theta}^2} \quad (4)$$

c) First, using the initial condition $x_b(0) = 0.1$, it yields:

$$x_b(0) = A = 0.1$$

. Secondly, using $\dot{x}_b(0) = 0$:

$$\dot{x}_b(0) = [-A\omega \sin(\omega t) + B\omega \cos(\omega t)]_{t=0} = B\omega = 0.$$

Therefore:

$$B = 0$$

and (4) can be rewritten as follows:

$$x_b(t) = 0.1 \cos(\omega t) \text{ [m]}, \quad \omega = \sqrt{\frac{k}{m} - \dot{\theta}^2}. \quad (5)$$

Lastly,

$$\dot{x}_b = -0.1\omega \sin(\omega t) \text{ [m/s]}, \quad (6)$$

$$\ddot{x}_b = -0.1\omega^2 \cos(\omega t) \text{ [m/s}^2\text{]}. \quad (7)$$

Using MATLAB, we obtain the following plots:

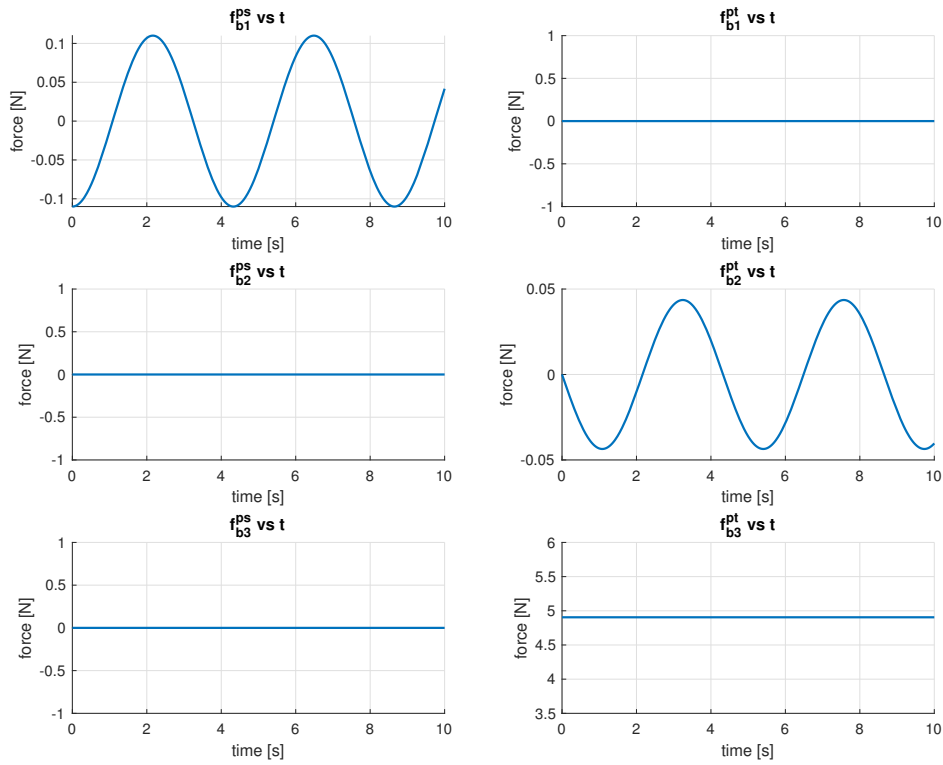


Figure 1: f_b^{pt} and f_b^{ps} vs time.

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a) Let θ be the angle between \underline{b}^2 and \underline{a}^2 . Therefore

$$\mathbf{C}_{ba} = \mathbf{C}_1(\theta) = \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos(\theta) & \sin(\theta) \\ 0 & -\sin(\theta) & \cos(\theta) \end{bmatrix}.$$

Moreover,

$$\underline{\omega}^{ba} = \underline{\mathcal{F}}_b^\top \begin{bmatrix} \dot{\theta} \\ 0 \\ 0 \end{bmatrix},$$

$$\begin{aligned} \underline{r}^{\kappa w} &= \underline{r}^{\kappa c} + \underline{r}^{cw} \\ &= \underline{\mathcal{F}}_b^\top \begin{bmatrix} 0 \\ y \\ 0 \end{bmatrix} + \underline{\mathcal{F}}_b^\top \begin{bmatrix} 0 \\ 0 \\ -d \end{bmatrix} \\ &= \underline{\mathcal{F}}_b^\top \begin{bmatrix} 0 \\ y \\ -d \end{bmatrix}, \end{aligned}$$

$$\begin{aligned} \underline{r}^{dmw} &= \underline{r}^{dmc} + \underline{r}^{cw} \\ &= \underline{\mathcal{F}}_b^\top \begin{bmatrix} \rho_{b1} \\ \rho_{b2} \\ \rho_{b3} \end{bmatrix} + \underline{\mathcal{F}}_b^\top \begin{bmatrix} 0 \\ 0 \\ -d \end{bmatrix} \\ &= \underline{\mathcal{F}}_b^\top \begin{bmatrix} \rho_{b1} \\ \rho_{b2} \\ \rho_{b3} - d \end{bmatrix}, \end{aligned}$$

$$\begin{aligned} \underline{r}^{\kappa w \bullet a} &= \underline{r}^{\kappa w \bullet b} + \underline{\omega}^{ba} \times \underline{r}^{\kappa w} \\ &= \underline{\mathcal{F}}_b^\top \left(\dot{\mathbf{r}}_b^{\kappa w} + \boldsymbol{\omega}_b^{ba \times} \mathbf{r}_b^{\kappa w} \right) \\ &= \underline{\mathcal{F}}_b^\top \left(\begin{bmatrix} 0 \\ \dot{y} \\ 0 \end{bmatrix} + \begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & -\dot{\theta} \\ 0 & \dot{\theta} & 0 \end{bmatrix} \begin{bmatrix} 0 \\ y \\ -d \end{bmatrix} \right) \\ &= \underline{\mathcal{F}}_b^\top \begin{bmatrix} 0 \\ \dot{y} + d\dot{\theta} \\ y\dot{\theta} \end{bmatrix}, \end{aligned}$$

$$\begin{aligned}
 \vec{r}^{dmw \cdot a} &= \vec{r}^{dmw \cdot b} + \vec{\omega}^{ba} \times \vec{r}^{dmw} \\
 &= \mathcal{F}_{\vec{r}^b}^T \left(\underbrace{\dot{\mathbf{r}}_b^{dmw}}_{=0} + \omega_b^{ba \times} \mathbf{r}_b^{dmw} \right) \\
 &= \mathcal{F}_{\vec{r}^b}^T \left(\begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & -\dot{\theta} \\ 0 & \dot{\theta} & 0 \end{bmatrix} \begin{bmatrix} \rho_{b1} \\ \rho_{b2} \\ \rho_{b3} - d \end{bmatrix} \right) \\
 &= \mathcal{F}_{\vec{r}^b}^T \begin{bmatrix} 0 \\ (d - \rho_{b3})\dot{\theta} \\ \rho_{b2}\dot{\theta} \end{bmatrix}.
 \end{aligned}$$

b) Figures 2 and 3 show the Free Body Diagrams of the particle κ and the body \mathcal{B} . Let \vec{f}^{r1} and \vec{f}^{r1} be the reaction forces applied by the massless bars on the body \mathcal{B} .

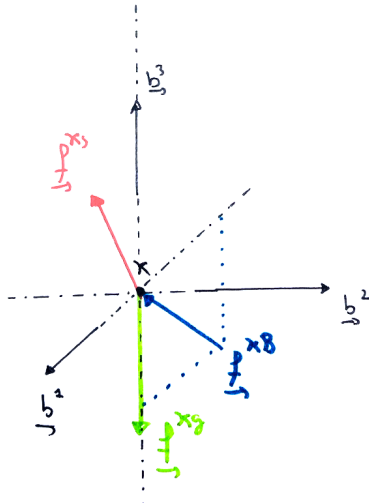


Figure 2: FBD of κ .

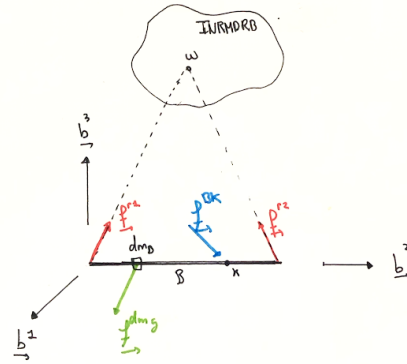


Figure 3: FBD of \mathcal{B} .

The norm of $\vec{r}^{\kappa w}$ is

$$\|\vec{r}^{\kappa w}\|_2 = \mathbf{r}_b^{\kappa w T} \mathbf{r}_b^{\kappa w} = y^2 + d^2.$$

Therefore, the total force applied on κ is given by:

$$\begin{aligned}\vec{f}_{\rightarrow \kappa} &= \vec{f}_{\rightarrow \kappa \mathcal{B}} + \vec{f}_{\rightarrow \kappa g} + \vec{f}_{\rightarrow \kappa s} \\ &= \mathcal{F}_{\rightarrow b}^T \left(\begin{bmatrix} f_{b1}^{\kappa \mathcal{B}} \\ 0 \\ f_{b3}^{\kappa \mathcal{B}} \end{bmatrix} + \mathcal{F}_{\rightarrow b}^T \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos(\theta) & \sin(\theta) \\ 0 & -\sin(\theta) & \cos(\theta) \end{bmatrix} \begin{bmatrix} 0 \\ 0 \\ -m_\kappa g \end{bmatrix} - k \frac{l_s - \bar{l}_s}{y^2 + d^2} \begin{bmatrix} 0 \\ y \\ -d \end{bmatrix} \right) \\ &= \mathcal{F}_{\rightarrow b}^T \begin{bmatrix} f_{b1}^{\kappa \mathcal{B}} \\ -m_\kappa g \sin(\theta) - ky \frac{l_s - \bar{l}_s}{y^2 + d^2} \\ f_{b3}^{\kappa \mathcal{B}} - m_\kappa g \cos(\theta) + kd \frac{l_s - \bar{l}_s}{y^2 + d^2} \end{bmatrix}.\end{aligned}$$

The total force acting on \mathcal{B} is given by:

$$\begin{aligned}\vec{f}_{\rightarrow \mathcal{B}} &= \vec{f}_{\rightarrow r1} + \vec{f}_{\rightarrow r2} + \vec{f}_{\rightarrow \mathcal{B}\kappa} + \int_{\mathcal{B}} d\vec{f}_{\rightarrow dm g} \\ &= \mathcal{F}_{\rightarrow b}^T \left(\begin{bmatrix} f_{b1}^{r1} \\ f_{b2}^{r1} \\ f_{b3}^{r1} \end{bmatrix} + \begin{bmatrix} f_{b1}^{r2} \\ f_{b2}^{r2} \\ f_{b3}^{r2} \end{bmatrix} - \begin{bmatrix} f_{b1}^{\kappa \mathcal{B}} \\ 0 \\ f_{b3}^{\kappa \mathcal{B}} \end{bmatrix} + \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos(\theta) & \sin(\theta) \\ 0 & -\sin(\theta) & \cos(\theta) \end{bmatrix} \int_{\mathcal{B}} \begin{bmatrix} 0 \\ 0 \\ -g \end{bmatrix} dm \right) \\ &= \mathcal{F}_{\rightarrow b}^T \begin{bmatrix} f_{b1}^{r1} + f_{b1}^{r2} - f_{b1}^{\kappa \mathcal{B}} \\ f_{b2}^{r1} + f_{b2}^{r2} - m_{\mathcal{B}} g \sin(\theta) \\ f_{b3}^{r1} + f_{b3}^{r2} - f_{b3}^{\kappa \mathcal{B}} - m_{\mathcal{B}} g \cos(\theta) \end{bmatrix}.\end{aligned}$$

Finally, the total moment applied on \mathcal{B} relative to w is given by:

$$\begin{aligned}\vec{m}_{\rightarrow \mathcal{B} w} &= \underbrace{\vec{r}_{\rightarrow}^{r1 w} \times \vec{f}_{\rightarrow}^{r1}}_{= \vec{0}} + \underbrace{\vec{r}_{\rightarrow}^{r2 w} \times \vec{f}_{\rightarrow}^{r2}}_{= \vec{0}} + \vec{r}_{\rightarrow}^{\kappa w} \times \vec{f}_{\rightarrow}^{\mathcal{B}\kappa} + \int_{\mathcal{B}} \vec{r}_{\rightarrow}^{dm w} \times d\vec{f}_{\rightarrow dm g} \\ &= \vec{r}_{\rightarrow}^{\kappa w} \times \vec{f}_{\rightarrow}^{\mathcal{B}\kappa} + \underbrace{\left(\int_{\mathcal{B}} \vec{r}_{\rightarrow}^{dm w} dm \right)}_{= m_{\mathcal{B}} \vec{r}_{\rightarrow}^{cw}} \times \vec{g} \\ &= \mathcal{F}_{\rightarrow b}^T \left(\begin{bmatrix} 0 \\ y \\ -d \end{bmatrix} \times \begin{bmatrix} -f_{b1}^{\kappa \mathcal{B}} \\ 0 \\ -f_{b3}^{\kappa \mathcal{B}} \end{bmatrix} + m_{\mathcal{B}} \begin{bmatrix} 0 \\ 0 \\ -d \end{bmatrix} \times \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos(\theta) & \sin(\theta) \\ 0 & -\sin(\theta) & \cos(\theta) \end{bmatrix} \begin{bmatrix} 0 \\ 0 \\ -g \end{bmatrix} \right) \\ &= \mathcal{F}_{\rightarrow b}^T \begin{bmatrix} -yf_{b3}^{\kappa \mathcal{B}} - dgm_{\mathcal{B}} \sin(\theta) \\ df_{b1}^{\kappa \mathcal{B}} \\ yf_{b1}^{\kappa \mathcal{B}} \end{bmatrix}\end{aligned}$$

c)

$$\vec{p}_{\rightarrow}^{\kappa w/a} = m_\kappa \vec{r}_{\rightarrow}^{\kappa w/a \cdot a} = m_\kappa \mathcal{F}_{\rightarrow b}^T \begin{bmatrix} 0 \\ \dot{y} + d\dot{\theta} \\ y\dot{\theta} \end{bmatrix} = \begin{bmatrix} 0 \\ m_\kappa(\dot{y} + d\dot{\theta}) \\ m_\kappa y\dot{\theta} \end{bmatrix}. \quad \square$$

$$\begin{aligned}
\vec{h}^{Bw/a} &= \int_{\mathcal{B}} \vec{r}^{dmw} \times \vec{r}^{dmw} \cdot^a dm \\
&= \mathcal{F}_{\vec{r}b}^T \left(\int_{\mathcal{B}} \begin{bmatrix} \rho_{b1} \\ \rho_{b2} \\ \rho_{b3} - d \end{bmatrix} \times \begin{bmatrix} 0 \\ (d - \rho_{b3})\dot{\theta} \\ \rho_{b2}\dot{\theta} \end{bmatrix} dm \right) \\
&= \mathcal{F}_{\vec{r}b}^T \left(\int_{\mathcal{B}} \begin{bmatrix} 0 & -(\rho_{b3} - d) & \rho_{b2} \\ (\rho_{b3} - d) & 0 & -\rho_{b1} \\ -\rho_{b2} & \rho_{b1} & 0 \end{bmatrix} \begin{bmatrix} 0 \\ (d - \rho_{b3})\dot{\theta} \\ \rho_{b2}\dot{\theta} \end{bmatrix} dm \right) \\
&= \mathcal{F}_{\vec{r}b}^T \left(\dot{\theta} \int_{\mathcal{B}} \begin{bmatrix} (d - \rho_{b3})^2 + \rho_{b2}^2 \\ -\rho_{b1}\rho_{b2} \\ \rho_{b1}(d - \rho_{b3}) \end{bmatrix} dm \right) \\
&= \mathcal{F}_{\vec{r}b}^T \left(\dot{\theta} \int_{V_{\mathcal{B}}} \begin{bmatrix} (d - \rho_{b3})^2 + \rho_{b2}^2 \\ -\rho_{b1}\rho_{b2} \\ \rho_{b1}(d - \rho_{b3}) \end{bmatrix} \left(\frac{m_{\mathcal{B}}}{lth} \right) dV \right) \\
&= \mathcal{F}_{\vec{r}b}^T \left(\frac{m_{\mathcal{B}}\dot{\theta}}{lth} \begin{bmatrix} lt[\int_{-h/2}^{h/2} (d - \rho_{b3})^2 d\rho_{b3}] + th[\int_{-l/2}^{l/2} \rho_{b2}^2 d\rho_{b2}] \\ -lth^2[\underbrace{\int_{-t/2}^{t/2} \rho_{b1} d\rho_{b1}}_0][\underbrace{\int_{-l/2}^{l/2} \rho_{b2} d\rho_{b2}}_0] \\ l^2ht[\underbrace{\int_{-t/2}^{t/2} \rho_{b1} d\rho_{b1}}_0][\int_{-h/2}^{h/2} (d - \rho_{b3}) d\rho_{b3}] \end{bmatrix} \right) \\
&= \mathcal{F}_{\vec{r}b}^T \left(\frac{m_{\mathcal{B}}\dot{\theta}}{lth} \begin{bmatrix} -\frac{lt}{3}[(d - \rho_{b3})^3]_{-h/2}^{h/2} + \frac{th}{3}[\rho_{b2}^3]_{-l/2}^{l/2} \\ 0 \\ 0 \end{bmatrix} \right) \\
&= \mathcal{F}_{\vec{r}b}^T \left(\frac{m_{\mathcal{B}}\dot{\theta}}{lth} \begin{bmatrix} -\frac{lt}{3}[-3d^2h - \frac{h^3}{4}] + \frac{th}{3}\frac{l^3}{4} \\ 0 \\ 0 \end{bmatrix} \right) \\
&= \mathcal{F}_{\vec{r}b}^T \left(m_{\mathcal{B}}\dot{\theta} \begin{bmatrix} d^2 + \frac{1}{12}(h^2 + l^2) \\ 0 \\ 0 \end{bmatrix} \right) . \quad \square
\end{aligned}$$

d) First, from N2L,

$$\vec{p}^{\kappa w/a} \cdot^a = \vec{f}^{\kappa}.$$

Using the Transport Theorem and developing:

$$\begin{aligned}
 \underline{\dot{p}}^{\kappa w/a \cdot a} &= \underline{\dot{p}}^{\kappa w/a \cdot b} + \underline{\omega}^{ba} \times \underline{\dot{p}}^{\kappa w/a} \\
 &= \underline{\mathcal{F}}_b^T \left(\begin{bmatrix} 0 \\ m_\kappa(\ddot{y} + d\ddot{\theta}) \\ m_\kappa(\dot{y}\dot{\theta} + y\ddot{\theta}) \end{bmatrix} + \begin{bmatrix} \dot{\theta} \\ 0 \\ 0 \end{bmatrix} \times \begin{bmatrix} 0 \\ m_\kappa(\dot{y} + d\dot{\theta}) \\ m_\kappa y\dot{\theta} \end{bmatrix} \right) \\
 &= \underline{\mathcal{F}}_b^T \begin{bmatrix} 0 \\ m_\kappa(\ddot{y} + d\ddot{\theta}) - m_\kappa y\dot{\theta}^2 \\ m_\kappa(\dot{y}\dot{\theta} + y\ddot{\theta}) + \dot{\theta}m_\kappa(\dot{y} + d\dot{\theta}) \end{bmatrix} \\
 &= \underline{\mathcal{F}}_b^T \begin{bmatrix} 0 \\ m_\kappa(\ddot{y} + d\ddot{\theta}) - m_\kappa y\dot{\theta}^2 \\ 2m_\kappa\dot{y}\dot{\theta} + m_\kappa y\ddot{\theta} + m_\kappa d\dot{\theta}^2 \end{bmatrix}
 \end{aligned}$$

Therefore,

$$\begin{bmatrix} 0 \\ m_\kappa(\ddot{y} + d\ddot{\theta}) - m_\kappa y\dot{\theta}^2 \\ 2m_\kappa\dot{y}\dot{\theta} + m_\kappa y\ddot{\theta} + m_\kappa d\dot{\theta}^2 \end{bmatrix} = \begin{bmatrix} f_{b1}^{\kappa B} \\ -m_\kappa g \sin(\theta) - ky \frac{l_s - \bar{l}_s}{y^2 + d^2} \\ f_{b3}^{\kappa B} - m_\kappa g \cos(\theta) + kd \frac{l_s - \bar{l}_s}{y^2 + d^2} \end{bmatrix}. \quad (8)$$

We can see straight away that

$$f_{b1}^{\kappa B} = 0.$$

Secondly,

$$\begin{aligned}
 \underline{\dot{h}}^{\mathcal{B}w/a \cdot a} &= \underline{\dot{h}}^{\mathcal{B}w/a \cdot b} + \underline{\omega}^{ba} \times \underline{\dot{h}}^{\mathcal{B}w/a} \\
 &= \underline{\mathcal{F}}_b^T \left(\begin{bmatrix} m_B\ddot{\theta}[d^2 + \frac{1}{12}(h^2 + l^2)] \\ 0 \\ 0 \end{bmatrix} + \begin{bmatrix} \dot{\theta} \\ 0 \\ 0 \end{bmatrix} \times \begin{bmatrix} m_B\dot{\theta}[d^2 + \frac{1}{12}(h^2 + l^2)] \\ 0 \\ 0 \end{bmatrix} \right) \\
 &= \underline{\mathcal{F}}_b^T \begin{bmatrix} m_B\ddot{\theta}[d^2 + \frac{1}{12}(h^2 + l^2)] \\ 0 \\ 0 \end{bmatrix}.
 \end{aligned}$$

From N2LR,

$$\underline{\dot{h}}^{\mathcal{B}w/a \cdot a} = \underline{\dot{m}}^{\mathcal{B}w}.$$

Therefore,

$$\underline{\mathcal{F}}_b^T \begin{bmatrix} m_B\ddot{\theta}[d^2 + \frac{1}{12}(h^2 + l^2)] \\ 0 \\ 0 \end{bmatrix} = \underline{\mathcal{F}}_b^T \begin{bmatrix} -yf_{b3}^{\kappa B} - dgm_B \sin(\theta) \\ df_{b1}^{\kappa B} \\ yf_{b1}^{\kappa B} \end{bmatrix}$$

In particular,

$$f_{b3}^{\kappa B} = -\frac{m_B}{y} \left(\ddot{\theta} [d^2 + \frac{1}{12}(h^2 + l^2)] + dg \sin(\theta) \right) \quad (9)$$

Finally, substituting (9) into (8),

$$m_\kappa(\ddot{y} + d\ddot{\theta}) - m_\kappa y \dot{\theta}^2 = -m_\kappa g \sin(\theta) - ky \frac{l_s - \bar{l}_s}{y^2 + d^2} \quad (10)$$

$$\begin{aligned} 2m_\kappa \dot{y} \dot{\theta} + m_\kappa y \ddot{\theta} + m_\kappa d \dot{\theta}^2 &= -\frac{m_B}{y} \left(\ddot{\theta} [d^2 + \frac{1}{12}(h^2 + l^2)] + dg \sin(\theta) \right) \\ &\quad - m_\kappa g \cos(\theta) + kd \frac{l_s - \bar{l}_s}{y^2 + d^2} \end{aligned} \quad (11)$$

e) The total moment applied on \mathcal{S} relative to w is given by:

$$\begin{aligned} \underline{M}_{\rightarrow}^{Sw} &= m_B \underline{r}_{\rightarrow}^{cw} \times \underline{g}_{\rightarrow} + m_\kappa \underline{r}_{\rightarrow}^{\kappa w} \times \underline{g}_{\rightarrow} \\ &= \underline{\mathcal{F}}_{\rightarrow b}^T \left(m_B \begin{bmatrix} 0 \\ 0 \\ -d \end{bmatrix} \times \begin{bmatrix} 0 \\ -\sin(\theta)g \\ -\cos(\theta)g \end{bmatrix} + m_\kappa \begin{bmatrix} 0 \\ y \\ -d \end{bmatrix} \times \begin{bmatrix} 0 \\ -\sin(\theta)g \\ -\cos(\theta)g \end{bmatrix} \right) \\ &= \underline{\mathcal{F}}_{\rightarrow b}^T \begin{bmatrix} -m_B dg \sin(\theta) + m_\kappa [-yg \cos(\theta) - dg \sin(\theta)] \\ 0 \\ 0 \end{bmatrix}. \quad \square \end{aligned}$$

Secondly,

$$\begin{aligned} \underline{h}_{\rightarrow}^{Sw/a} &= \underline{h}_{\rightarrow}^{Bw/a} + \underline{r}_{\rightarrow}^{\kappa w} \times \underline{p}_{\rightarrow}^{\kappa w/a} \\ &= \underline{\mathcal{F}}_{\rightarrow b}^T \left(\begin{bmatrix} m_B \dot{\theta} [d^2 + \frac{1}{12}(h^2 + l^2)] \\ 0 \\ 0 \end{bmatrix} + \begin{bmatrix} 0 \\ y \\ -d \end{bmatrix} \times \begin{bmatrix} 0 \\ m_\kappa(\dot{y} + d\dot{\theta}) \\ m_\kappa y \dot{\theta} \end{bmatrix} \right) \\ &= \underline{\mathcal{F}}_{\rightarrow b}^T \begin{bmatrix} m_B \dot{\theta} [d^2 + \frac{1}{12}(h^2 + l^2)] + m_\kappa [y^2 \dot{\theta} + d(\dot{y} + d\dot{\theta})] \\ 0 \\ 0 \end{bmatrix}. \end{aligned}$$

Therefore,

$$\begin{aligned} \underline{h}_{\rightarrow}^{Sw/a \cdot a} &= \underline{h}_{\rightarrow}^{Sw/a \cdot b} + \underbrace{\underline{\omega}^{ba} \times \underline{h}_{\rightarrow}^{Sw/a}}_{=0} \\ &= \underline{\mathcal{F}}_{\rightarrow b}^T \begin{bmatrix} m_B \ddot{\theta} [d^2 + \frac{1}{12}(h^2 + l^2)] + m_\kappa [2y \dot{y} \dot{\theta} + y^2 \ddot{\theta} + d(\ddot{y} + d\ddot{\theta})] \\ 0 \\ 0 \end{bmatrix}. \end{aligned}$$

And finally, applying N2LR, i.e. $\underline{h}^{\mathcal{S}w/a \bullet a} = \underline{m}^{\mathcal{S}w}$:

$$\begin{aligned} m_B \ddot{\theta} [d^2 + \frac{1}{12}(h^2 + l^2)] + m_\kappa [2y\dot{y}\dot{\theta} + y^2\ddot{\theta} + d(\ddot{y} + d\ddot{\theta})] \\ = -m_B dg \sin(\theta) + m_\kappa [-yg \cos(\theta) - dg \sin(\theta)] \end{aligned} \quad (12)$$

We can easily check that (12) is nothing else than $d \cdot (10) + y \cdot (11)$, and thus the two sets of DEs describe the same motion.