## Onde piane in un mezzo con perdite I

$$\nabla \times \hat{\mathbf{H}} = \hat{\mathbf{j}} + j\omega\varepsilon \hat{\mathbf{E}}$$

$$\nabla \times \hat{\mathbf{E}} = -j\omega\mu \hat{\mathbf{H}}$$

Legge di Ohm:

$$\hat{\mathbf{j}} = \boldsymbol{\sigma} \stackrel{\frown}{\mathbf{E}}$$

## Onde piane in un mezzo con perdite II

$$\nabla \times \hat{\mathbf{E}} = -j\omega\mu \hat{\mathbf{H}}$$

$$\nabla \times \hat{\mathbf{H}} = \sigma \hat{\mathbf{E}} + j\omega\varepsilon \hat{\mathbf{E}}$$

$$\nabla \times \hat{\mathbf{E}} = -j\omega\mu \hat{\mathbf{H}}$$

$$\nabla \times \hat{\mathbf{H}} = [\sigma + j\omega\varepsilon]\hat{\mathbf{E}}$$

## Onde piane in un mezzo con perdite III

$$\nabla \times \nabla \times \hat{\mathbf{E}} = -j\omega\mu \ \nabla \times \hat{\mathbf{H}} = -j\omega\mu \left[ \boldsymbol{\sigma} + j\omega\varepsilon \right] \hat{\mathbf{E}}$$

$$\nabla \times \nabla \times \hat{\mathbf{E}} = \nabla \nabla \cdot \hat{\mathbf{E}} - \nabla^2 \hat{\mathbf{E}}$$

$$\nabla \cdot \hat{\mathbf{E}} = 0$$

$$\nabla^{2} \hat{\mathbf{E}} - \gamma^{2} \hat{\mathbf{E}} = 0 \qquad \qquad \gamma^{2} = j \omega \mu \left[ \sigma + j \omega \varepsilon \right]$$

## Onde piane in un mezzo con perdite IV

$$\gamma = j\omega \sqrt{\varepsilon\mu} \left[ 1 + \frac{\sigma}{j\omega\varepsilon} \right]^{1/2}$$

$$\gamma = j\omega \sqrt{(\varepsilon' - j\varepsilon'')\mu} = j\omega \sqrt{\mu\varepsilon'(1 - j\tan\delta)}$$

γè la costante di fase

Se assumiamo che l'onda sia uniforme nel piano trasversale alla propagazione:

$$\partial_z^2 \hat{E}_x - \gamma^2 \hat{E}_x = 0$$

$$\hat{E}_{x} = E_{x}^{+} \exp(-\gamma z) + E_{x}^{-} \exp(+\gamma z)$$

## Onda piana progressiva con perdite: E

$$\gamma = \alpha + j\beta$$
  $\hat{E}_x = E_x^+ \exp(-(\alpha + j\beta)z) =$ 

$$\hat{E}_{x} = E_{x}^{+} \exp(-\alpha z) \exp(-j\beta z)$$

$$E_x(z,t) = \operatorname{Re} \left\{ \hat{E}_x \exp \left( j\omega t \right) \right\} =$$

$$= E_x^+ \exp(-\alpha z)\cos(\omega t - \beta z)$$

## Onda piana progressiva con perdite: H

$$\hat{H}_{y} = \frac{-j}{\omega\mu} \partial_{z} \hat{E}_{x} = \frac{-j\gamma}{\omega\mu} E_{x}^{+} \exp(-\gamma z)$$

$$H_{y}(z,t) = -\operatorname{Re}\left\{\frac{j(\alpha + j\beta)}{\omega\mu}E_{x}^{+}\exp\left(-(\alpha + j\beta)z\right)\exp\left(j\omega t\right)\right\} =$$

$$H_{y}(z,t) = -\operatorname{Re}\left\{\frac{j\alpha - \beta}{\omega\mu}E_{x}^{+}\exp\left(-(\alpha + j\beta)z\right)\exp\left(j\omega t\right)\right\} =$$

$$H_{y}(z,t) = -E_{x}^{+} \frac{\exp(-\alpha z)}{\omega \mu} \operatorname{Re} \left\{ (j\alpha - \beta) \exp \left( j(\omega t - \beta z) \right) \right\} =$$

$$= + E_{x}^{+} \frac{\exp(-\alpha z)}{\omega \mu} [\beta \cos(\omega t - \beta z) + \alpha \sin(\omega t - \beta z)]$$

## Propagazione buon conduttore

$$\sigma$$
 molto maggiore  $\omega \varepsilon$   $\sigma = 5.81 \cdot 10^{-7} \text{ S/m}$  (Cu)

a 1 GHz 
$$\omega \varepsilon = 2\pi \cdot 10^{-9} \cdot 8.854 \cdot 10^{-12} = 0.055 \text{ S/m}$$

$$\gamma = j\omega \sqrt{\varepsilon\mu} \left[ 1 + \frac{\sigma}{j\omega\varepsilon} \right]^{1/2} \approx \sqrt{j\omega\mu\sigma}$$

$$= \frac{1+j}{\sqrt{2}} \sqrt{\omega \mu \sigma} = (1+j) \sqrt{\pi f \mu \sigma}$$

# Profondità di penetrazione

$$\delta = \frac{1}{\sqrt{\pi f \mu \sigma}}$$

$$\hat{E}_{x} = E_{x}^{+} \exp(-z/\delta) \exp(-jz/\delta)$$

#### Profondità di penetrazione di Al, Cu, Au, Ag

$$f = 10 \text{ GHz}$$

$$\delta = \frac{1}{\sqrt{\pi f \mu \sigma}}$$

$$\delta_{AI} = 8.14 \cdot 10^{-7} \text{ m}$$

$$\delta_{Al} = 8.14 \cdot 10^{-7} \text{ m} \qquad \delta_{Au} = 7.86 \cdot 10^{-7} \text{ m}$$

$$\delta_{Cu} = 6.6 \cdot 10^{-7} \text{ m}$$

$$\delta_{Ag} = 6.4 \cdot 10^{-7} \text{ m}$$

# A 100 Hz...

$$\delta_{Al} = 8.14 \text{ mm}$$

$$\delta_{Au} = 7.86 \text{ mm}$$

$$\delta_{Cu} = 6.6 \text{ mm}$$

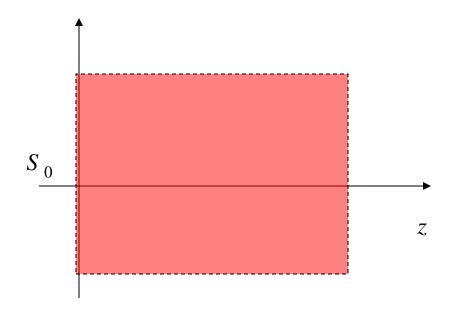
$$\delta_{Ag} = 6.4 \text{ mm}$$

## Impedenza d'onda in un buon conduttore

$$\frac{j\omega\mu_0}{jk} = \frac{j\omega\mu_0}{\gamma} \Rightarrow \eta \approx (1+j)\sqrt{\frac{\omega\mu_0}{2\sigma}} = (1+j)\frac{1}{\sigma\delta}$$

L'angolo di fase dell'impedenza d'onda vale 0° per un Dielettrico senza perdite, mentre è un valore compreso tra –45° e +45 per un mezzo qualsiasi.

#### Potenza assorbita da un buon conduttore



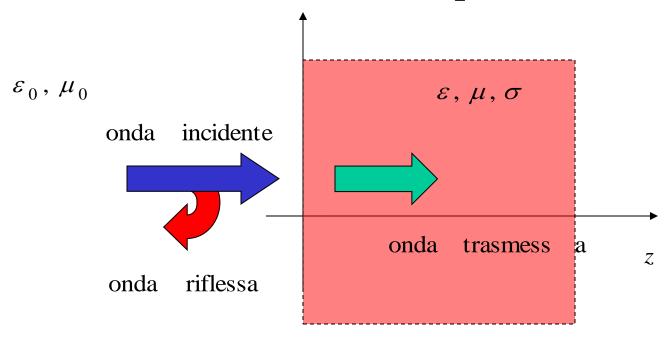
$$P_{av} = \frac{1}{2} \operatorname{Re} \int_{\partial V} \hat{\mathbf{E}} \times \hat{\mathbf{H}}^* \cdot \mathbf{n} \, dS = \frac{1}{2} \operatorname{Re} \int_{S_0} \hat{\mathbf{E}} \times \hat{\mathbf{H}}^* \cdot \mathbf{u}_z \, dS =$$

$$P_{av} = \frac{1}{2} \operatorname{Re} \left\{ \eta \int_{S_0} \hat{\mathbf{H}} \cdot \hat{\mathbf{H}}^* dS \right\} = \frac{1}{2} \operatorname{Re} \left\{ \eta \right\} \int_{S_0} \left| \hat{\mathbf{H}} \right|^2 dS = \frac{1}{2} R_s \int_{S_0} \left| \hat{\mathbf{H}} \right|^2 dS = \frac{1}{2} R_s \int_{S_0} \left| \hat{\mathbf{J}}_s \right|^2 dS$$

# Resistenza superficiale $[\Omega]$

$$R_s = \text{Re}\left\{ (1+j)\sqrt{\frac{\omega\mu}{2\sigma}} \right\} = \sqrt{\frac{\omega\mu}{2\sigma}} = \frac{1}{\sigma\delta}$$

## Riflessione di un'onda piana



$$\hat{\mathbf{E}}_{i} = \mathbf{u}_{x} E_{0} \exp \left(-jk_{0} z\right)$$

$$\hat{\mathbf{H}}_{i} = \mathbf{u}_{y} \frac{E_{0}}{\eta_{0}} \exp\left(-jk_{0}z\right)$$

$$\hat{\mathbf{E}}_{r} = \mathbf{u}_{x} \Gamma E_{0} \exp \left( j k_{0} z \right)$$

$$\hat{\mathbf{H}}_{r} = -\mathbf{u}_{y} \Gamma \frac{E_{0}}{\eta_{0}} \exp \left(jk_{0}z\right)$$

## Continuità dei campi tangenziali

#### Onda trasmessa:

$$\hat{\mathbf{E}}_{t} = \mathbf{u}_{x} T E_{0} \exp(-\gamma z) \qquad \eta = \frac{j \omega \mu}{\gamma}$$

$$\hat{\mathbf{H}}_{t} = \mathbf{u}_{y} T \frac{E_{0}}{\eta} \exp(-\gamma z) \qquad \gamma = j \omega \sqrt{\mu \varepsilon} \sqrt{1 - j \sigma /(\omega \varepsilon)}$$

Continuità delle componenti tangenziali:

$$\hat{\mathbf{E}}_{i}(z=0) + \hat{\mathbf{E}}_{r}(z=0) = \hat{\mathbf{E}}_{t}(z=0) \qquad \Leftrightarrow 1 + \Gamma = T$$

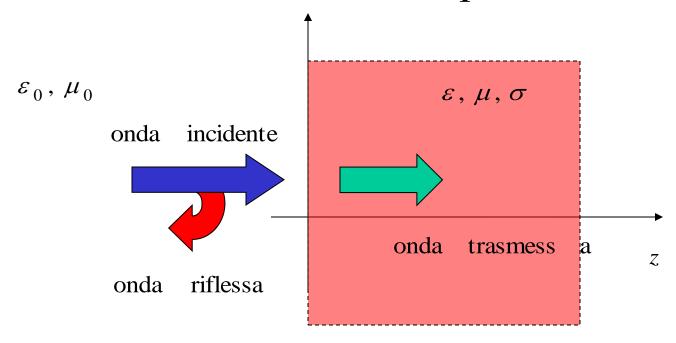
$$\hat{\mathbf{H}}_{i}(z=0) + \hat{\mathbf{H}}_{r}(z=0) = \hat{\mathbf{H}}_{t}(z=0) \qquad \Leftrightarrow \frac{1-\Gamma}{\eta_{0}} = \frac{T}{\eta_{0}}$$

#### Coefficienti di riflessione e trasmissione

$$\Gamma = \frac{\eta - \eta_0}{\eta + \eta_0}$$

$$T = 1 + \Gamma = \frac{2\eta}{\eta + \eta_0}$$

#### Riflessione di un'onda piana



$$\hat{\mathbf{E}} = \hat{\mathbf{E}}_{i} + \hat{\mathbf{E}}_{r} = \mathbf{u}_{x} E_{0} \left[ \exp \left( -jk_{0}z \right) + \Gamma \exp \left( jk_{0}z \right) \right]$$

$$\hat{\mathbf{H}} = \hat{\mathbf{H}}_{i} + \hat{\mathbf{H}}_{r} = \mathbf{u}_{y} \frac{E_{0}}{\eta_{0}} \left[ \exp\left(-jk_{0}z\right) - \Gamma \exp\left(+jk_{0}z\right) \right]$$

#### Vettore di Poynting (z < 0)

$$\hat{\mathbf{E}} \times \hat{\mathbf{H}}^* = \mathbf{u}_x \times \mathbf{u}_y E_0 \left[ \exp\left(-jk_0 z\right) + \Gamma \exp\left(jk_0 z\right) \right] \cdot \frac{E_0^*}{\eta_0} \left[ \exp\left(jk_0 z\right) - \Gamma^* \exp\left(-jk_0 z\right) \right]$$

$$= \mathbf{u}_{z} \frac{\left| E_{0} \right|^{2}}{\eta_{0}} \left\{ 1 - \left| \Gamma \right|^{2} + 2 j \operatorname{Im} \left[ \Gamma \exp \left( + 2 j k_{0} z \right) \right] \right\}$$

#### Vettore di Poynting (z > 0)

$$\hat{\mathbf{E}} \times \hat{\mathbf{H}}^* = \mathbf{u}_x \times \mathbf{u}_y E_0 T \exp(-\gamma z) \cdot \frac{E_0 T}{\eta^*} \exp(-\gamma * z) =$$

$$\Gamma = \frac{\eta - \eta_0}{\eta + \eta_0}$$

$$T = 1 + \Gamma = \frac{2\eta}{\eta + \eta_0}$$

$$= \mathbf{u}_{z} \frac{\left| E_{0} \right|^{2}}{\eta^{*}} \left| T \right|^{2} \exp(-2\alpha z)$$

$$\eta_0 = \sqrt{\frac{\mu_0}{\varepsilon_0}}; \quad \eta = \frac{j\omega\mu_0}{\gamma} \gamma = j\omega\sqrt{\mu\varepsilon}\sqrt{1 - j\sigma/(\omega\varepsilon)}$$

#### Assenza di perdite $\sigma=0$ , $\alpha=0$

$$\gamma = j\omega \sqrt{\mu\varepsilon}$$

$$\gamma = j\omega\sqrt{\mu\varepsilon}$$

$$\eta_0 = \sqrt{\frac{\mu_0}{\varepsilon_0}}; \quad \eta = \frac{j\omega\mu}{j\omega\sqrt{\mu\varepsilon}} = \sqrt{\frac{\mu}{\varepsilon}}$$

$$\Gamma = \frac{\eta - \eta_0}{\eta + \eta_0} \quad T = 1 + \Gamma = \frac{2\eta}{\eta + \eta_0} \quad Entrambi \ reali$$

$$(\mathbf{z} < 0) \qquad \hat{\mathbf{E}} \times \hat{\mathbf{H}}^* = \mathbf{u}_z \frac{\left| E_0 \right|^2}{\eta_0} \left\{ 1 - \left| \Gamma \right|^2 + 2 j \Gamma \sin \left( 2 k_0 z \right) \right\}$$

$$(\mathbf{z} > 0) \qquad \hat{\mathbf{E}} \times \hat{\mathbf{H}}^* = \mathbf{u}_z \frac{\left| E_0 \right|^2}{n} \left| T \right|^2$$

$$(\mathbf{z} > 0) \hat{\mathbf{E}} \times \hat{\mathbf{H}}^* = \mathbf{u}_z \frac{\left| E_0 \right|^2}{\eta} \left| \frac{2\eta}{\eta + \eta_0} \right|^2 = \mathbf{u}_z \frac{\left| E_0 \right|^2}{(\eta + \eta_0)^2} 4\eta$$

$$(\mathbf{z} < 0) \quad \text{Re } \left\{ \hat{\mathbf{E}} \times \hat{\mathbf{H}}^* \right\} = \mathbf{u}_z \frac{\left| E_0 \right|^2}{\eta_0} \left( 1 - \frac{(\eta - \eta_0)^2}{(\eta + \eta_0)^2} \right) =$$

$$= \mathbf{u}_z \frac{\left| E_0 \right|^2}{\eta_0} \frac{4\eta\eta_0}{(\eta + \eta_0)^2}$$

#### Buon conduttore

$$\eta = (1+j)\sqrt{\frac{\omega\mu_0}{2\sigma}} = \frac{1+j}{\sigma\delta}$$

$$\gamma = \alpha+j\beta = \frac{1+j}{\delta}$$

$$\gamma = \alpha + j\beta = \frac{1+j}{\delta}$$

$$(\mathbf{z} > 0) \quad \hat{\mathbf{E}} \times \hat{\mathbf{H}}^* = \mathbf{u}_z \frac{\left| E_0 \right|^2}{\eta^*} \left| T \right|^2 \exp(-2\alpha z) =$$

$$= \mathbf{u}_{z} \frac{\left| E_{0} \right|^{2}}{2} \sigma \delta (1+j) \left| T \right|^{2} \exp(-2\alpha z) =$$

$$\left|\Gamma\right|^{2} = \left|\frac{(1+j)/(\sigma\delta) - \eta_{0}}{(1+j)/(\sigma\delta) + \eta_{0}}\right|^{2} = \frac{(1/(\sigma\delta) - \eta_{0})^{2} + 1/(\sigma\delta)^{2}}{(1/(\sigma\delta) + \eta_{0})^{2} + 1/(\sigma\delta)^{2}}$$

$$1 - \left| \Gamma \right|^2 = \frac{\left( 1 / (\sigma \delta) + \eta_0 \right)^2 - \left( 1 / (\sigma \delta) - \eta_0 \right)^2}{\left( 1 / (\sigma \delta) + \eta_0 \right)^2 + 1 / (\sigma \delta)^2} =$$

$$= \frac{4\eta_0 /(\sigma \delta)}{\left(1/(\sigma \delta) + \eta_0\right)^2 + 1/(\sigma \delta)^2}$$

$$\left|T\right|^{2} = \left|1 + \Gamma\right|^{2} = \left|1 + \frac{\left(1 + j\right)/(\sigma\delta) - \eta_{0}}{\left(1 + j\right)/(\sigma\delta) + \eta_{0}}\right|^{2} =$$

$$= \left| \frac{(1+j)/(\sigma\delta) + \eta_0 + (1+j)/(\sigma\delta) - \eta_0}{(1+j)/(\sigma\delta) + \eta_0} \right|^2 =$$

$$= \left| \frac{2(1+j)/(\sigma\delta)}{(1+j)/(\sigma\delta) + \eta_0} \right|^2 = \frac{8/(\sigma\delta)^2}{(1/(\sigma\delta) + \eta_0)^2 + 1/(\sigma\delta)^2}$$

$$(\mathbf{Z}=\mathbf{0}^{\scriptscriptstyle +})$$

$$\hat{\mathbf{E}} \times \hat{\mathbf{H}}^* = \mathbf{u}_z \frac{\left| E_0 \right|^2}{2} \sigma \delta (1+j) \frac{8/(\sigma \delta)^2}{\left( 1/(\sigma \delta) + \eta_0 \right)^2 + 1/(\sigma \delta)^2} =$$

$$\Rightarrow \operatorname{Re}\left(\hat{\mathbf{E}} \times \hat{\mathbf{H}}^*\right) = \mathbf{u}_z \left| E_0 \right|^2 \frac{4 / (\sigma \delta)}{\left(1 / (\sigma \delta) + \eta_0\right)^2 + 1 / (\sigma \delta)^2}$$

$$\operatorname{Re}\left(\hat{\mathbf{E}} \times \hat{\mathbf{H}}^*\right) = \mathbf{u}_z \frac{\left|E_0\right|^2}{\eta_0} \frac{4\eta_0 /(\sigma\delta)}{\left(1/(\sigma\delta) + \eta_0\right)^2 + 1/(\sigma\delta)^2}$$

#### Onda piana riflessa da un conduttore

Un'onda piana incide normalmente su un semispazio riempito di rame. Se f=1GHz, si calcoli la costante di propagazione, l'impedenza, la profondità di penetrazione. Si calcolino inoltre i coefficienti di riflessione e di trasmissione.

$$\sigma = 5.83 \cdot 10^{7} \text{ S/m}$$
  $\delta = \frac{1}{\sqrt{\pi f \mu \sigma}} = 2.088 \cdot 10^{-6} \text{ m}$ 

$$\gamma = \frac{1+j}{\delta} = (4.789 + j4.789) \cdot 10^5 \text{ m}^{-1}$$

$$\eta = \frac{1+j}{\sigma \delta} = (8.239 + j8.239) \cdot 10^{-3} \Omega$$

Onda piana riflessa da un conduttore II

$$\Gamma = \frac{\eta - \eta_0}{\eta + \eta_0} = 1 \angle 179.99^{\circ}$$

$$T = \frac{2\eta}{\eta + \eta_0} = 6.181 \times 10^{-5} \angle 45^{\circ}$$

#### Onda piana incidente su uno slab dielettrico

