

## AE 410 Assignment -2

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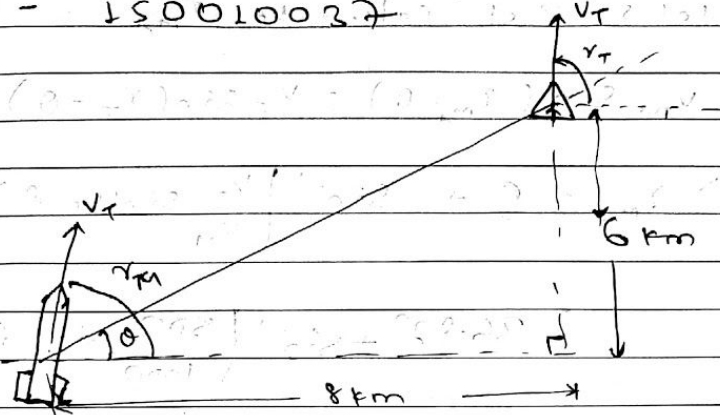
### ASSIGNMENT-2

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Name:- Ram Milan Kumar Verma

Roll - 150010037

Q.1.



from above figure, we have  $\tan \theta = \frac{6}{8}$

$$\Rightarrow \theta = \tan^{-1}\left(\frac{3}{4}\right) = 36.87^\circ$$

Also according to question

$$V_T = 500 \text{ m/s} \quad ; \quad \gamma_T = 0^\circ$$

$$V_M = 1000 \text{ m/s} \quad ; \quad \gamma_M = 60^\circ$$

(a.) LOS rate calculation,  $\dot{\theta}$

$$\dot{\theta} = \frac{V_T \sin(\gamma_T - \theta) - V_M \sin(\gamma_M - \theta)}{r}$$

$$= \frac{500 \times \sin(0^\circ - 36.87^\circ) - 1000 \times \sin(60^\circ - 36.87^\circ)}{\sqrt{8000^2 + 6000^2}}$$

$$= \frac{-500 \sin(36.87^\circ) - 1000 \sin(23.13^\circ)}{\sqrt{8000^2 + 6000^2}}$$

$$= -0.0693 \text{ rad/s} \approx -0.07 \text{ rad/s}$$

Closing speed,  $V_c = -V_r$

$$= -[V_T \cos(\gamma_T - \theta) - V_M \cos(\gamma_M - \theta)]$$

$$= -[500 \times \cos(0^\circ - 36.87^\circ) - 1000 \times \cos(60^\circ - 36.87^\circ)]$$

$$= 519.62 \text{ m/s}$$

Missile's heading error calculation

let's first calculate  $r_{M_d}$

$$v_M \sin(r_{M_d} - \theta) = v_T \sin(r_T - \theta)$$

$$\Rightarrow r_{M_d} = \theta + \sin^{-1} \left[ \frac{v_T \sin(r_T - \theta)}{v_M} \right]$$

$$= 36.87^\circ + \sin^{-1} \left( \frac{500}{1000} \sin(0^\circ - 36.87^\circ) \right)$$

$$= 19.41^\circ$$

$$\text{Heading error, HE} = r_M - r_{M_d} = 60^\circ - 19.41^\circ = 40.59^\circ$$

(b) If target moves towards missile at flight path angle of  $150^\circ$  with reference,

$$r_T = 150^\circ$$

$$\dot{\theta} = \frac{v_T \sin(r_T - \theta) - v_M \sin(r_M - \theta)}{r} = 6.31 \times 10^{-3} \text{ rad/s}$$

$$\dot{\theta} \approx 0.0063 \text{ rad/s}$$

Since LOS rate is non zero, hence not on collision triangle but rate is small and nearly zero.

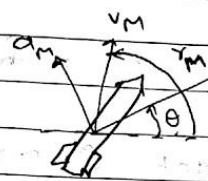
$$2.1) V_{x_0} = v_T \cos(r_T - \theta) - v_M \cos(r_M - \theta) = -1116.03 \text{ m/s}$$

$$V_{y_0} = v_T \sin(r_T - \theta) - v_M \sin(r_M - \theta) = 66.99 \text{ m/s}$$

$$r_{\text{miss}} = r_0 \sqrt{\frac{V_{y_0}^2}{V_{x_0}^2 + V_{y_0}^2}} = 599.17 \text{ m}$$

Q.2.

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$V_M = 500 \text{ m/s}$   
 $V_T = 300 \text{ m/s}$   
 $\gamma_T = 120^\circ$   
 $\theta_0 = 30^\circ$   
 $r_0 = 10 \text{ km}$

for pure pursuit guidance,  $\gamma_M = 0$

Since the missile always chases the target by directly moving towards it.

Now, we have the relation

$$t = \frac{r_0 [V_T \cos(\gamma_T - \theta_0) + V_M] - r [V_T \cos(\gamma_T - \theta) + V_M]}{-V_T^2 + V_M^2} \quad \text{--- (i)}$$

At the collision,  $t = t_f$  &  $r = 0$

$$\Rightarrow t_f = \frac{r_0 [V_T \cos(\gamma_T - \theta_0) + V_M]}{-V_T^2 + V_M^2} = 31.25 \text{ sec.} \quad \text{--- (ii)}$$

We have relation between  $r$  and  $\theta$  as

$$r = \frac{k \{\sin(\gamma_T - \theta)\}^{v-1}}{[1 + \cos(\gamma_T - \theta)]^v} \quad \text{--- (iii)}$$

$v = \frac{V_T}{V_M} = 0.6$

$k = \frac{r_0 [1 + \cos(\gamma_T - \theta_0)]^v}{[\sin(\gamma_T - \theta_0)]^{v-1}} = 10000$

from (i) & (ii) we have

$$\theta = \gamma_T - \cos^{-1} \left[ \frac{(t_f - t)(V_T^2 - V_M^2)}{r V_T} \right] \quad \text{--- (iv)}$$

$$\theta = \gamma_T - \cos^{-1} \left[ \frac{(t_f - t)(V_T^2 - V_M^2)}{r V_T} - \frac{V_M}{V_T} \right] \quad \text{--- (iv)}$$

Now we will form an array of time from  $[0, t_f]$  and using (iii) & (iv)

we'll find  $r$  as a function of time

then we can get  $\theta$  as function of time then we can get trajectories of missile and target

And Guidance command can be found by

$$a_m = \frac{V_m V_r \sin^2(\gamma_r - \theta)}{K \left\{ \tan\left(\frac{\gamma_r - \theta}{2}\right) \right\}^2}$$

but since no solver of MATLAB (fsolve, fzero, isignonlin) was able to give a solution to implicit equations correctly.

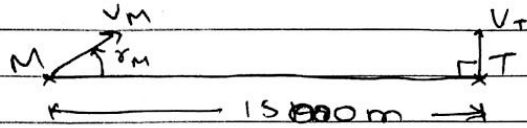
So I tried another way.

used  $\dot{r}$ ,  $\dot{\theta}$ ,  $\dot{r}_m$ ,  $a_m$  expressions and integrated for a small time step to get next step value by

$$r(t+dt) = r(t) + \dot{r} dt$$

Plots:-

Q.3:



$$r_0 = 15000 \text{ m}; \quad V_M = 500 \text{ m/s}; \quad V_T = 300 \text{ m/s}$$

$$\theta_0 = 0^\circ; \quad \gamma_T = 90^\circ$$

$$V_r = V_T \cos(\gamma_T - \theta) - V_M \cos(\gamma_M - \theta)$$

$$= V_T \cos(90^\circ) - V_M \cos(\gamma_M - 0)$$

$$V_\theta = V_T \sin(\gamma_T - \theta) - V_M \sin(\gamma_M - \theta) = 0$$

$$\Rightarrow 300 \times \sin(90^\circ) - 500 \sin(\gamma_M) = 0$$

$$\Rightarrow \gamma_M = \sin^{-1}\left(\frac{3}{5}\right) = 36.87^\circ$$

Q.3.(a)  $\gamma_M$ , launch angle =  $36.87^\circ$ .

Q.3.(b)  $HE = \pm 2^\circ$

$$\text{gn PPN}, \quad \dot{\gamma}_M = N\dot{\theta} \Rightarrow a_M = NV_M\dot{\theta}$$

$$\text{for TPN} \quad \dot{\gamma}_M = \frac{a_M \cos(\gamma_M - \theta)}{V_M} \Rightarrow a_M = -N'V_T\dot{\theta}$$

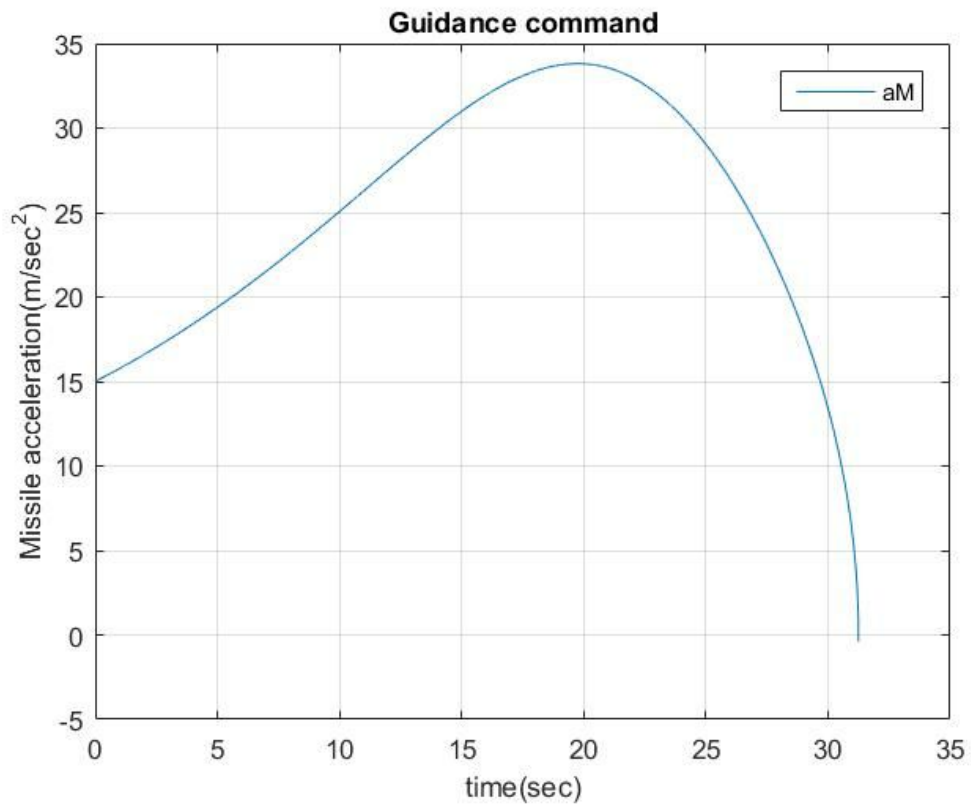
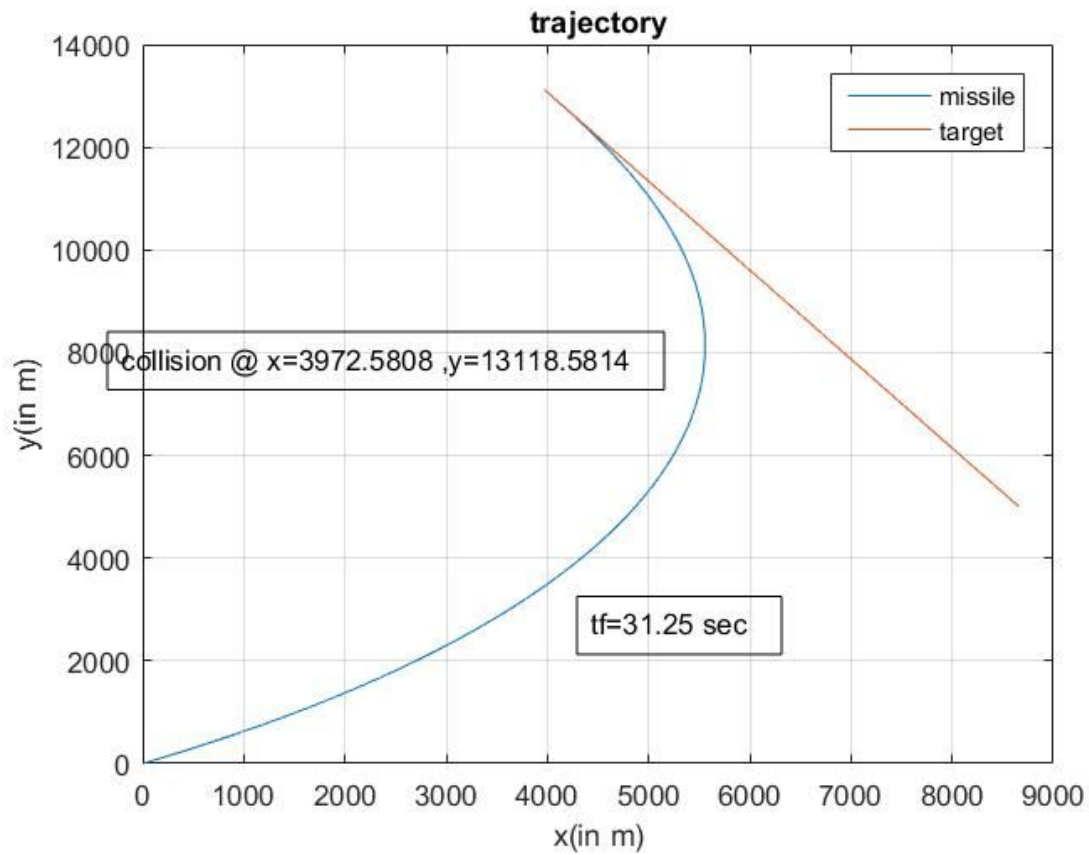
$$\dot{V}_M = a_M \sin(\gamma_M - \theta)$$

Plots:-

## Plots for Question 2 and 3

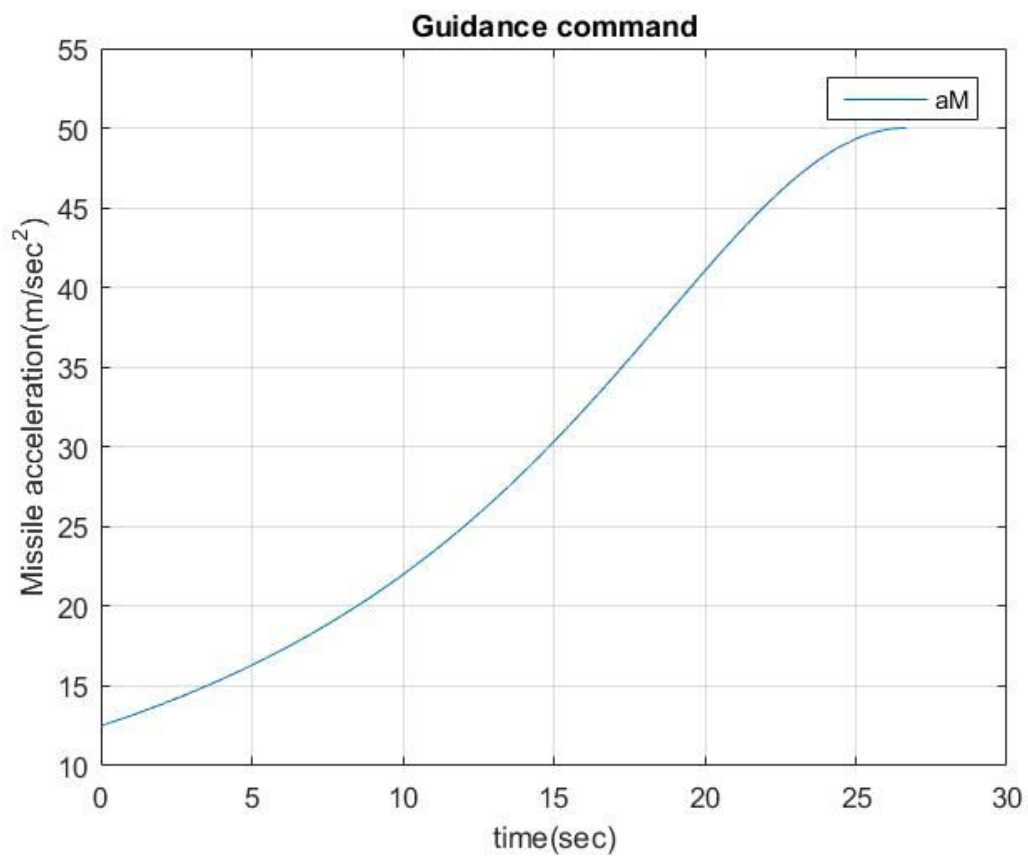
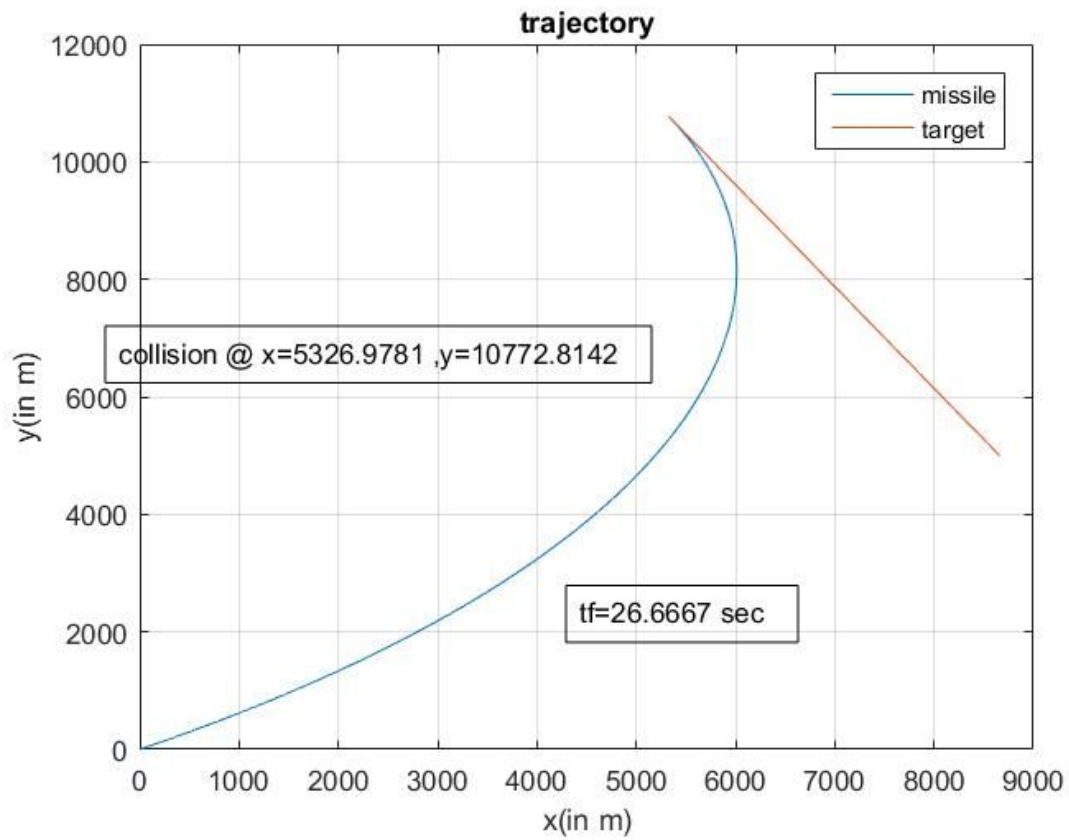
### Q.2.(a)

Trajectory and guidance command plot when missile follows pure pursuit guidance.



### Q.2.(b)

When velocity of target,  $V_T = 250$  m/s



Here, result agrees with the theory. The acceleration requirement towards the interception depends upon  $v = \frac{V_M}{V_T}$

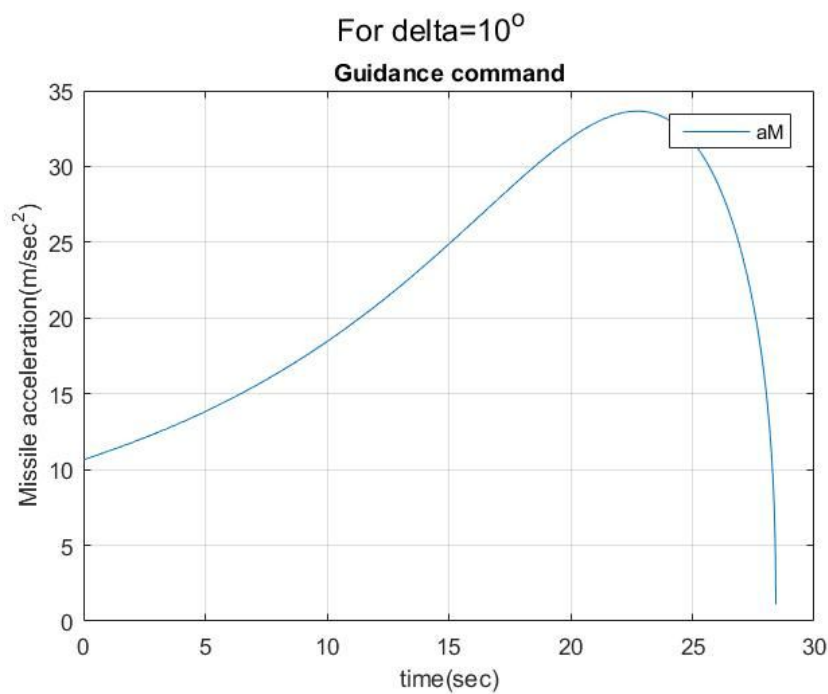
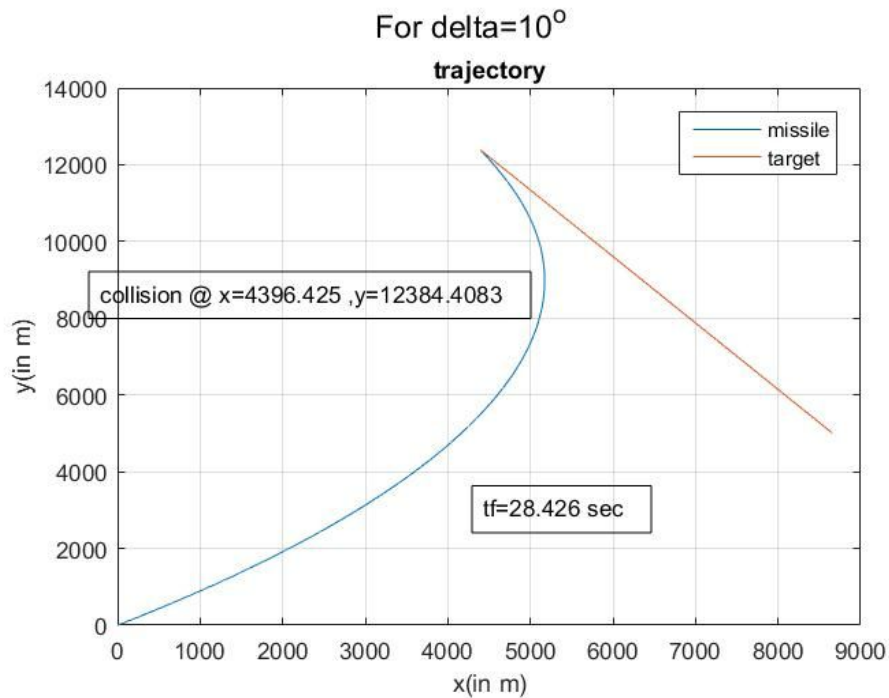
For  $1 < v < 2$   $a_M$  is zero

For  $v = 2$   $a_M$  is finite which is the case when  $V_T = 250$

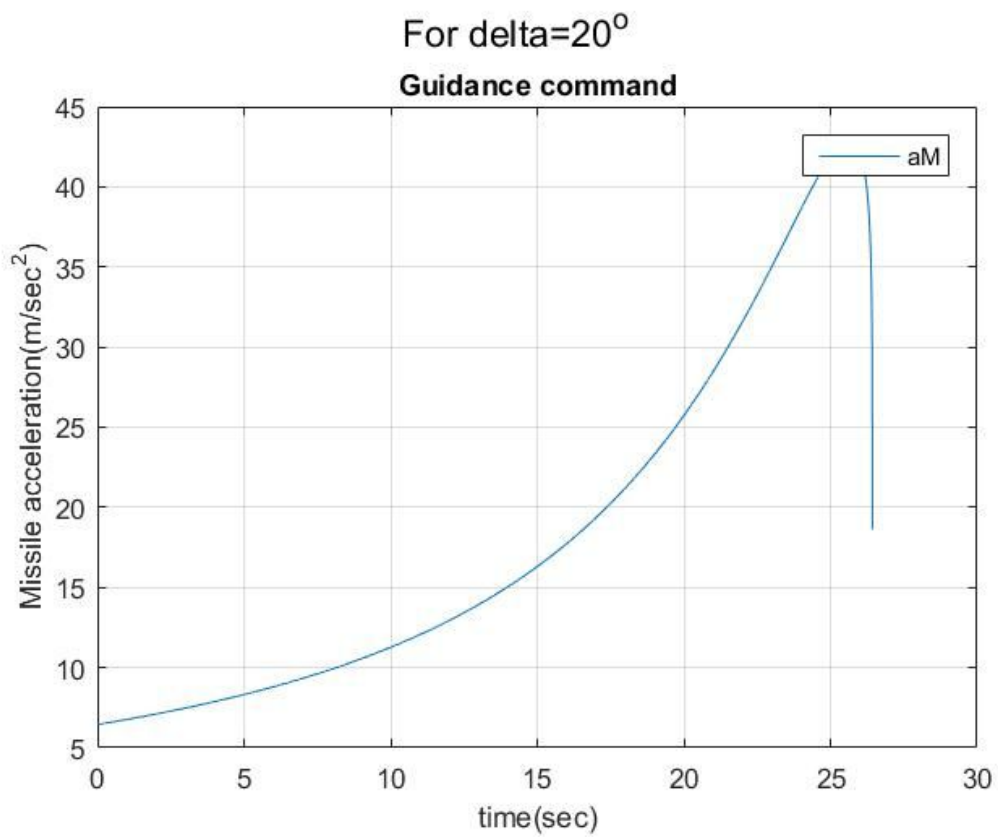
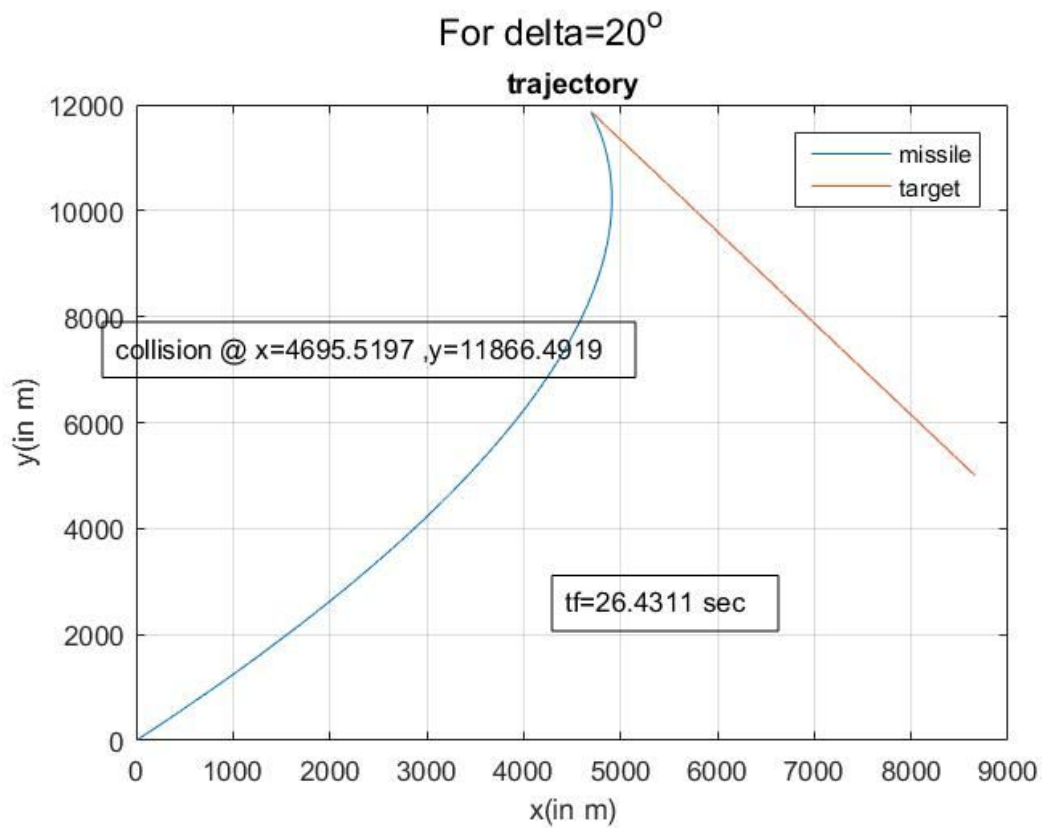
For  $v > 2$   $a_M$  is infinite

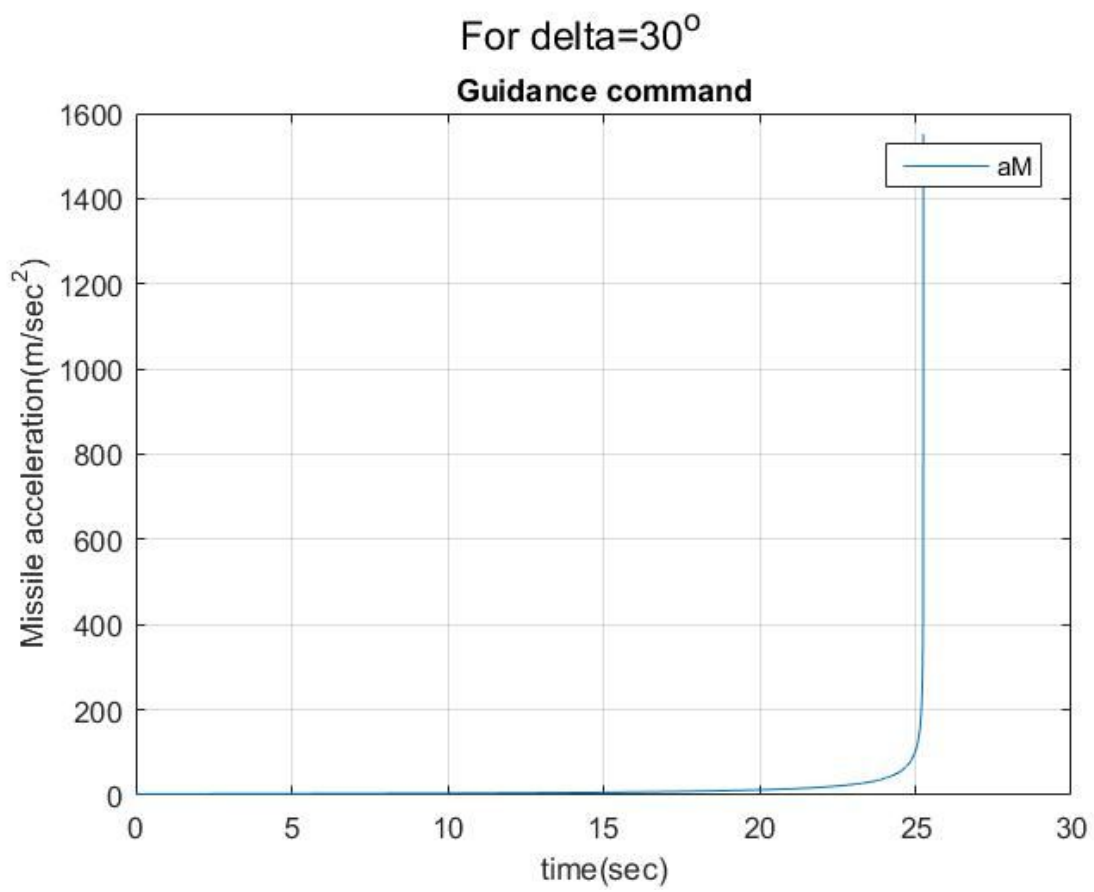
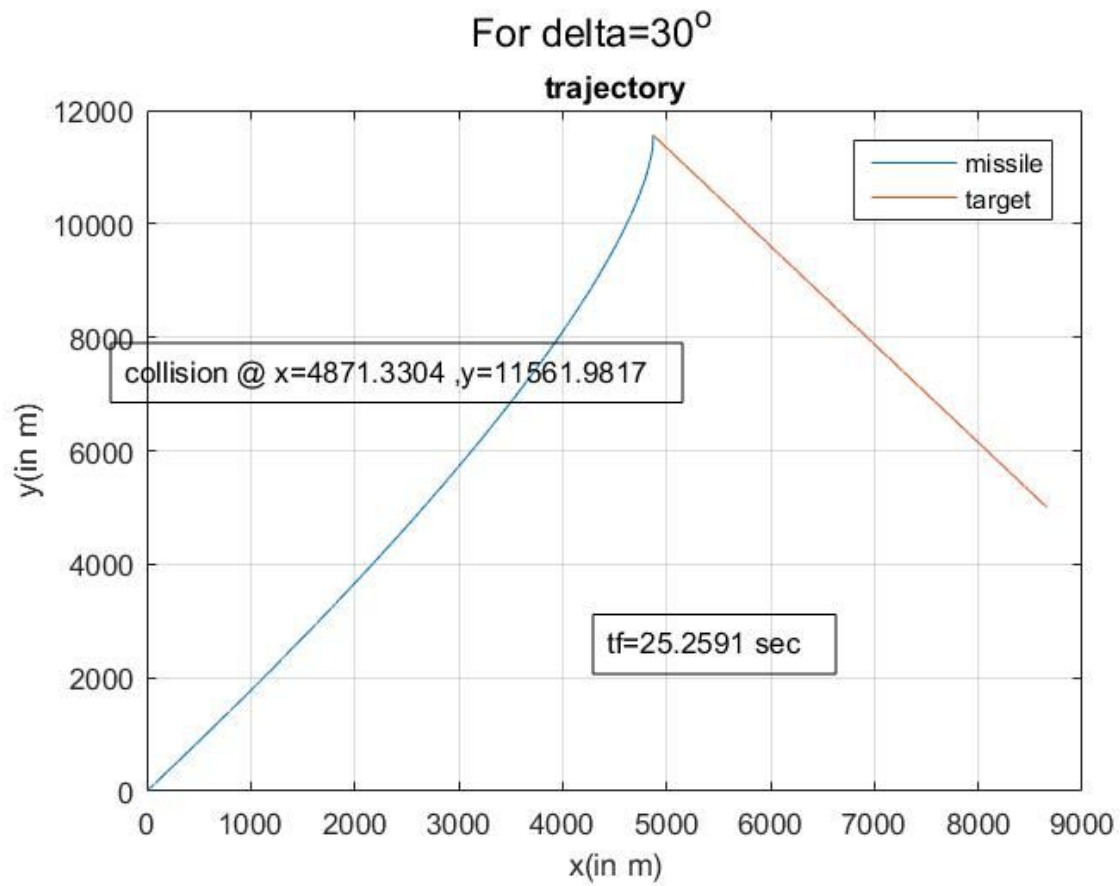
### Q.2(c)

Plots of trajectories and guidance commands for deviated pursuit guidance for various deviation angles.







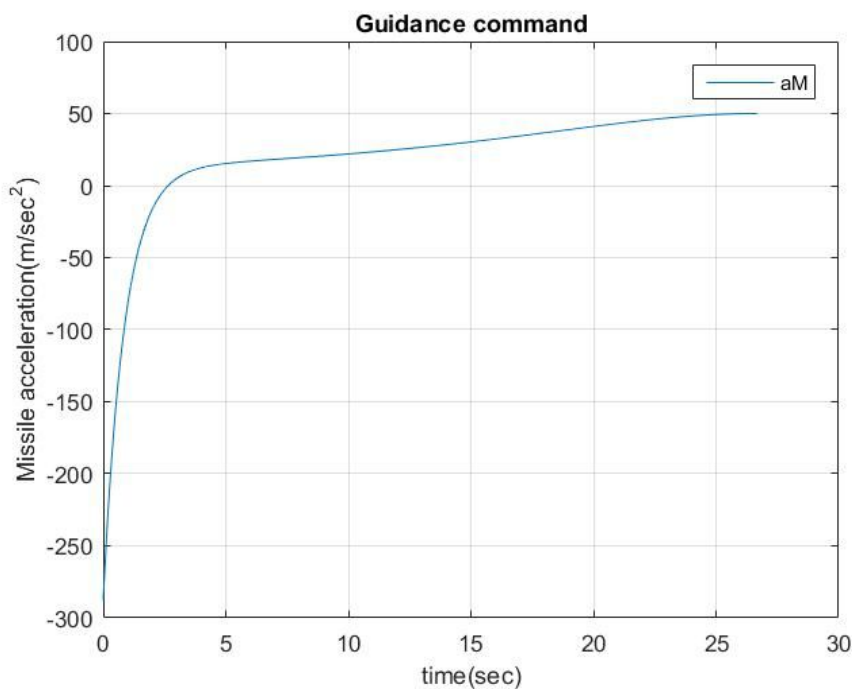
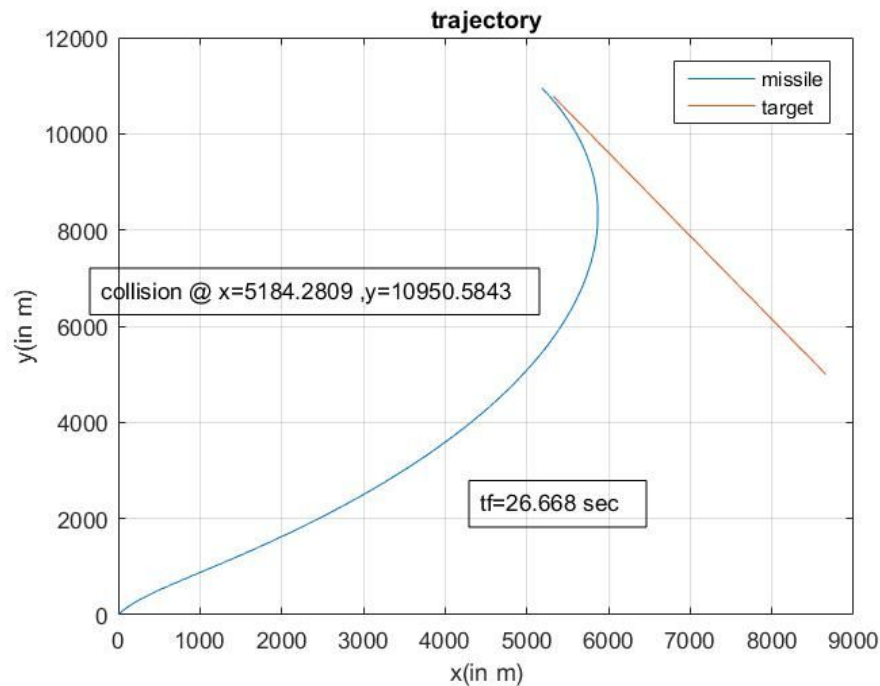


From the plots for different deviation angle it's seen that the guidance command first increases then decreases with increasing deviation angle but for further increase in delta causes the required guidance command to be very high ( a very steep increase). Also with increasing delta the collision time is decreasing slightly, the x coordinate of collision is increasing and y coordinate of collision is decreasing.

### Q.2.(d)

The missile has an initial deviation of 30° anticlockwise in its velocity direction. We can

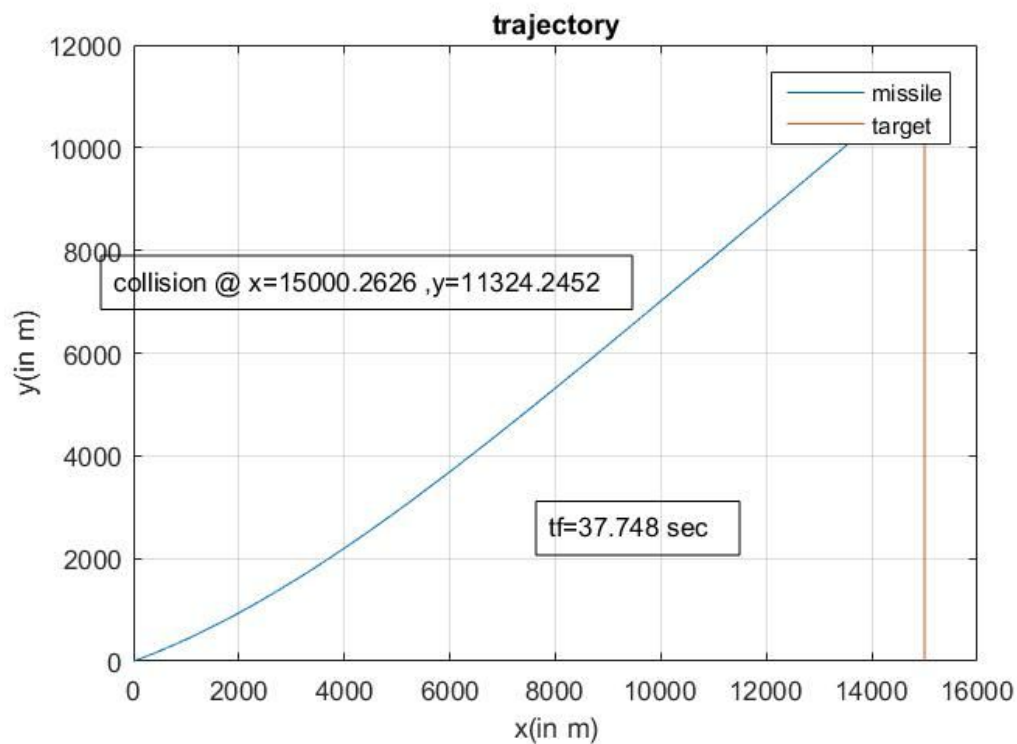
implement the pure pursuit law for this as  $a_M = V_M \dot{\theta} - K(\gamma_M - \theta)$ , Here I used K=10



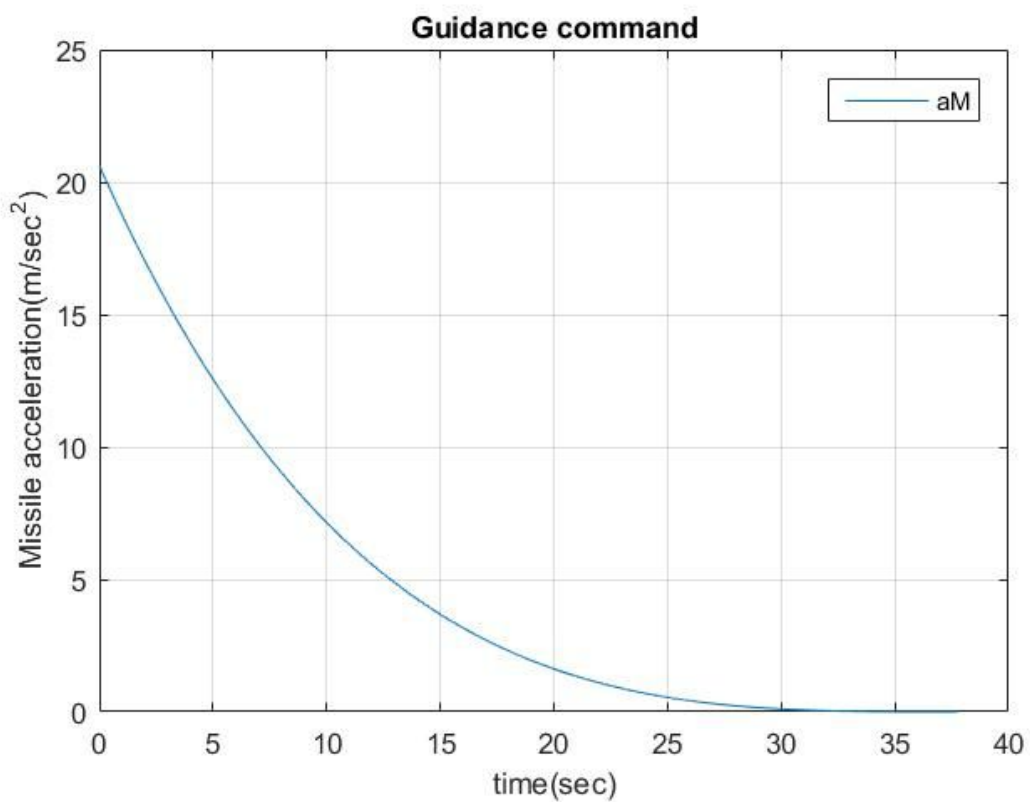
**Q.3.(b).**

Plots for PPN with Heading error =  $+20^\circ$  and  $N = 5$

For PPN Guidance Law with  $HE=20^\circ$

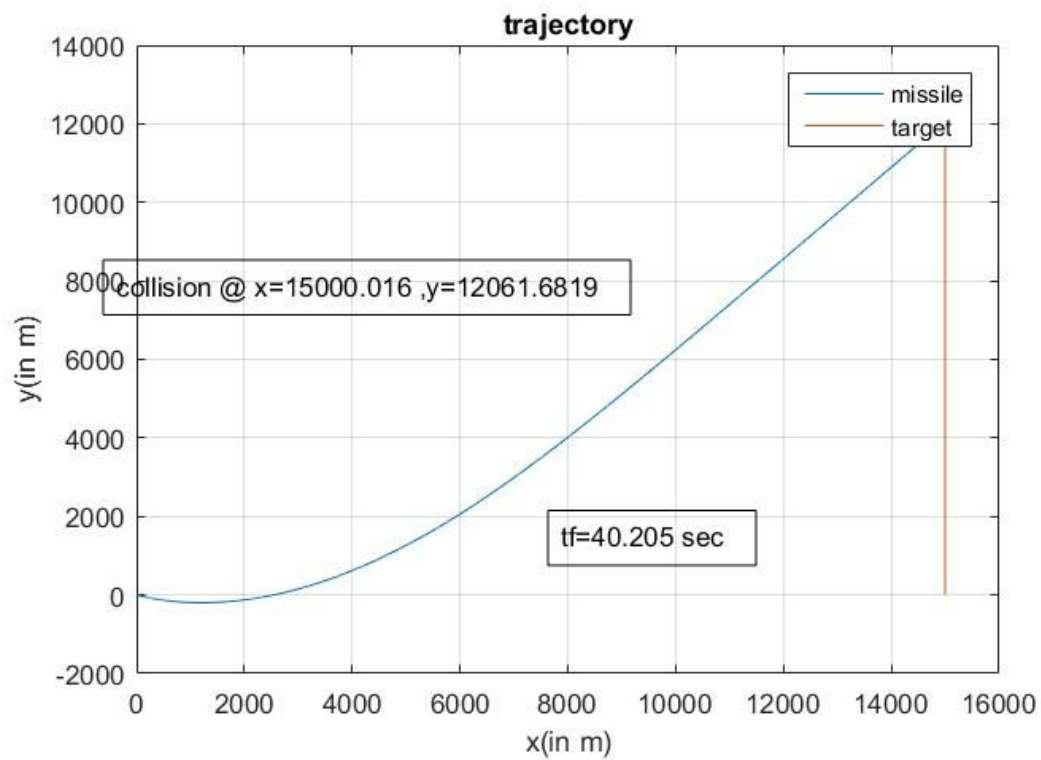


For PPN Guidance Law with  $HE=20^\circ$

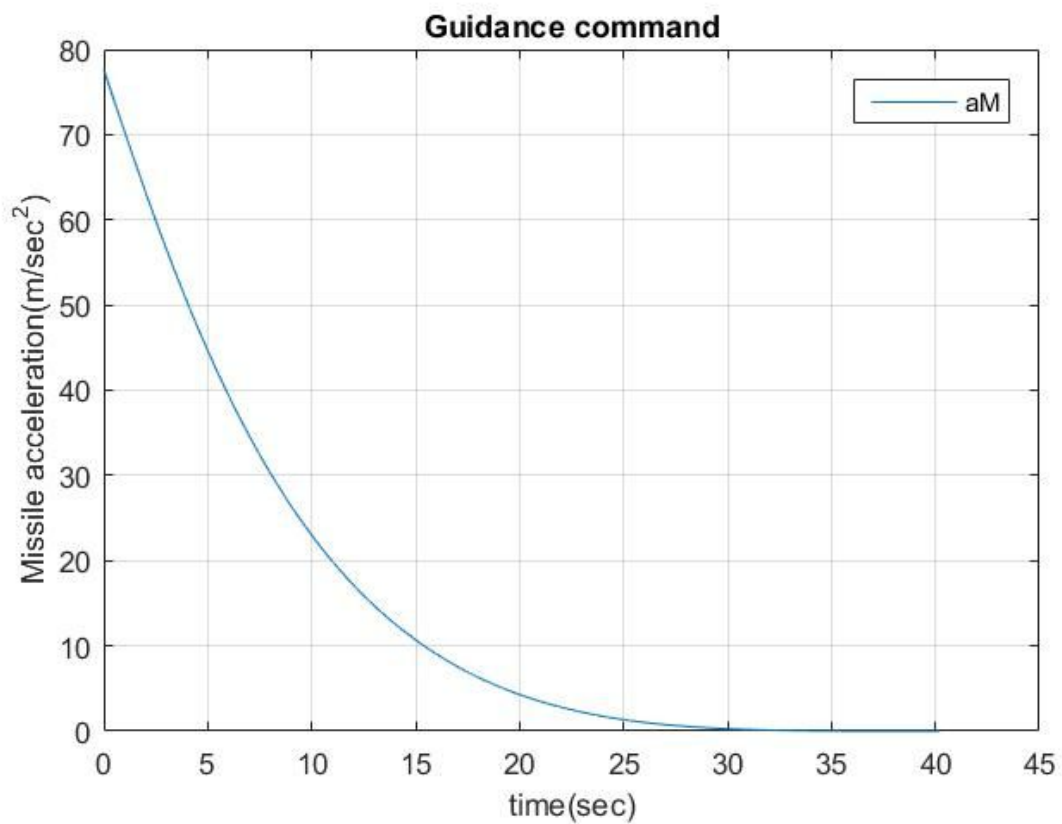


For HE = -20°

For PPN Guidance Law with HE=-20°

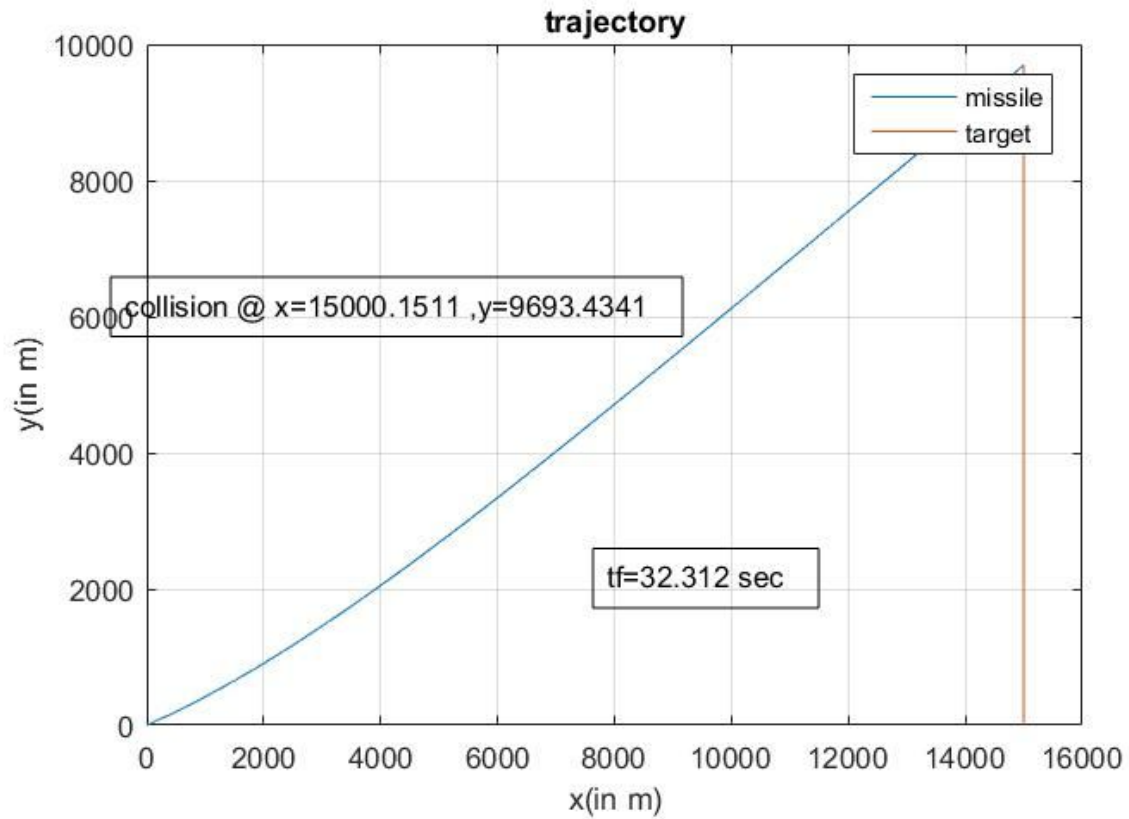


For PPN Guidance Law with HE=-20°

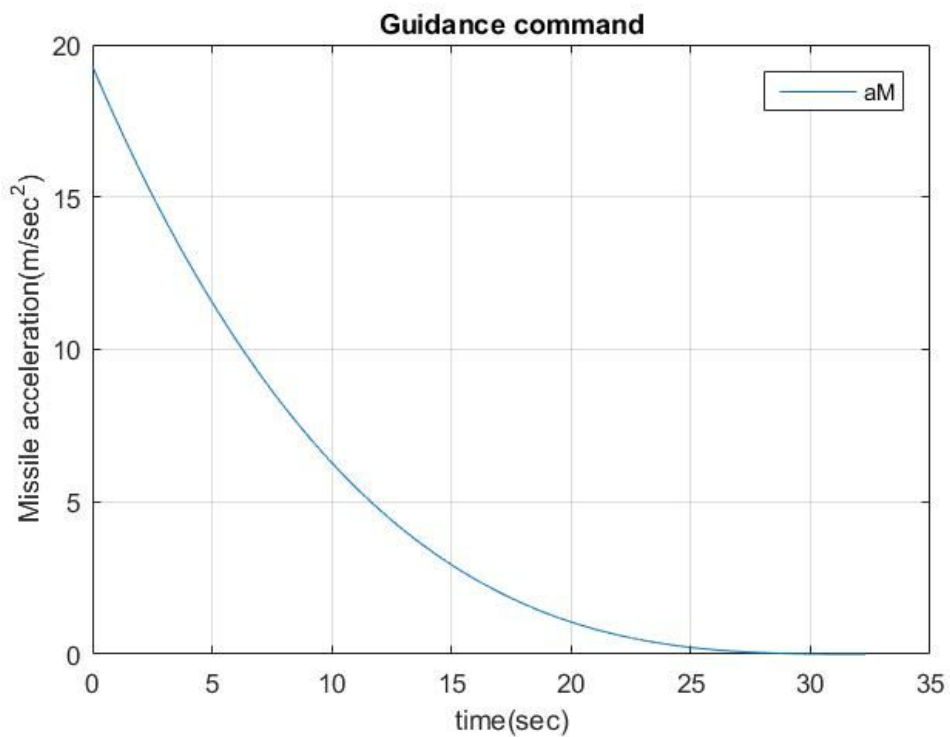


Plots for RTPN with HE = +20° and N=5

For RTPN Guidance Law with HE= +20°

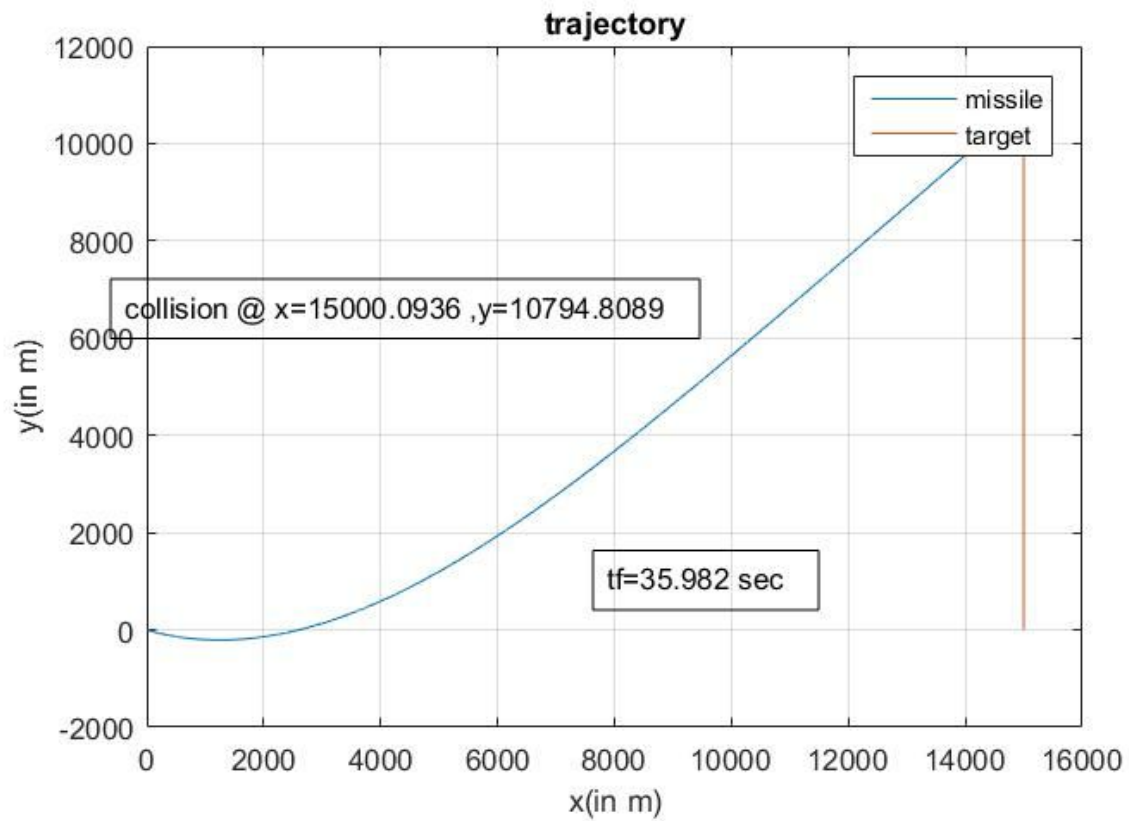


For RTPN Guidance Law with HE= +20°

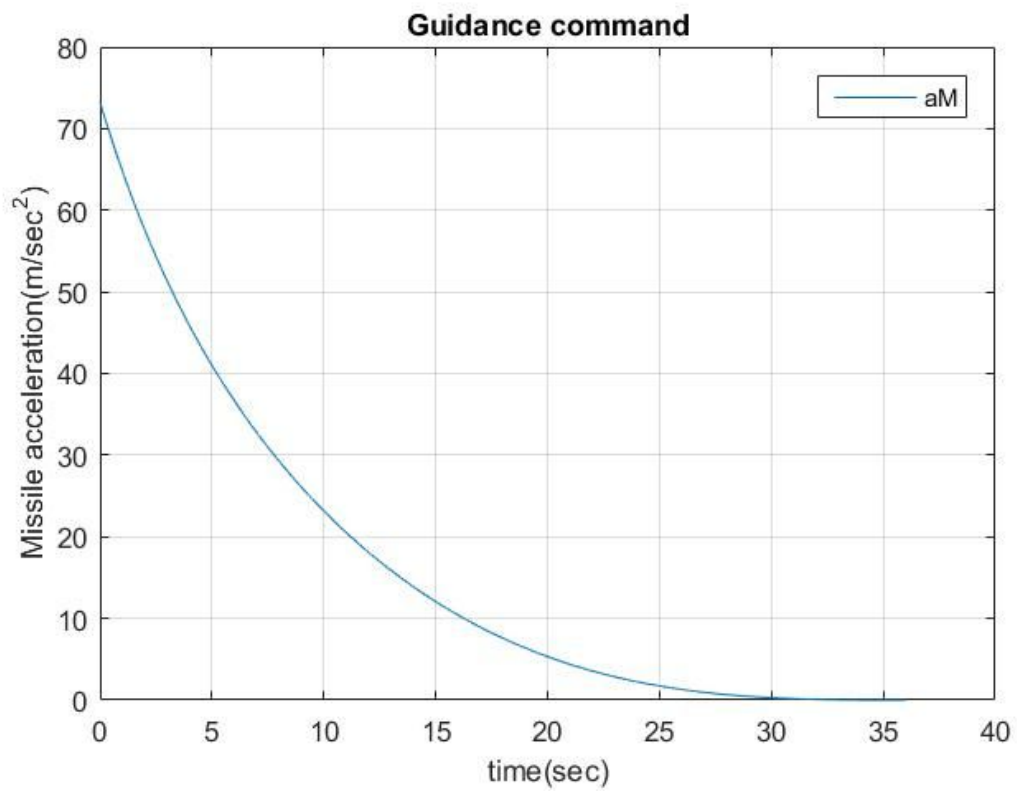


Plots for RTPN with HE = -20°

For RTPN Guidance Law with HE = -20°



For RTPN Guidance Law with HE = -20°

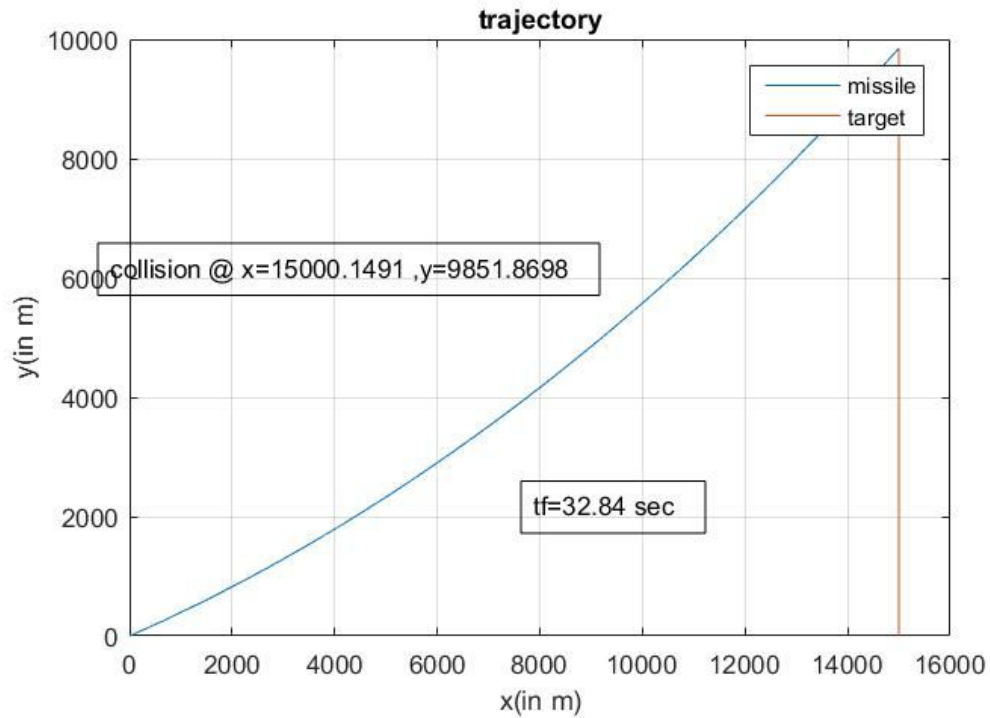


**Q.3.(c).**

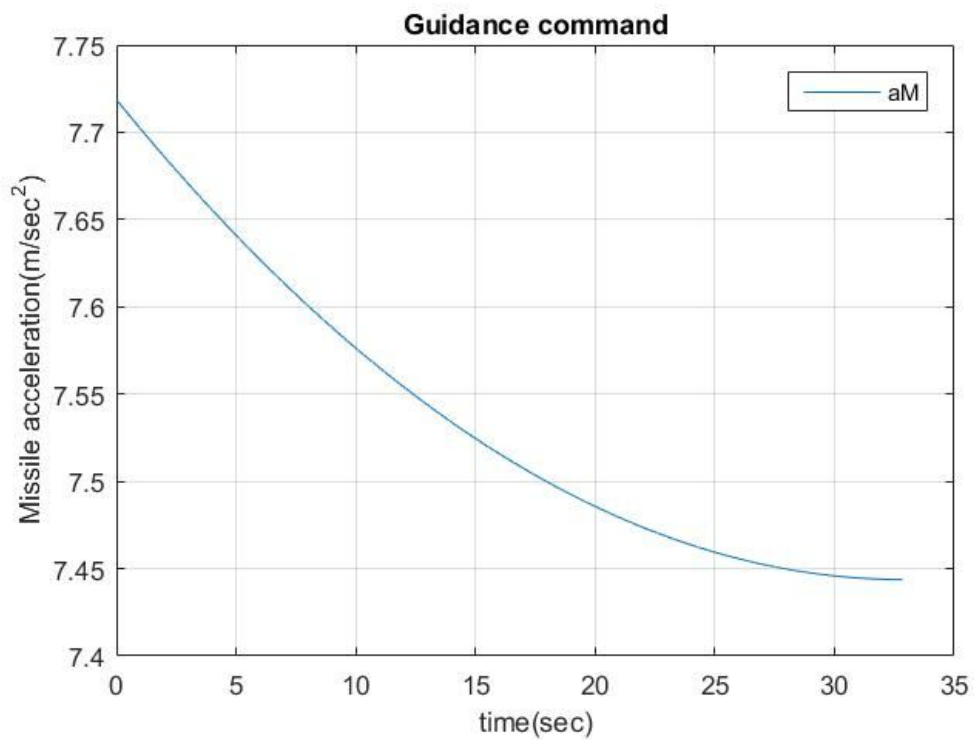
Note plots for  $N=5$  have already been done in (b) part

Plots for RTPN with  $HE=20^\circ$  and  $N=2$

For RTPN Guidance Law with  $HE=20^\circ$  and  $N=2$



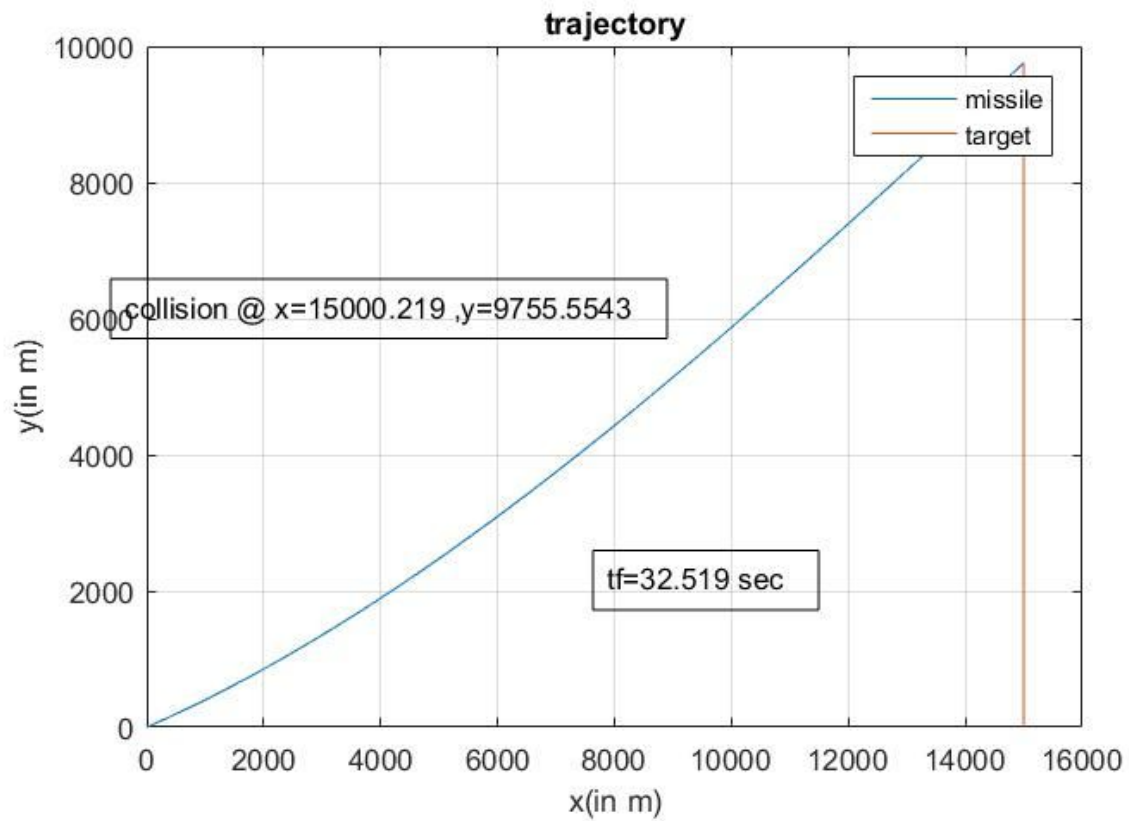
For RTPN Guidance Law with  $HE=20^\circ$  and  $N=2$



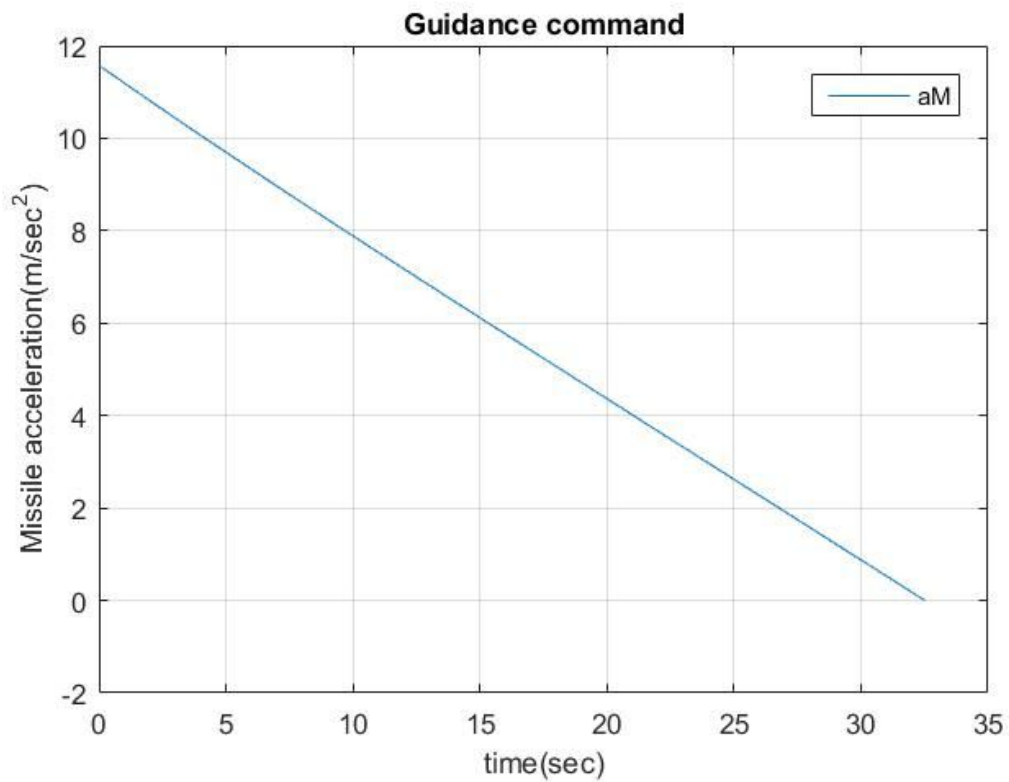


For N= 3

For RTPN Guidance Law with HE=20° and N=3

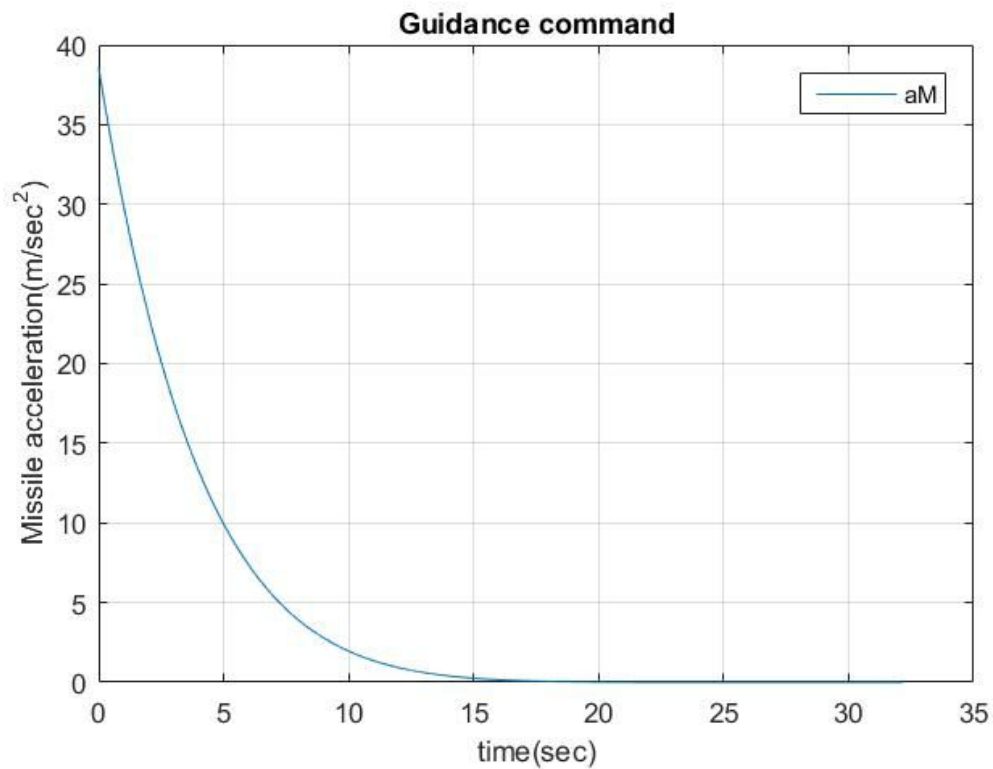


For RTPN Guidance Law with HE=20° and N=3

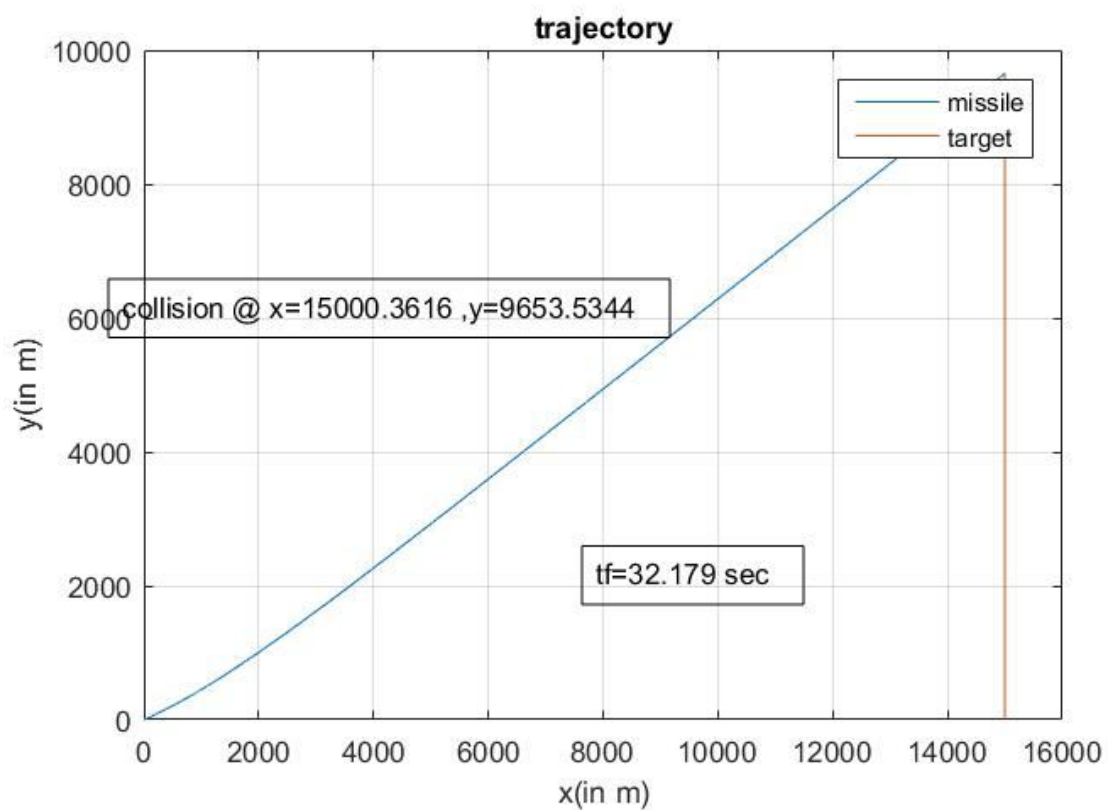


For N=10

For RTPN Guidance Law with  $HE=20^\circ$  and  $N=10$

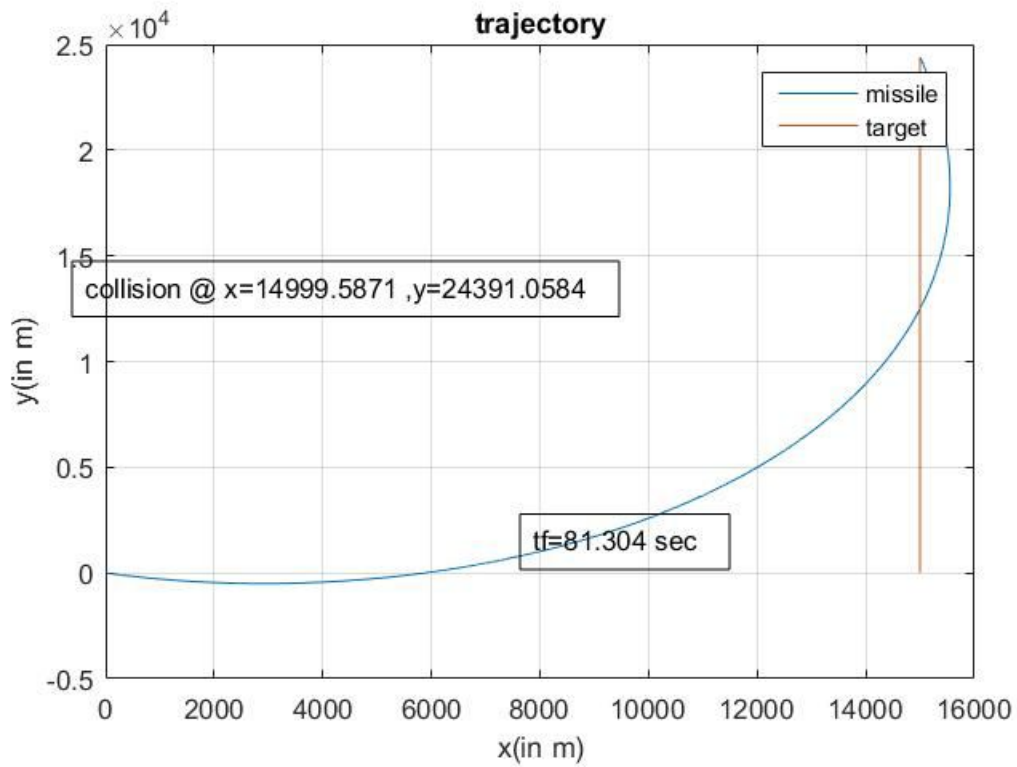


For RTPN Guidance Law with  $HE=20^\circ$  and  $N=10$

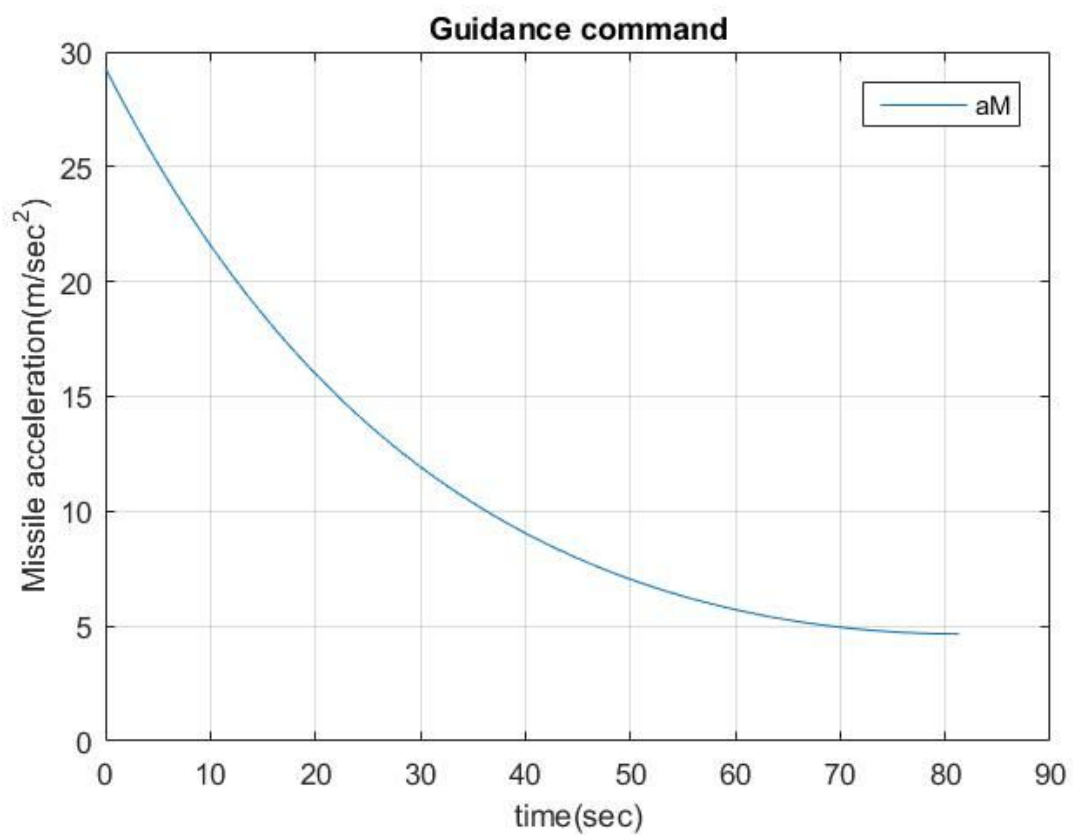


Plots for RTPN with HE = -20

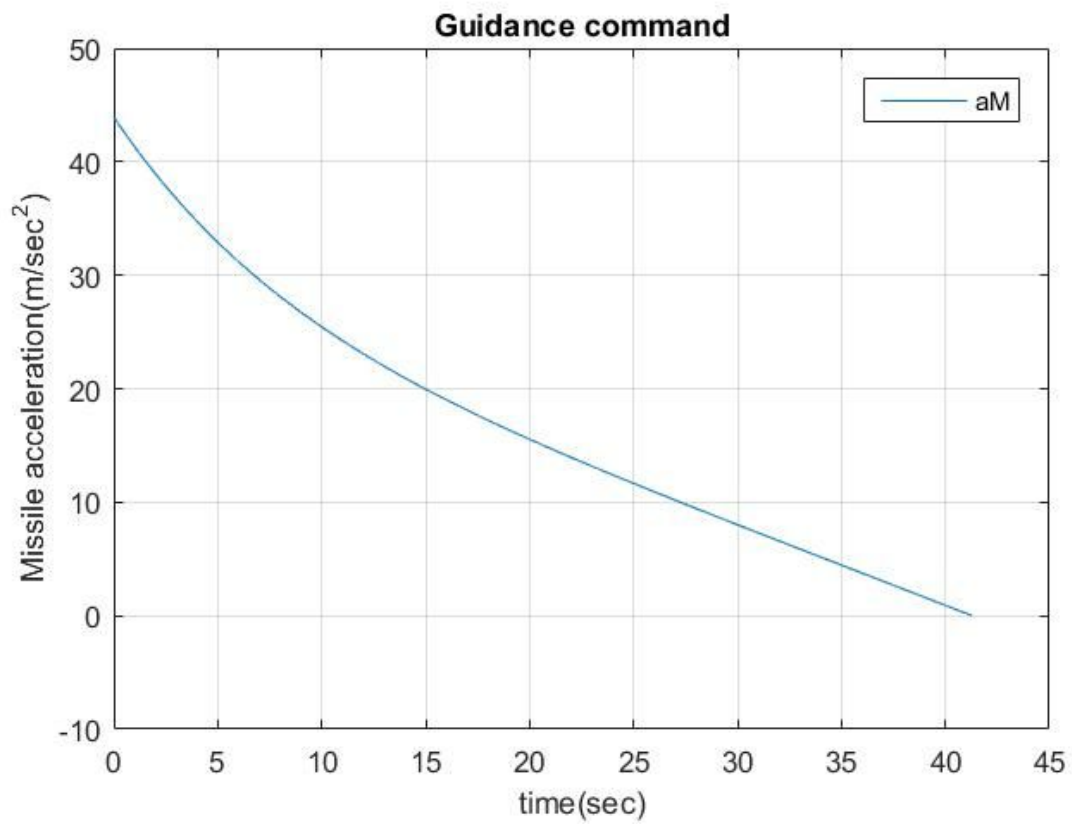
For RTPN Guidance Law with HE=-20° and N=2



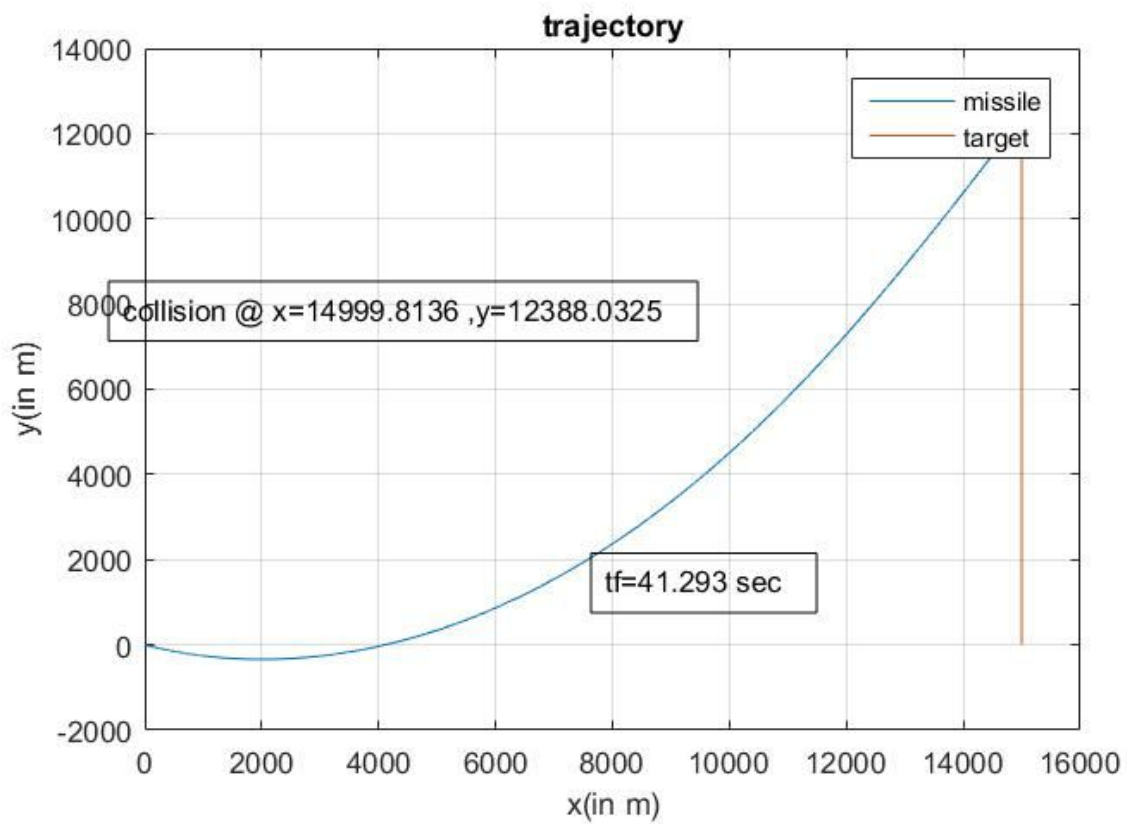
For RTPN Guidance Law with HE=-20° and N=2



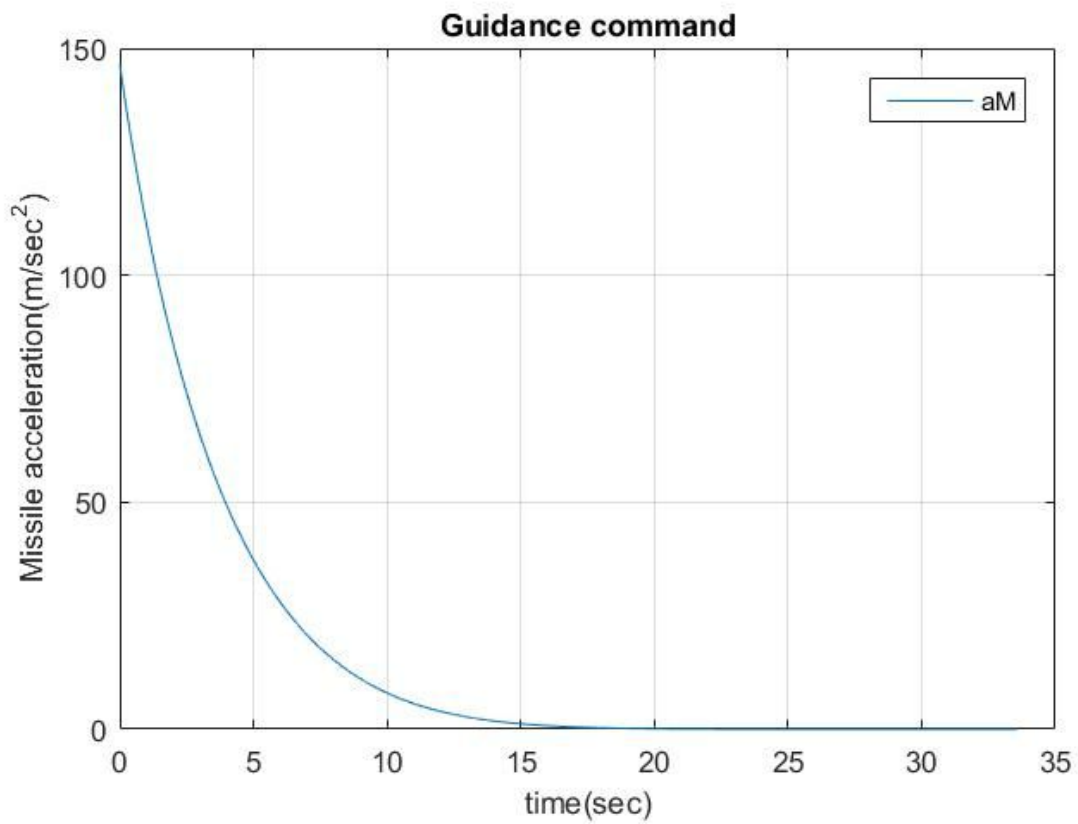
For RTPN Guidance Law with  $HE=-20^\circ$  and  $N=3$



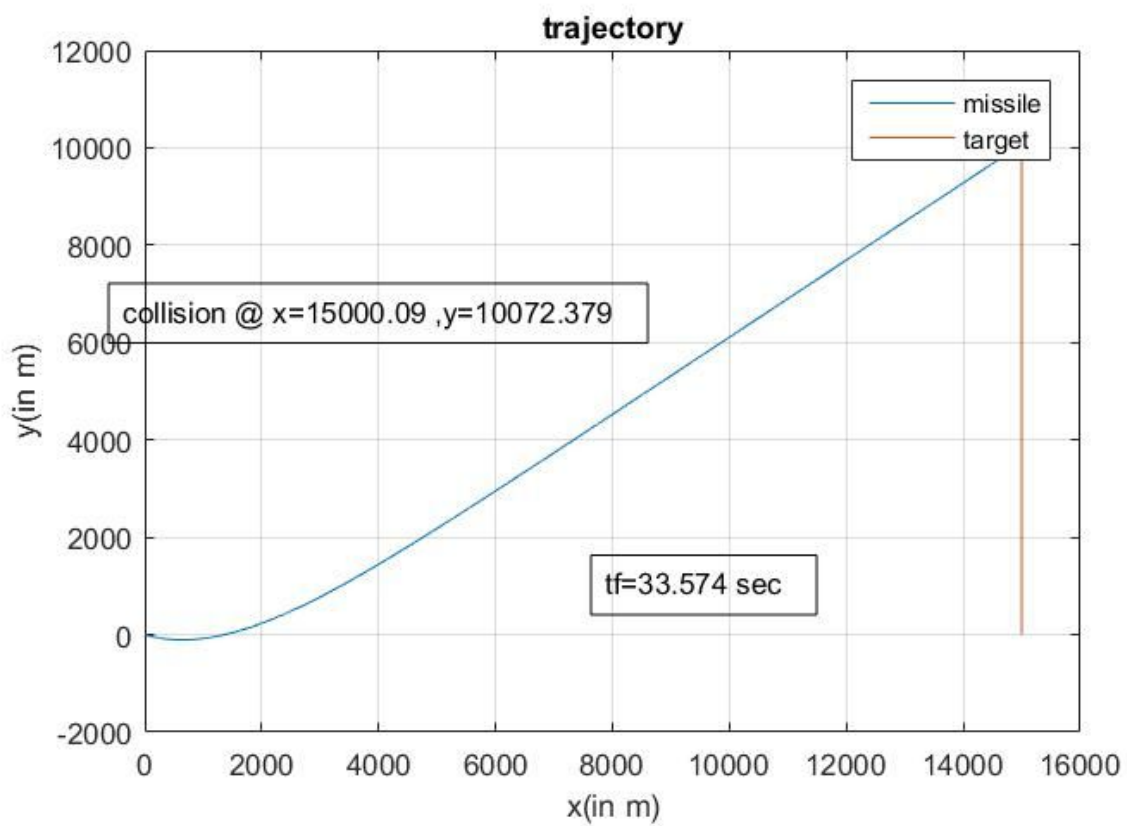
For RTPN Guidance Law with  $HE=-20^\circ$  and  $N=3$



For RTPN Guidance Law with  $HE = -20^\circ$  and  $N = 10$

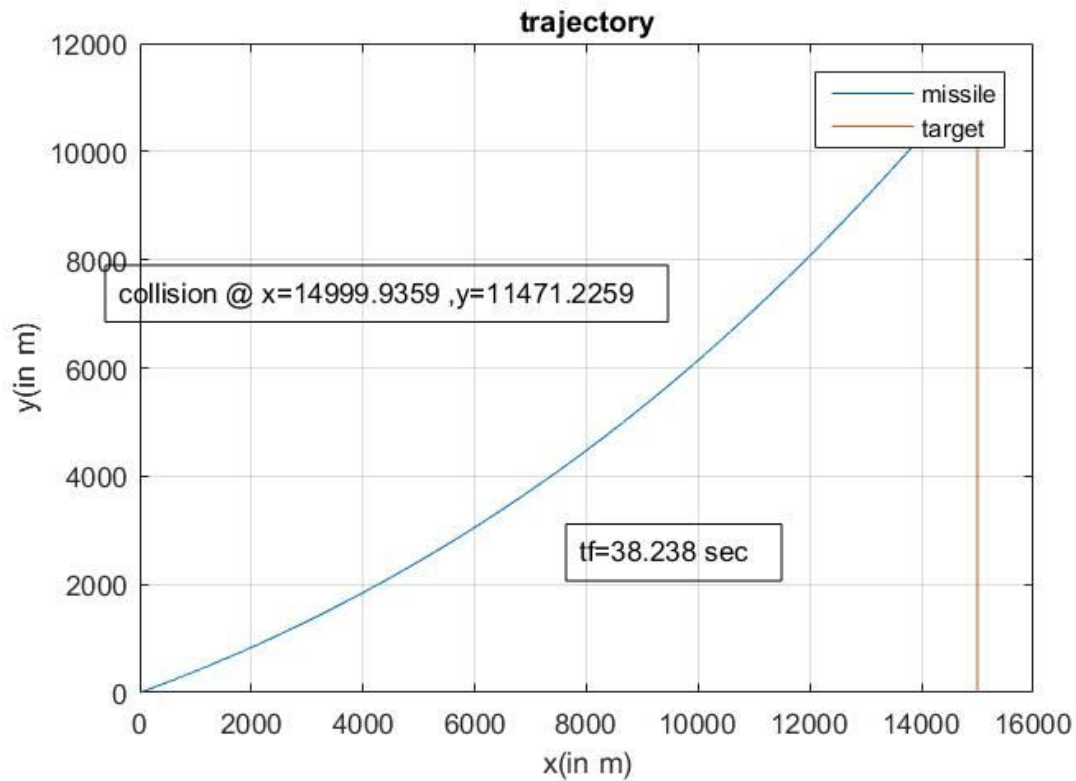


For RTPN Guidance Law with  $HE = -20^\circ$  and  $N = 10$

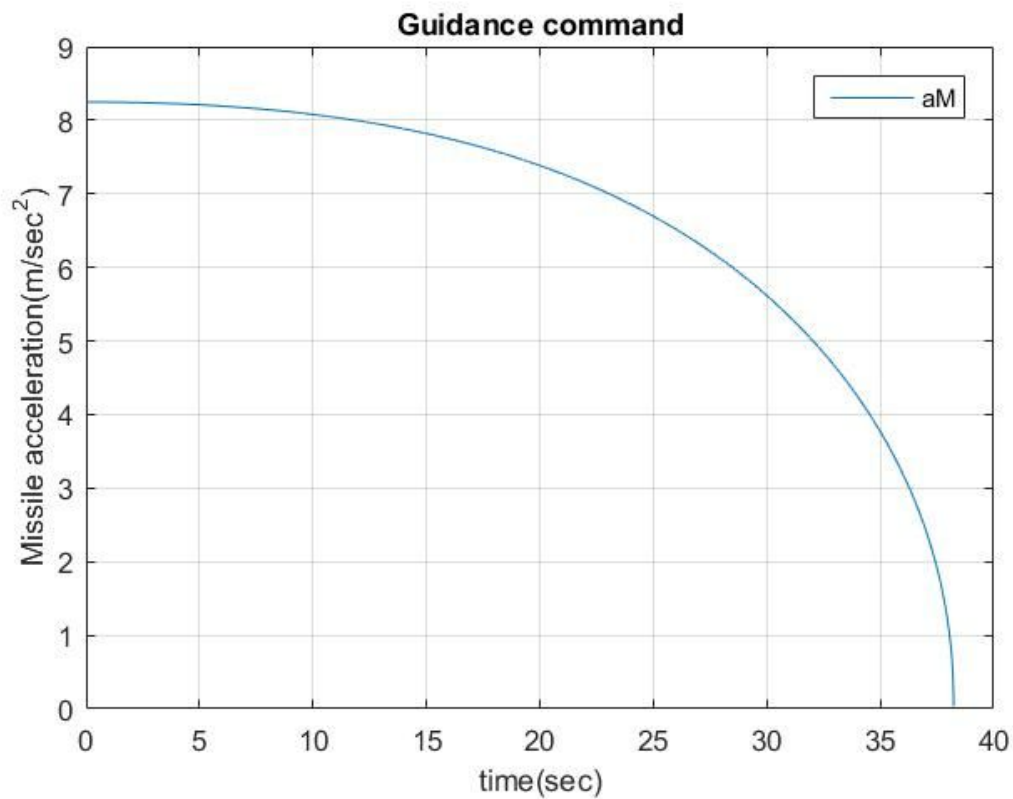


Plots for PPN with HE =20° ; Plots for N=5 have already been generated in part(b)

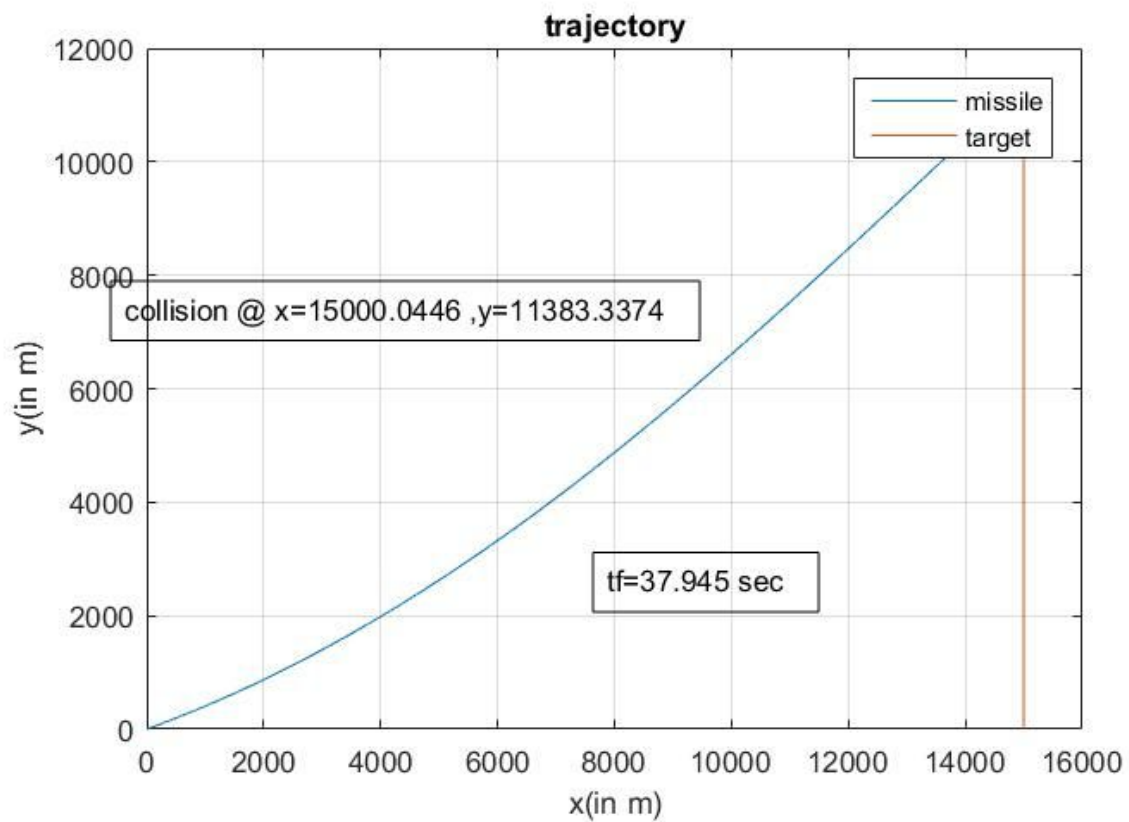
For PPN Guidance Law with HE=20° and N=2



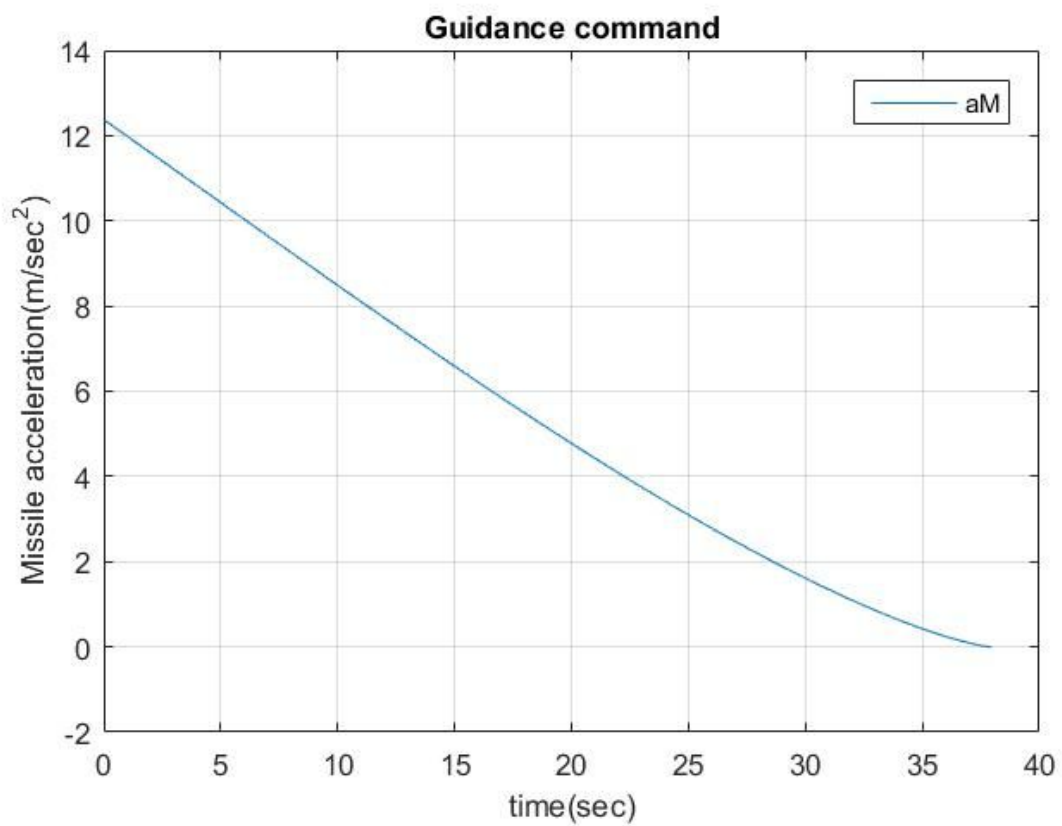
For PPN Guidance Law with HE=20° and N=2



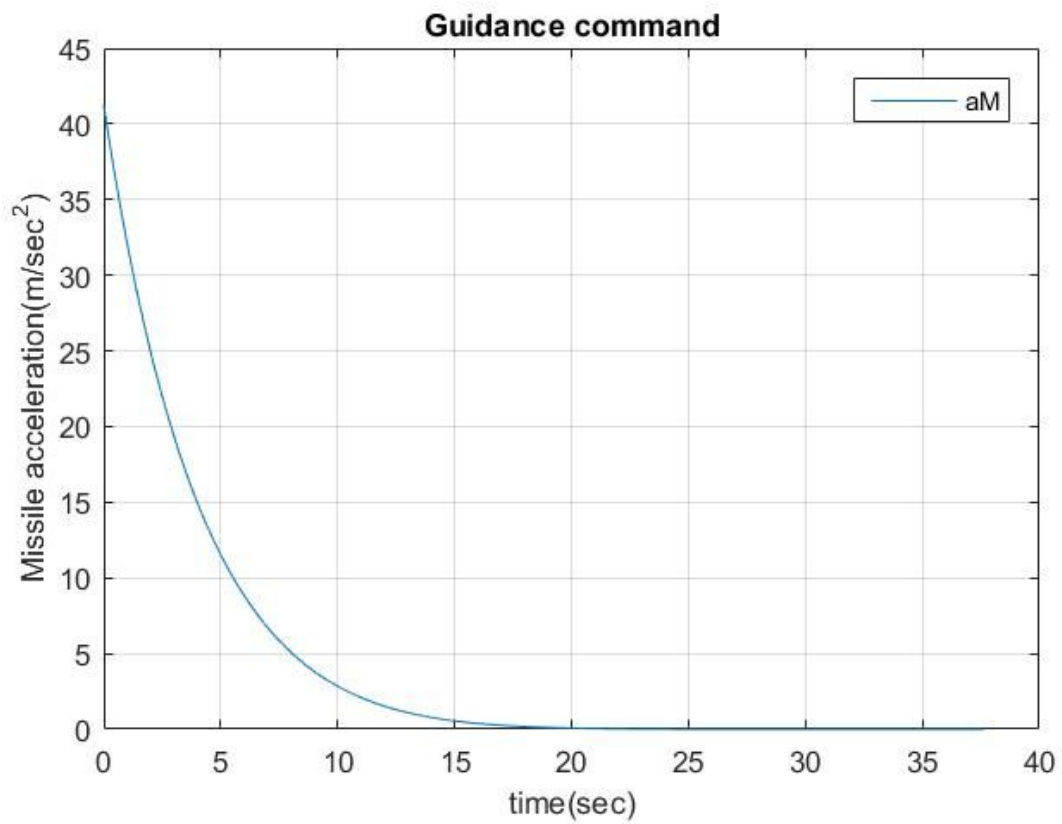
For PPN Guidance Law with  $HE=20^\circ$  and  $N=3$



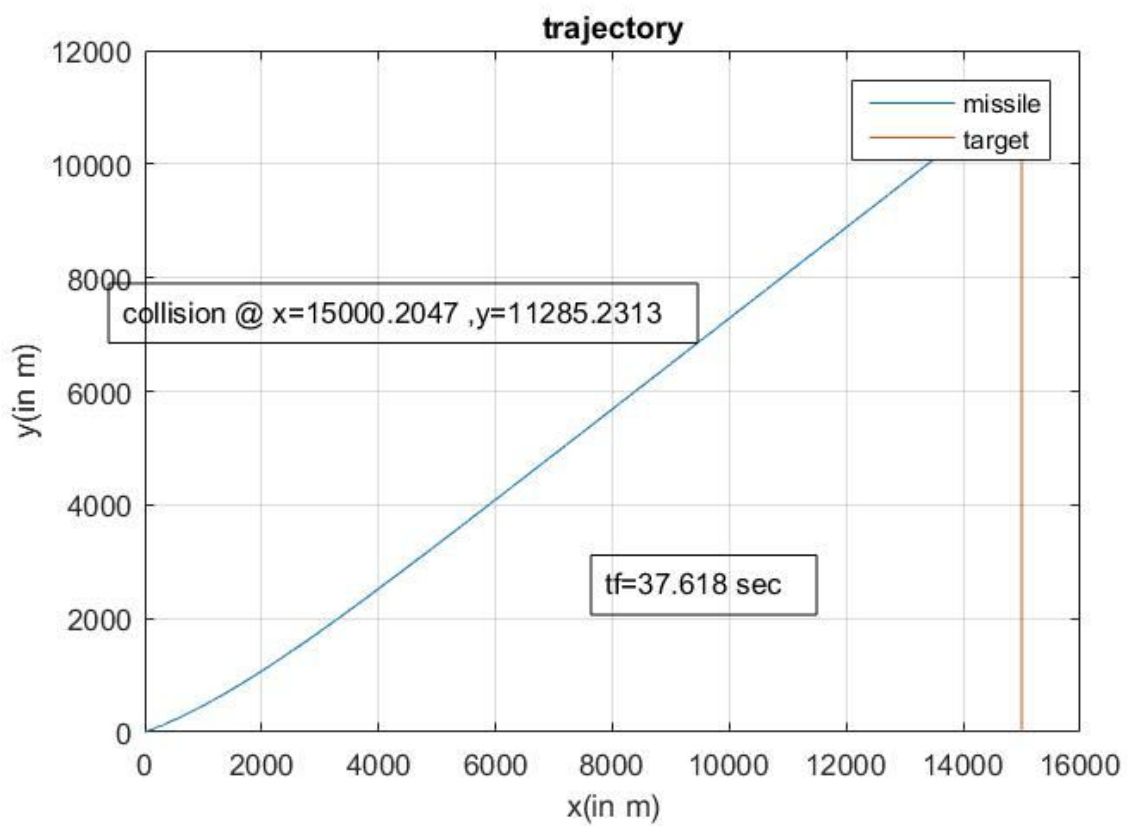
For PPN Guidance Law with  $HE=20^\circ$  and  $N=3$



For PPN Guidance Law with  $HE=20^\circ$  and  $N=10$



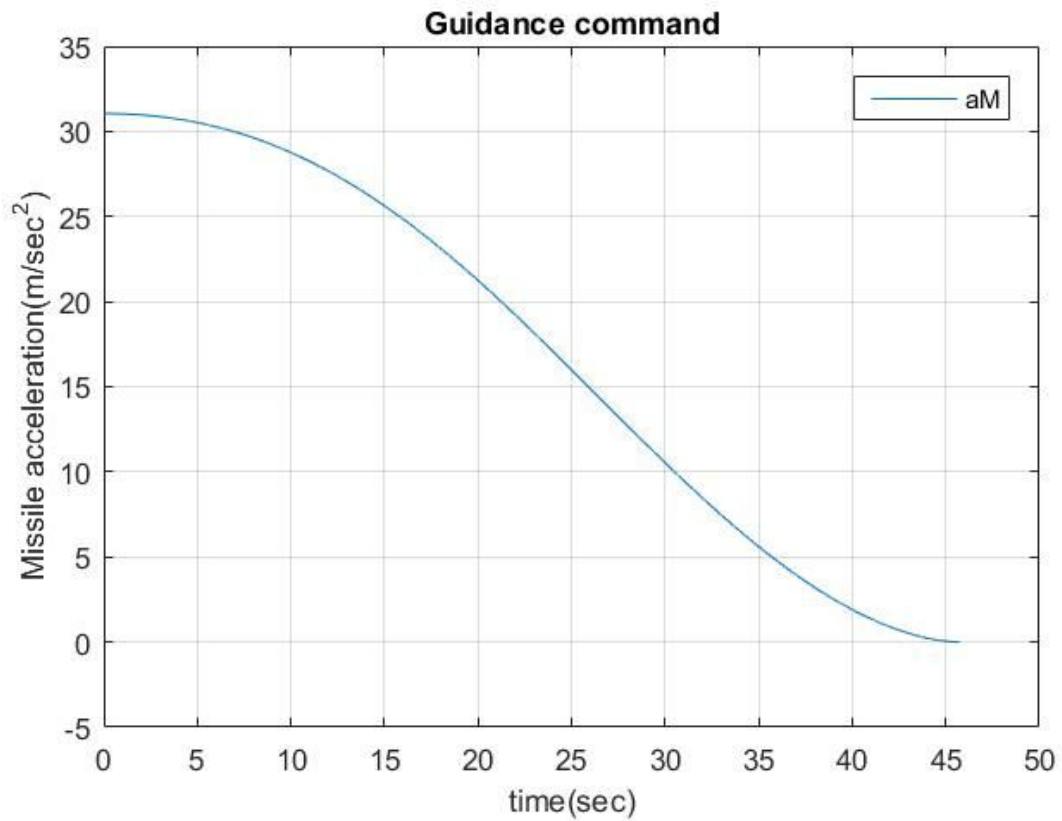
For PPN Guidance Law with  $HE=20^\circ$  and  $N=10$



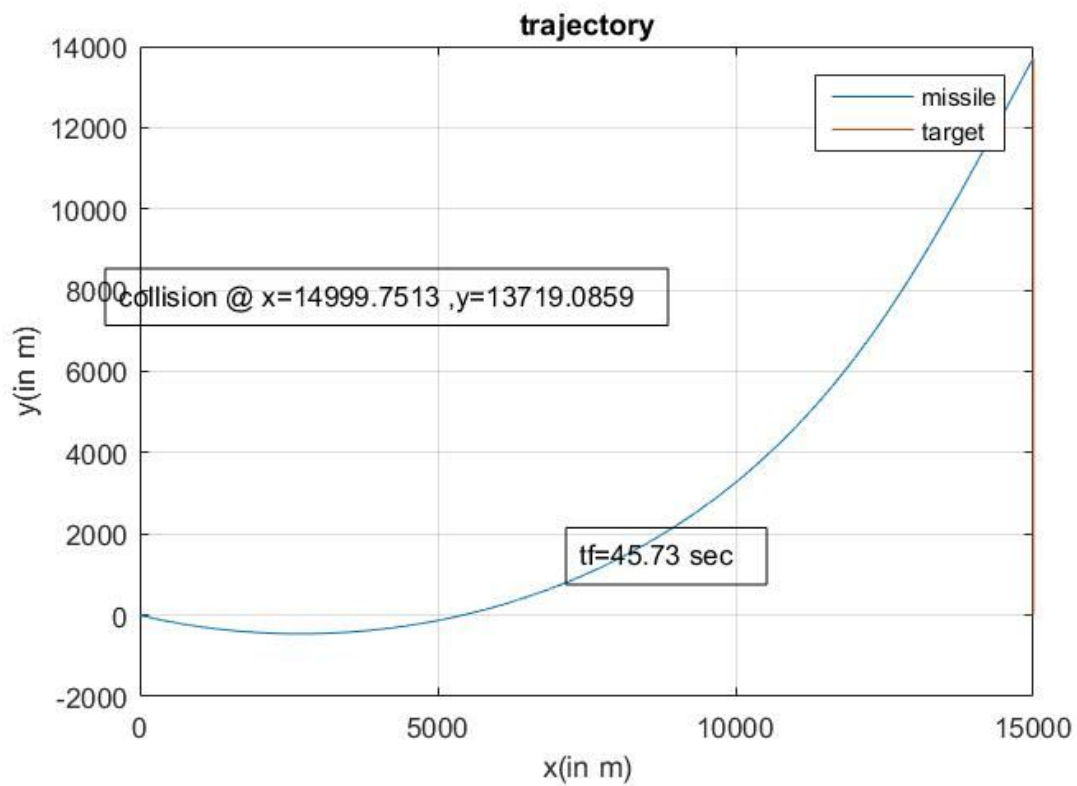


Plots for PPN with HE = -20°

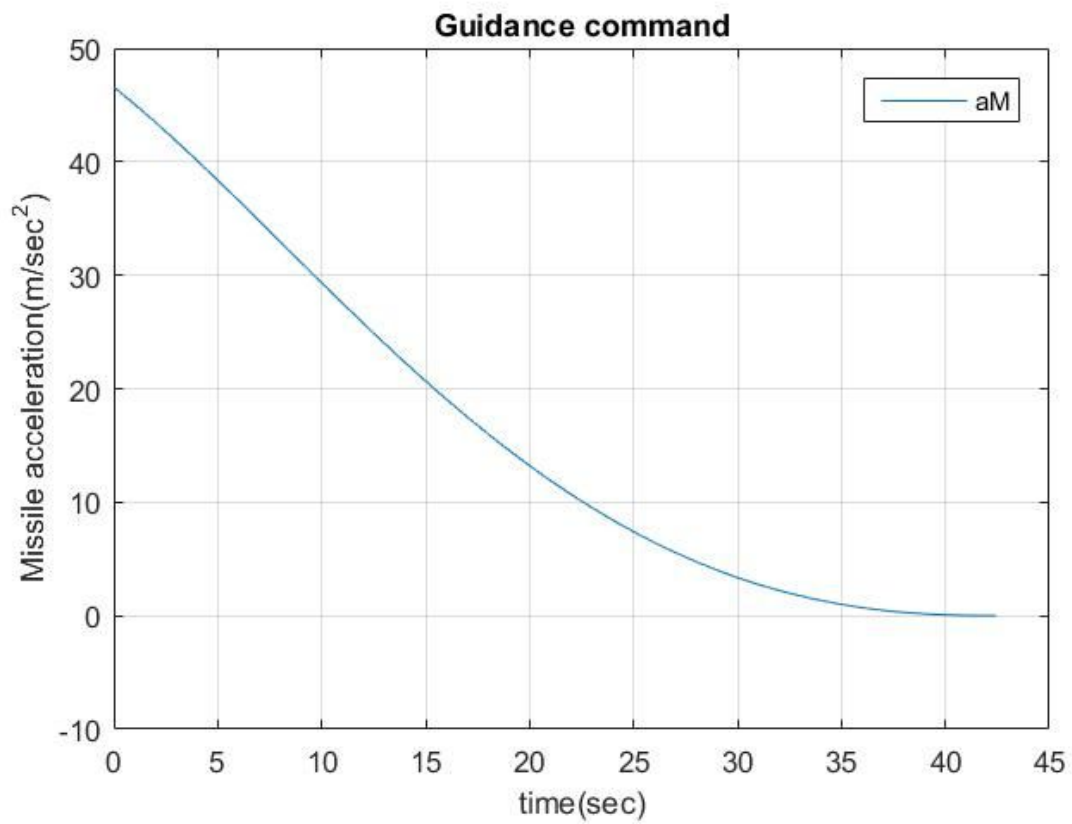
For PPN Guidance Law with HE=-20° and N=2



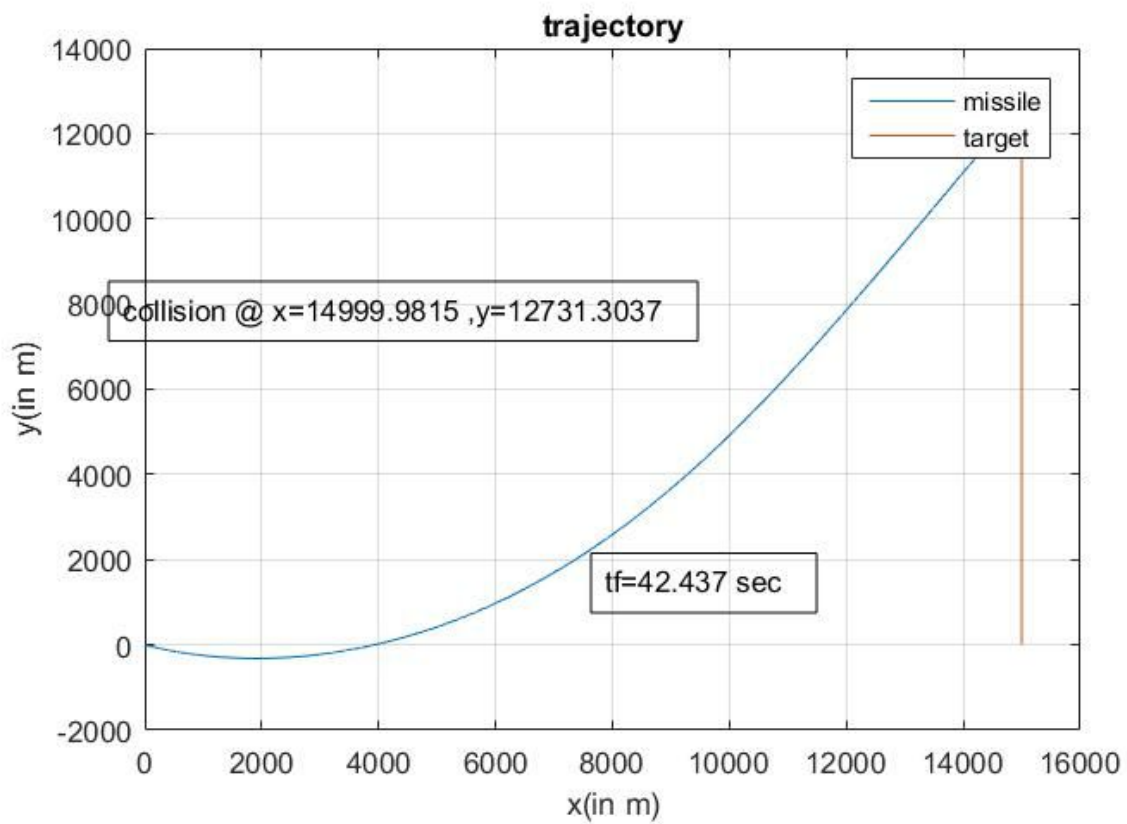
For PPN Guidance Law with HE=-20° and N=2



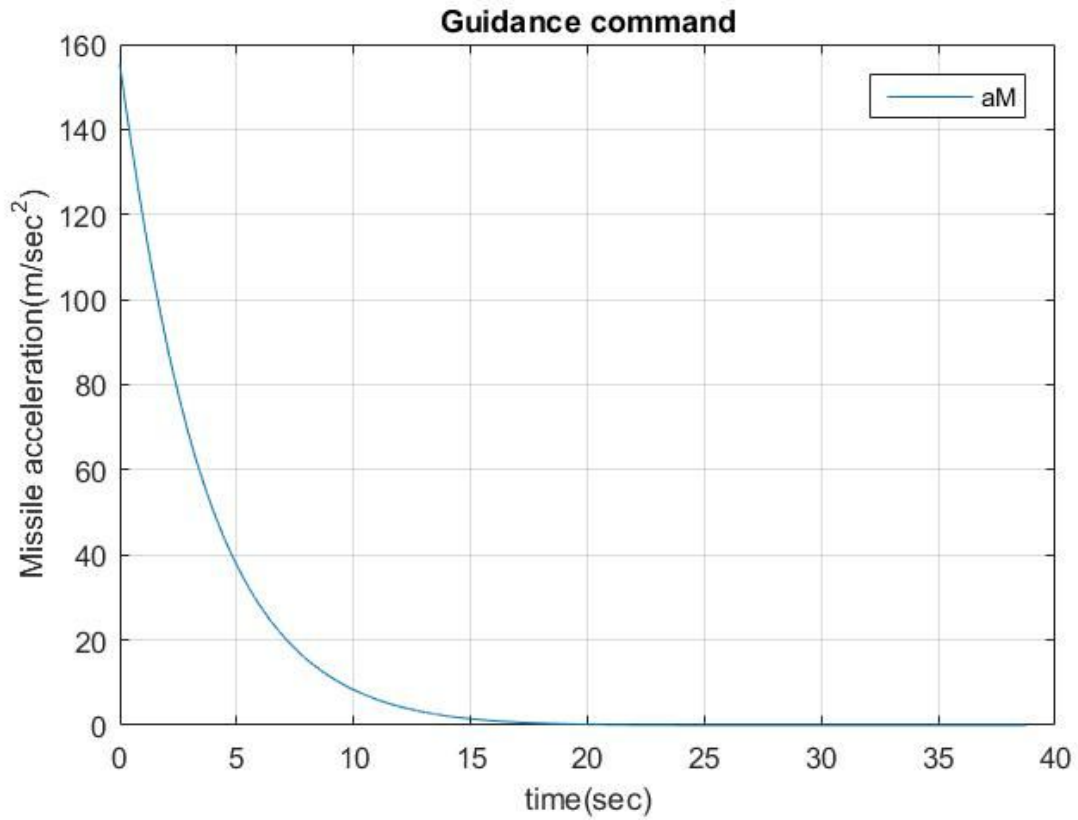
For PPN Guidance Law with  $HE=-20^\circ$  and  $N=3$



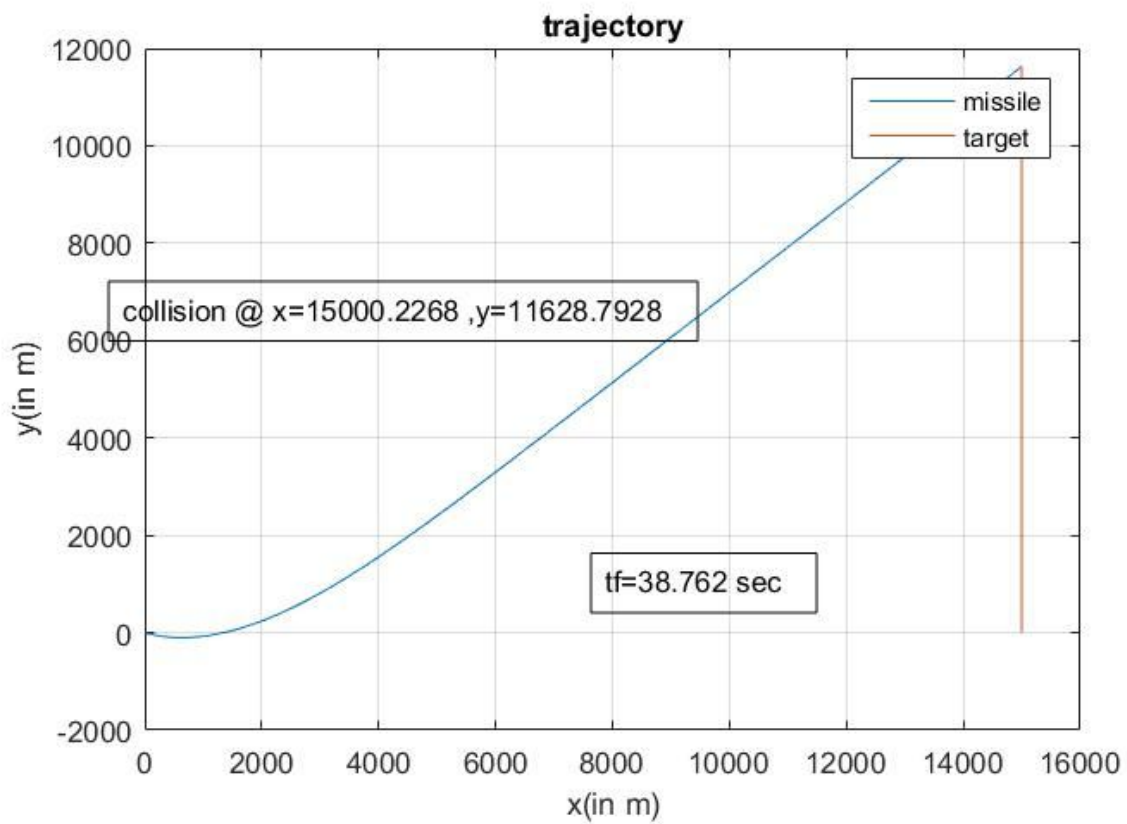
For PPN Guidance Law with  $HE=-20^\circ$  and  $N=3$



For PPN Guidance Law with  $HE=-20^\circ$  and  $N=10$



For PPN Guidance Law with  $HE=-20^\circ$  and  $N=10$



For RTPN with  $HE = 20$ : As the value of  $N$  increases the guidance command requirement decreases with time. Also with increase in  $N$  the acceleration requirement decreases more rapidly. Collision time is almost same for all cases. But for  $HE = -20$  the collision time varies significantly. Guidance command follows the same pattern.

For PPN with  $HE = -20$ : In this case also as the acceleration requirement decreases but the collision time does not differ much. For  $HE = 20$  the nature of curve of the guidance command changes its nature from concave to convex.

Note: The MATLAB Code used to generate the code is in separate file for each part of the problem. The same code can be run for multiple times by changing variables like  $N$  or deviation angle and plots will get generated for each case.