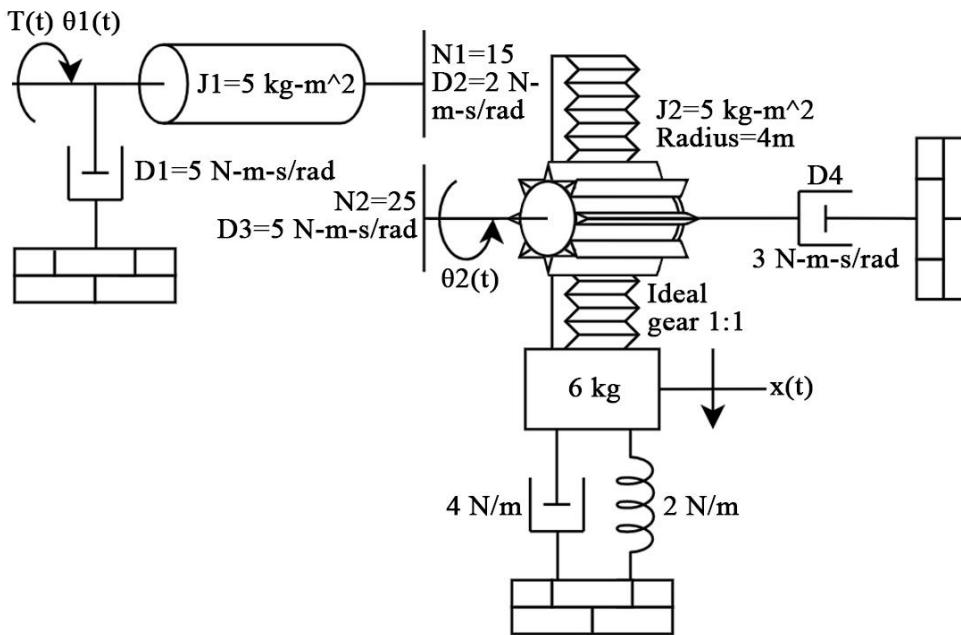


System Design



Transfer Function

Handwritten derivation of the transfer function:

Block diagram for transfer function derivation:

1. Input torque $T_1(s)$ is applied to a shaft with $J_1 = 5$ and $D_1 = 5$. The output is $\theta_1(s)$.

2. Gear 1 with $N_1 = 15$ and $D_2 = 2$ is connected to Gear 2 with $N_2 = 25$ and $D_3 = 5$. The output is $\theta_2(s)$.

3. Gear 2 is connected to Gear 3 with $N_3 = 15$ and $D_4 = 3$. The output is $\theta_3(s)$.

4. Gear 3 is connected to a mass of 6 kg via an ideal gear with a 1:1 ratio. The output is $x(s)$.

5. The mass is supported by a spring with stiffness 4 N/m and a damper with coefficient 2 N-m-s/rad .

Transfer function derivation:

$$J_{eq} = J_1 \left(\frac{N_2}{N_1} \right)^2 + J_2 = 5 \left(\frac{25}{15} \right)^2 + 5 = 18.89$$

$$D_{eq} = D_1 \left(\frac{N_2}{N_1} \right)^2 + D_2 \left(\frac{N_2}{N_1} \right)^2 + D_3 + D_4 = 5 \left(\frac{25}{15} \right)^2 + 2 \left(\frac{25}{15} \right)^2 + 5 + 3 = 27.44$$

$$\left(\frac{N_2}{N_1} \right) T_1(s) = (J_{eq} s^2 + D_{eq} s) \theta_2(s) + F(s) r$$

$$F(s) = (M s^2 + D_s + K) X(s) = (6 s^2 + 4 s + 2) X(s)$$

$$1.67 T_1(s) = (18.89 s^2 + 27.44 s) \theta_2(s) + (6 s^2 + 4 s + 2) X(s) r$$

$$\Rightarrow 1.67 T_1(s) = (18.89 s^2 + 27.44 s) \frac{X(s)}{r} + 4(6 s^2 + 4 s + 2) X(s)$$

$$\Rightarrow 1.67 T_1(s) = \frac{(18.89 s^2 + 27.44 s)}{4} X(s) + (96 s^2 + 64 s + 32) X(s)$$

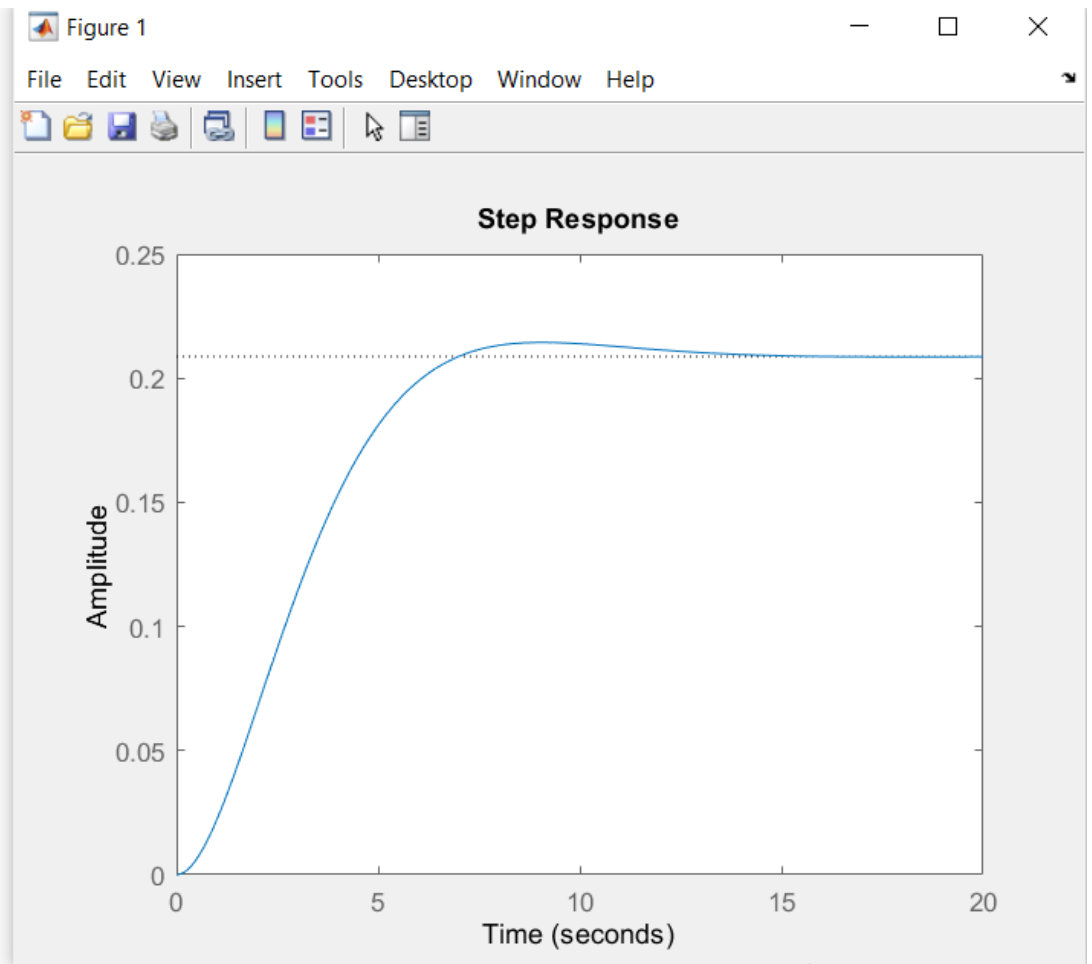
$$\Rightarrow 1.67 T_1(s) = \frac{(114.89 s^2 + 91.44 s + 32)}{4} X(s)$$

$$\Rightarrow \frac{X(s)}{T_1(s)} = \frac{6.68}{114.89 s^2 + 91.44 s + 32}$$

PID Controller

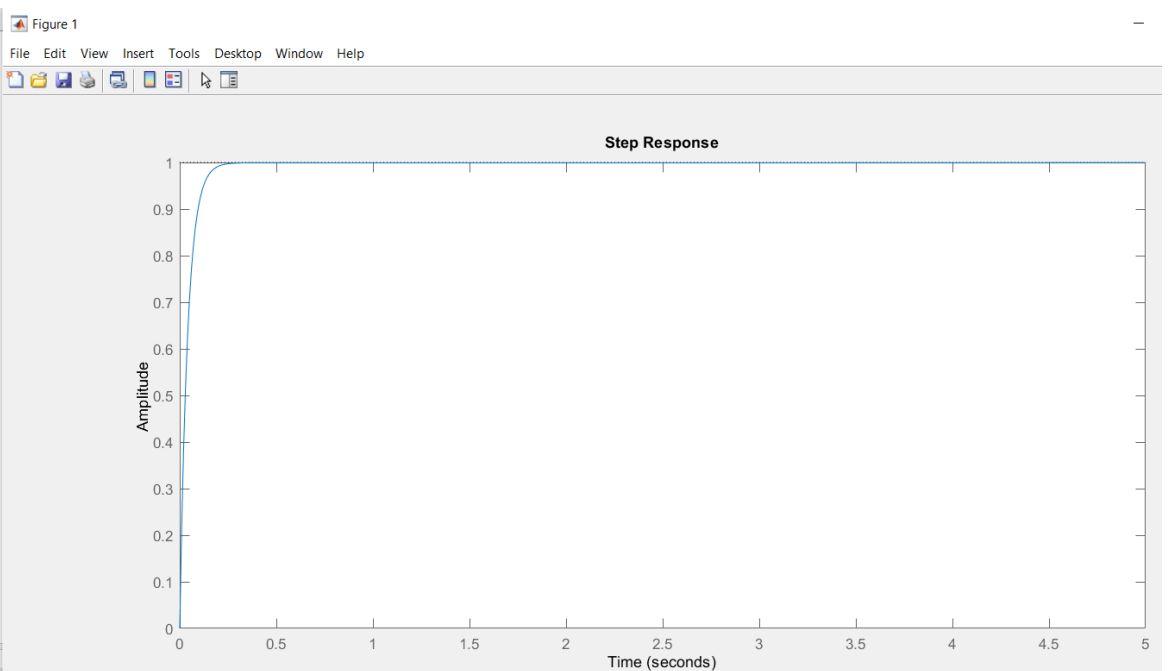
1. Original

```
num=6.68;  
den=[114.89 91.44 32];  
t=0:0.01:20;  
step(num,den,t);
```



2. Modified

```
h.mlx fdcsys_proj.m  
Kp = 2200;  
Kd = 2800;  
Ki = 700;  
num=[Kd Kp Ki];  
den=[114.89 91.44+Kd 32+Kp Ki];  
t=0:0.01:5;  
step(num,den,t);
```



Routh Table

s^2	114.89	32	$-\frac{\begin{vmatrix} 114.89 & 32 \\ 91.44 & 0 \end{vmatrix}}{91.44} = -\frac{0 - (91.44)(32)}{91.44}$
s^1	91.44	\emptyset	$= 32$
s^0	$-\frac{\begin{vmatrix} 114.89 & 32 \\ 91.44 & 0 \end{vmatrix}}{91.44} = 32$	$-\frac{\begin{vmatrix} 114.89 & 0 \\ 91.44 & 0 \end{vmatrix}}{91.44} = \emptyset$	\therefore stable due to no sign change.

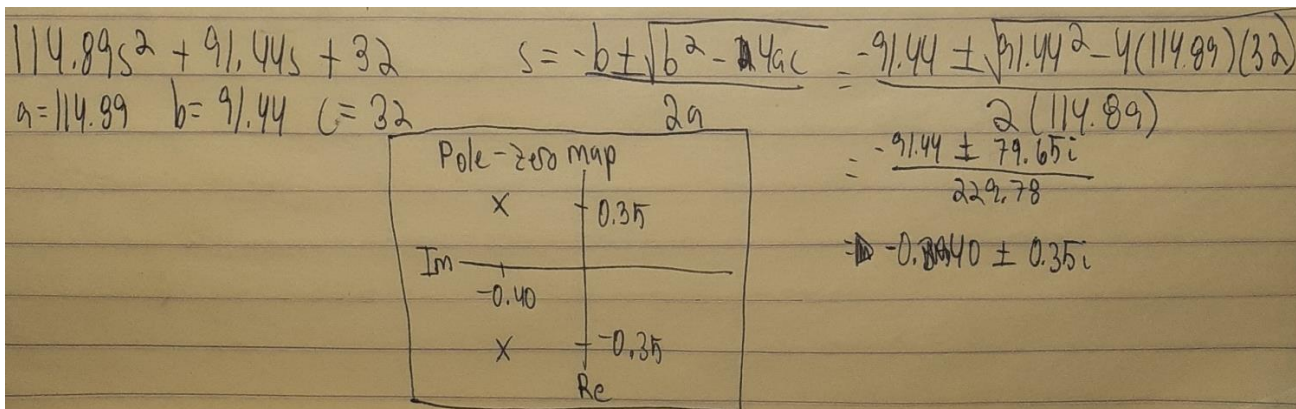
```
1 - syms EPS
2 - ra = routh([114.89 91.44 32], EPS)
```

Command Window

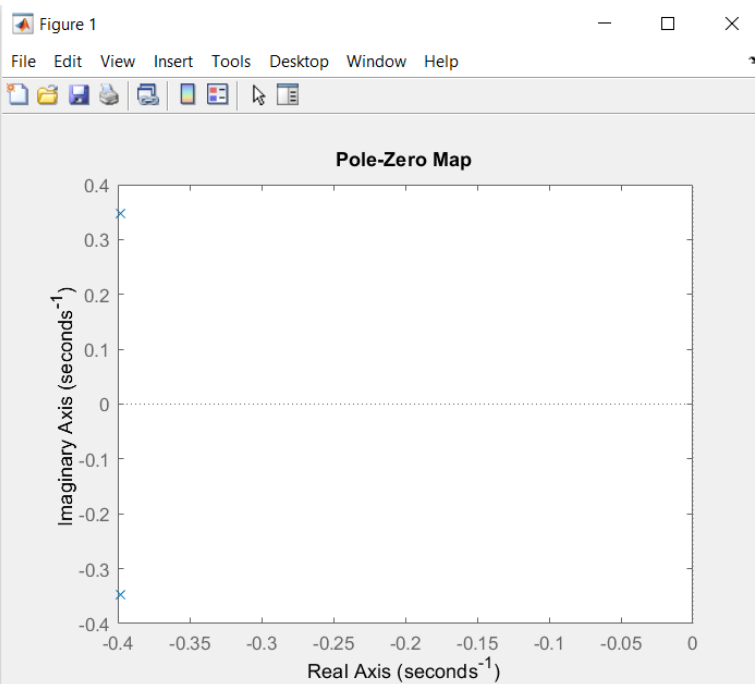
```
ra =

[11489/100, 32]
[ 2286/25, 0]
[      32, 0]
```

Pole-Zero Map



```
>> sys = tf([6.68], [114.89 91.44 32]);
>> h = pzplot(sys);
fx >>
```



State Space Representation

$$X(s) \rightarrow \frac{6.68}{(117.89s^2 + 91.44s + 32)} \rightarrow Y(s)$$

$$X(s) \left((117.89s^2 + 91.44s + 32) \right) = 6.68 Y(s)$$

$$117.89\ddot{x} + 91.44\dot{x} + 32x = 6.68 Y(s)$$

$$117.89\ddot{x} = -91.44\dot{x} - 32x + 6.68 Y(s)$$

$$\ddot{x} = -0.80\dot{x} - 0.28x + 0.06 Y(s)$$

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -0.28 & -0.80 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 0 \\ 0.06 \end{bmatrix} Y(s)$$

$$Y = \begin{bmatrix} 1 & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + 0 \cdot Y(s)$$

```

>> b = [6.68];
a = [114.89, 91.44, 32];
[A,B,C,D] = tf2ss(b,a)

```

```

A =
    -0.7959    -0.2785
    1.0000         0

```

```

B =
    1
    0

```

```

C =
    0    0.0581

```

```

D =
    0

```

Explanation: The controllable canonical form is shown in the left image, given the transfer function. However, MATLAB's tf2ss function output is not yet in controllable canonical form. To reformat the output, matrix A is flipped horizontally and vertically while matrix B and C are interchanged and transposed, while D remains the same.