# 7 Numerical Results and Discussion

This section aims to show and discuss the main results obtained from the parametric analysis considering different constitutive models and distances between the longitudinal tunnels.

## 7.1 Constitutive parameters and observations about results

The parametric analysis uses the constitutive parameters of the incompressible clay rock mass of the eastern Paris basin (Aisne, France), as detailed in [], [] and [] and summarized in Table [2](#table2). The parameter values are derived qualitatively from various triaxial compression tests, including creep tests conducted mainly in undrained conditions. The Aisne clay rocks exhibits high density (2.01 to 2.57 g/cm), a low average water content (between 3 to 11%) and, are characterized by low porosity (typically less then 20%). Therefore, hydromechanical coupling has minimal significance. The long-term effects primarily stem from material viscosity, with a low proportion attributable to pore pressure redistribution (hydraulic diffusion). Another characteristic is that irreversible deformations are observed in cyclic tests even at very small values of axial deformation (less than 0.3%). Furthermore, for in situ confinement values (approximaly 450 m deep), the maximum deviator remains practically constant, suggesting a Tresca-type failure criterion. In the creep tests, the magnitude of delayed deformations is comparable to that observed during instantaneous tests, with a deviatoric stress threshold beyond which creep phenomena initiate. Moreover, the influence of confining pressure on creep phenomena can be disregarded, and comparing both behaviors, instantaneous and delayed, reveals that short-term cohesion exceeds long-term cohesion, with the ratio between these two cohesion values ranging from 1.2 and 2.

Table [2](#table2) also presents the constitutive parameters for the lining, based on typical values for reinforced concrete. For the elastic analyses, Young’s modulus at 28 days is employed. In the viscoelastic analyses, however, Young’s modulus evolves as the lining ages. Each segment of the lining begins aging from the moment it is activated during the construction process. The effect of shrinkage begins at the age of days and creep begins at the age of loading, at day.

Table 2 Constitutive parameters used in the parametric analysis

| PARAMETERS | SYMBOL | UNIT | VALUES |
| --- | --- | --- | --- |
| Constitutive model of rock mass | | | |
| Young’s modulus |  | MPa |  |
| Poisson’s ratio |  | - |  |
| Plastic cohesion |  | MPa | 4 |
| Plastic friction angle |  |  | 0 |
| Viscoplastic cohesion |  | MPa | 2 |
| Viscoplastic friction angle |  |  | 0 |
| Power law parameter |  | - | 1 |
| Reference parameter |  | MPa | 1 |
| Viscosity coefficient |  | day |  |
| Constitutive model of lining | | | |
| Characteristic compressive strength at age of 28 days |  | MPa |  |
| Modulus of elasticity at a age of 28 days |  | MPa |  |
| Poisson’s ratio |  | - |  |
| Coefficient which depends on the type of cement |  | - |  |
| Relative humidity of ambient environment |  | % |  |
| Notional size of member - longitudinal concrete lining |  | cm |  |
| Notional size of member - gallery concrete lining |  | cm |  |
| Age of concrete at the beginning of shrinkage |  | days |  |
| Coefficient in shrinkage which depends on the type of cement |  | - |  |
| Temperature |  | C |  |
| Age of concrete at loading |  | days |  |

In this study, an initial hydrostatic stress of MPa, corresponding to a depth of 450 m, was adopted, simulating the conditions of the rock mass characterization. The study examines the long-term and short-term convergence profiles using various constitutive models for the rock mass (elastic, elastoplastic, and viscoplastic) and the lining (elastic, and viscoelastic), including scenarios without lining. For clarity, Table [3](#table3) lists the abbreviations used throughout the text and in the results legends. These analyses are conducted for three different distances between the longitudinal tunnels (, , and ), using a tunnel radius m and an excavation speed of 12.5 m/day. Additional geometric parameters for the domain, excavation, and lining installation are provided in Table [1](#table1), with further details discussed in Section  [5](#section_spatial).

Table 3 Abbreviation to the constitutive models and scenarios

| DESCRIPTION | ABBREVIATION |
| --- | --- |
| Elastic rock mass | E |
| Elastoplastic rock mass | EP |
| Elastoviscoplastic rock mass | VP |
| Elastoplastic-Viscoplastic rock mass | EPVP |
| Not lining | NL |
| Elastic lining | EL |
| Viscoelastic lining | VEL |
| Long-term | LT |
| Final excavation (Short-term) | ST |
| With Gallery | WG |
| Not Gallery | NG |

Denoting by the displacement component along the y-axis, all the results presented in the following analyses, show the convergence profile , which characterize the inward movement of the tunnel roof as a function of the normalized longitudinal distance from the excavation face. In addition, point was chosen to denote the equilibrium convergence outside the region of influence of the excavation face and the gallery. When the gallery is present, the highest convergence value, is highlighted at the coordinate where the gallery intersects the longitudinal tunnels .

An important observation is that in single tunnels, under rock mass isotropy and hidrostatic initial stress state conditions, the symmetry of the tunnel wall is preserved throughout the excavation process. Thus, the deformed tunnel wall remains circular. On the other hand, one of the effects of the mutual interaction induced by the proximity of the twin tunnels is the loss of symmetry of the deformed tunnel wall. Fig. [21](#Ovalization effect and monitoring point) presents tunnel roof B and the effect of ovalization due to the proximity of the tunnels. In this context, is not representative of the entire deformation of the tunnel wall.

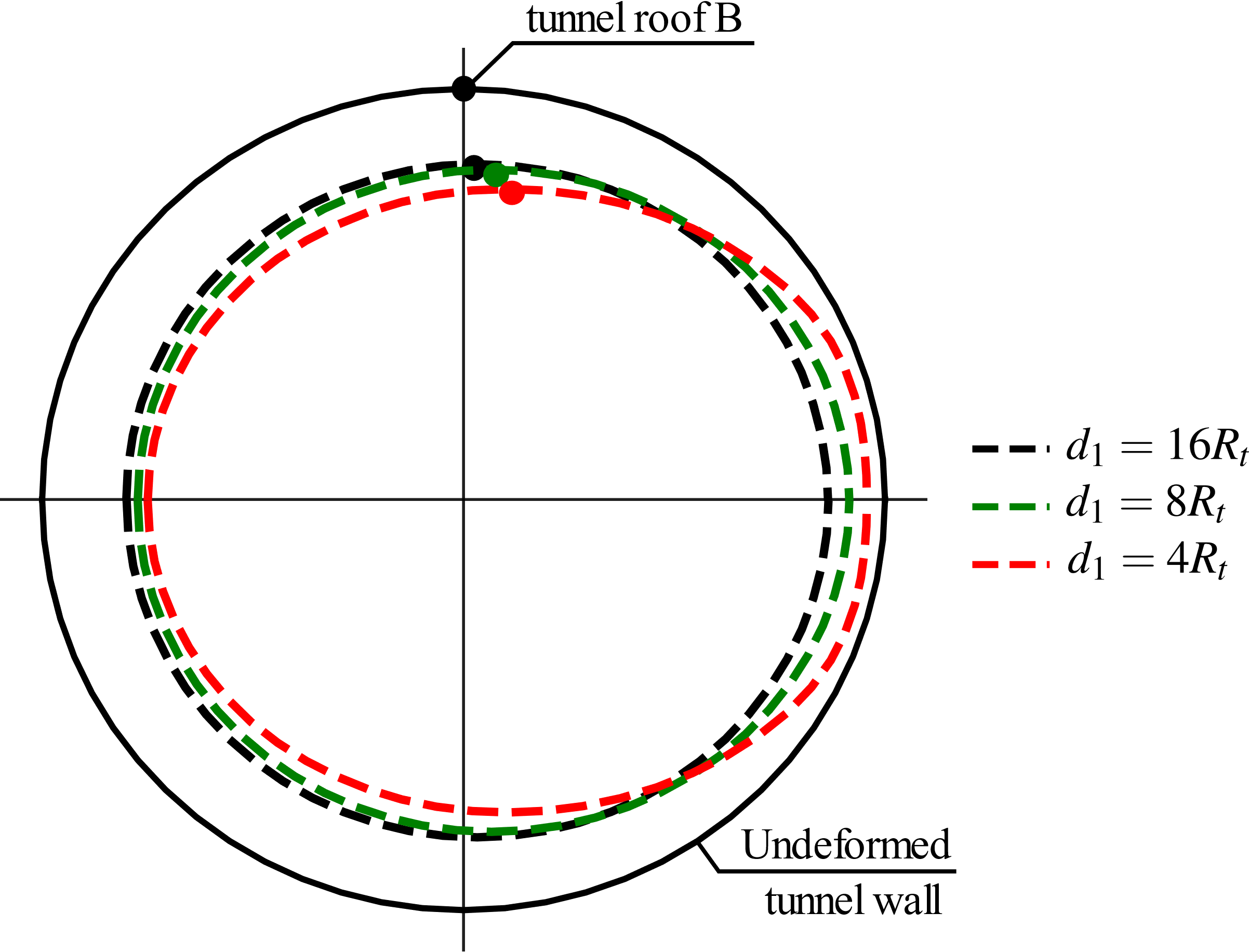


Figure 21 Monitoring point and ovalization effect

Another important observation regarding the material properties shown in Table [2](#table2) is that the value adopted for plastic cohesion () is greater than the value for viscoplastic cohesion (): > . This implies that, in the regime of irreversible deformations, the viscoplasticity of the material will be activated first. The generic configurations of the rock mass deformation zones during the excavation process are illustrated in Fig. [22](#zones).

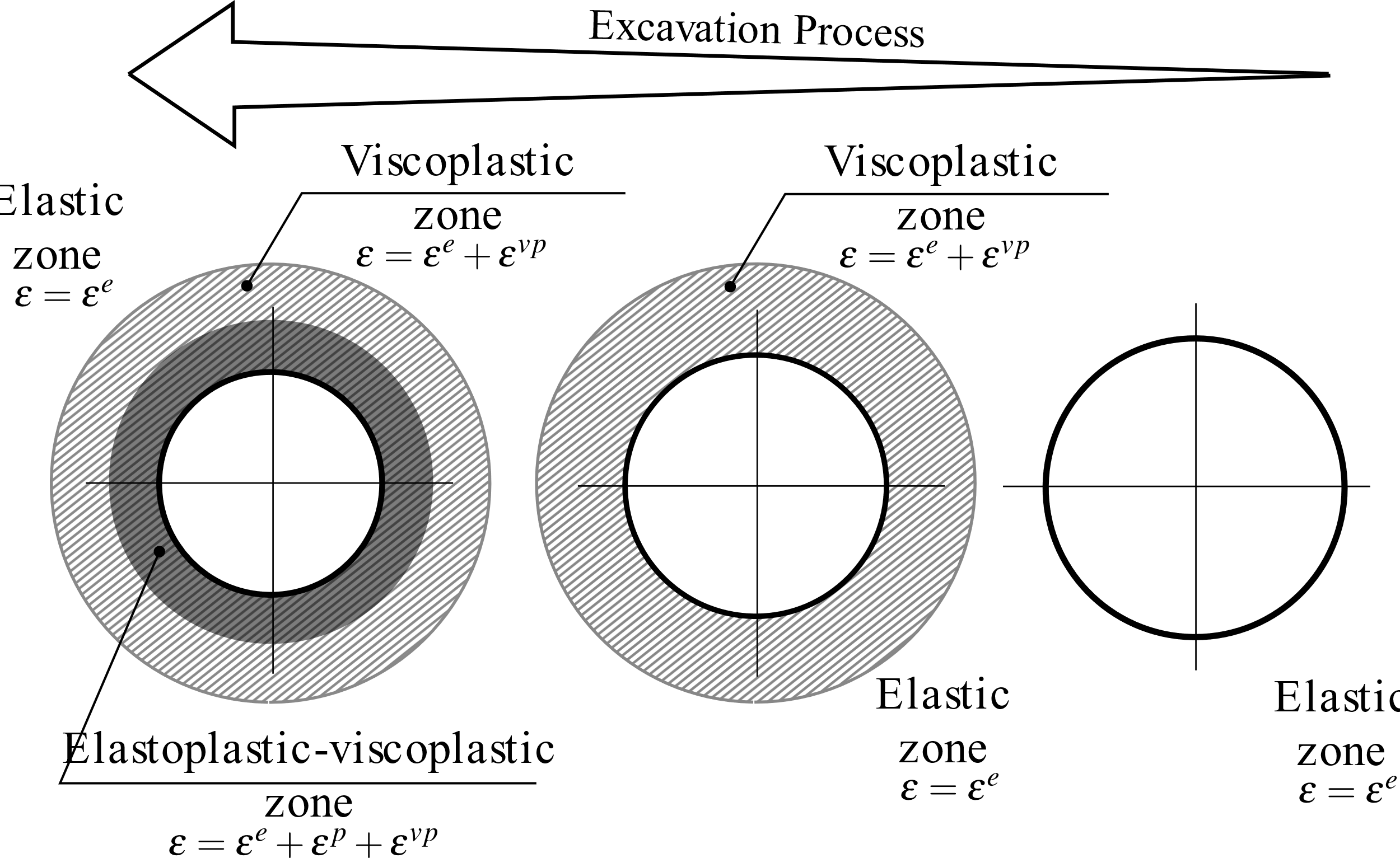


Figure 22 Configurations for the zones with irreversible deformations in the rock mass

## 7.2 Short and long-term analysis and ovalization effect

Figs. [23](#WG-ST-LT-D1-16RI), [24](#WG-ST-LT-D1-8RI), and [25](#WG-ST-LT-D1-4RI) show the convergence profiles of the twin tunnels with gallery (WG) for all the constitutive models of the rock mass (E - blue, EP - yellow, VP - magenta, EPVP - red and green) and the lining (EL and VEL) in the short-term (ST - solid lines) and the long-term (LT - dashed lines), for and respectively.

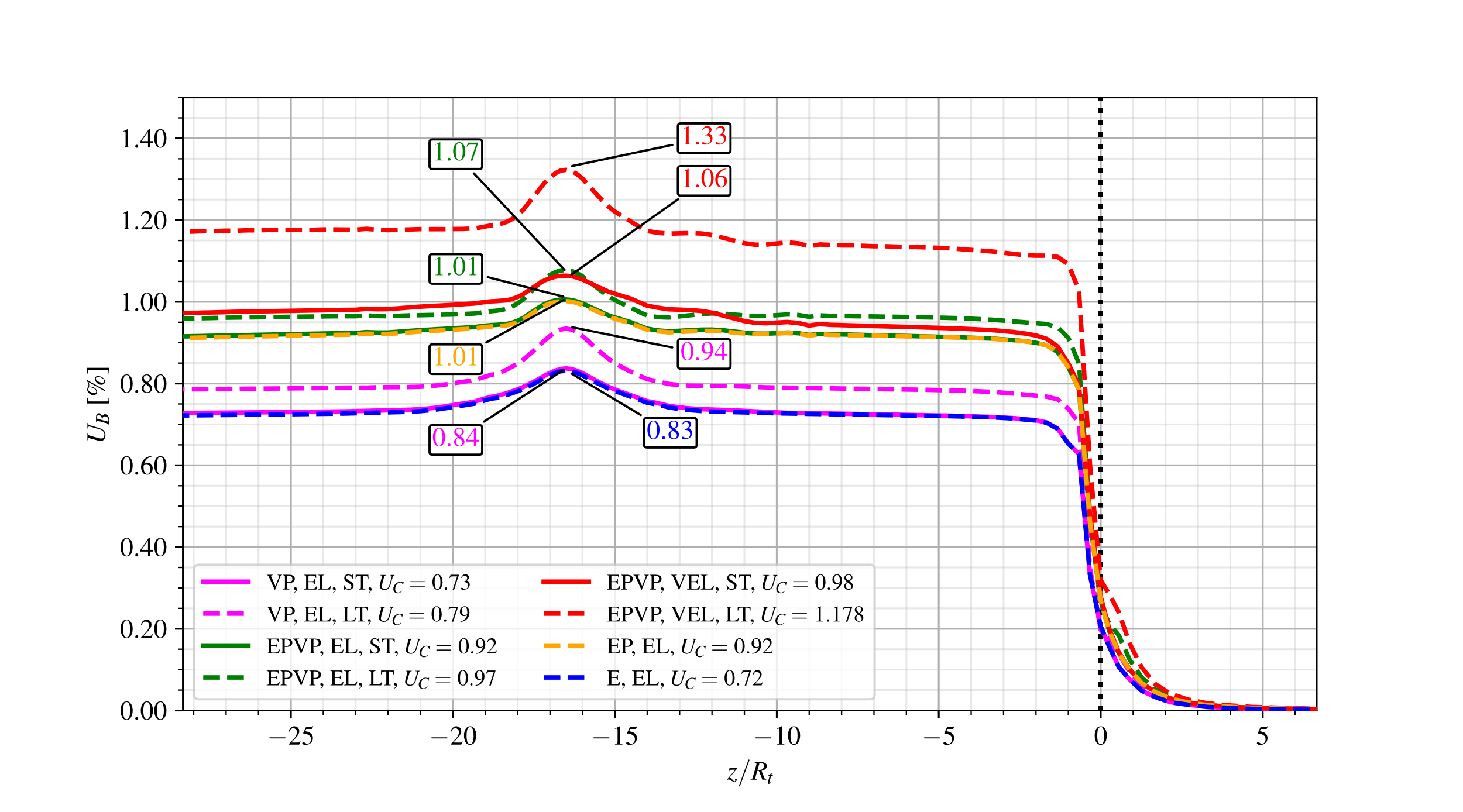


Figure 23 Convergence Profiles - with gallery (WG), short-term (ST) and long-term (LT) for

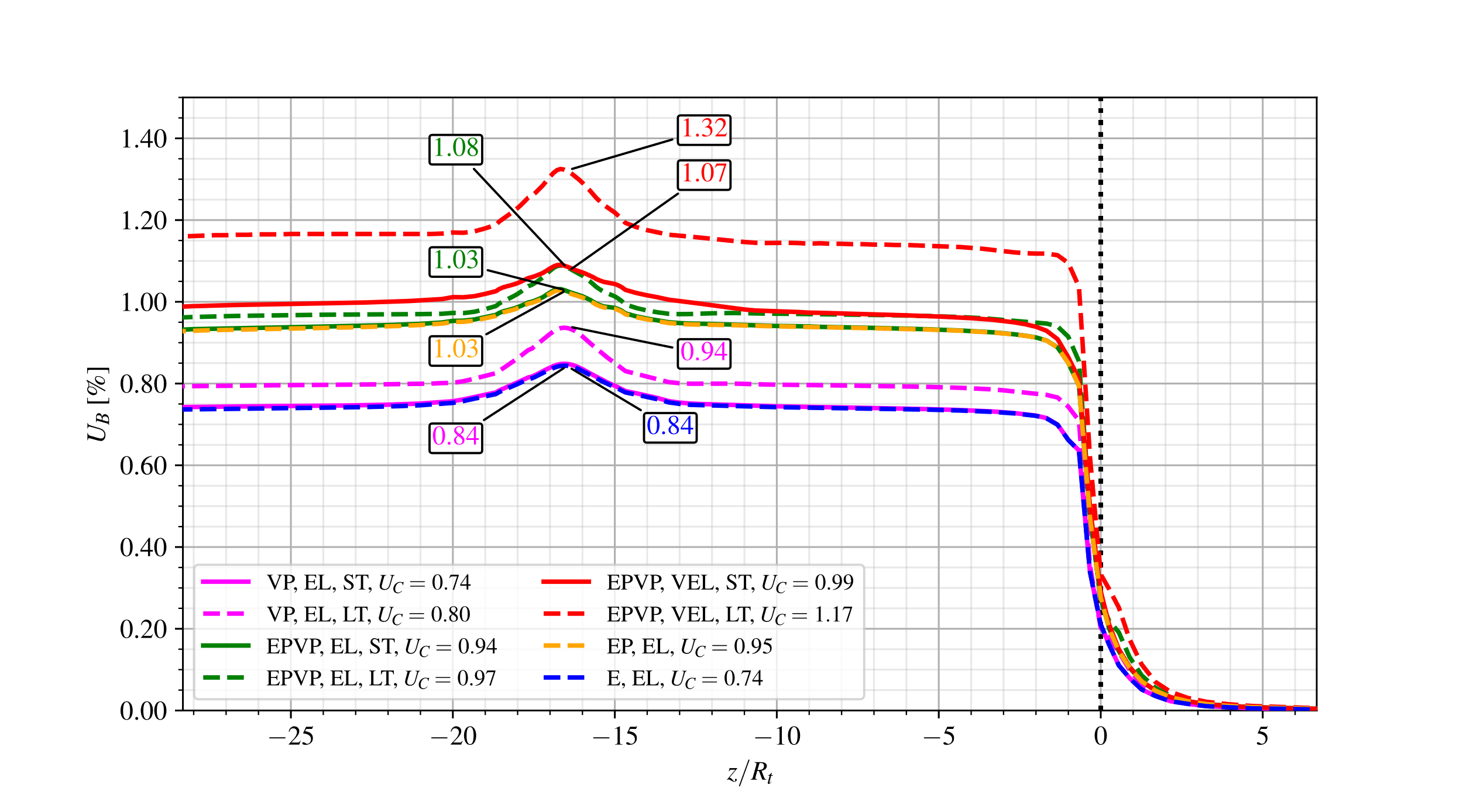


Figure 24 Convergence Profiles - with gallery (WG), short-term (ST) and long-term (LT) for

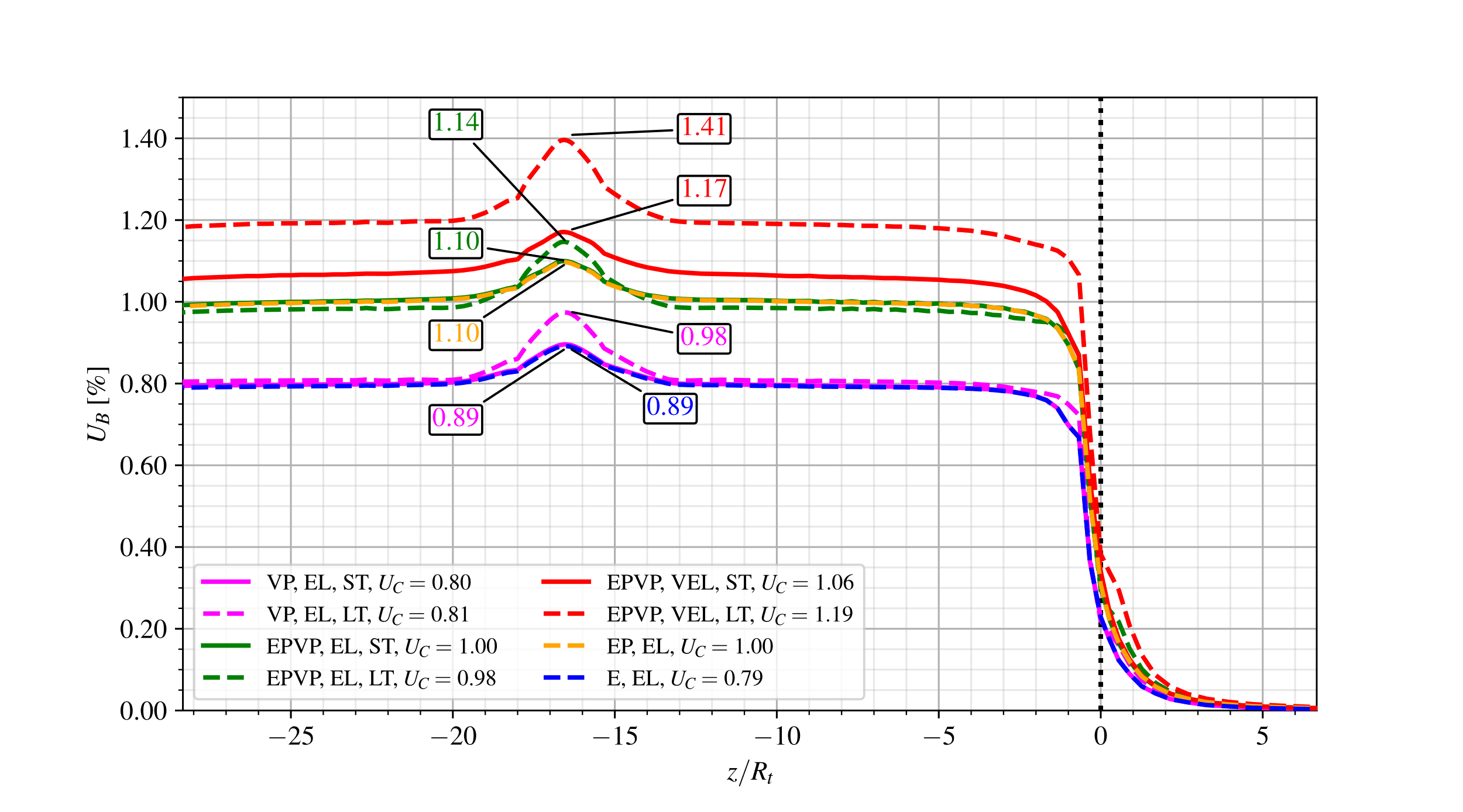


Figure 25 Convergence Profiles - with gallery (WG), short-term (ST) and long-term (LT) for

In all distances, the convergence profiles of the E-EL (blue dashed line) and the VP-EL (magenta solid line) in the short-term (ST) are equivalent, due to the high excavation speed. The high speed of the excavation and installation of the lining limits the time for the viscous effects to manifest themselves also taking into account the restriction imposed by the stiffness of the lining.

In the short-term (ST), the EPVP-EL model (green solid line) is equivalent to the EP-EL (yellow dashed line) because, although plasticization around the section has already occurred due to excavation, the viscous effects have not yet evolved considerably due to the short time between the start and end of excavation process. However, in the long-term (LT), as convergence continues (dashed green line), differences become apparent. When the rheological effects of the lining are considered, the profile continues to evolve significantly, as seen in the EPVP-VEL model (solid and dashed red lines).

An important aspect is that the stiffness of the elastic lining significantly impeded the evolution of convergence under viscous effects. This is particularly evident in the VP-EL model with (solid and dashed magenta line). In this case, the interaction between nearby twin tunnels causes a substantial increase in the value of in the short-term (ST). However, the long-term profile (LT) hardly changes, remaining close to the short-term one due to the limitation imposed by the stiffness of the lining.

Another noteworthy aspect is that the EPVP-VEL model with (red dashed line) has a reduction in convergence after 15 excavation steps () from the gallery. This phenomenon is due to the evolving viscous effects of the already-excavated longitudinal tunnel during the gallery excavation. This effect becomes more pronounced with which spends the longest time excavating the gallery. When the gallery lenght is smaller ( and ), the time elapsed is shorter, and this effect is less pronounced.

The effect of ovalization can also be seen in the convergence profile. The EPVP-EL-LT model (green solid line) has a slightly lower convergence than the EPVP-EL-ST (green dashed line) for . The ovalization effect is responsible for the roof’s convergence decreasing over time. However, another point in the tunnel wall experiences an increase in convergence. Fig. [26](#ovalization) illustrates this effect away from the gallery influence region with a single tunnel reference.

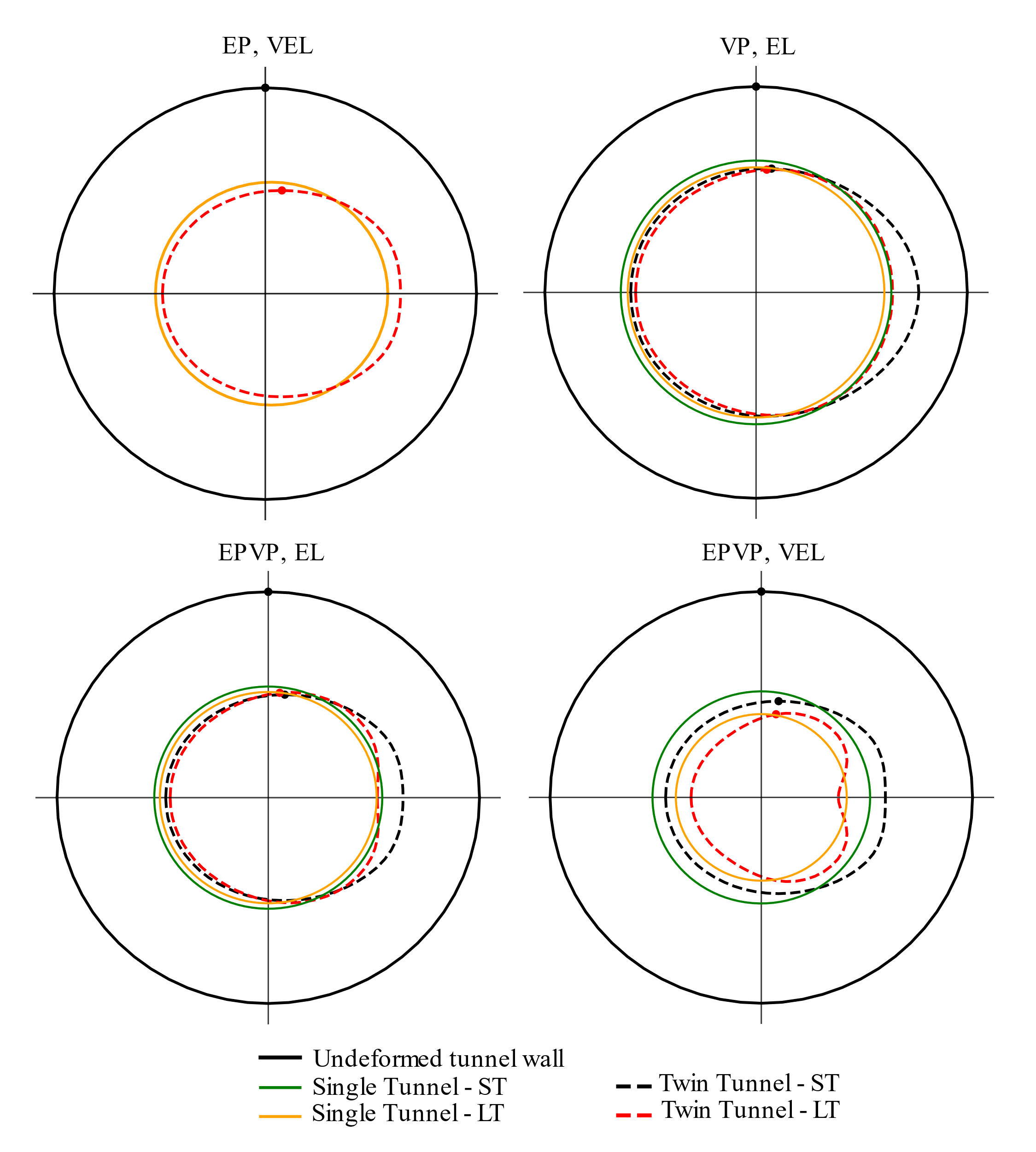


Figure 26 Ovalization effect for with deformations magnified 50x

Figs. [27](#UB-UAUB-D1_4RT) show ovalization effect between the vertical displacement at the roof B and the horizontal displacement at the side wall , for without gallery. The effect is more pronounced in the short-term (solid lines).

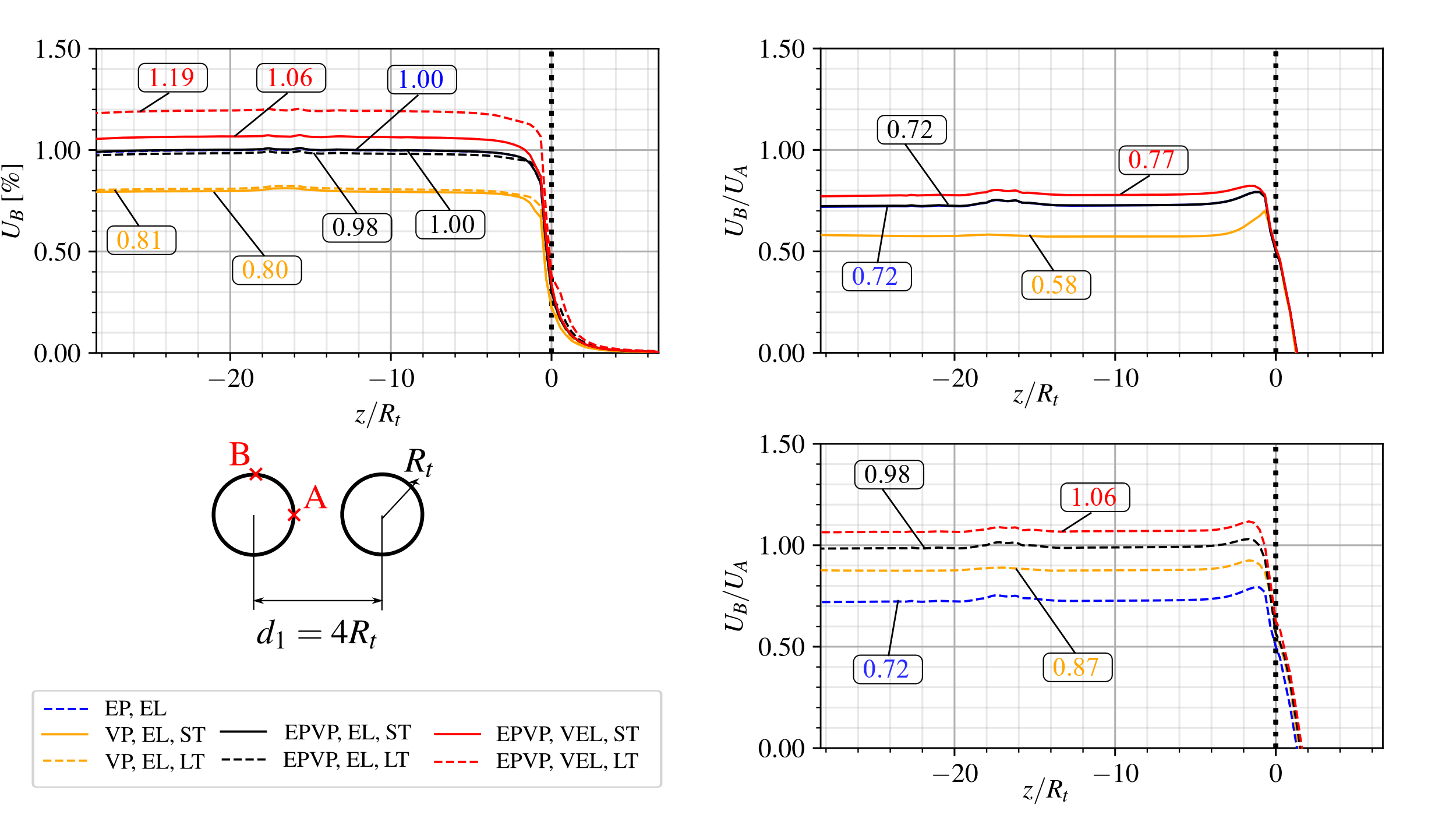


Figure 27 Convergence Profiles - ovalization effect for without gallery

## 7.3 Long-term analysis with viscous models

Fig. [28](#VP-EL-EPVP-VEL-WG-LT) shows the convergence profiles for and (yellow, green and red lines, respectively) with viscous constitutive models: viscoplastic rock mass with elastic lining (VP-EL - solid lines), elastoplastic-viscoplastic rock mass with elastic lining (EPVP-EL - dashed line) and viscoelastic lining (EPVP-VEL - dotted lines). As a reference, it also shows the results of a single tunnel (black lines). A slight increase in the peak value of convergence can be seen for the EPVP-VEL model when comparing (yellow dotted line) and (green dotted line). In the case of , the proximity of the tunnel compensates the convergence difference due the gallery excavation eplapsed time between and . However, when (red dotted line) the effect of the gallery is more pronounced due to the interaction between the proximity of the twin tunnels and the viscous effect.

Moreover, it is possible to observe higher convergence values in the excavated length that precedes the excavation of the gallery, specifically, in the EPVP-VEL model for and (green and yellow dotted lines). This effect is due to the viscoelastic behavior of the lining during the elapsed time to excavate the gallery. Unlike the highly rigid elastic lining, the viscoelastic lining allows the convergence to evolve during the excavation of the gallery. Consequently, the values of convergences before the gallery tend to be higher than after the gallery.

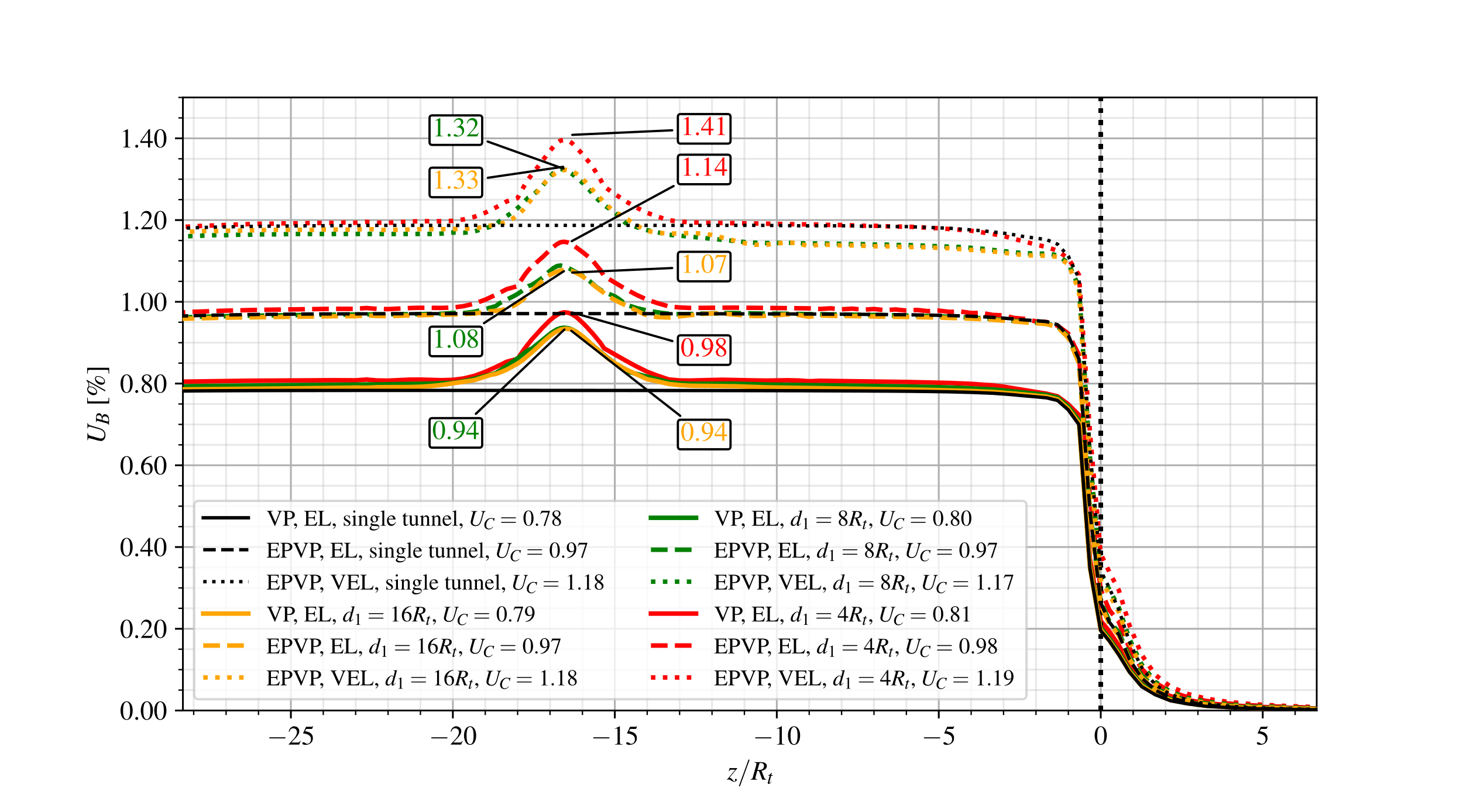


Figure 28 Convergence Profiles - viscoplastic rock mass (VP) with elastic lining (EL) compared to elastoplastic-viscoplastic rock mass (EPVP) with elastic (EL) and viscoelastic lining (VEL) in long-term (LT)

Fig. [29](#EP-EL-EPVP-VEL-WG-ST-LT) shows the convergence profiles for and (yellow, green and red lines, respectively) with elastoplastic rock mass with elastic lining (EP-EL - solid lines), elastoplastic-viscoplastic rock mass with viscoelastic lining in short-term (EPVP-VEL-ST - dotted lines) and long-term (EPVP-VEL-LT - dashed lines). As a reference, it also shows the results of a single tunnel (black lines).

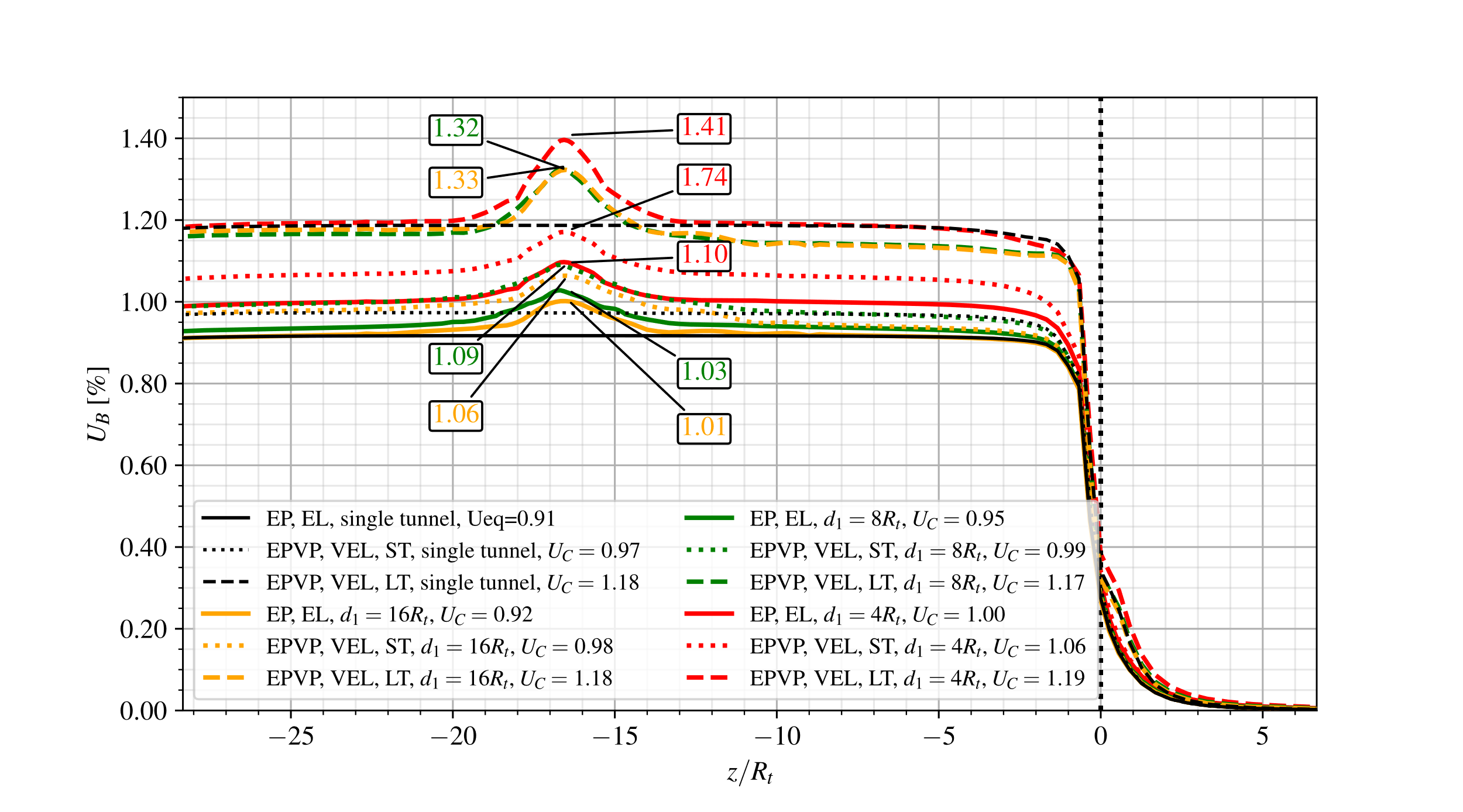


Figure 29 Convergence Profiles - elastoplastic rock mass (EP) with elastic lining (EL) compared to elastoplastic-viscoplastic rock mass (EPVP) with viscoelastic lining (VEL) in short-term (ST) and long-term (LT)

The results shows the crucial effect of the viscoelastic lining to the convergence profile of the tunnels. In the short-term (ST), the elastoplastic-viscoplastic rock mass with viscoelastic lining (EPVP-VEL - dotted lines) shows higher convergences compared to the elastoplastic with elastic lining (EP-EL - solid lines). Because the young age of the viscoelastic lining (VEL) has a lower modulus of elasticity, resulting in lower stiffness. Therefore, compared to the elastic lining (EL), the lower initial value of the modulus of elasticity contributes more to the development of convergence. In the long-term (LT), even though the viscoelastic lining (VEL) (dashed lindes) has a higher stiffness due to a aging of lining, the viscous effects over time result in a significantly more discrepant convergence profile compared to the elastoplastic with elastic lining (EP-EL - solid lines). There is a noticeable increase in the magnitude of between the short-term (dotted lines) and the long-term (dashed lines) at the gallery position, highlighting the influence of the viscoelastic lining.

## 7.4 Effect of lining stiffness on convergence evolution

To study the effect of the lining stiffness, Fig. [30](#EP_d1_16Ri) and [31](#EP_d1_4Ri) show the elastoplastic rock mass (EP) under various conditions: without lining (NL - dashed lines), with a moderately stiff elastic lining ( MPa - dotted lines), and with a higher stiff elastic lining ( MPa - solid lines) with gallery (WG - blue lines) and without gallery (NG - yellow lines) for and , respectively. As a reference, it also shows the results of a single tunnel (black lines). The stiffness values, MPa and MPa, are obtained from following expression in [] for single tunnels, considering Young’s modulus at 28 days MPa, Poisson’s ratio and lining thickness of and , respectively.



Figure 30 Convergence Profiles - elastoplastic rock mass (EP) without lining (NL) with a higher stiff elastic lining ( MPa) and a moderately stiff elastic lining ( MPa), without (NG) and with gallery (WG) for

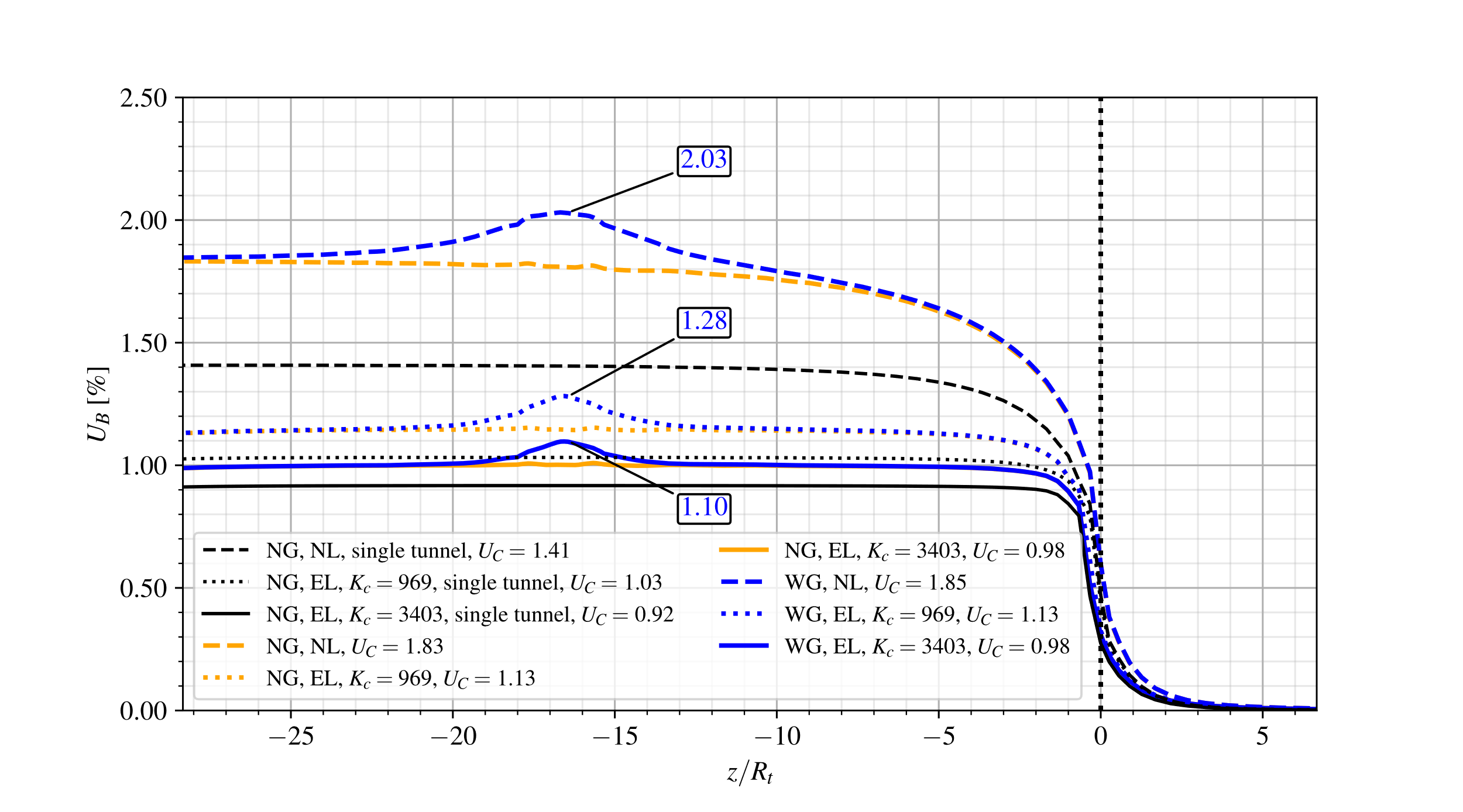


Figure 31 Convergence Profiles - elastoplastic rock mass (EP) without lining (NL) with a higher stiff elastic lining ( MPa) and a moderately stiff elastic lining ( MPa), without (NG) and with gallery (WG) for

For the single tunnel, the higher stifness lining (black solid line) reduced convergence by approximately 35% compared to the unlined scenario (black dashed line). Conversely, the moderately stiff lining (black dotted line) increases convergence by 12% compared to the rigid lining.

When (blue and yellow lines), the results of are similar to the isolated tunnel (black line). However, with a distance reduced to , the interaction between the tunnels becomes significant. A smaller , the high stiffness lining (yellow and blue solid lines) can restrict convergence by up to 46% of the unlined convergence (yellow and blue dashed lines). A moderate stiffness lining (dotted lines) leads to an increase of up to 16% in convergence compared to the higher stiffness lining (solid lines).

When comparing results between twin lined tunnels with and , differences of 6% with higher stiffness lining (yellow and blue solid lines), 10% with moderate stiffness lining (yellow and blue dotted lines), and 30% without lining (yellow and blue dashed lines) are observed. These results show the direct impact of lining stiffness and the distance between twin tunnels on convergence.

When analyzing the convergence at the point where the gallery meets the longitudinal tunnel, there is an increase of 16% when using an moderate stiffness lining (dotted blue line) compared to a higher stiffness lining (blue solid line). However, when analyzing the difference between the and , there is a difference of up to 12% for the higher stiffness lining (blue solid line to and ) and up to 13% for the moderate stiffness lining (blue dotted line to and ) for . In both figures it can be seen that the increase in stiffness reduces the extent of the disturbed region caused by the gallery in the longitudinal tunnel convergence profile. The range decreases from 22.5 (without lining) to 10.5 and 7.5 (with lining). Additionally, the proximity of the longitudinal tunnels has a minimal impact on the length of this gallery influence zone.

In line with the previous analysis of lining stiffness, Fig. [32](#EPVP_VEL_d1_16Ri) and Fig. [33](#EPVP_VEL_d1_4Ri) present the results for elastoplastic-viscoplastic rock mass (EPVP), considering a viscoelastic lining (VEL) with (WG - blue lines) and without gallery (NG - yellow lines) for and , respectively. For reference, results for a single tunnel are also included (black lines). This analysis aims to assess the influence of the lining stiffness, particularly when twin tunnels are in close proximity.

The results indicate that, once again, the convergence profile under these conditions, with a distance of between the tunnels, closely resembles that of an isolated tunnel. Differences are on the order of 1.8% for a moderately stiff lining and 0.8% for a higher stiff lining.

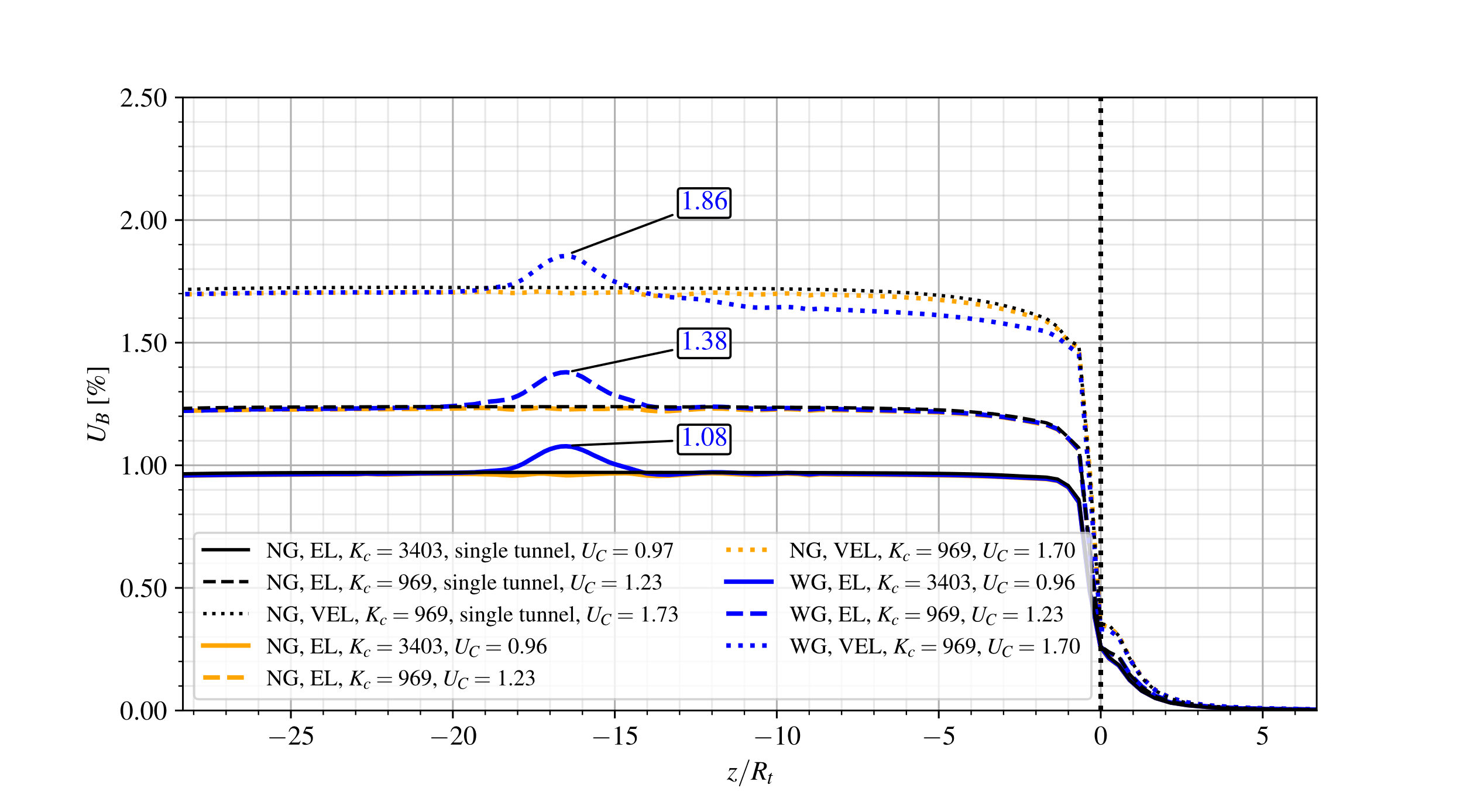


Figure 32 Convergence Profiles - elastoplastic-viscoplastic rock mass (EPVP) with a higher stiff viscoelastic lining ( MPa) and a moderately stiff viscoelastic lining ( MPa), without (NG) and with gallery (WG) for

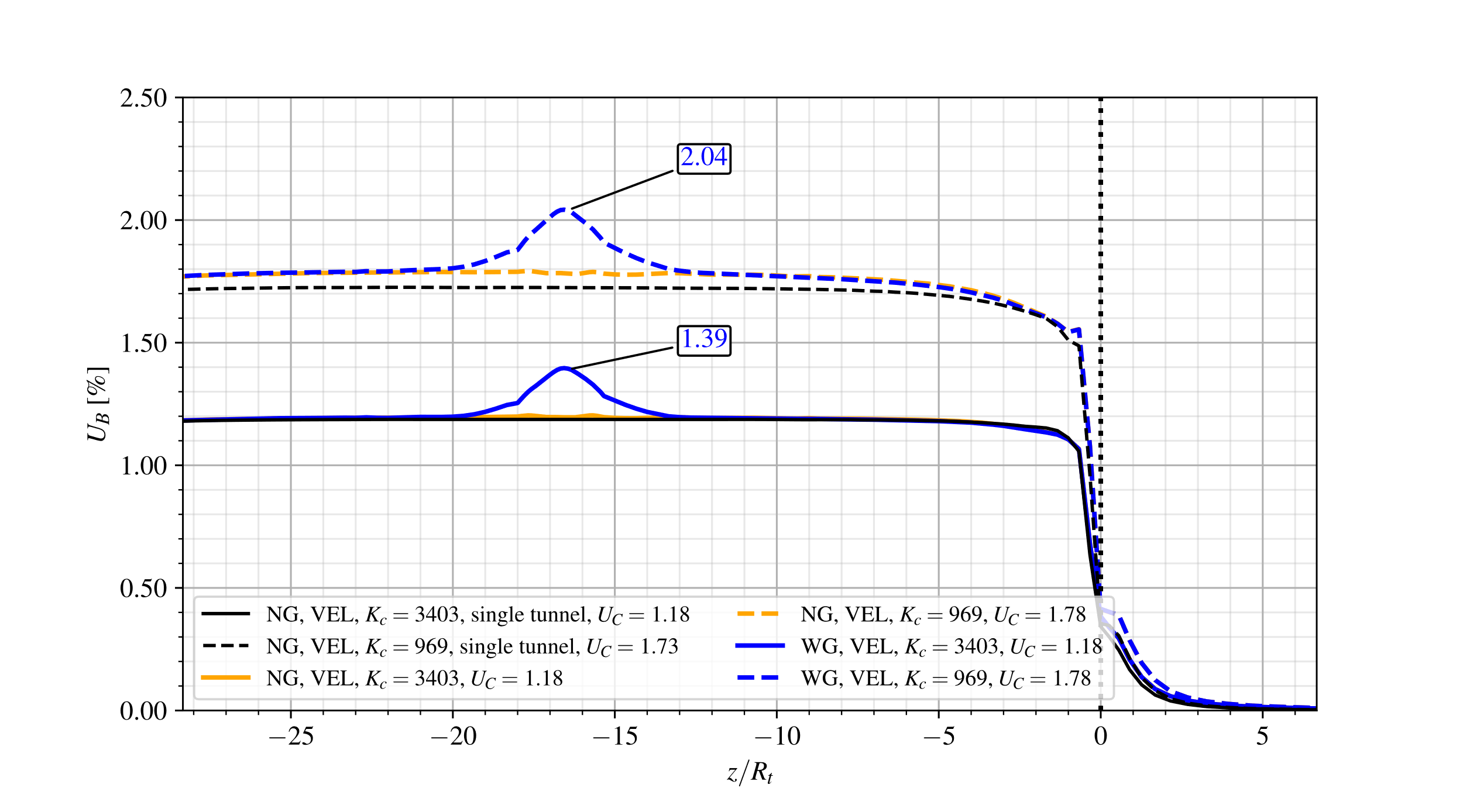


Figure 33 Convergence Profiles - elastoplastic-viscoplastic rock mass (EPVP) with a higher stiff viscoelastic lining ( MPa) and a moderately stiff viscoelastic lining ( MPa), without (NG) and with gallery (WG) for

In the case of , when the higher stiffness lining is applied (blue and yellow solid lines), there is practically no difference compared to the single tunnel (black solid line). This occurs because the higher stiffness of the lining blocks convergence in the interaction between the tunnels. However, when using a moderately stiff lining (blue and yellow dashed lines), there is a difference of approximately 3% in the convergence compared to the single tunnel (black dashed line).

When comparing the results for and , considering each lining separately, there is a difference of 0.8% when there is a higher stiffness lining (solid yellow and blue lines to and ) and 4.8% for a moderate stiffness lining (dashed yellow and blue lines to and ). Thus, once again, the importance of the stiffness of the lining when associated with the distance between the twin tunnels.

When analyzing the convergence at the point where the gallery meets the longitudinal tunnel, there is an increase of 47% for when using an moderate stiffness lining (dashed blue line) compared to a high stiffness lining (solid blue line). However, when analyzing the difference between the and , there is a difference of up to 18% for the high stiffness lining (solid blue line) and up to 15% for the moderate stiffness lining (dashed blue line) for .

The following results (Figs. [34](#EPVP_EL_VEL_d1_16Ri) and  [35](#EPVP_EL_VEL_d1_4Ri)) compare the elastic (EL - dashed and solid lines) and viscoelastic (VEL - dotted line) lining, considering the elastoplastic-viscoplastic model (EPVP) for the rock mass.

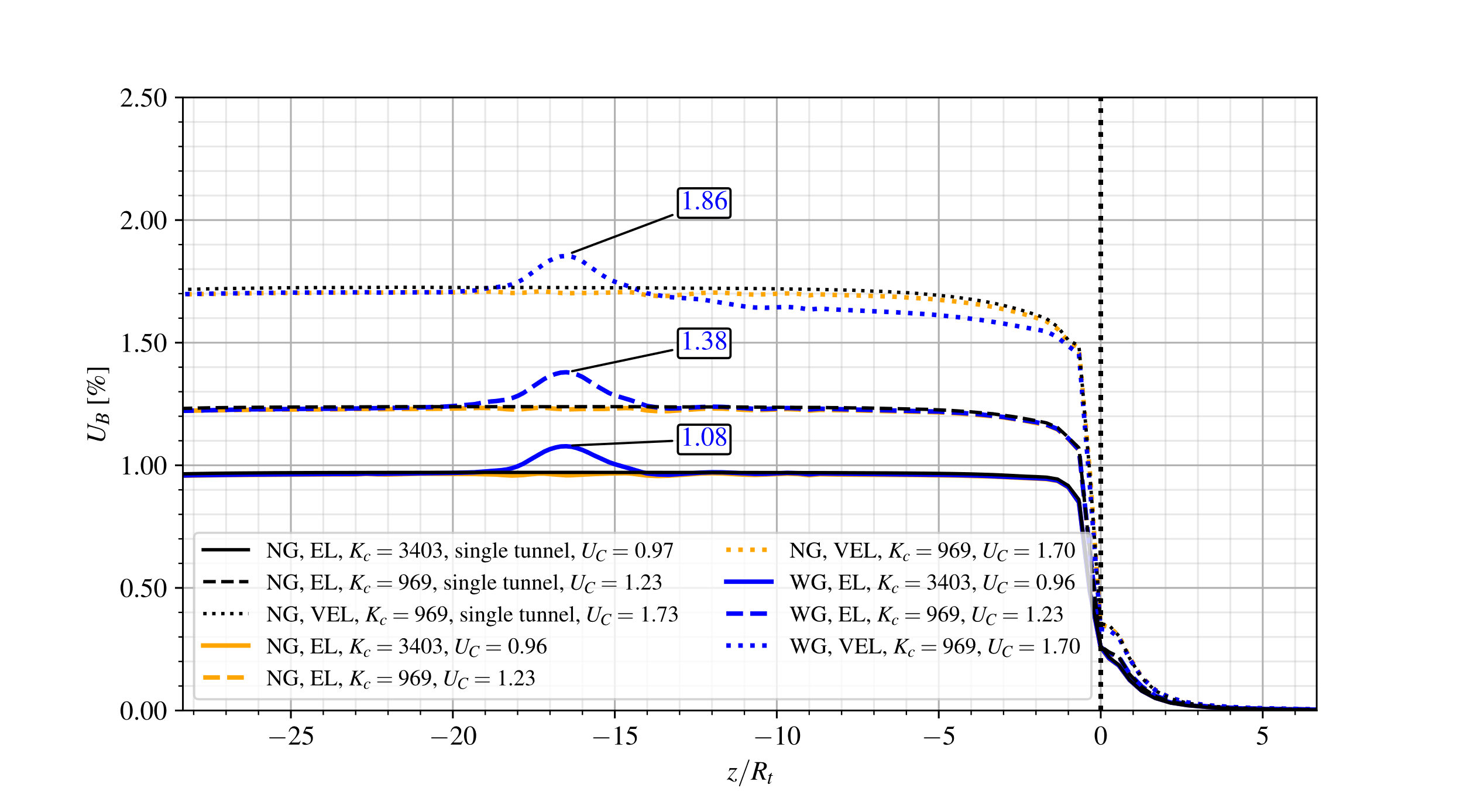


Figure 34 Convergence Profiles - elastoplastic-viscoplastic rock mass (EPVP) without lining (NL) with a higher stiff ( MPa) and a moderately stiff ( MPa) elastic (EL) and viscoelastic (VEL) lining, without (NG) and with gallery (WG) for

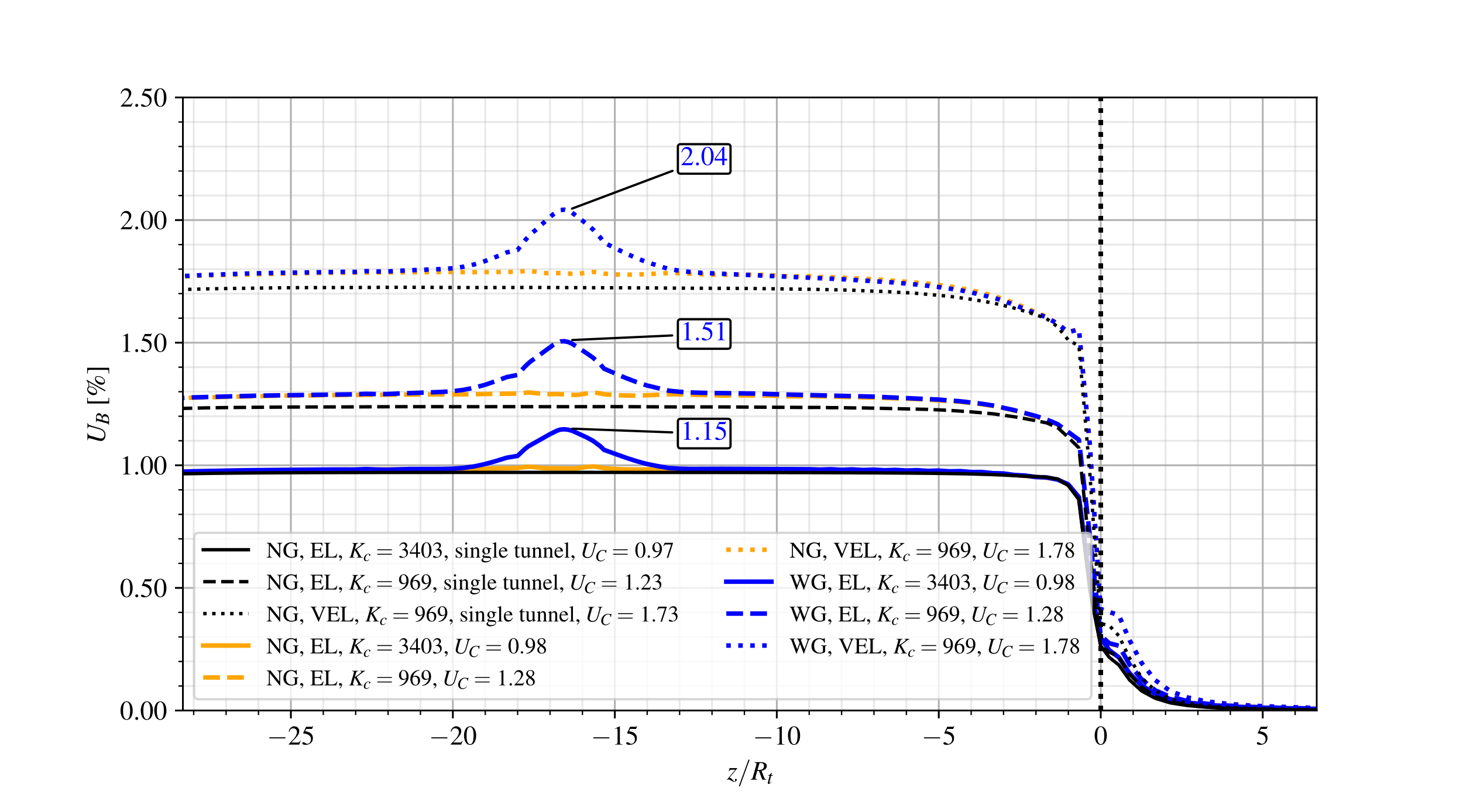


Figure 35 Convergence Profiles - elastoplastic-viscoplastic rock mass (EPVP) without lining (NL) with a higher stiff ( MPa) and a moderately stiff ( MPa) elastic (EL) and viscoelastic (VEL) lining, without (NG) and with gallery (WG) for

For , the most significant difference in compared to the isolated tunnel (black dotted line) occurs with the moderately stiff viscoelastic lining (blue dotted line), showing an increase of approximately 1.8%. In contrast, for , the differences increase to 4% for the elastic lining (dashed lines) and 3% for the moderately stiff viscoelastic lining (dotted lines). Using the higher stiffness elastic lining as a reference (solid lines), for , the differences rise to 27% for the elastic (dashed lines) and 78% for viscoelastic (dotted lines) lining with moderate stifness. For , these differences further increase to 31% and 81%, respectively.

When analyzing the convergence at the peak , which corresponds to the point where the gallery meets the longitudinal tunnel, and using the value of the higher stiffness elastic lining (solid lines) as the reference, an increase of up to 31% and 77% is observed for when using the elastic (dashed lines) and viscoelastic (dotted lines) linings of moderate stiffness, respectively. However, when analyzing the difference between the and , there is a difference of up to 18% for the moderate stiffness elastic lining (blue dashed line) and up to 15% for the moderate stiffness viscoelastic lining (blue dotted line) for .

Finally, Fig. [36](#EP_EPVP_NG_LT_single tunnel) shows a comparison between the elastic and viscoelastic lining, considering higher (solid lines) and moderate stiffness (dotted lines), and between the elastoplastic (black lines) and elastoplastic-viscoplastic (red and blue) rock mass. Results without the lining (NL - dashed lines) are also included.

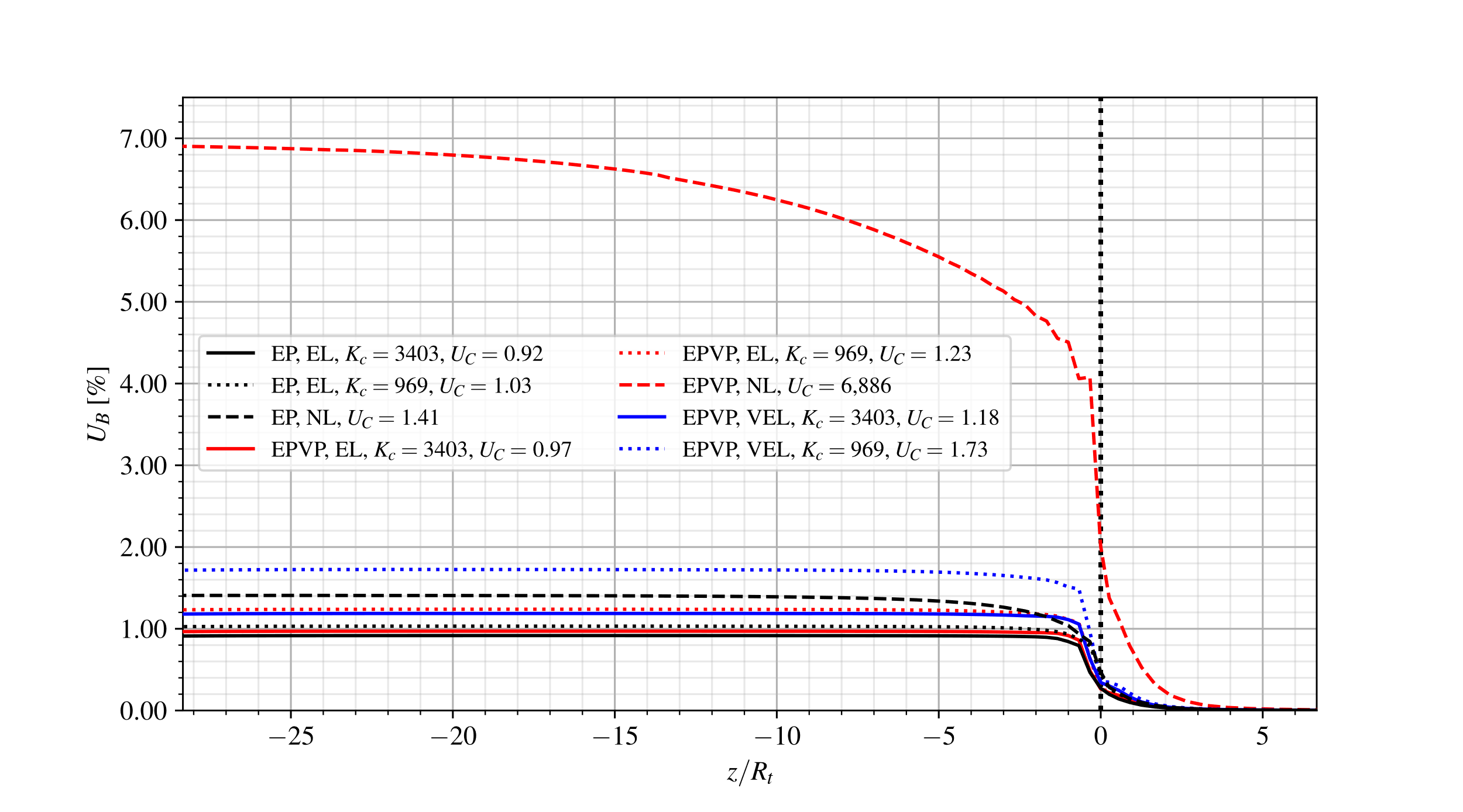


Figure 36 Convergence Profiles - single tunnel with elastoplastic (EP) and elastoplastic-viscoplastic rock mass (EPVP), without lining (NL) with a higher stiff ( MPa) and a moderately stiff ( MPa) elastic (EL) and viscoelastic (VEL) lining

Taking as a reference the elastoplastic model with the higher stiffness lining (solid black line) we observed a difference of 12% and 53.5%, respectively, in the cases of the elastoplastic rock mass with an elastic lining of moderate stiffness (dotted black) and without a lining (dashed black line), respectively. We also identified a difference of 5.5%, 33.5%, and 748% when using the elastoplastic-viscoplastic rock mass with an elastic lining of higher stiffness (solid red line), moderate stiffness (dotted red line), and no lining (dashed red line), respectively. In addition, we found a difference of 28% and 87.5% when comparing with the elastoplastic-viscoplastic rock mass with the higher stiffness (solid blue line) and moderate stiffness viscoelastic lining (dotted blue line), respectively.

# 8. Conclusions

The fundamental role of the stiffness of the concrete lining in the convergence profile of twin tunnels is understood from the analyses. Depending on the value of this stiffness, it is possible to condition the restriction of viscous effects that tend to manifest over time after the completion of the excavation process.

Additionally, the effect of the interaction between longitudinal tunnels is notable when considering proximity, with significant influence from a distance of 4 radii. However, in many cases, this effect may be subtle or almost imperceptible due to the presence of a higher rigid lining.

In models considering the viscosity of the rock mass, the time factor plays a significant role in convergence. In this scenario, when excavating the gallery with , the portion of the tunnel already excavated remains subject to viscous effects for a more extended period compared to other distances. In any case, when , the proximity interaction between twin tunnels, along with viscous effects over time, results in a higher value compared to cases where and .

Another important observation related to EPVP-EL and EPVP-VEL models concerns the possible ovalization of the section over time, concerning the analyzed reference point on the section perimeter (in the crown). Instead of following the logic of following the closing direction of the section, it may undergo some negative displacement in the long-term. The result, for the same observation point, is a convergence value that in the short-term may indicate section closure but in the long-term may indicate the opposite.

Another crucial observation regarding EPVP-EL and EPVP-VEL models pertains to the potential ovalization of the section over time, particularly concerning the analyzed reference point on the section perimeter (in the crown). Instead of conforming to the expected logic of closing in the section’s direction, it might experience negative displacement in the long-term. Consequently, for the same observation point, the convergence value may initially suggest section closure in the short-term but indicate the opposite in the long-term.

Concerning the EPVP-VEL model, specifically with distances of 16 and 8 radii between twin tunnels, we observe that Ueq in the section ahead of the gallery region is slightly smaller than Ueq in the section preceding the gallery. This variation in the convergence profile results from the shorter exposure time to viscous effects in the portion excavated later than the transverse gallery. Therefore, during the gallery excavation process, the portion of the longitudinal tunnel already excavated experiences viscous effects until completing the gallery excavation.

However, concerning the existence of a transverse gallery and adopting the constitutive parameters while considering the presence of lining, its influence is highly localized, spanning approximately four radii on each side from its axis. Consequently, there is no significant impact on the remaining convergence profile of the tunnels, except for the model with viscoelastic lining, where lower convergences occur after the gallery.