

ARTICLE IN PRESS



Available online at www.sciencedirect.com

SCIENCE @ DIRECT®

Biomaterials

Biomaterials ■ (■■■) ■■■

www.elsevier.com/locate/biomaterials

Technical note

AC electrospray biomaterials synthesis

Leslie Y. Yeo, Zachary Gagnon, Hsueh-Chia Chang*

Department of Chemical & Biomolecular Engineering, Center for Microfluidics & Medical Diagnostics, University of Notre Dame, Notre Dame, IN 46556, USA

Received 14 February 2005; accepted 23 March 2005

Abstract

A rapid, viable and safe fabrication method for biomaterials synthesis is reported using high-frequency AC electrospraying. We demonstrate its potential for polymeric nanoparticle fabrication, drug encapsulation in mono-dispersed micron-sized biodegradable polymer shells and the synthesis of 1 µm biodegradable fibers with adjustable pore sizes as bioscaffolds for tissue/orthopaedic engineering and wound care therapy. The absence of charge in the ejected drops and fibers facilitates pulmonary drug delivery, polymer encapsulation and minimizes protein/DNA denaturing or compound ionization.

© 2005 Published by Elsevier Ltd.

Keywords: Electrospraying; Microencapsulation; Bioscaffold; Nanoparticles; Biodegradable polymer**1. Introduction**

Advances in biomaterials research have produced an arsenal of natural and synthetic materials (e.g. lactide and glycolide polymers, polyanhydrides, collagen, etc.) that can be utilized for tissue/bone engineering, targeted and controlled drug delivery and wound therapy [1]. Two key criteria are biodegradability and biocompatibility. The former requires the material to naturally decompose and absorb in vivo, either enzymatically or non-enzymatically, over a desired period of time, therefore eliminating difficult and complicated surgical procedures involved in its retrieval or removal. The latter requires that the material be non-toxic such that it does not invoke a chronic inflammatory response by the immune system. Whilst the synthesis of such materials has been successful at a laboratory scale through a host of fabrication methods, a viable, rapid, safe and economical technique that can be scaled up to mass production lines but also scaled down to dimensions

commensurate with portable devices for direct in-situ administration of the material to the patient is required.

Recently, a new electrospray mechanism using high-frequency AC electric fields above 10 kHz has been developed [2,3]. We report preliminary investigations to exploit the AC electrospray for biomaterials synthesis and propose its potential for scalability to both portable in-situ delivery devices and mass production lines. Applications are focused on two major areas, namely, micro/nano-encapsulation for drug delivery and fiber synthesis for tissue/orthopaedic engineering and wound healing.

The encapsulation of DNA, peptides, proteins and other therapeutic molecules within a biodegradable spherical shell of polymeric excipient is a vital vehicle for the controlled and targeted ophthalmic, oral, intravenous or implanted delivery of vaccines/drugs. The encapsulation shell provides a shield that isolates these substances from hostile environments thus preventing their susceptibility to decomposition, enzymatic degradation, aggregation and denaturation, and hence prolonging their half-lives in the blood stream as well as their shelf life; hydrophobic compounds therefore can be encapsulated in hydrophilic capsules to allow injection

*Corresponding author. Tel.: +1 574 631 5697; fax: +1 574 631 8366.
E-mail address: chang.2@nd.edu (H.-C. Chang).

1 into the blood stream and muscle tissue. Furthermore,
 3 the diffusion of the molecules through the polymeric
 5 shell as well as the biodegradation of the shell can be
 7 controlled, therefore preventing initial bursts of dosage
 9 and thus providing a means for the slow controlled
 11 release of the drug over time. In addition, by choosing
 13 polymers with different characteristic surface properties
 15 or by modifying its surface functionality, drug specificity
 17 can be engineered to avoid uptake by the liver, spleen or
 19 other parts of the reticularendothelial system and to
 21 locally target the diseased lesion or tumor [4]. This
 23 demonstrates the exciting possibility to design specific
 25 drug delivery systems for individuals, which could
 27 represent the future generation of drugs.

29 The synthesis of fibrous biomaterials, on the other
 31 hand, has also emerged as an important technology
 33 given its relevance to bioapplications such as tissue/bone
 35 engineering, wound healing therapy and vascular grafting.
 37 These biomaterials also function as a 'skin' for
 39 implanted non-biocompatible devices made of materials
 41 that would otherwise trigger an undesirable inflammatory
 43 response. In tissue/bone engineering, there have been
 45 collective efforts to develop highly porous bioscaffolds
 47 that progressively imitate the structure and
 49 function of the *in vivo* extracellular matrix of tissues/
 51 organs, thus providing mechanical support to the cells
 53 and maintaining the organizational definition of the
 55 tissue space whilst preserving its biocompatibility and
 reabsorbability.

57 In each of these applications, we discuss current
 59 fabrication strategies and suggest why the AC electro-
 61 spray has definite advantages over these methods and
 63 over DC electrospraying in increasing administration
 65 efficiency, patient compliance, comfort and convenience.

37 2. Materials and methods

39 A schematic depiction of the experimental apparatus
 41 is shown in Fig. 1. A high-frequency ($>10\text{ kHz}$) AC
 43 electric field, generated using a high-voltage output
 45 transformer (Industrial Test Equipment 113459-1), RF
 47 amplifier (Powertron 250 A, 10 Hz–1 MHz) and
 49 function/arbitrary waveform generator (Hewlett-Packard
 51 33120A), is applied across a metal hub micro-syringe
 53 (Hamilton N733) filled with the working fluid and a
 55 ground electrode consisting of a copper strip placed
 5 mm away. The syringe is mounted at an inclination
 angle of 50° to the horizontal to provide an adequate
 hydrostatic head to deliver the fluid to the syringe tip.

57 The polymeric excipient consisted of poly-DL-lactic-
 59 acid (PLA) with molecular weight 6000–16,000 (Poly-
 61 sciences Inc. 22505), received in the form of small white
 63 crystalline pellets in sealed containers to prevent
 65 hydrolysis by moisture in the air. The pellets were
 67 subsequently stored refrigerated in tightly closed con-

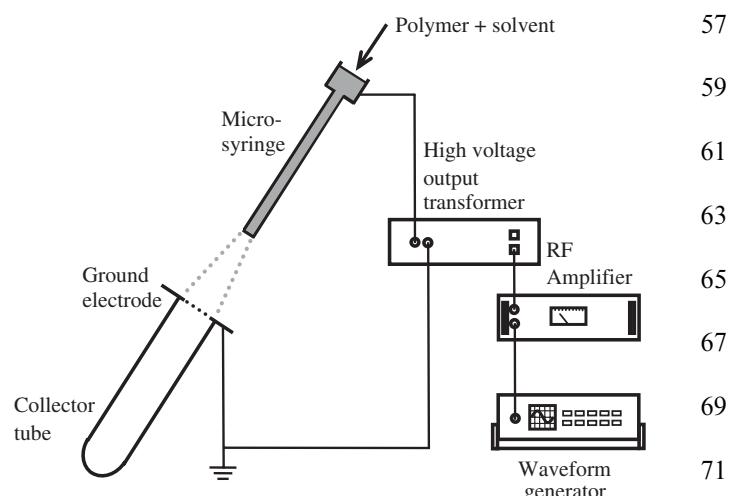


Fig. 1. Schematic of the AC electrospray apparatus used for microencapsulation and fiber synthesis.

tainers; dessicant was used to absorb the surrounding
 77 moisture. The solvent used to dissolve PLA is a 20% 1-
 79 butanol (Fisher Scientific ACS grade A399-500) and
 80% methylene chloride (Spectrum Chemicals HPLC
 81 grade HP732) mixture. The density, viscosity, interfacial
 83 tension and relative permittivity of butanol are 810 kg/m^3 ,
 3 mPa s , 26.28 mN/m and 17.8 , respectively, whereas
 85 those for methylene chloride are 911 kg/m^3 , 0.244 mPa s ,
 28.12 mN/m and 12.6 , respectively.

The concentration of the polymeric excipient in the
 87 solvent depends on the nature of the application. For
 89 electrospray microencapsulation, 10 mg of PLA was
 91 dissolved in 2 ml of the 20%/80% butanol/methylene
 93 chloride mixture. A water-in-oil microemulsion is
 95 created by adding 0.5 ml of deionized (DI) water into
 97 the polymer/solvent solution followed by vigorous
 agitation; the microemulsion was stabilized by adding
 99 trace amounts of surfactant (99% hydrolyzed poly-
 101 vinyl-alcohol, Aldrich Chemical Co.). The mixture was
 103 then electrosprayed directly using high-frequency AC
 105 electric fields at 20 kHz and 4.5 kV (peak-to-peak) to
 107 produce compound drops below $10\text{ }\mu\text{m}$ in dimension.
 109 Polymer solidification occurred in-flight leaving behind
 111 a hardened polymer shell containing an aqueous core.
 To allow for an extended flight length such that
 complete solidification is ensured before impact, a
 5 mm hole was drilled into the ground electrode behind
 which a tubular collector greater than 3 cm in length was
 placed, as shown in Fig. 1. The collector was then rinsed
 with DI water and its contents passed through a porous
 membrane filter (Millipore Type GS $0.22\text{ }\mu\text{m}$) to recover
 the microspheres. To test for encapsulation, an aqueous
 phase fluorescent dye uranine/sodium fluorescein (Sigma
 F6377 fluorescent sodium salt) was added to DI water in a subset of experiments. The recovered micro-
 spheres were then thoroughly washed with DI water to

remove any traces of the dye external to the micro-spheres. Any evidence of fluorescence in the micro-spheres after the rinse then suggests that the fluorescence labeled DI water is encapsulated within the micro-spheres.

For the synthesis of biodegradable fibers, a water-in-oil microemulsion is not required. The fibers were generated by directly spraying higher polymer concentrations (0.05–0.1 g of PLA) dissolved in the 2 ml 20%/80% butanol/methylene chloride solution described above under the same conditions. Due to the higher concentration of polymeric excipient in the solvent, partial solidification of the meniscus occurred. However, as a result of hydrodynamic stresses, thin long jets of fibers were extruded from the meniscus. In some instances, the polymer drops continued to be ejected from the meniscus tip concurrently with the fiber formation, which occurred a small offset away from the tip. In place of an electrode orifice and collector, however, the fibers are sprayed directly onto the ground electrode to form a fibrous mat consisting of a mesh/network of single-strand fibers.

Electrospray images were obtained using a high-speed video camera (Kodak Ektapro 1000 Imager and High Spec Processor) at record rates between 1000 and 6000 fps. The camera was connected to a telescopic lens and background illumination was provided by a fiber-optic lamp (Dolan-Jenner PL-800). The drops and fibers were inspected using an inverted microscope (Olympus IX71) with 10× to 60× magnification objectives. A scanning electron microscope (Oxford Instruments INCAEnergy) was also used to obtain images of the drops and fibers.

3. Results and discussion

In AC electrospraying, the Maxwell stress arising due to the applied electric field overcomes the capillary stresses on the liquid and acts to stretch and deform the

protruding meniscus. The drop subsequently pinches off due to viscous or inertial effects, the latter occurring at higher frequencies above a viscous-capillary pinch-off frequency that is typically between 20 and 50 kHz. Fig. 2 shows the resulting drop ejection mechanisms: viscous pinch-off leads to tip streaming (Fig. 2a) whereas inertial pinch-off results in a long slender microjet, at the tip of which the drop detaches (Figs. 2b and c). The AC electrospray is thus capable of producing mono- and poly-dispersed electroneutral drops below 10 μm. Scanning electron microscopy (SEM) images as will be shown also reveal that the AC electrospray can produce submicron particles that cannot be observed using conventional microscopy.

A distinct advantage of using high-frequency AC over its traditional DC counterpart is that the micron-sized AC drops produced are typically larger and are electroneutral [2]. For direct local administration to target organs in respiratory drug delivery, an optimum drop size of approximately 2.8 μm is required for optimum dose efficiency for the maximum amount of drug to reach the lower respiratory airways [5]. The DC charged drops undergo Rayleigh fission and are typically too small (~10 nm) to penetrate into the respiratory airways. Moreover, due to the charged nature of the nanometer DC electrospray drops, they are prone to surface adsorption and the encapsulated drug content potentially susceptible to destabilization as a result of electroporation or ionization.

Rayleigh fission, on the other hand, does not occur in the electroneutral AC drops. Furthermore, the current and hence the power requirement is low [2], demonstrating the potential for the miniaturization of the AC electrospray to portable devices. The absence of charge also precludes the need for cumbersome ancillary equipment such as corona discharge tips to neutralize charged drops [6,7] before delivery to the patient is possible. In addition, drops are produced at lower voltages using AC fields. Typically, the critical onset voltage for drop ejection in AC electrosprays is around

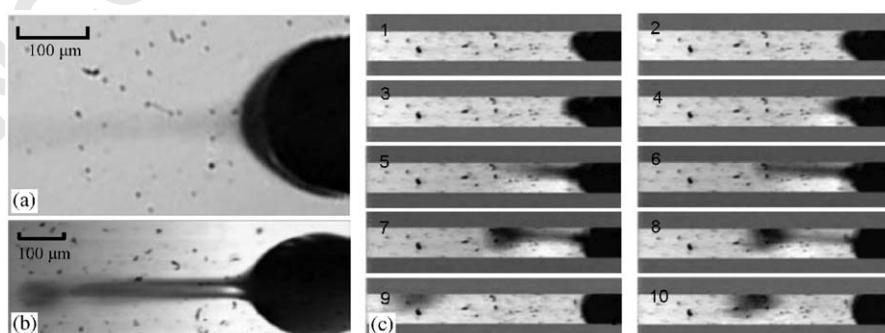


Fig. 2. AC electrospray drop ejection mechanisms. (a) Drop ejection due to viscous pinch-off (tip streaming); (b) drop ejection due to inertial pinch-off resulting in microjet formation; (c) sequences of images at 6000 frames/s showing the development of the microjet and subsequent drop detachment.

1 1 kV (peak-to-peak) in comparison to several kV in DC
 3 electrosprays; extremely large DC voltages up to 30 kV
 5 are not uncommon [8]. One reason why DC electro-
 7 spraying has failed to emerge as a viable option in
 9 commercial devices is because of safety issues regarding
 body.

11 3.1. Electrospray encapsulation

13 Current encapsulation technologies involve polymer
 15 solvent extraction from a double emulsion by evapora-
 17 tion, phase separation (coacervation) or spray drying
 19 [9], the latter involving the addition of a third compound
 21 to the polymer solution dissolved in the organic solvent
 23 in order to reduce the solubility of the polymer. While
 25 these methods are relatively effective, the process is
 27 slow. Furthermore, the encapsulation can only be
 29 carried out within the context of laboratory or mass
 31 production settings. Electrospray microencapsulation,
 33 on the other hand, is a powerful technique that could be
 35 parallelized for rapid mass production but can also be
 37 miniaturized to portable devices that encapsulate and
 39 deliver the drug concurrently on demand by medical
 practitioners and patients alike. An encapsulation
 method based on DC electrospraying using co-axial
 liquid jets has been proposed [10]. In this method, DC
 electric fields are employed to extrude a liquid jet of
 aqueous phase containing the material to be encapsu-
 lated. The stresses associated with this liquid jet
 concurrently pull along with it an outer annulus sheath
 of immiscible organic liquid containing a photopoly-
 meric excipient thus producing a co-axial bi-layered jet
 which subsequently breaks up to form a spray of
 compound drops. In order to solidify the photopolymer,
 a beam of UV light is passed through the drops.

41 A major drawback of the DC electrospray-based co-
 43 axial jet method is evident in the need for a complicated
 two needle sheath device design in which the inner
 needle used to electrospray the aqueous liquid contain-
 ing the encapsulation material is housed within an
 annular sheath of organic liquid solvent and polymer
 contained by an outer needle. This is because the direct
 electrospraying of the polymer dissolved in an organic
 solvent, i.e. dielectric liquids which have low ionic
 concentrations and hence surface charge density, is not
 possible since only electrolytes which possess free charge
 can be sprayed using DC electric fields. Moreover, this
 poses a further disadvantage in that the encapsulation
 materials are restricted to substances that are only
 soluble in aqueous phases, which precludes a large array
 of organic soluble drug compounds. In addition, the
 extremely high DC electric fields used pose considerable

concern in the denaturing of biological particles when
 protein/DNA is to be encapsulated.

We have demonstrated the potential of the AC
 electrospray device as a viable and attractive alternative
 to both encapsulation technologies described above. The
 recovered compound microspheres are shown in Fig. 3a.
 Evidence of the encapsulation can be observed in Fig. 3b
 in which the DI water used to create the water-in-oil
 microemulsion was labeled with the uranine fluorescent
 dye; any traces of the aqueous phase dye external to the
 microspheres would have been washed away during the
 rinse. SEM images of the microspheres are shown in Fig.
 3c. A relative monodispersed distribution of drop sizes
 were obtained as shown in Fig. 3d, with population
 mean $\sim 3.7 \mu\text{m}$ and standard deviation $1.9 \mu\text{m}$; the
 characterization method however was not able to
 account for microsphere sizes below $1 \mu\text{m}$ (the SEM
 images in Fig. 3c, and those to be shown subsequently,
 indicate however a rich presence of submicron particles).
 The monodispersity can be controlled by varying system
 parameters such as the applied voltage and frequency.
 Aggregation of the encapsulated drops was observed
 resulting from capillary action as the contact line of
 water receded during evaporation, providing a conven-
 tient method of collecting the drops.

Organic phase soluble therapeutic molecules can also
 be encapsulated with the AC electrospray by dissolving
 the drug with the polymeric excipient in the organic
 solvent and electrospraying directly. Given that the
 ejected drops do not possess net charge, post-ejection
 neutralization procedures are also not required. The AC
 electrospray therefore has the advantage over DC
 electrospraying of not only being simpler in design but
 also provides greater flexibility for the encapsulation of
 organic soluble drug compounds and liposomes [1].

3.2. Fiber synthesis

Conventional indirect fabrication techniques such as
 crystal deposition/polymer precipitation and the use of
 molds have been somewhat successful in producing
 three-dimensional bioscaffold architectures [11]. There
 has also been a parallel effort for synthesizing bioscaf-
 fold prototypes by direct deposition methods such as
 polymer melt spinning [12], pressure assisted microsyring-
 e extrusion [13], fused deposition modeling [14],
 selective laser sintering [15], stereolithography [16] and
 three-dimensional printing [17]. Nevertheless, design
 issues remain in overcoming the limitations of reduced
 or compromised porosity, large scaffold sizes, reproduc-
 ility, extensive effort consumption, cost and scal-
 ability [18].

An attractive direct deposition method is electrospin-
 ning [19–23]. Whilst electrospinning utilizes the same
 principle of electrostatic atomization in DC electro-
 spraying, the spraying of polymeric liquids in electro-

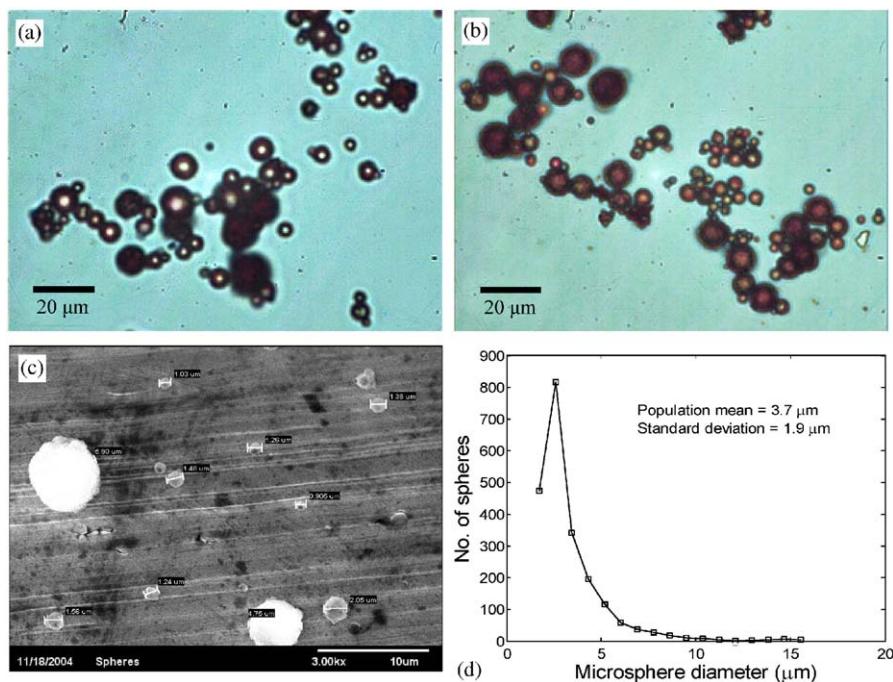


Fig. 3. Microspheres produced by the AC electrospray. (a) DI water encapsulated within microspheres; (b) DI water and uranine dye encapsulated within microspheres; (c) SEM micrograph of 1–10 µm biodegradable microspheres; (d) size distribution of the microspheres. Although the visual method of size characterization in (d) could only account for microspheres above 1 µm, the SEM image in (c) and those shown subsequently indicate that sub-micron particles are present in abundance.

spinning results in the persistence of an elongated jet that would have otherwise broken up into drops due to hydrodynamic instabilities had a monomeric liquid been used [24]. The exposure of the jet to the atmosphere causes the polymer to solidify thus creating a polymeric fiber that can be wound by a rotating ground electrode or deposited as a fibrous mat onto a flat ground electrode plate. DC electrospinning has a significant advantage in its ability to produce 100 nm diameter fibers far smaller than the typical 100 µm structures that can be achieved by the conventional fabrication methods discussed above. These smaller fibers therefore provide a greater surface contact area for the adhesion of cells and for the diffusion of encapsulated dermatological/osteogenic growth factors.

Using AC electrospraying, fibrous mats consisting of a mesh/network of single strand 1 µm diameter fibers as shown in Fig. 4a have been successfully synthesized using polymer concentrations of 0.05 g. At higher polymer concentrations of 0.1 g, a single composite 10 µm fiber, as depicted in Figs. 4b–d, is produced when single micron fiber strands are entangled. There is a high level of controllability of both pore and fiber sizes by varying polymer concentration, field intensity, frequency and spray duration. The AC electrospinning process, however, differs slightly from DC electrospinning in that the solidified fibers are extruded from a partially solidified meniscus due to extensional stresses

and dynamic pressure as opposed to in-flight polymer solidification in DC electrospinning.

The ability to produce smaller fibers and controllable structure sizes using AC and DC electrospinning therefore constitutes an attractive bioscaffold fabrication method over conventional techniques. Moreover, it is easier to encapsulate skin/osteogenic growth factors in the fibers using electrospinning. In addition, the conventional fabrication techniques are not suitable for direct implementation for wound care therapy unlike electrospinning. Indeed, fibers have been directly electrospun in situ onto living tissue and human hands to demonstrate its potential in wound healing [25]. Nevertheless, static discharge occurs during grounding since the DC fibers are charged [22]. Furthermore, the typically large DC voltages used raises safety concerns for general public usage. AC electrospinning thus has the added advantage of lower voltages, safety and potential for portability. Additionally, only a small subset of biodegradable polymers, specifically those that are aqueous or acid soluble such as poly ethylene oxide and collagen, can be spun using DC electrospinning [23,24], thus limiting its utility. However, the trade-off in using AC fields in place of DC fields is that the fiber sizes are limited to 1 µm; nevertheless, this is still considerably smaller than the structures obtained using conventional techniques.

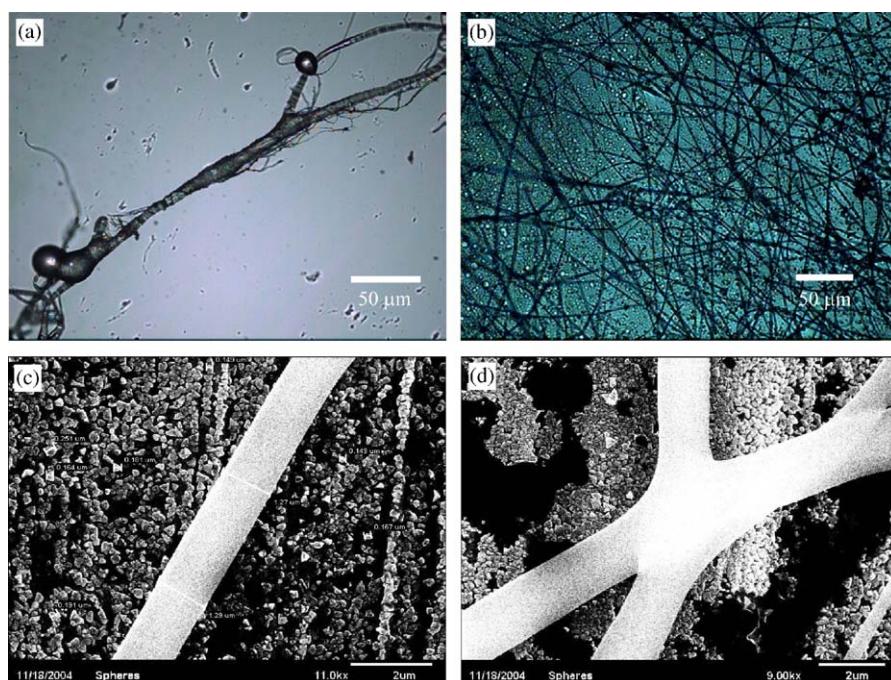


Fig. 4. AC electrospray fiber synthesis. (a) A 10 μm compound fiber. (b) A network of 1 μm single strand fibers produced by the AC electrospray. SEM images of (c) a single-strand fiber, and (d) a network junction of single strand fibers. Both (c) and (d) are magnified from the fiber mesh network in (b). The compound fiber in (a) consists of an entanglement of sub-micron fiber strands. In (c) and (d), the background shows submicron polymer particles similar to those obtained in Fig. 3c, obtained concurrently with the fiber synthesis.

3.3. Polymeric nanoparticles

The SEM images in Figs. 4c and d also reveal a monodispersion of 100 nm crystal-like polymer particles, obtained through the tip streaming mechanism (Fig. 2a) concurrently during AC electrospray fiber synthesis. These nanoparticles, however, are not generated from charged drops as in DC electrosprays. They are also not obtained in DC electrospinning. Their generation therefore represents a significant opportunity for the rapid fabrication of biodegradable polymeric nanoparticles using AC electrospraying, which are currently synthesized by relatively slow and complex methods such as emulsion solvent evaporation/extraction [26], nanoprecipitation or emulsion photo-cross-linking [27]. To stabilize the nanoparticles, large amounts of surfactant/co-surfactant are added, limiting both polymer solid content and polymer application [28].

4. Conclusion

We have demonstrated the capability of the AC electrospray as a viable, safe and attractive alternative for micro/nano-encapsulation, bioscaffold production as well as polymeric nanoparticle fabrication over conventional fabrication techniques as well as DC electrospraying/electrospinning. Whilst conventional

techniques of biomaterials synthesis involve slow and complex processes (e.g. evaporation, phase separation and extraction) and are subject to several limitations as discussed above, AC electrospraying is relatively quick and has the potential to be scaled up for rapid mass production. Efforts are currently underway to fabricate parallel arrays of micro-syringe tips such that the synthesis can be carried out cost effectively on a large production scale. Moreover, the AC electrospray technique also presents an opportunity for direct in-situ administration of the material to the patient, which cannot be achieved with conventional fabrication techniques.

In addition, AC electrospraying also has several advantages over DC electrospraying/electrospinning. Unlike its DC counterpart, the AC electrospray is capable of producing larger micron sized polymeric encapsulation shells, which is within the optimal size range for maximum delivery to the lower respiratory airways [5]. It has also a greater flexibility to encapsulate organic phase soluble therapeutic molecules and drug compounds as well as liposomes. Moreover, the polymer microspheres and fibers that are ejected do not possess net charge and hence eliminates the possibility of surface adsorption or destabilization of the encapsulated material due to electroporation or compound ionization. Furthermore, post-neutralization procedures involving ancillary equipment are not required, thus simplifying the spray design. The absence of charge

also stipulates negligible current through the spray and hence the power requirement is low. As such, the AC electrospray benefits from the potential to be miniaturized to portable devices for direct patient delivery. Perhaps the most important drawback of DC electrospraying, however, is the danger involved in using high voltages. The lower threshold voltages involved and the use of AC electric fields nevertheless renders AC electrospraying inherently safe as a portable device for general public use.

Acknowledgements

The authors thank K. Hidlay and S.-C. Wang for their valuable assistance in the experiments. They also gratefully acknowledge the help of T. Hall in acquiring the SEM images in Figs. 3 and 4.

References

- [1] Chasin M, Langer R, editors. Biodegradable polymers as drug delivery systems. New York: Marcel Dekker; 1990.
- [2] Yeo LY, Lastochkin D, Wang S-C, Chang H-C. A new AC electrospray mechanism by Maxwell–Wagner polarization and capillary resonance. *Phys Rev Lett* 2004;92:133902.
- [3] Chang H-C, Yeo L, Lastochkin D, Wang S-C, Gagnon Z, Maheshwari S. Method and apparatus for AC electrospray, United States Patent Application, 2004 (Patent Pending).
- [4] Brannon-Peppas L, Blanchette JO. Nanoparticle and targeted systems for cancer therapy. *Adv Drug Del Rev* 2004;56:1649–59.
- [5] Ijsebaert JC, Geerse KB, Marijnissen JCM, Lammers J-WJ, Zanen P. Electro-hydrodynamic atomization of drug solutions for inhalation purposes. *J Appl Physiol* 2001;91:2735–41.
- [6] Grace JM, Marijnissen JCM. A review of liquid atomization by electrical means. *J Aerosol Sci* 1994;25:1005–19.
- [7] Clopeau M, Prunet-Foch B. Electrohydrodynamical spraying functioning modes: a critical review. *J Aerosol Sci* 1994;25:1021–36.
- [8] Kenawy E-R, Bowlin GL, Mansfield K, Layman J, Simpson DG, Sanders EH, Wnek GE. Release of tetracycline hydrochloride from electrospun poly(ethylene-*co*-vinylacetate), poly(lactic-acid), and a blend. *J Controlled Release* 2002;81:57–64.
- [9] Jain RA. The manufacturing techniques of various drug loaded biodegradable poly(lactide-*co*-glycolide) (PLGA) devices. *Biomaterials* 2000;21:2475–90.
- [10] Loscertales IG, Barrero A, Guerrero I, Cortijo R, Marquez M, Gañán-Calvo AM. Micro/nano encapsulation via electrified co-axial liquid jets. *Science* 2002;295:1695–8.
- [11] Tsang VL, Bhatia SN. Three-dimensional tissue fabrication. *Adv Drug Del Rev* 2004;56:1635–47.
- [12] Dees JR, Spruiell JE. Structure development during melt spinning of linear polyethylene fibers. *J Appl Polym Sci* 1974;18:1053–78.
- [13] Vozzi G, Previti A, De Rossi D, Ahluwalia A. Fabrication of PLGA scaffolds using soft lithography and microsyringe deposition. *Tissue Eng* 2003;8:2533–40.
- [14] Zein I, Hutmacher DW, Tan KC, Teoh SH. Fused deposition modeling of novel scaffold architectures for tissue engineering applications. *Biomaterials* 2002;23:1169–85.
- [15] Vail NK, Barlow JW, Beaman JJ, Marcus HL, Bourell DL. Development of a poly(methyl methacrylate-*co*-*n*-butyl methacrylate) copolymer binder system. *J Appl Polym Sci* 1994;52:789–812.
- [16] Cooke MN, Fisher JP, Dean D, Rimnac C, Mikos AG. Use of stereolithography to manufacture critical-sized 3D biodegradable scaffolds for bone ingrowth. *J Biomed Mater Res B* 2002;64:65–9.
- [17] Wu BM, Borland SW, Giordano RA, Cima LG, Sachs EM, Cima MJ. Solid free-form fabrication of drug delivery devices. *J Controlled Release* 1996;40:77–87.
- [18] Karp JM, Rzeszutek K, Shiochet MS, Davies JE. Fabrication of precise cylindrical three-dimensional tissue engineering scaffolds for *in vitro* and *in vivo* bone engineering applications. *J Cranofacial Surg* 2003;14:317–23.
- [19] Fong H, Reneker DH. Electrospinning and the formation of nanofibers. In: Salem DR, Sussman MV, editors. *Structure formation in polymeric fibers*. Munich: Hauser; 2000. p. 225–46.
- [20] Huang Z-M, Zhang Y-Z, Kotaki M, Ramakrishna S. A review on polymer nanofibers by electrospinning and their applications in nanocomposites. *Composites Sci Tech* 2003;63:2223–53.
- [21] Frenot A, Chronakis IS. Polymer nanofibers assembled by electrospinning. *Curr Opin Colloid Interface Sci* 2003;8:64–75.
- [22] Doshi J, Reneker DH. Electrospinning process and applications of electrospun fibers. *J Electrostatics* 1995;35:151–60.
- [23] Matthews JA, Wnek GE, Simpson DG, Bowlin GL. Electrospinning of collagen nanofibers. *Biomacromolecules* 2002;3:232–8.
- [24] Deitzel JM, Kleinmeyer J, Harris D, Beck Tan NC. The effect of processing variables on the morphology of electrospun nanofibers and textiles. *Polymer* 2001;42:261–72.
- [25] Kenawy E-R, Layman JM, Watkins JR, Bowlin GL, Matthews JA, Simpson DG, Wnek GE. Electrospinning of poly(ethylene-*co*-vinyl alcohol) fibers. *Biomaterials* 2003;24:907–13.
- [26] Mu L, Feng SS. A novel controlled release formulation for the anticancer drug paclitaxel (Taxol®): PLGA nanoparticles containing vitamin E TPGS. *J Controlled Release* 2002;80:33–48.
- [27] Craparo EF, Cavallaro G, Bondi ML, Giammona G. Preparation of polymeric nanoparticles by photo-crosslinking of an acryloylated polyaspartamide in w/o microemulsion. *Macromol Chem Phys* 2004;205:1955–64.
- [28] Zhang G, Niu A, Peng S, Jiang M, Tu Y, Li M, Wu C. Formation of novel polymeric nanoparticles. *Acc Chem Res* 2001;34:249–56.