

电子学基础——第八次作业

LXQ

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6.38 Construct the small-signal model of the circuits depicted in Fig. 6-50. Assume all transistors operate in saturation and $\lambda \neq 0$

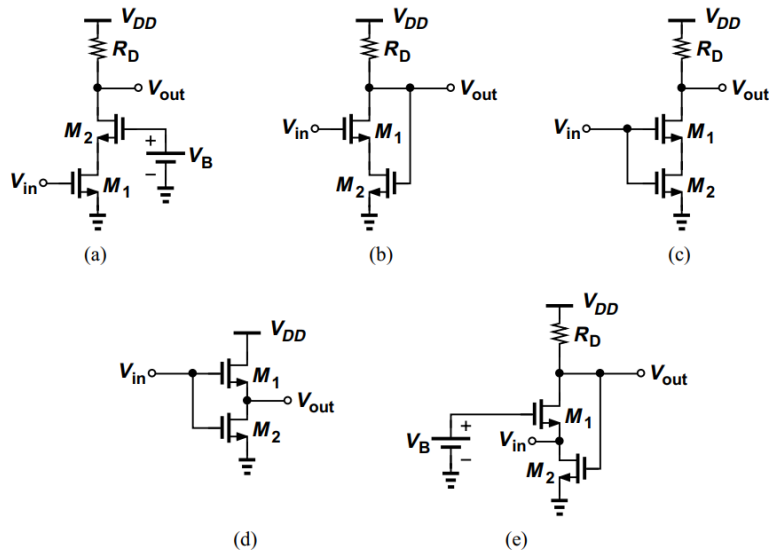


Figure 6-50

解 如图 p6-38 所示。

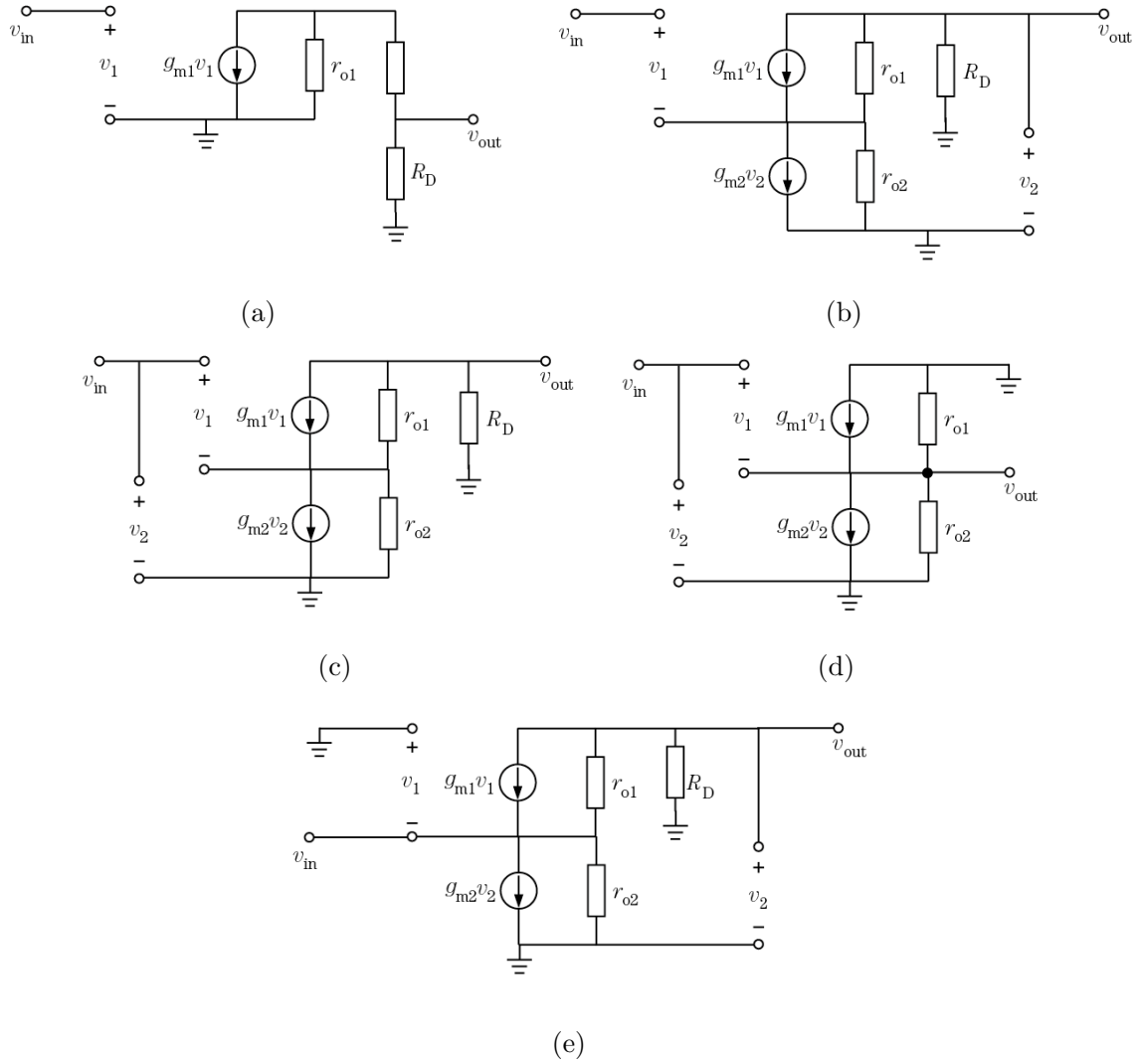


Figure p6-38

6.46 Consider the circuit depicted in Fig. 6-57, where M_1 and M_2 operate in saturation and exhibit channel-length modulation coefficients λ_n and λ_p , respectively.

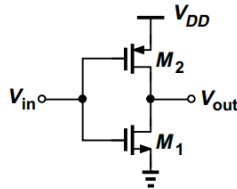


Figure 6-57

- (a) Construct the small-signal equivalent circuit and explain why M_1 and M_2 appear in "parallel."
 (b) Determine the small-signal voltage gain of the circuit.

解 (a) 小信号电路图如图 p6-46 所示。由于两个 MOSFET 管的 D 端即 v_{out} ，而 S 端接地，从而在小信号电路中表现为并联。

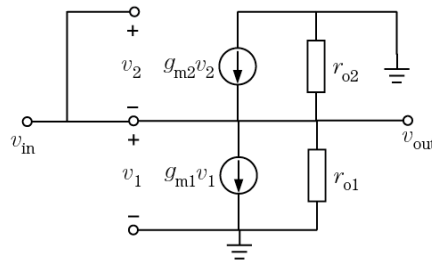


Figure p6-46

(b) 可列得以下方程

$$\begin{cases} \frac{v_{out}}{r_{o1}} + \frac{v_{out}}{r_{o2}} = g_{m2}v_2 + g_{m2}v_1 \\ v_2 = v_{in} - v_{out} \\ v_1 = v_{in} \end{cases}$$

$$\therefore A_v = \frac{v_{out}}{v_{in}} = \frac{g_{m1} + g_{m2}}{\frac{1}{r_{o1}} + \frac{1}{r_{o2}} + g_{m2}}$$

7.28 If $\lambda \neq 0$, determine the voltage gain of the stages shown in Fig. 7-60.

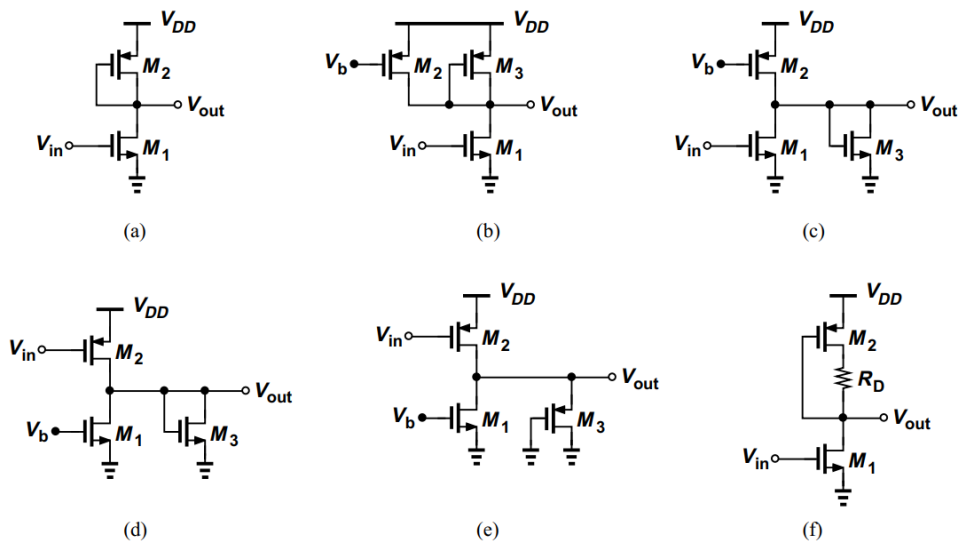


Figure 7-60

解 (a) M_2 为二极管接法，可看作电阻 $\frac{1}{g_{m2}} // r_{o2}$ ，则 M_1 为共源放大器，

$$A_v = -g_{m1}(r_{o1} // r_{o2} // \frac{1}{g_{m2}})$$

(b) M_2 可视为 r_{o2} , M_3 为二极管接法, 可视为 $\frac{1}{g_{m3}} // r_{o3}$, 则 M_1 为共源接法,

$$A_v = -g_{m1}(r_{o1} // r_{o2} // r_{o3} // \frac{1}{g_{m3}})$$

(c) M_2 可视为 r_{o2} , M_3 为二极管接法, 可视为 $\frac{1}{g_{m3}} // r_{o3}$, 则 M_1 为共源接法,

$$A_v = -g_{m1}(r_{o1} // r_{o2} // r_{o3} // \frac{1}{g_{m3}})$$

(d) M_1 可视为 r_{o1} , M_3 可视为 $\frac{1}{g_{m3}} // r_{o3}$, M_2 为共源接法,

$$A_v = -g_{m2}(r_{o2} // r_{o1} // r_{o3} // \frac{1}{g_{m3}})$$

(e) M_1 可视为 r_{o1} , M_3 D,G 端接地, 是为二极管接法, 可视为 $\frac{1}{g_{m3}} // r_{o3}$, M_2 为共源放大器,

$$A_v = -g_{m2}(r_{o2} // r_{o1} // r_{o3} // \frac{1}{g_{m3}})$$

(f) 首先考察从 M_1 的漏端向上看的输出电阻, 其小信号电路如图 p7-28-f 所示。可设输入信号为 v , 产生 i 的电流。

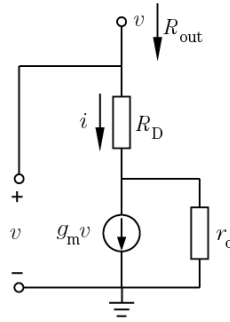


Figure p7-28-f

则

$$iR_D + (i - vg_m)r_o = v$$

$$\therefore R_{out} = \frac{v}{i} = \frac{R_D + r_o}{1 + g_m r_o}$$

从而 M_2 等效为 $r_2 = \frac{v}{i} = \frac{R_D + r_o}{1 + g_m r_o}$, M_1 为共源接法, 则

$$A_v = -g_{m1}(r_{o1} // r_2) = -g_{m1}(r_{o1} // \frac{R_D + r_o}{1 + g_m r_o})$$

7.46 Consider the circuit of Fig. 7-73, where a common-source stage (M_1 and R_{D1}) is followed by a common-gate stage (M_2 and M_{D2}).

(a) Writing $v_{out}/v_{in} = (v_X/v_{in})(v_{out}/v_X)$ and assuming $\lambda = 0$, compute the overall voltage gain.

(b) Simplify the result obtained in (a) if $R_{D1} \rightarrow \infty$. Explain why this result is to be expected.

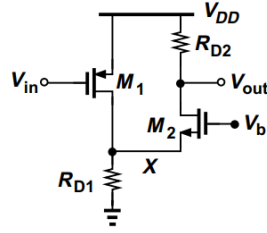


Figure 7-73

解 (a) M_1 放大器为共源放大器，负载 $R_1 = R_{D1} // \frac{1}{g_{m2}}$ 则

$$\frac{v_x}{v_{in}} = -g_{m1}(R_{D1} // \frac{1}{g_{m2}})$$

而 M_2 为共栅放大器，则

$$\frac{v_{out}}{v_x} = g_{m2}R_{D2}$$

从而 $\frac{v_{out}}{v_{in}} = -g_{m1}g_{m2}R_{D2}(R_{D1} // \frac{1}{g_{m2}})$
(b)

$$R_{D1} \rightarrow \infty, \frac{v_{out}}{v_{in}} \rightarrow -g_{m1}R_{D2}$$

$R_{D1} \rightarrow \infty$ 时，原电路中可视 R_{D1} 为断路，而 M_2 共栅，可视为导线，则原电路简化为仅有 M_1 作为共源放大器负载 R_{D2} 的电路，则 $A_v = -g_{m1}R_{D2}$ 。

7.47 Assuming $\lambda = 0$, calculate the voltage gain of the circuit shown in Fig. 7-74. Explain why this stage is *not* a common-gate amplifier.

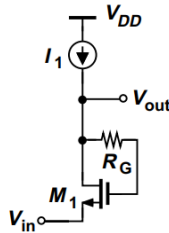


Figure 7-74

解 小信号电路如图 p7-47 所示

$$\begin{cases} v_{in} + v_1 = v_{out} \\ g_m v_1 = 0 \end{cases}$$

$$\therefore v_{in} = v_{out}, A_v = 1$$

该电路不是共栅放大器的原因是栅端和漏端并非直接相连而是通过电阻。

7.55 Determine the voltage gain of the stages shown in Fig. 7-80. Assume $\lambda \neq 0$.

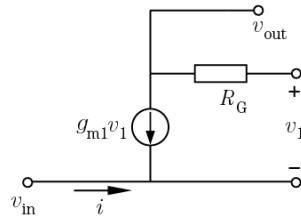


Figure p7-47

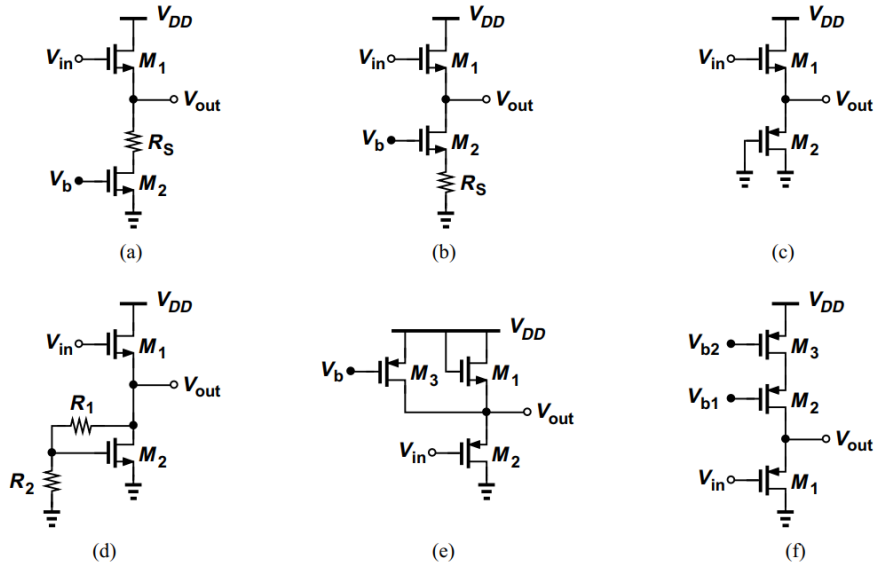


Figure 7-80

解 (a) M_2 可视为 r_{o2} , M_1 为源极跟随器, 则

$$A_v = \frac{g_{m1}[r_{o1} // (R_S + r_{o2})]}{1 + g_{m1}[r_{o1} // (R_S + r_{o2})]}$$

(b) M_2 与 R_S 构成源简并放大器, 可等效为 $(1 + g_{m2}r_{o2})R_S + r_{o2}$, M_1 为源极跟随器, 则

$$A_v = \frac{g_{m1}[r_{o1} // ((1 + g_{m2}r_{o2})R_S + r_{o2})]}{1 + g_{m1}[r_{o1} // ((1 + g_{m2}r_{o2})R_S + r_{o2})]}$$

(c) M_2 为二极管接法, 等效于 $\frac{1}{g_{m2}} // r_{o2}$, M_1 为源极跟随器, 则

$$A_v = \frac{g_{m1}(r_{o1} // \frac{1}{g_{m2}} // r_{o2})}{1 + g_{m1}(r_{o1} // \frac{1}{g_{m2}} // r_{o2})}$$

(d) 可先求 v_{out} 以下部分的等效电阻 r_{out} , 小信号电路如图 p7-55-d 所示。

$$\begin{cases} v = [i_1 - g_m(v - (i - i_1)R_1)]r_o \\ v = (i - i_1)(R_1 + R_2) \end{cases}$$

$$\therefore r_{out} = \frac{v}{i} = \frac{r_o(R_1 + R_2)}{R_1 + R_2 + r_o + g_m r_o R_2}$$

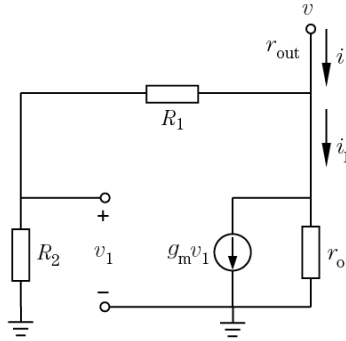


Figure 1

而 M_1 为源极跟随器，从而

$$A_v = \frac{g_{m1}(r_{o1} // \frac{r_{o2}(R_1+R_2)}{R_1+R_2+r_{o2}+g_{m2}r_{o2}R_2})}{1 + g_{m1}(r_{o1} // \frac{r_{o2}(R_1+R_2)}{R_1+R_2+r_{o2}+g_{m2}r_{o2}R_2})}$$

(e) M_3 可视作 r_{o3} ， M_1 可视作 $\frac{1}{g_{m1}} // r_{o1}$ ， M_2 为源极跟随器，则

$$A_v = \frac{g_{m2}(r_{o2} // r_{o1} // r_{o3} // \frac{1}{g_{m1}})}{1 + g_{m2}(r_{o2} // r_{o1} // r_{o3} // \frac{1}{g_{m1}})}$$

(f) M_2, M_3 可视为电阻 $r = (1 + g_{m2}r_{o2})r_{o3} + r_{o2}$ ，而 M_1 为源极跟随器，则

$$A_v = \frac{g_{m1}[r_{o1} // ((1 + g_{m2}r_{o2})r_{o3} + r_{o2})]}{1 + g_{m1}[r_{o1} // ((1 + g_{m2}r_{o2})r_{o3} + r_{o2})]}$$

7.56 Consider the circuit of Fig. 7-81, where a source follower (M_1 and I_1) precedes a common-gate stage (M_2 and M_D).

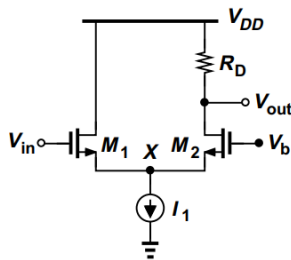


Figure 7-81

(a) Writing $v_{out}/v_{in} = (v_X/v_{in})(v_{out}/v_X)$, compute the overall voltage gain.

(b) Simplify the result obtained in (a) if $g_{m1} = g_{m2}$.

解 (a) M_1 为源极跟随器， $R_L = R_{2in} = \frac{1}{g_{m2}}$

$$\therefore \frac{v_x}{v_{in}} = \frac{g_{m1} \cdot \frac{1}{g_{m2}}}{1 + g_{m1} \cdot \frac{1}{g_{m2}}} = \frac{g_{m1}}{g_{m1} + g_{m2}}$$

M_2 为共栅放大器，则

$$\frac{v_{out}}{v_x} = g_{m2}R_D$$

$$\therefore \frac{v_{out}}{v_{in}} = \frac{g_{m1}g_{m2}R_D}{g_{m1} + g_{m2}}$$

(b) $g_{m1} = g_{m2} = g_m$ 时

$$\frac{v_{out}}{v_{in}} = \frac{g_m R_D}{2}$$

9.19 Determine the output impedance of the stages shown in Fig. 9-52. Assume all of the transistors operate in saturation and $g_m r_{o1} \gg 1$.

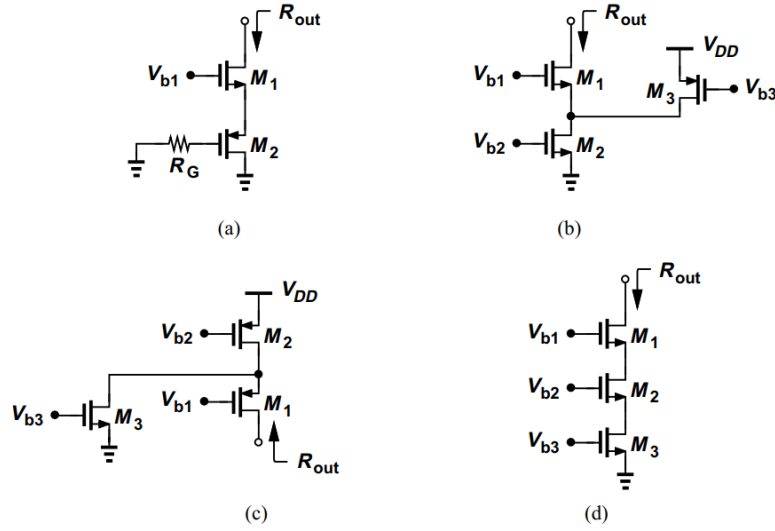


Figure 9-52

解 (a) R_G 上无电流，则 M_2 为二极管接法，可视为 $r = \frac{1}{g_{m2}} // r_{o2}$ ，而 M_1 为源简并放大器，则

$$r_{out} = (1 + g_{m1}r_{o1})\left(\frac{1}{g_{m2}} // r_{o2}\right) + r_{o1} \approx r_{o1}\left(\frac{g_m}{g_{m2}} + 1\right)$$

(b) M_2, M_3 均共源，则可分别视为 r_{o2}, r_{o3} ，而 M_1 为源简并放大器，则

$$r_{out} = (1 + g_{m1}r_{o1})(r_{o2} // r_{o3}) + r_{o1} \approx g_{m1}r_{o1}(r_{o2} // r_{o3}) + r_{o1}$$

(c) M_2, M_3 均共源，则可分别视为 r_{o2}, r_{o3} ，而 M_1 为源简并放大器，则

$$r_{out} = (1 + g_{m1}r_{o1})(r_{o2} // r_{o3}) + r_{o1} \approx g_{m1}r_{o1}(r_{o2} // r_{o3}) + r_{o1}$$

(d) M_3 共源，可视为 r_{o3} ， M_2 为源简并放大器，可视为

$$r_2 = (1 + g_{m2}r_{o2})r_{o3} + r_{o2} \approx g_{m2}r_{o2}r_{o3}$$

M_1 亦为源简并放大器，则

$$r_{out} = (1 + g_{m1}r_{o1})g_{m2}r_{o2}r_{o3} + r_{o1} \approx g_{m1}g_{m2}r_{o1}r_{o2}r_{o3}$$

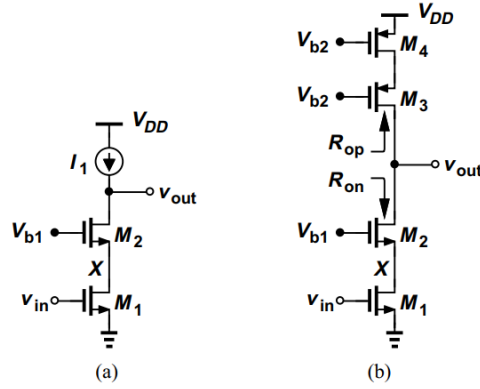


Figure 9-20

9.32 In the cascode stage of Fig. 9-20(b), $(W/L)_1 = \dots = (W/L)_4 = 20/0.18$. If $\mu_n C_{ox} = 100 \mu\text{A}/\text{V}^2$, and $\mu_p C_{ox} = 50 \mu\text{A}/\text{V}^2$, $\lambda_n = 0.1 \text{V}^{-1}$, and $\lambda_p = 0.15 \text{V}^{-1}$, calculate the bias current such that the circuit achieves a voltage gain of 500.

解

$$\begin{aligned}
 g_{m1} &= g_{m2} = \sqrt{2\mu_n C_{ox} (W/L) I_D} = 149\sqrt{I_D} \\
 g_{m3} &= g_{m4} = \sqrt{2\mu_p C_{ox} (W/L) I_D} = 105\sqrt{I_D} \\
 r_{o1} &= r_{o2} = \frac{1}{\lambda_n I_D} = \frac{10}{I_D} \\
 r_{o3} &= r_{o4} = \frac{1}{\lambda_p I_D} = \frac{6.67}{I_D} \\
 A_v &\approx -g_{m1}(((1 + g_{m3}r_{o3})r_{o4} + r_{o3})/((1 + g_{m2}r_{o2})r_{o1} + r_{o2})) \\
 &\approx -g_{m1}[(g_{m3}r_{o3}r_{o4})/(g_{m2}r_{o2}r_{o1})] \\
 &= -531400/I_D
 \end{aligned}$$

上式中 I_D 以 μA 为单位。

欲使增益达到 500, 则 $I_D = 1.06 \text{mA}$ 。

9.34 Determine the voltage gain of each circuit in Fig. 9-59. Assume $g_m r_O \gg 1$.

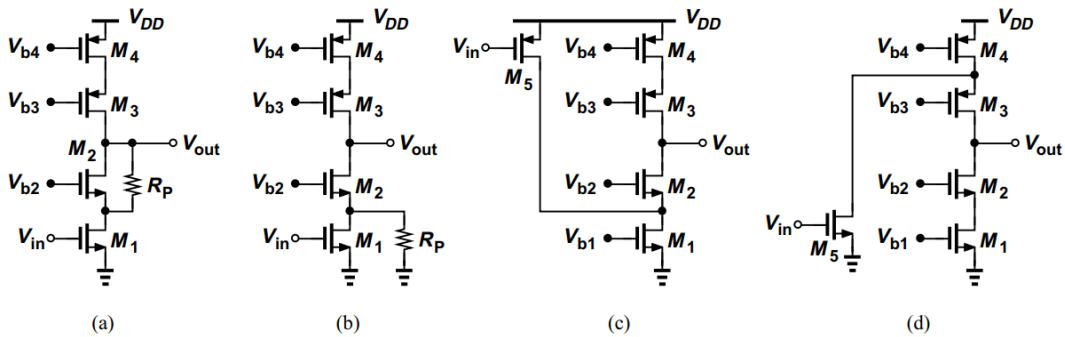


Figure 9-59

解 (a)

$$G_m = g_{m1} \cdot \frac{r_{o1}}{r_{o1} + \frac{1}{\frac{1}{g_{m2}} // r_{o2} // R_P}} \approx \frac{g_{m1} r_{o1}}{r_{o1} + \frac{1}{g_{m2}} // R_P}$$

$$R_{out} = [(1 + g_{m3})r_{o4} + r_{o3}] / [(1 + g_{m2}(r_{o2} // R_P))r_{o1} + r_{o2} // R_P] \approx [g_{m3}r_{o3}r_{o4}] / [g_{m2}r_{o1}(r_{o2} // R_P)]$$

$$A_v = -G_m R_{out} = -\frac{g_{m1} r_{o1}}{r_{o1} + \frac{1}{g_{m2}} // R_P} \cdot [(g_{m3}r_{o3}r_{o4}) / (g_{m2}r_{o1}(r_{o2} // R_P))]$$

(b)

$$G_m = g_{m1} \cdot \frac{r_{o1} // R_P}{r_{o1} // R_P + \frac{1}{\frac{1}{g_{m2}} // r_{o2}}} \approx g_{m1}$$

$$R_{out} = [(1 + g_{m3})r_{o4} + r_{o3}] / [(1 + g_{m2}r_{o2})(r_{o1} // R_P) + r_{o2}] \approx [g_{m3}r_{o3}r_{o4}] / [g_{m2}r_{o2}(r_{o1} // R_P)]$$

$$A_v = -G_m R_{out} = -g_{m1} [(g_{m3}r_{o3}r_{o4}) / (g_{m2}r_{o2}(r_{o1} // R_P))]$$

(c) 设 M_5 漏端电压为 v_x

$$\begin{aligned} \frac{v_x}{v_{in}} &= -g_{m5}(r_{o5} // r_{out1} // r_{in2}) \\ &= -g_{m5}(r_{o5} // r_{o1} // \frac{1}{g_{m2}} // r_{o2}) \\ &\approx -g_{m5}(r_{o1} // r_{o5} // \frac{1}{g_{m2}}) \end{aligned}$$

对于从 v_x 到 v_{out} 的放大器

$$G_m = \frac{1}{r_{in2}} \approx g_{m2}$$

$$R_{out} = [(1 + g_{m3})r_{o4} + r_{o3}] / [(1 + g_{m2}r_{o2})(r_{o1} // r_{o5}) + r_{o2}] \approx [g_{m3}r_{o3}r_{o4}] / [g_{m2}r_{o2}(r_{o1} // r_{o5})]$$

$$\therefore \frac{v_{out}}{v_x} = -g_{m1} [(g_{m3}r_{o3}r_{o4}) / (g_{m2}r_{o2}(r_{o1} // r_{o5}))]$$

$$\therefore \frac{v_{out}}{v_{in}} = g_{m1}g_{m5}(r_{o1} // r_{o5} // \frac{1}{g_{m2}}) [(g_{m3}r_{o3}r_{o4}) / (g_{m2}r_{o2}(r_{o1} // r_{o5}))]$$

(d) 设 M_5 漏端电压为 v_x

$$\begin{aligned} \frac{v_x}{v_{in}} &= -g_{m5}(r_{o5} // r_{out4} // r_{in3}) \\ &= -g_{m5}(r_{o5} // r_{o4} // \frac{1}{g_{m3}} // r_{o3}) \\ &\approx -g_{m5}(r_{o4} // r_{o5} // \frac{1}{g_{m3}}) \end{aligned}$$

对于从 v_x 到 v_{out} 的放大器

$$G_m = \frac{1}{r_{in3}} \approx g_{m3}$$

$$R_{out} \approx [g_{m2}r_{o2}r_{o1}]/[g_{m3}r_{o3}(r_{o4}/r_{o5})]$$

$$\therefore \frac{v_{out}}{v_x} = -g_{m3}[(g_{m2}r_{o2}r_{o1})/(g_{m3}r_{o3}(r_{o4}/r_{o5}))]$$

$$\therefore \frac{v_{out}}{v_{in}} = g_{m3}g_{m5}(r_{o4}/r_{o5}/\frac{1}{g_{m3}})[(g_{m2}r_{o2}r_{o1})/(g_{m3}r_{o3}(r_{o4}/r_{o5}))]$$