# Metacontrol: a Python based software for self-optimizing control strucutre selection using metamodels

Campina Grande, Paraíba, Brasil Março, 2020

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Dissertação apresentada ao Programa de Pós-Graduação em Engenharia Química da Universidade Federal de Campina Grande, como requisito parcial para obtenção do grau de Mestre. Área de concentração: Engenharia Química.

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Unidade Acadêmica de Engenharia Química
Programa de Pós-Graduação em Engenharia Química

Supervisor: Dr. Antônio Carlos Brandão de Araújo

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http://www.cpai.unb.br/

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## **Abstract**

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## List of abbreviations and acronyms

CPU Compression Purification Unit

CV Controlled Variable

DOE Design Of Experiments

DOF Degree of Freedom

IEAGHG International Agency Greenhouse Gas

LHS Latin Hypercube Sampling

MV Manipulated Variable

NLP Non Linear Problem

RTO Real Time Optimization

SOC Self-Optimizing Control

#### List of symbols

#### Chapter 2

Controlled variable dProcess disturbances FOptimal measurement sensitivity matrix with respect to the disturbances  $G^y$ Gain matrix with respect to the measurements  $G_d^y$ Gain matrix with respect to the disturbances HLinear combination matrix JProcess objective function  $J_{opt}$ Optimal value of JHessian of cost function with respect to the disturbance variables  $\left(\frac{\partial^2 J}{\partial u \partial d}\right)$  $J_{ud}$ Hessian of cost function with respect to the manipulated variables  $\left(\frac{\partial^2 J}{\partial^2 u}\right)$  $J_{uu}$ LLoss Implementation error  $n^{y'}$ Implementation error with respect to the measurements Manipulated variable uProcess degrees of freedom  $u_0$  $W_d$ Diagonal magnitude matrix of disturbances  $W_n$ Diagonal magnitude matrix of measurement errors Process states Measurements Loss variable

#### Chapter 3

- $\hat{y}$  Metamodel (approximation) of y
- $\mathcal{F}, f(x)$  Polynomial regression function
- $\sigma_l^2$  Process variance

- $\theta$  Kriging hyperparameter of variable activity
- $\varepsilon$  Residuals or random noise
- p Kriging hyperparameter of correlation smoothness
- x Input of a process, or sample
- y Function that calculates the output of a process
- z Stochastic departure function

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#### 1 Introduction

This dissertation is about an assembly of several methodologies into a software tool, called *Metacontrol*, which enables a fast implementation of the Self-Optimizing Control (SOC) technique. This assembly consist of three major methodologies: *Kriging* metamodels, optimization through infill criteria and SOC. The dissertation is organized as follows:

Chapter 2 gives a brief summary of the key concepts involving SOC methodology and the main the reason why this research and software tool development was needed.

Chapter 3 presents a discussion of *Kriging* metamodels and its reasoning.

Chapter 4 introduces the process of constrained nonlinear optimization using Kriging metamodels. This process is also known as infill criteria.

Chapter 5 demonstrates how the assembly of the methodologies shown in chapters 2, 3 and 4 are combined to form the core concept behind *Metacontrol*.

Chapter 6 is dedicated to case-studies using *Metacontrol*. In addition, there is a brief discussion on good practices involving the use of the software tool.

The *Metacontrol* software is publicly available at https://github.com/feslima/metacontrol. There, the reader can find instructions on how to install the open-source tool. Also, for each technique discussed in chapters 2, 3 and 4, there is an open-source Python package as result. Their links are found in their respective chapters.

## 2 The Self-Optimizing Control overview

Every industrial process is under limitations ranging from design/safety (e.g. temperature or pressure which an equipment can operate, etc.), environmental (e.g. pollutant emissions), to quality specifications (e.g. product purity), and economic viability. More often than not, these constraints are applied all at once and can be conflicting. Therefore, it is mandatory to operate such processes optimally (or, at least, close to its optimal point) in order to attain maximum profits or keep expenses at minimum while still obeying these specifications.

One way to achieve this is through the application of plantwide control methodologies. In particular, Self-Optimizing Control (MORARI; STEPHANOPOULOS, 1980; SKOGESTAD, 2000; ALSTAD; SKOGESTAD; HORI, 2009) is a practical way to design a control structure of a process following a criterion (for instance: economic, environmental, performance) considering a constant set-point policy (ALVES et al., 2018). The SOC methodology is advantageous in this scenario because there is no need to reoptimize the process every time that a disturbance occurs.

However, the review presented here contains merely the paramount elements needed to understand the main concepts and expressions that translate the ideas behind the method. The author recommends them if the reader needs a more detailed explanation (SKOGESTAD, 2000; HALVORSEN et al., 2003; HORI; SKOGESTAD; ALSTAD, 2005; HORI, Eduardo S.; SKOGESTAD, 2007; ALSTAD; SKOGESTAD; HORI, 2009; ALVES et al., 2018; KARIWALA; CAO; JANARDHANAN, 2008; KARIWALA; CAO, 2009; UMAR et al., 2012).

The main concept of Self-optimizing control consists in the pursue of a control structure that is based on a constant setpoint policy, leading to near-optimal operation. From Skogestad (2004):

"Self-optimizing control is when one can achieve an acceptable loss with constant setpoint values for the controlled variables without the need to reoptimize when disturbances occur."

It is assumed the process objective function, assumed scalar, is influenced by its steady-state operation. Therefore, the optimization problem described in Equation 2.1 is formed, with  $u_0$  being the degrees of freedom available, x and d representing the states

and the disturbances of the system, respectively.

minimize 
$$J_0(x, u_0, d)$$
  
subject to  $g_1(x, u_0, d) = 0$   
 $g_2(x, u_0, d) \le 0$  (2.1)

Regarding the disturbances, these can be: change in feed conditions, prices of the products and raw materials, specifications (constraints) and/or changes in the model. Using NLP solvers, the objective function can be optimized considering the expected disturbances and implementation errors.

Since the whole technology considers near-optimal operation, as a result of keeping constant setpoints (differently from RTO, for instance), there will always exist a (positive) loss, given by Equation 2.2

$$L = J_0(d, n) - J_{opt}(d) (2.2)$$

Metacontrol focus on the first four steps of the Self-Optimizing Control technology, named by Skogestad (2000) as "top-down" analysis. In these steps, the variable selection seeking the usage of the steady-state degrees of freedom is the main problem to be addressed with the systematic procedure proposed. It is possible to search for a Self-Optimizing Control structure basically using two methods:

- 1. Manually testing each CV candidate, reoptimizing the process for different disturbances' scenarios, and choosing the strucutre that yields the lowest (worst-case or average-case) loss;
- 2. Using local methods based on second-order Taylor series expansion of the objective function, that are capable of easily and quickly "pre-screening" the most promising CV candidates.

The manual nature of method 1 and the possibility of creating an automated framework using method 2 motivated the creation of *Metacontrol* itself. Applying, comprehensively, the second method in a software was also a key motivation for this work. Therefore, it is logical that the usage of the linear methods will be discussed in this section, since they are the ones implemented within *Metacontrol*.

A linear model with respect to the plant measurements can be represented as Equation 2.3

$$\Delta y = G^y \Delta u + G_d^y \Delta d \tag{2.3}$$

With

$$\Delta y = y - y^*$$

$$\Delta u = u - u^*$$

$$\Delta d = d - d^*$$
(2.4)

 $G^y$  and  $G_d^y$  are the gain matrices with respect to the measurements and disturbances, respectively. Regarding the CVs, linearization will give Equation 2.5

$$\Delta c = H\Delta y = G\Delta u + G_d\Delta d \tag{2.5}$$

With

$$G = HG^y$$

$$G_d = HG_d^y$$
(2.6)

Linearizing the loss function results in Equation 2.7:

$$L = J(u,d) - J_{opt}(d) = \frac{1}{2} ||z||_{2}^{2}$$

$$z = J_{uu}^{\frac{1}{2}} (u - u_{opt}) = J_{uu}^{\frac{1}{2}} G^{-1} (c - c_{opt})$$
(2.7)

Later, Halvorsen et al. (2003) developing the exact local method, showed that the loss function can be rewritten as in Equation 2.8

$$z = J_{uu}^{\frac{1}{2}} \left[ \left( J_{uu}^{-1} J_{ud} - G^{-1} G_d \right) \Delta d + G^{-1} n \right]$$
 (2.8)

With  $J_{ud}$  and  $J_{uu}$  corresponding to the hessian with respect to the disturbances and manipulated variables  $\left(\frac{\partial^2 J}{\partial u \partial d}\right)$  and with respect to the manipulated variables  $\left(\frac{\partial^2 J}{\partial^2 u}\right)$ , respectively. If one assumes that  $W_d$  is a (diagonal) magnitude matrix that considers the disturbances and  $W_n^y$  the magnitude matrix that takes into account the measurement error, and considering that both are 2-norm-bounded (Halvorsen et al. (2003) and Alstad,

Skogestad, and Hori (2009) contains a discussion and justification for using 2-norm), Equations 2.9 to 2.11 can be defined to scale the system:

$$d - d^* = W_d d' \tag{2.9}$$

$$n = HW_n^y n^{y'} = W_n n^{y'} (2.10)$$

$$\left\| \left( \begin{array}{c} d' \\ n^{y'} \end{array} \right) \right\|_{2} \le 1 \tag{2.11}$$

The loss function from Equation 2.7 can be also written in a more appropriate way considering the definition of (ALSTAD; SKOGESTAD; HORI, 2009) of the uncertainty variables regarding the contribution of the disturbances and measurement error on the incurred loss, Equation 2.12 and considering the scaled system from Equations 2.9 to 2.11

$$M \triangleq [M_d \quad M_n^y] \tag{2.12}$$

where

$$M_d = -J_{uu}^{1/2} (HG^y)^{-1} HFW_d$$

$$M_{ny} = -J_{uu}^{1/2} (HG^y)^{-1} HW_{nv}$$
(2.13)

with F corresponding to the optimal measurement sensitivity matrix with respect to the disturbances.

Finally, if one uses all the definitions described so far, the worst-case loss for the effect of the disturbances and measurement error is given by Equation 2.14

$$L_{worst-case} = \max_{\left\| \begin{pmatrix} d' \\ n^{y'} \end{pmatrix} \right\|_{2} \le 1} = \frac{\bar{\sigma}(M)^{2}}{2}$$

$$(2.14)$$

Equation 2.14 shows that in order to minimize the worst-case loss, it is necessary to minimize  $\bar{\sigma}(M)$ , Equation 2.15:

$$H = \arg\min_{H} \bar{\sigma}(M) \tag{2.15}$$

This optimization problem was initially solved using a numerical search, as proposed by Halvorsen et al. (2003). Fortunately, Alstad, Skogestad, and Hori (2009) derived an explicit solution that gives the optimal linear combination of measurements coefficient matrix (H) that minimize the worst-case loss that exists due to the effect of the disturbances and measurement errors, in Equation 2.16

$$H^{T} = (\tilde{F}\tilde{F}^{T})^{-1} G^{y} \left( G^{yT} \left( \tilde{F}\tilde{F}^{T} \right)^{-1} G^{y} \right)^{-1} J_{uu}^{1/2}$$
 (2.16)

where

$$\tilde{F} = [FW_dW_n^y] \tag{2.17}$$

Assuming that  $\tilde{F}\tilde{F}^T$  is full rank.

Equation 2.16 has three interesting properties proved by Alstad, Skogestad, and Hori (2009):

- 1. It applies to any number of measurements  $(n_y)$ .
- 2. The solution for H was proved to minimize not only the worst-case, but also the average-case loss. Therefore, if one uses Equation 2.16 seeking the determination of a control structure that minimizes the loss at the worst-case scenario, he is also minimizing the loss for the average-case scenario. This was called as a "super-optimality" by Alstad, Skogestad, and Hori (2009).
- 3. The solution proposed minimizes the *combined* effect of the disturbances and the measurement errors, simultaneously.

Therefore, the usage of the explicit solution will give both the minimized worst and average case losses using a single evaluation, and will also consider the combined effect of the disturbances and measurement errors of the problem. Therefore, this solution it is the default one used in *Metacontrol*.

Another way of solving the optimization problem from Equation 2.15 is to use the Extended nullspace method (ALSTAD; SKOGESTAD; HORI, 2009). Differently from Equation 2.16, this solution does not consider the combined effect of the disturbances and measurement errors simultaneously. Instead, the problem is solved in two steps. The first regards "disturbance rejection": The loss is minimized with respect to disturbances. If there are remaining degrees of freedom, then the effect of the measurement errors can be minimized. The extended nullspace, differently from the exact local method, is not an optimal solution, instead being considered sub-optimal. (ALSTAD; SKOGESTAD, 2007; ALSTAD; SKOGESTAD; HORI, 2009). However, the authors of Alves et al. (2018) also

translated the mathematical formulations of the extended nullspace method into Python, and it is intended to be implemented within *Metacontrol* GUI in future releases merely as a secondary feature, giving its sub-optimality. The solution using the extended nullspace method is depicted in Equation 2.18:

$$H = M_n^{-1} \tilde{J} \left( W_{n^y}^{-1} \tilde{G}^y \right)^{\dagger} W_{n^y}^{-1}$$
 (2.18)

Since Equation 2.16 also minimizes the worst-case loss, its evaluation was also considered inside *Metacontrol*: the user can inspect the expected average-case loss for each control structure that can exist in the combinatorial problem. The expression for the average-case loss is a result of the work of Kariwala, Cao, and Janardhanan (2008) and is described in Equation 2.19:

$$L_{\text{average}} = \frac{1}{6(n_y + n_d)} \left\| J_{uu}^{\frac{1}{2}} (HG^y)^{-1} H \tilde{F} \right\|_F^2$$
 (2.19)

Lastly, it was necessary to implement within *Metacontrol* a branch-and-bound algorithm capable of quickly searching the best control structures for each possible subset of a given process, using the incurred loss as metric. This was considered by the authors of Alves et al. (2018) as an obligatory feature, since when *Metacontrol* is being used, it was understood that the main idea was to, in a comprehensive software, the user operating it should be capable of inspecting the most promising control structures, and discarding the unnecessary evaluation of the unpromising structures (i.e.: With a high incurred loss both average of worst-case scenario) to save time and effort. It is important to remember that there is an evident combinatorial problem that grows in an explosive fashion, as the number of the unconstrained degrees of freedom of the reduced space problem and the number of available measurements both increases. Without a search method that is capable of quickly discarding undesired solutions, the usability of *Metacontrol* would be seriously compromised. Luckily, there are several implementations of branch-and-bound algorithms tailored for Self-Optimizing Control studies purposes, such as in Cao and Saha (2005), Cao and Kariwala (2008) and Kariwala and Cao (2009).

From the aforementioned works, Kariwala and Cao (2009) it is of particular interest: the monotonic criterion implemented consists of the exact local method from Halvorsen et al. (2003) and derived explicitly by Alstad, Skogestad, and Hori (2009), which is used as the default methodology to pre-screen the most promising self-optimizing CV candidates in *Metacontrol*. Therefore, the usage of the proposed branch-and-bound algorithm by Kariwala and Cao (2009) it is not only convenient, making the software more effective, but also keeps the "calculation engine" from *Metacontrol* using the same criterion. It would not make any sense, for instance, using a branch-and-bound algorithm that outputs the index of the most promising CVs using the maximum singular value rule from Skogestad

and Postlethwaite (2007) and use the CV index sequence from this algorithm to evaluate the worst-case loss. Fundamentally speaking, the orders of "best" control structures would not be the same, simply because the search method would be using an different criterion from the linear method implemented to evaluate the H matrix.

The Branch-and-Bound algorithm developed by Kariwala and Cao (2009) that was originally implemented in MATLAB® by them was translated to Python by the main author of Alves et al. (2018). The same is true for equations of Exact Local and Extended Nullspace methods described by Alstad, Skogestad, and Hori (2009). Those Python routines were packaged under the name of *pySOC* (Python-based Self-Optimizing Control), and can be found in https://github.com/feslima/pySOC, with the code being freely available for inspection, revision and suggestions.

# 3 Kriging reasoning

Metamodels are a way to represent the world in simpler terms. Think of them as a photograph, they do not capture the moment as whole but can represent it good enough. In this analogy, the moment is a complex process that it is too cumbersome to explain it completely in mathematical terms, and metamodels, as photographs, may serve the purpose of capturing the core trends of this process without being too unwieldy and not losing too much information.

There is a family of metamodeling methodologies, ranging from a simple linear regression to complex neural networks. However, this chapter will be dedicated to discuss *Kriging* surrogates.

The simplest form to represent a real world process (y) through a metamodel  $(\hat{y})$  and its error  $(\varepsilon)$  is done through Equation 3.1.

$$y(x) = \hat{y}(x) + \varepsilon \tag{3.1}$$

The error  $\varepsilon$  is associated with the unmodeled effects of the inputs x and random noise (i.e. it cannot be explained in detail but cannot be ignored as well.). When using the *Kriging* methodology as metamodel, this error is assumed to be a probabilistic function of x, or in other words, this error is assumed to be *not* independent and identically distributed. The specific probabilistic function is represented by a Gaussian distribution with mean zero and variance  $\sigma^2$ .

$$\varepsilon = \varepsilon(x) \sim \mathcal{N}(0, \sigma^2)$$
 (3.2)

As from Søren Nymand Lophaven, Hans Bruun Nielsen, and Jacob Søndergaard (2002), a *Kriging* metamodel is comprised of two parts: a polynomial regression  $\mathcal{F}$  and departure function z of stochastic nature, as can be seen in Equation 3.3.

$$\hat{y}_l(x) = \mathcal{F}(\beta_{:,l}, x) + z_l(x), \quad l = 1, \dots, q$$
 (3.3)

The regression model, considered as a linear combination of t functions  $(f_j : \mathbb{R}^n \to \mathbb{R})$ , as defined in Equation 3.4.

$$\mathcal{F}(\beta_{:,l}, x) \equiv f(x)^T \beta_{:,l} \tag{3.4}$$

The most common choices for f(x) are polynomials with orders ranging from zero (constant) to two (quadratic). It is assumed that z has mean zero, and the covariance between to given points, arbitrarily named w and x for instance, is defined by Equation 3.5:

$$Cov [z_l(w), z_l(x)] = \sigma_l^2 \mathcal{R}(\theta_l, w, x), \quad l = 1, \dots, q$$
(3.5)

With  $\sigma_l^2$  being the process variance for the *lth* response component, and  $\mathcal{R}(\theta, w, x)$  defined as the correlation model. In *Metacontrol*, the correlation model used is described in Equation 3.6.

$$\mathcal{R}(\theta_l, w, x) = \exp\left(-\sum_{i=1}^m \theta_l (w - x_i)^p\right), \quad (\theta_l \ge 0, p_l \in [0, 2])$$
 (3.6)

Two important concepts must be addressed at this point: The first regards the meaning of the hyperparameter  $\theta$ , being interpreted as the "activity" of variable x, meaning that, a low value of  $\theta$  indicates that the points are highly correlated (ALVES et al., 2018). In addition, the value of  $\theta$  also indicates how fast the correlation goes to zero as the process moves in the lth direction, as discussed by Caballero and Grossmann (2008). The second concept regards the parameter p in Equation 3.6, that represents the "smoothness" of the correlation. As its value reduces, the rate of the initial correlation drops as the distance between w and  $x_i$  increases. When  $p \approx 0$ , there is a discontinuity between Y(w) and  $Y(x_i)$  (FORRESTER; SOBESTER; KEANE, 2008) and there is no immediate correlation between the given points.

The hyperparameters  $\theta$  are degrees of freedom available for optimization purposes, seeking the improvement of the metamodel fitness. In Søren Nymand Lophaven, Hans Bruun Nielsen, and Jacob Søndergaard (2002), the optimal set of hyperparameters  $\theta^*$  corresponds to the maximum likelihood estimation. Assuming a Gaussian process (LOPHAVEN, S.; NIELSEN, H.; SØNDERGAARD, Jacob, 2002), the optimal values of the hyperparameters solves Equation 3.9:

$$\min_{\theta} \left\{ \psi(\theta) \equiv |R|^{\frac{1}{m}} \sigma^2 \right\} \tag{3.7}$$

Where |R| is the determinant of the correlation matrix. The internal optimizer used in *DACE* corresponds to a modified version of the *Hooke & Jeeves* method, as showed by S. N. Lophaven, H. B. Nielsen, and J. Søndergaard (2002).

As stated before, high-order data obtainment it is an obligatory step in the proposed methodology implemented in *Metacontrol*. Fortunately, Søren Nymand Lophaven, Hans Bruun Nielsen, and Jacob Søndergaard (2002) also derived expressions for Jacobian

evaluation of a *Kriging* prediction (for full demonstration, consult Søren Nymand Lophaven, Hans Bruun Nielsen, and Jacob Søndergaard (2002)), given in Equation 3.8:

$$\hat{y}'(x) = J_f(x)^T \beta^* + J_r(x)^T \gamma^*$$
(3.8)

The expression for Hessian evaluation was derived by Alves et al. (2018) (full demonstration in appendix A of their work), and it is depicted in Equation 3.9:

$$\hat{y}''(x) = H_f(x)\beta^* + H_r(x)\gamma^*$$
(3.9)

Equations 3.8 and 3.9, differently from numeric/automatic differentiation, are not approximations and, instead, are analytical expressions derived by Søren Nymand Lophaven, Hans Bruun Nielsen, and Jacob Søndergaard (2002) and Alves et al. (2018). Therefore, it is expected a reduced error when one is using these expressions, if compared to techniques based in numerical approximation, considering that the *Kriging* metamodel used is precise enough.

For the design of experiments part, it was decided to implement the Latin Hypercube Sampling (LHS) because it allows to better sample the optimization domain without introducing ill-conditioning in the spatial correlation matrix calculated by the *Kriging* builder.

Lastly, both the LHS function and *Kriging* model builder/predictor were implemented as a separated package in Python under the name of *pydace* (from *Python toolbox for Design and Analysis of Experiments*). This package is a partial code translation from the MATLAB® toolbox implemented by Søren Nymand Lophaven, Hans Bruun Nielsen, and Jacob Søndergaard (2002) named *DACE* to the Python programming language. The link to the open-source code is https://github.com/feslima/pydace. There the reader can find a brief documentation on how to install and example of usage.

### 4 Non linear optimization and infill criteria

When dealing with a non linear problem, such as in Equation 2.1, typically it is resorted to classical solvers (e.g. SQP, trust-region-dogleg, genetic algorithms, simulated annealing, etc.) to obtain its solution, depending on the nature of the NLP (e.g. presence of discontinuities, whether or not the function is differentiable, etc.).

There is a entire field of study dedicated to find these NLP solutions with *Kriging* surrogates. In the works of Jones (2001), Sasena (2002), Forrester, Sobester, and Keane (2008) and Alexandrov et al. (2000), there are entire discussions and frameworks on how to solve non linear problems and comparisons of several metrics involved in the optimization process with metamodels.

The premise of performing a optimization using surrogates is that the model to be optimized is too time consuming or computationally expensive to be solved with classical solvers. To circumvent this, the following steps are proposed:

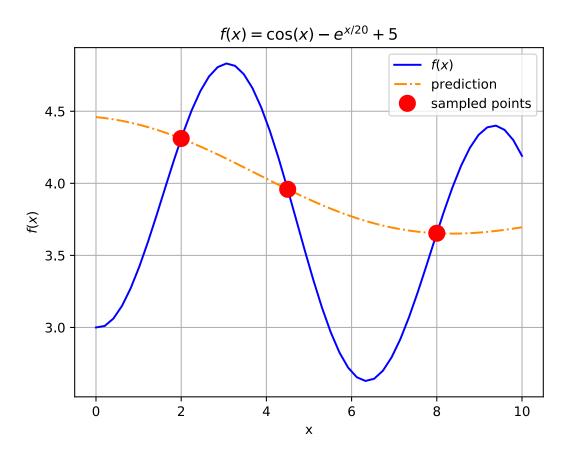
- 1. Build an approximation model with *Kriging* surrogates using a limited number of initial samples. This approximation is a "generalistic" enough representation of the real model;
- 2. Perform a optimization of the approximation model using classical NLP solvers and an infill criteria. The surrogate model reduces the "search area" needed by the solver;
- 3. Compare the surrogate optimum found in step 2 with the result from original model. In other words: feed the results from the *Kriging* metamodel optimum into the original model and see if they are close enough;
- 4. If the optimum from the metamodel is close enough (based on a chosen metric) to the original model, then this may be the true optimum. Otherwise, update the *Kriging* model by introducing the value found and return to step 2;

This process is basically "filling holes" (hence the name *infill*) in our *Kriging* metamodel until original model optimum is found. To illustrate this in the simplest way, suppose a complex process that we need to optimize that is represented by the following function:

$$f(x) = -\cos(x) - e^{\frac{x}{20}} + 5$$

Assuming that we only have three initial points sampled from this model function, we build our *Kriging* model. As can be seen in Figure 1.

Figure 1 – Initial plot of our complex model. The solid blue line represents the function behavior. The dashed line is the *Kriging* metamodel of the three sampled points (red circles) available.



Source: Author.

When applying an optimization solver on the *Kriging* model, we get a new optimal value for x near 7.8 (3.47 for f(x) when we consult the original model). Now, we include these values of (x, f(x)) in the sample and rebuild the *Kriging* metamodel. The result is shown Figure 2. We keep repeating this procedure until we get the result in Figure 3.

This example is a trivial one because the problem involves a single input variable and infill criteria is the own Kriging prediction of the model. As discussed in Jones (2001), this criteria has its pitfalls if used without other precautions.

Caballero and Grossmann (2008) presented an algorithm, based on the "method 2" in the work of Jones (2001), referred as a gradient matching technique where the gradient of the surrogate is forced to match with the true function gradient, this is done through trust-region approach to ensure local convergence which was proven in the work of Alexandrov et al. (2000). The basic idea of this approach is: minimize the NLP problem

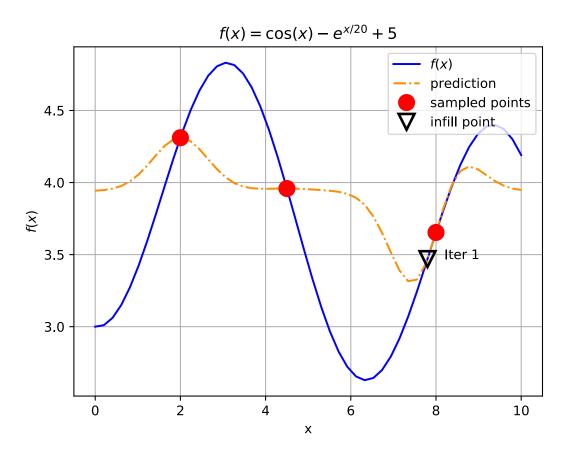


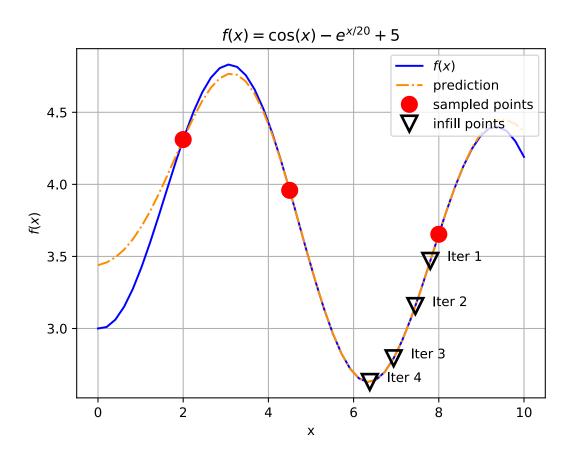
Figure 2 – The *Kriging* model after one update.

Source: Author.

metamodel, consult the original function at the minimum found in the metamodel, update the sample matrix used to build the surrogate. Repeat this until a convergence criteria is met. The flowchart depicting the whole procedure is defined in Figure 4. For detailed explanation of each step of the proposed algorithm, one must refer to Caballero and Grossmann (2008) and Alves et al. (2018).

This approach was implemented as a procedure of the Python package *surropt* (from *Surrogate Optimization*). It uses as internal NLP solver a Python wrapper authored by Kummerer and Moore (2019) of the well-established *IpOpt* package (WÄCHTER; BIEGLER, 2006). The *surropt* package is found on https://github.com/feslima/surropt.

Figure 3 – The  $\mathit{Kriging}$  model after four updates. Notice how the  $\mathit{Kriging}$  model adjusts to the true function.



Source: Author.

Start
Select the number of sampling points (N), and apply a sampling plan (stratification, space filling LHS, etc.) for the optimization domain. Start refinement Specify refinement (tol1) and termination (tol2) tolerances. The latter must be at least one order magnitude larger than the estimated noise of function  $(\mathbf{x}^\star)_k = (\mathbf{x}_j)_k$ funEvals >= MaxFunEvals No Start the iterations count (k = 1 and funEvals = 1) Sample the function based on the sampling plan lefined earlier, and build the surrogate model. If k>1, (x\*)<sub>k-1</sub> must be included in the sampled points No If k = 1 and j = 1, validate the model through cross-validation to make sure it is accurate enough. Yes Optional step (if k = 1 and j = 1) If there are feasible points in the sampled points, use the best feasible point as initial estimate of the minimization problem to help convergence. If there aren't feasible points, try a new initial sample.  $1(x^*)_k - (x^*)_{k-1} | <= tol2?$ No Is (x\*)k inside or at the limit of the  $\begin{array}{ll} j=1 \\ \text{Minimize the response surface model RSM(x) subject to the constraints G(x). These can be metamodels on their own, based on their evaluation difficulty. \\ The optimal solution is <math>(x)_k$ . Inside sampling hypercube? Contract sampling hypercube and cente it in (x\*)<sub>k</sub> Sample the point  $(x_j)_k$  to get  $g((x_j)_k)$  and  $y((x_j)_k)$ . funEvals = funEvals + 1 Update the surrogate model. In ase of kriging, do not optimize the hyperparemeters. At Limit Starting from  $(x_j)_k$  minimize the RSM(x) to get  $(x_{j+1})_k$ Move sampling percube and cent it in (x\*)<sub>k</sub>  $\begin{aligned} j &= j+1 \\ (x_j)_k &= (x_{j+1})_k \end{aligned}$ **k** = k + 1  $|(x_j)_k - (x_{j+1})_k| \le tol1?$ Yes No

Figure 4 – Flowchart of Caballero and Grossmann (2008) algorithm, translated to Python by the authors of this work and implemented within *Metacontrol*.

Source: Alves et al. (2018)

### 5 The *Metacontrol* framework

To apply the "top-down" part (SKOGESTAD, 2000) of the SOC methodology the conventional way (ALVES et al., 2018; ALSTAD; SKOGESTAD; HORI, 2009; SKOGESTAD, 2000), the following steps are typically involved:

- 1. Identify the relevant process variables: manipulated variables, disturbances and potential CV candidates (process measurements) in order to perform a Degree of Freedom (DOF) analysis (taking into account both steady and dynamic state of the process);
- 2. Define optimal operation: Define the objective function to be used in order to seek an optimal operating point;
- 3. Modeling of the industrial process (using a process simulator or or any numerical environment, for instance) as close as possible to the reality;
- 4. Optimize the process model;
- 5. Implement the control loops of active constraints found in the previous step "active constraint control" (SKOGESTAD, 2000);
- 6. Evaluate the loss (result of a constant setpoint policy as showed by Skogestad (2000) and Halvorsen et al. (2003)) for each possible control structures for the remaining (unconstrained) degrees of freedom available: This can be done manually, evaluating each possible control structures one at a time ("brute-force" approach (UMAR et al., 2012)), which is, very often, an impracticable approach due to combinatorial explosion (ARAÚJO; GOVATSMARK; SKOGESTAD, 2007). Therefore, it is more efficient to "pre-screen" the most promising CV candidates using local (linear) methods that have been developed and applied by several authors such as Halvorsen et al. (2003), Hori, Skogestad, and Alstad (2005), Eduardo Shigueo Hori and Skogestad (2008) and Alstad, Skogestad, and Hori (2009). For the latter approach, it is necessary to obtain the reduced-space problem (unconstrained) differential information (gradient with respect to CV candidates and disturbances, and also the objective function Hessian) evaluated at the optimal point found in step 4;
  - a) When using the local methods, it is necessary to define disturbances magnitudes and the measurement errors of the candidates of step 1;
  - b) To evaluate the loss using local methods, one have to apply the mathematical formulations involved in these methods to obtain the candidates variables

combinations and their respective losses. The mathematical formulations that can be used are mainly: The maximum gain rule authored by Skogestad and Postlethwaite (2007), the exact local method derived by Halvorsen et al. (2003) and analytically solved by Alstad, Skogestad, and Hori (2009) or the nullspace method derived by Alstad and Skogestad (2007);

7. Perform a controllability analysis based on the results from step 6 in order to determine the most efficient MV-CV pairings.

Even though it is possible to describe the methodology in steps, its application is not so simple. That is, many of those steps take place in different environments. For instance:

- In steps 1 amd 2, it is the closest as engineers, have to a brainstorming session, where it is considered the variables that best describe the process, which of these will yield better convergence in the process simulator; which of them will be realistic enough when designing a control system, etc. Then perform a degree of freedom analysis for both steady state and dynamic state (i.e. the DOF analysis of one seldom is the same as the other). In addition, there is the performance criteria decision in the objective function it is going to be optimized.
- In step 3, it is necessary to simulate with a software package, the process to a minimum satisfaction standard. Or in other words, is this simulation a realistic enough representation of the process?
- Sometimes, the process simulator (e.g. Aspen Plus, Aspen HYSYS, Unisim, etc.) optimization routines are not capable of solving the nonlinear problem that has been defined. So, in step 4, it may be needed to resort an external optimization package (e.g. IpOpt, GAMS, MATLAB® optimization toolbox, etc). This is another environment to work with. In other words, an additional "layer" of complexity.
- If it is necessary the usage of an external NLP solver, then one have to go back to
  the process simulator and implement the active constraints, as required by the SOC
  methodology.
- In step 6, to obtain the differential information required, there are different approaches in order to do so:
  - 1. Extracting manually from the simulator (i.e. performing a first and second order numerical differentiation by applying the differentiation steps and collecting the output from the simulator);

- 2. Using another external package to extract the gradient and hessian (i.e. Automatic differentiation packages);
- 3. Using a surrogate approximation of the process simulation in the optimum region, and extracting the differential information from this metamodel;

Option 3 was proposed as solution in the work of Alves et al. (2018), and is implemented in *Metacontrol*. Options 1 and 2 are not implemented due to difficult nature inherent to them. For example, option 1 is a tedious task, even impossible depending on the number of variables to apply the differentiation steps required, and human-error prone since each step applied is done manually. In both options, another limitation that one faces regards the physical meaning of the variables involved in the numeric differentiation process. Strictly speaking: the simulation package does not accept negative values for variables such as flowrates. Compositions are limited to values between 0 and 1. Temperatures may or not accept negative values depending on their units (from 0 to infinity for Kelvin, or -273 to infinity in degree Celsius), etc. Thus, if the numeric differentiation package try to step into outside of these valid value ranges, the simulation software will simply not converge.

• In Step 6 and 7, one have to use another numeric environment to implement algorithms and equations from Kariwala and Cao (2009), Alstad, Skogestad, and Hori (2009) and Alves et al. (2018) in order to perform the calculations necessary to obtain the controlled variables candidates combinations and analyze the controllability of the process studied, respectively.

As can be seen, this is a methodology implementation that goes back-and-forth between several numeric computation (e.g. MATLAB®, Octave, Microsoft Excel, etc.) and simulation (e.g. Aspen Plus, Aspen HYSYS, Unisim, etc.) environments. Therefore, *Metacontrol* was created as a software package that allows all of these steps to be done in a single environment (or at least, keep the necessity of transition to a minimum) for the sake of convenience to apply the SOC methodology.

#### 5.1 *Metacontrol* workflow

The tool has two modes of operation:

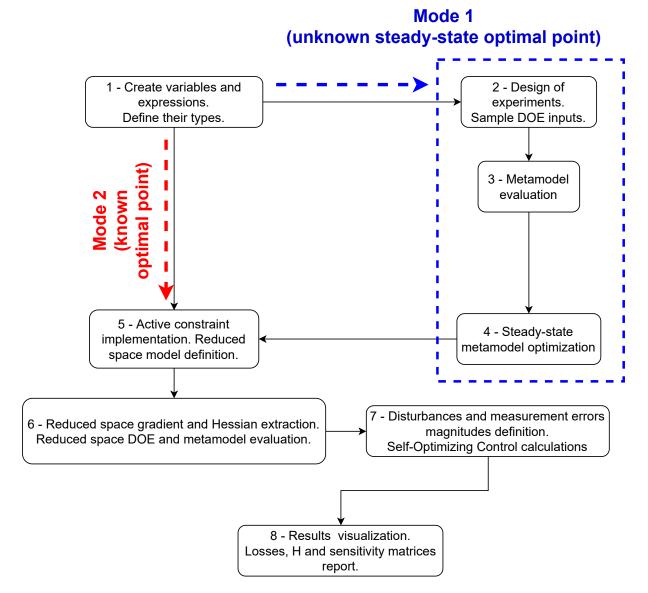
1. The user wishes to apply the methodology proposed by Alves et al. (2018) completely, as seen in Figure 5 represented by the blue dashed arrow and rectangle. That is, he needs to create and define variables and expressions (1), perform a Design of Experiments (DOE) of the industrial process (2), build its NLP constraints and objective function metamodels (3), optimize this NLP metamodel (4). If the

optimization process is successful, implement its active constraints and obtain the reduced space model (5), build another metamodel of the objective function and controlled candidates variables in reduced space, then extract the gradient and Hessian (6). Finally, apply the SOC methodology described by Alstad, Skogestad, and Hori (2009) (7-8).

2. The user already knows the process steady-state optimum, and wishes to apply the methodology partially, see the red dashed arrow in Figure 5. He needs to create the variables/expressions (1), then he implements the active constraints and generate the reduced space metamodels (5). Extract the gradients and hessian needed (6), define the rest of inputs needed to perform the SOC analysis (7) and analyze its results (8).

The only difference between modes 1 and 2, is that the user, when opting for mode 2, skips steps (2) to (4) in mode 1. Everything else is the same.

Figure 5 – Flowchart describing how *Metacontrol* works.



Source: Author

## 6 Case studies applied in *Metacontrol*

In this chapter will be presented three case studies of Self-Optimizing Control that are applied in the *Metacontrol* software. Each one of them use different objective function criteria with varying complexity. They are:

- 1. A CO<sub>2</sub> compression purification unit (CPU). The optimization criteria here is the performance enhancement of the process through the reduction in the energy consumption;
- 2. A hydrocarbon distillation column. The optimization criteria is the minimization of nominal setpoint deviation;
- 3. An isomerization process that seeks to convert n-butane into isobutane. The objective is maximization of profits;

### 6.1 The CO<sub>2</sub> Compression and Purification Unit (CPU)

The first case-study to be used as a test-bed in *Metacontrol* consists in a CO<sub>2</sub> compression and purification unit that uses phase separation method to obtain purified CO<sub>2</sub> from oxy-fuel combustion. This process is one of the several that exist in the industry that are capable of reducing the greenhouse effect on climate change (JIN; ZHAO; ZHENG, 2015). The process and its simulation are based on the work of Liu et al. (2019). In addition, their unit is based on the prototype proposed by the International Agency Greenhouse Gas (IEAGHG) R&D program study (DILLON et al., 2005).

The process is depicted in Figure 6. Flue gas is compressed by a three-stage after-cooled compressor before being sent to the cold box, where two multi-stream heat exchangers (E1 and E2) and two separators (F1 and F2) take place. In the base case from Liu et al. (2019), the flue gas is first cooled to  $-24.51^{\circ}$ C and sent to to F1, with its bottom stream being the first product of the process. Afterwards, The top stream from F1 is sent to the second multi-stream heat-exchanger (E2) being cooled to  $-54.69^{\circ}$ C before going to separator F2. The bottom stream from this separator consists in the second product of the process, and the top stream from F2 is discarded as vent. Both CO<sub>2</sub> product streams and the vent gas are reheated on both multi-stream heat exchangers. The CO<sub>2</sub> product streams are mixed and become ready for storage. The reader can consult Jin, Zhao, and Zheng (2015) and Liu et al. (2019) for more information about the simulation (i.e.: Raw flue gas conditions, detailed stream and equipment conditions, etc).

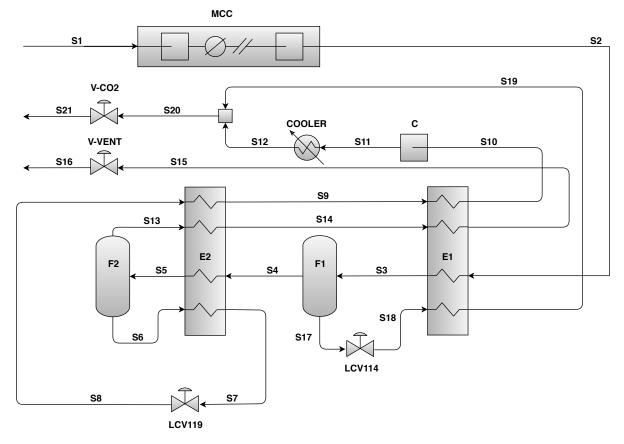


Figure 6 - CPU process flowsheet

Source: Author

From Liu et al. (2019), the authors of this paper have selected the objective function described in Equation 6.1, that consists in the specific energy consumption, defined as the ratio of energy used in both compressors (MCC and C) to total CO<sub>2</sub> flow rate produced. Therefore:

$$J = \frac{W_{\text{MCC}} + W_{\text{C}}}{F_{\text{CO}_2}} \tag{6.1}$$

The units of specific energy consumption of the objective function are  $kWh/tCO_2$ .

Regarding the CPU process constraints, from Jin, Zhao, and Zheng (2015), Liu et al. (2019) and Dillon et al. (2005), the following apply:

- C-1:  $CO_2$  recovery rate  $\geq 90\%$
- C-2:  $CO_2$  purity on product stream  $\geq 96\%$
- C-3: Temperature of F2 bottom stream > -56.6°C

C-1 aims to meet the environmental requirements (LIU et al., 2019) and reduce CO<sub>2</sub> atmospheric emissions (TOFTEGAARD et al., 2010; BUHRE et al., 2005). C-2 is a

result of the demand of CO<sub>2</sub> storage and transportation (LIU et al., 2019). In addition, according to Posch and Haider (2012), the purity addressed in this constraint would realize acceptable energy consumption. Lastly, C-3 exists to avoid CO<sub>2</sub> solidification in the pipeline, since the value of C-3 corresponds to the CO<sub>2</sub> three-phase freezing point (POSCH; HAIDER, 2012; KOOHESTANIAN et al., 2017).

As stated by Liu et al. (2019), the main disturbances in the CPU process are:

- D-1: Flue gas flow rate
- D-2:  $CO_2$  concentration in the flue gas

D-1 and D-2 are a result of the oxy-fuel combustion boiler island (LIU et al., 2019), given the variation of the boiler operation. Load changes in the boiler island and variations of the combustion conditions can generate D-1 and D-2, as also stated by Liu et al. (2019). It is considered a  $\pm 5\%$  disturbance amplitude for CO<sub>2</sub> feed composition and flue gas flow rate of the base-case, similarly as Jin, Zhao, and Zheng (2015) and Liu et al. (2019).

The number of degrees of freedom for the CPU process is 4 (JIN; ZHAO; ZHENG, 2015; LIU et al., 2019) for Mode I (Given feed). For the sake of simplicity and without loss of generality, the same DOFs from Jin, Zhao, and Zheng (2015) were used here:

- 1. MCC outlet pressure (bar)
- 2. MCC outlet temperature (°C)
- 3. F1 temperature (°C)
- 4. F2 temperature (°C)

Using this information and based on the review of control configurations for  $CO_2$  CPU process (LIU et al., 2019), the CV candidates in Table 1 that were considered in this case study are listed.

Table 1 – CV Candidate	es for $CO_2$ CPU process.
ias used in <i>Metacontrol</i> )	Description

Variable (alias used in <i>Metacontrol</i> )	Description
mccp/mccpout	Compressor outlet pressure (bar)
mcct/mcctout	Compressor outlet temperature (°C)
f1t/f1tout	F1 temperature (°C)
f2t/f2tout	F2 temperature (°C)
s8t	S8 stream temperature (°C)
fco2out	$CO_2$ product flowrate $(t/h)$
xco2out	$CO_2$ product molar fraction
co2rr	$CO_2$ recovery rate

With 4 degrees of freedom and 8 CV candidates, there are (Equation 6.2)

$$\binom{8!}{4!} = \frac{8!}{4! \times (8-4)!} = 70 \tag{6.2}$$

possible control structures for a single measurement policy (excluding the possible ways of controlling the regulatory layer and the possibility of using linear combinations of measurements). Therefore, the manual evaluation of all possibilities is impracticable and also would need the usage of different software environments. This tedious evaluation, however, can be mitigated by *Metacontrol*.

With the problem defined and the possible CV candidates being listed, it is possible to start to use the capabilities of *Metacontrol* in order to aid the search for a Self-Optimizing Control structure for this case-study. Initially, it is necessary to seek for the variables of the process simulator (Aspen Plus) using the COM interface between the *Metacontrol* software and the process simulator.

Figures 7 and 8 illustrate the process of selecting a \*.bkp file, selecting the relevant variables, and adding alias to them.

From Figure 7 the user can see that *Metacontrol* shows on its main screen some relevant information: Block names, flowsheet operations (i.e.: Optimizations, sensitivities, calculators), the components selected in the process simulated and the thermodynamic package used. These are enumerated on "Simulation Info" panel and the name of each object is present on "Simulation Description" panel.

After selecting the relevant variables (Decision variables and process measurements) the user can go back to the main screen, where expressions can be created. This functionality aims to give freedom for the user to build expressions based on variables from the process simulator, such as: Objective functions, CV candidates or constraints. Figure 9 shows the specific power consumption, the CO<sub>2</sub> recovery rate expressions being built, based on the auxiliary variables selected on Figure 8.

With the procedure aforementioned being completed, the user can generate the design of experiments (DOE) in order to build *Kriging* responses of the objective function, CV candidates and process constraints. The ranges for each decision variable are taken from Jin, Zhao, and Zheng (2015) (Table 3 from their paper), and this step is illustrated in Figures 10 to 12.

Figure 13 shows the sampling process running. After running all cases, the user can inspect the results of the design of experiments, as can be seen in Figure 14.

With the results of the sampling procedure, the user can go to the "Metamodel" Panel, and select which variables will have *Kriging* responses built, the bounds for the *Kriging* hyperparameters optimization, and the regression and correlation models to be

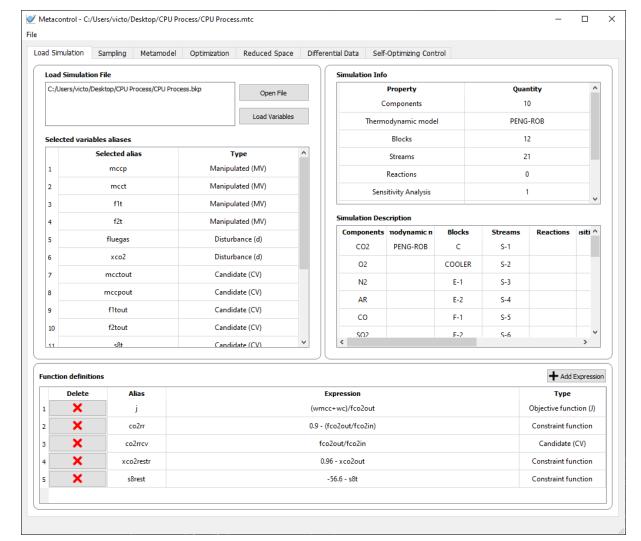


Figure 7 – Metacontrol main screen with CPU process simulation file loaded.

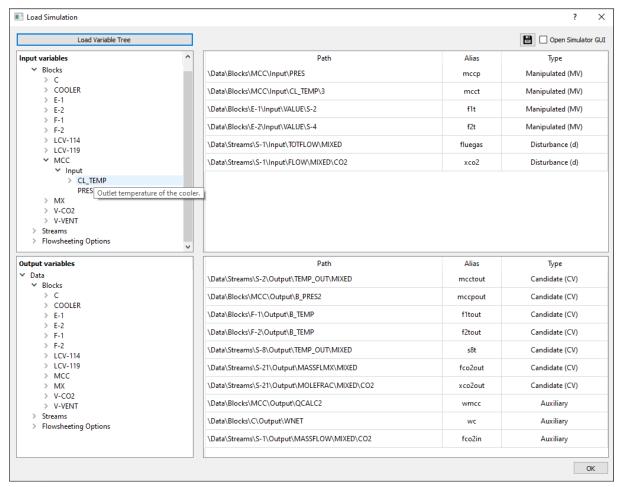
Source: Author.

used. This procedure can be depicted in Figure 15.

The user can also choose which type of validation is going to be performed: *Hold-out* or *K-fold* validation. It is important to point out that this first metamodel generation is performed only to give a quick view of the initial sampling. In other words, to check if the initial sampling is acceptable to be refined by the implementation of the algorithm proposed by Caballero and Grossmann (2008) that is bundled in *Metacontrol*. In addition, if the user chooses *Hold-out* validation, it is possible to view the graphical results (fitness of training set to the metamodel) of each *Kriging* interpolator generated, as can be seen in Figure 16.

In Figure 15, the reader can also inspect under the panel "Validation metrics", several metrics are used to evaluate reduced models performance, such as: Mean squared error (MSE), Root mean squared error (RMSE), Mean absolute error (MAE),  $R^2$  linear

Figure 8 – Loading variables for the CPU from Aspen Plus simulation and adding alias to them. At the top right corner of this screen, the user is able to select the option to reveal the GUI from Aspen Plus. This features allows the user to inspect inside the process simulator interface to remember any stream or block names. This can be helpful when one is selecting the variables using the COM technology and there are several unit operations blocks and streams, for instance. Another feature that was implemented in order to ease the search of the variables, regards the description of each variable: Hovering the mouse over a COM variable will show its description, extracted directly from the process simulator.



Source: Author.

coefficient, Explained variance (EV), the Sample mean and also its standard deviation.

In order to try to improve the initial sampling for optimization purposes, we go to the "Optimization" tab where the refinement algorithm proposed by Caballero and Grossmann (2008) is implemented. Figure 17 shows the parameters that can be tuned in order to attempt to improve the *Kriging* interpolator using the automated refinement procedure, with further discussion and details regarding each parameter can be found on caballero2008 and in the previous work from the author of this dissertation (ALVES)

Figure 9 – 0	Creating e	expressions	for specific	power	consumpti	ion (object	ive function),	$CO_2$
r	recovery ra	ate and S8	Temperatu	re (coi	astraint fur	nctions/CV	/ candidates).	

	Delete	Alias	Expression	Туре
1	×	j j	(wmcc+wc)/fco2out	Objective function (J
2	×	co2rr	0.9 - fco2out/fco2in	Constraint function
3	×	co2rrcv	fco2out/fco2in	Candidate (CV)
1	×	xco2restr	0.96 - xco2out	Constraint function
5	×	s8rest	-56.6 - s8t	Constraint function

et al., 2018). In addition, NLP solvers parameters can also be changed in this screen.

In Figure 17, the user can see the final result of the refinement algorithm: on the "Results" panel, the final results for the decision variables, constraints expressions defined previously and the objective function. In addition, a control panel showing the operations of contraction and movement of the hyperspace performed by the algorithm (and how many iterations on each operation) can be inspected. Figure 18 shows the control panel details of the procedure.

Inspecting Figures 17 and 18, it is clear that the optimal operating point found is

- MCC outlet pressure (bar) = 30.1849
- MCC outlet temperature = 25 °C
- F1 temperature = -30 °C
- F2 temperature =  $-55^{\circ}$ C

That indicates three active constraints that have to be controlled. Regarding stream S8 temperature, CO<sub>2</sub> product purity and recovery rate, these were inactive constraints. Therefore, the reduced space problem has one degree of freedom left for Self-Optimizing Control.

In order to prove the effectiveness of the proposed software and the procedures and algorithms used, an optimization using the process simulator (Aspen Plus) SQP implementation (an optimization block) was performed, and the results can be found in Tables 2 and 3, compared with the results found by Metacontrol. They identical, quantitatively and qualitatively (the active constraints found in both approaches). The constraints in Metacontrol are written internally in the form  $g(x) \le 0$ , and showed in the GUI in the same way, due to NLP solvers and refinement algorithm syntaxes.

After determining the nominal optimal operating point, the active constraints must be implemented in the simulation file externally using the process simulator (Using design

Metacontrol - C:/Users/victo/Desktop/CPU Process/CPU Process.mtc File Load Simulation Sampling Metamodel Optimization Reduced Space Differential Data Bounds definition Upper bound Manipulated variable Lower bound 25.0 35.0 mccp mcct 50.0 f1t -30.0 -20.0 f2t -55.0 -40.0 Open Sampling Assistant Generate input from LHS and sample the data O Load data from CSV file: DOE Results Out.. Out.. Obje... Case Status f2t

Figure 10 - Metacontrol "Sampling panel". The user can perform the sampling using the process simulator or import a .CSV file.

Table 2 – Optimization runs: Aspen Plus vs Metacontrol - Decision variables and objective function - CPU Process

	Objective function J ( $kWh/tCO_2$ )	MCC Pressure (bar)	MCC outlet temperature (°C)	F1 temperature (°C)	F2 temperature (°C)
Aspen Plus	112.3690	30.0316	25	-30	-55
Metacontrol	112.3691	30.1849	25	-30	-55

specifications for instance) and go back to Metacontrol, in order to generate the reduced space Kriging metamodel, seeking the obtainment of differential data (e.g.: the gradients  $G_y, G_y^d$ , and the hessians  $J_{uu}$  and  $J_{ud}$ ). The reduced space problem can be sampled using the process simulator linked with Metacontrol directly, or importing a \*.csv file. Both options mentioned are similar to the initial sampling procedure.

Over the tab "Differential data", the user is capable of checking which variables are active constraints (either decision variables or nonlinear constraints), inserting the values for the optimal operating point found on the previous step (refined surrogate optimization), and the value for the nominal disturbances. If the user sample the reduced space problem using the \*.bkp, he must also input the range for the remaining decision variables to be

Figure 11 – *Metacontrol* Sampling assistant. The limits for the decision variables used in the CPU process are the same from Jin, Zhao, and Zheng (2015) and Liu et al. (2019)

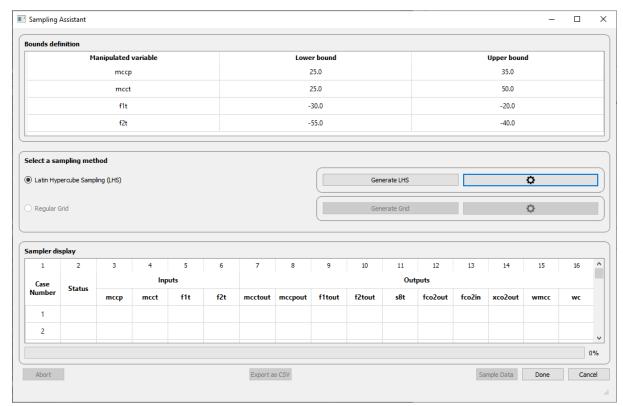


Table 3 – Optimization runs: Aspen Plus vs Metacontrol - Process constraints - CPU Process

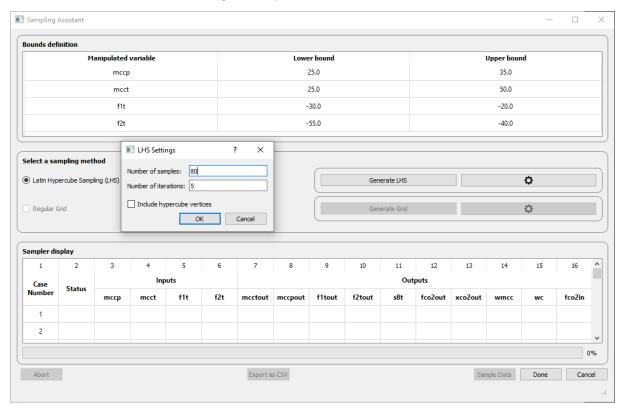
	Stream S8 temperature °C	CO <sub>2</sub> molar fraction	CO <sub>2</sub> recovery rate
Aspen Plus	-55.8201	0.9674	0.9658
Metacontrol	-55.4859	0.9666	0.9671

sampled and for the disturbances. The range for the remaining degrees of freedom and for the disturbances are suggested to be a small percentage of the nominal values ( $\pm 0.5\%$ , for instance) in order to train a surrogate model accurate enough at the optimal region, guaranteeing robust high-order data (gradients and hessians) obtainment, as suggested previously in Alves et al. (2018).

In the CPU process, the MCC operating pressure, MCC temperature, F1 temperature and F1 temperature are active constraints as mentioned previously. Therefore, they should be marked as "active" under the "Variable activity" panel, as shown in Figure 19.

Since in the initial sampling the process simulator was directly linked with *Metacontrol*, in Figure 19 under the "Data source" panel a .\*csv file was imported, originated from a sensitivity analysis run done in a \*.bkp file of the reduced space problem for the CPU process, in order to show this supplementary feature of *Metacontrol*. This is illustrated in Figures 20 and 21.

Figure 12 – *Metacontrol* Latin Hypercube Sampling settings. 80 samples were generated and 5 iterations were performed in order to try to maximize the minimum distance between the points (*maxmin* criterion). The user can also add the vertices of the design of experiments.



After importing the design of experiments from the external source (\*.csv) and associating each variable created in *Metacontrol* with the data (as shown in Figure 21), the user can go to "Differential data" tab, in order to generate the reduced space metamodel. Under the panel "Reduced space metamodel training" the button "Open training dialog" allows the modification of the *Kriging* parameters, similarly as done previously in the step of generating the first metamodel to inspect the initial sampling.

The method of high-order data obtainment currently implemented in *Metacontrol* is based on the analytical expressions for the gradients and Hessian derived by Søren Nymand Lophaven, Hans Bruun Nielsen, and Jacob Søndergaard (2002) and Alves et al. (2018), respectively. In future releases of *Metacontrol* there will be two more methods of differentiation as secondary features. These will be based on numeric and automatic differentiation (*numdifftools* and *autograd* Python toolboxes, respectively), using the surrogate model as source of high-order data obtainment. However, it is strongly recommended the usage of the *Kriging* predictor analytical expressions to ensure results robustness, as stated before in Alves et al. (2018), and also stressed previously on this work.

After opening the training dialog (Figure 23) and configuring the reduced metamodel settings, the user can generate the metamodel, click on "ok", go back to the main screen

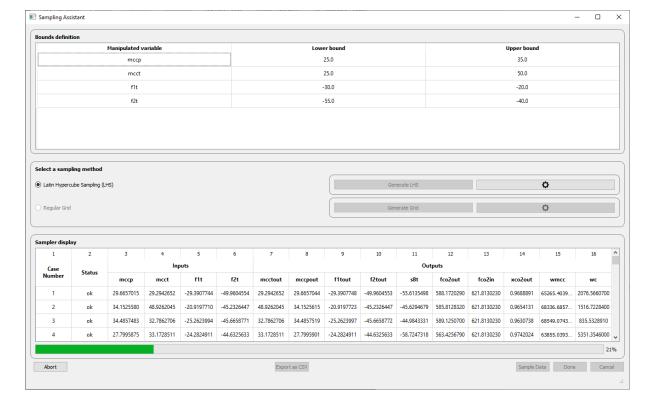


Figure 13 – Metacontrol Sampling for the CPU process.

and generate the estimation of the gradients and hessians necessary to carry on the Self-Optimizing Control study. These results are displayed on Figure 24.

In order to prove the effectiveness of the analytical expressions derived by Søren Nymand Lophaven, Hans Bruun Nielsen, and Jacob Søndergaard (2002) and already used in Alves et al. (2018), the gradients obtained using surrogate models in *Metacontrol* were compared against the ones generated in Aspen Plus (Equation-Oriented sensitivity mode). The process simulator does not provide the hessian of any function natively, and therefore  $J_{uu}$  and  $J_{ud}$  could not be compared. However, the excellent agreement between the values between the gradients found in both procedures can be considered as a sufficiently robust result.

Through inspection of Table 4, the reader can see how robust the results of the gradients obtained by the methodology proposed in the previous work from Alves et al. (2018) and now are automated in *Metacontrol*. The matrix mean-squared error in Table 5 also corroborates this affirmation.

After inspecting the gradients and hessians generated, the user can go to the "Self-Optimizing Control" tab, where the disturbances and measurement error magnitudes will be inserted. As stated previously in this case study, was considered a magnitude of  $\pm 5\%$  for the disturbances. For the  $CO_2$  inlet composition, it was considered the absolute value,

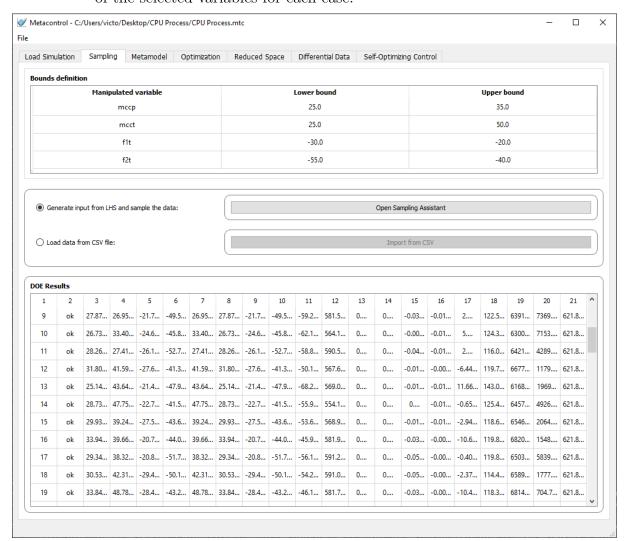


Figure 14 – Sampling results, where the user can inspect convergence status and the values of the selected variables for each case.

and for the flue gas flow rate,  $\pm 5\%$  of the nominal flow rate. Therefore, in Equation 6.3:

$$W_d = diag(0.05, 35.8595) \tag{6.3}$$

In addition, for the measurement errors, it was considered  $\pm 0.5$ °C for temperature measurements, 0.01 for pressure and flow measurements and 0.001 for ratios ( $CO_2$  recovery rate and product purity). These assumptions generated by Equation 6.4:

$$W_n^y = diag(0.001, 0.01, 0.01, 0.5, 0.001)$$
(6.4)

The order for Equations 6.3 and 6.4 it is the same from the column order from Figure 24. Figure 25 shows the magnitude matrix data being inserted in *Metacontrol*.

Under the "Subsets sizing options" panel, by default the best control structure for each subset size is evaluated by *Metacontrol*, but the user can change how many subsets

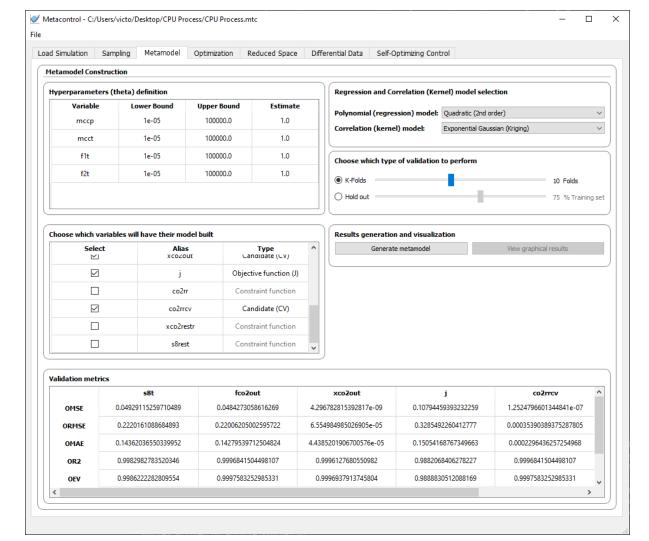


Figure 15 – Kriging configuration and validation metrics results.

he wants to evaluate, until the maximum number for each subset size.

After providing all the necessary inputs (magnitude matrices and number of best sets to be evaluated for each subset size), clicking in "Generate results" will show the *nth* best Self-Optimizing Control structures for each subset size, as can be seen for demonstration purposes in Figures 26 and 27, the results for a single measurement policy, and for linear combinations using 2 measurements at a time. The user can also inspect the H matrix (that will be of ones and zeros for single measurements and a full matrix for linear combinations) and the optimal sensitivity matrix for each subset evaluated.

For instance, considering a single measurement policy for the unconstrained degrees of freedom, Table 6 depicts the best CV candidates in worst-case loss ascending order. The best Self-Optimizing Control variable for the considered case consists in the multi-stage compressor (MCC) outlet pressure. This result can be related to the previous finding Liu et al. (2019).

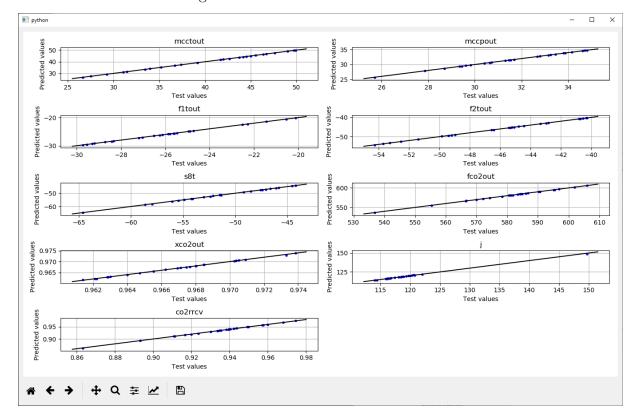


Figure 16 – Fitness for each metamodel.

Table 4 – High-order data obtainment: Aspen Plus vs Metacontrol

	$G^y$	$G_d^y$
Meta control	$\begin{bmatrix} 0.0036 \\ 2.2406 \\ 1.0000 \\ 2.7354 \\ -0.0017 \end{bmatrix}$	$\begin{bmatrix} -3.0148 \times 10^{-10} & 0.0799 \\ 0.8378 & 146.6549 \\ 5.2806 \times 10^{-9} & 2.5904 \times 10^{-5} \\ -3.4160 \times 10^{-5} & 0.0244 \\ -1.5455 \times 10^{-9} & 0.0040 \end{bmatrix}$
Aspen Plus	$\begin{bmatrix} 0.0036 \\ 2.2403 \\ 1 \\ 2.7330 \\ -0.0017 \end{bmatrix}$	$\begin{bmatrix} 1.3472 \times 10^{-7} & 0.0798 \\ 0.8378 & 146.6124 \\ 0 & 0 \\ 3.3797 \times 10^{-15} & 0.0250 \\ 1.6912 \times 10^{-16} & 0.0040 \end{bmatrix}$

Table 5 – Mean-squared error of high-order data obtaiment: Aspen Plus vs Metacontrol - CPU Process

	$G^y$	$G_d^y$
Mean-squared error	$1.1659 \times 10^{-6}$	$1.8088 \times 10^{-4}$

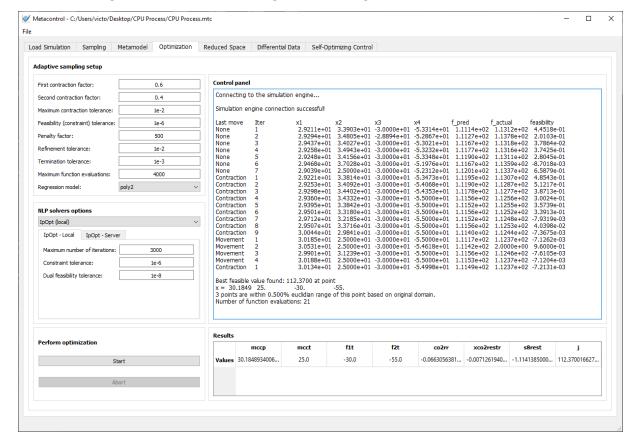


Figure 17 – Refinement algorithm configuration and results screen.

Figure 18 – Refinement algorithm control panel output.

Connecting to the simulation engine...

Simulation engine connection successful!

None 1 2.9211e+01 3.3903e+01 -3.0000e+01 -5.3314e+01 1.1114e+02 1.1312e+02 4.4518e-0	4
None 2 2 2.0004-01 2.4005-01 2.0004-01 5.0057-01 1.1127-02 1.1270-02 2.0102-0	1
None 2 2.9294e+01 3.4805e+01 -2.8894e+01 -5.2867e+01 1.1127e+02 1.1378e+02 2.0103e-0	1
None 3 2.9437e+01 3.4027e+01 -3.0000e+01 -5.3021e+01 1.1167e+02 1.1318e+02 3.7864e-02	2
None 4 2.9258e+01 3.4943e+01 -3.0000e+01 -5.3232e+01 1.1177e+02 1.1316e+02 3.7425e-0	1
None 5 2.9248e+01 3.4156e+01 -3.0000e+01 -5.3348e+01 1.1190e+02 1.1311e+02 2.8045e-0	1
None 6 2.9468e+01 3.7028e+01 -3.0000e+01 -5.1976e+01 1.1167e+02 1.1359e+02 -8.7018e-03	3
None 7 2.9039e+01 2.5000e+01 -3.0000e+01 -5.2312e+01 1.1201e+02 1.1337e+02 6.5879e-0	1
Contraction 1 2.9221e+01 3.3814e+01 -3.0000e+01 -5.3473e+01 1.1195e+02 1.1307e+02 4.8543e-0	1
Contraction 2 2.9253e+01 3.4092e+01 -3.0000e+01 -5.4068e+01 1.1190e+02 1.1287e+02 5.1217e-03	1
Contraction 3 2.9298e+01 3.4402e+01 -3.0000e+01 -5.4353e+01 1.1178e+02 1.1277e+02 3.8713e-0	1
Contraction 4 2.9360e+01 3.4332e+01 -3.0000e+01 -5.5000e+01 1.1156e+02 1.1256e+02 3.0024e-02	1
Contraction 5 2.9395e+01 3.3842e+01 -3.0000e+01 -5.5000e+01 1.1152e+02 1.1255e+02 3.5739e-0	1
Contraction 6 2.9501e+01 3.3180e+01 -3.0000e+01 -5.5000e+01 1.1156e+02 1.1252e+02 3.3913e-0	1
Contraction 7 2.9712e+01 3.2185e+01 -3.0000e+01 -5.5000e+01 1.1152e+02 1.1248e+02 -7.9319e-03	3
Contraction 8 2.9507e+01 3.3716e+01 -3.0000e+01 -5.5000e+01 1.1156e+02 1.1253e+02 4.0398e-02	2
Contraction 9 3.0044e+01 2.9841e+01 -3.0000e+01 -5.5000e+01 1.1140e+02 1.1244e+02 -7.3675e-03	3
Movement 1 3.0185e+01 2.5000e+01 -3.0000e+01 -5.5000e+01 1.1117e+02 1.1237e+02 -7.1262e-03	3
Movement 2 3.0531e+01 2.5000e+01 -3.0000e+01 -5.4618e+01 1.1142e+02 2.0000e+00 9.6000e-0	1
Movement 3 2.9901e+01 3.1239e+01 -3.0000e+01 -5.5000e+01 1.1156e+02 1.1246e+02 -7.6105e-03	3
Movement 4 3.0188e+01 2.5000e+01 -3.0000e+01 -5.5000e+01 1.1153e+02 1.1237e+02 -7.1204e-03	3
Contraction 1 3.0134e+01 2.5000e+01 -3.0000e+01 -5.4998e+01 1.1149e+02 1.1237e+02 -7.2131e-03	3

Best feasible value found: 112.3700 at point x = 30.1849 25. -30. -55.

Number of function evaluations: 21

<sup>3</sup> points are within 0.500% euclidian range of this point based on original domain.

Figure 19 – "Variable activity" panel, where the user is capable of highlighting which variables are active constraints and inputting values for them. If an active constraint is a nonlinear constraint, the user must pair this variable with a decision variable (MV) to consume a degree of freedom.

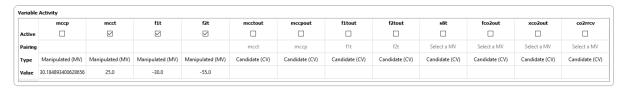
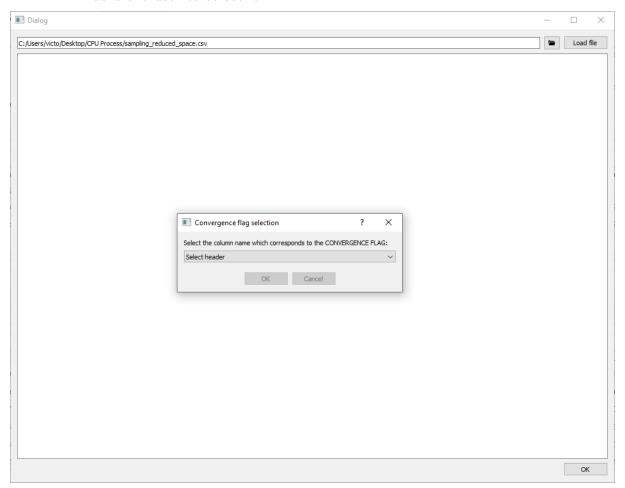


Figure 20 – Loading a \*.csv file in containing design of experiments data in *Metacontrol*: if the user chooses this option, he must provide a file containing all variables selected from the first step ("Load variables" under "Load simulation" tab). the convergence flag is used as a header to map the \*.csv, and the software asks the user to select it.



Dialog Load file C:/Users/Victor Alves/Desktop/Metacontrol/sampling\_reduced\_space.csv f1tout fco2in fluegas mcctout fco2out mccpout П ~  $\checkmark$  $\checkmark$  $\checkmark$  $\overline{}$  $\checkmark$  $\overline{}$  $\checkmark$  $\overline{\phantom{a}}$  $\overline{\phantom{a}}$  $\overline{\phantom{a}}$  $\checkmark$  $\checkmark$ Select alias mccp fluegas тсср mcct f1t f2t mcctout mccpout f1tout f2tout s8t fco2out fco2in mccp mcct 717.3752064 29,9997986 25 -30 -55 25 29,9998015 -30 -55 -55.8745660 600.5789880 621,9591060 ok 717,2142962 30.0100542 -30 -55 25 30.0100571 -30 -55 -55.8567178 600.5101880 621.8488290 ok 716.8474607 29.9876505 -30 -55 25 29.9876534 -30 -55 -55.8957245 600.1672120 621,5408260 fluegas mcctout ok 717,4417649 30.0380832 -30 -55 25 30.0380862 -30 -55 -55.8080830 600.7494710 622,0362110 ok 717,4930376 30.0132530 -30 -55 25 30.0132560 -30 -55 -55.8511604 600.7323150 622,0778770 ok 0.8241155 717.3574487 30.0629039 -30 -55 25 30.0629069 -30 -55 -55.7651662 600.7403370 621,9669000 ok 0.8240231 716.8809101 29.9859683 -30 -55 25 29.9859713 -30 -55 -55.8986635 600.1542980 621,5444590 ok 0.8236419 717.0694893 29,9744622 -30 -55 25 29,9744651 -30 -55 -55.9187565 600.2301870 621,6696940 ok 0.8241965 717,2345909 30.0489494 -30 -55 25 30.0489523 -30 -55 -55.7892747 600.6179180 621.8685100 ok 0.8244029 717.2827362 30.0600016 -30 -55 25 30.0600045 -30 -55 -55,7701710 600.7134100 621.9309590 10 ok 0.8238345 716,9571878 30.0226309 -30 -55 25 30.0226338 -30 -55 -55.8348787 600.2731940 621.5916750 11 ok 0.8243741 717.0216489 30.0019252 -30 -55 25 30.0019281 -30 -55 -55.8708540 600.3596460 621.7016840 12 ok 0.8238086 717.1551182 30.0297985 -30 -55 25 30.0298015 -30 -55 -55.8224453 600.4512630 621.7606730 13 ok 0.8243198 717.1065279 30.0175508 -30 -55 25 30.0175538 -30 -55 -55.8436883 600.4579970 621.7698360 ok 0.8239824 717.1240973 30.0455173 -30 -55 25 30.0455202 -30 -55 -55.7952162 600,4862340 621.7512240 15 ok 0.8239162 716.9841997 30.0670225 -30 -55 25 30.0670254 -30 -55 -55.7580631 600.4077980 621.6232930 ok 0.8237137 716.9047673 30.0555131 -30 -55 25 30.0555160 -30 -55 -55.7779386 600.2856460 621.5340990 17 ok 0.8236648 717.4398718 -30 -55 25 29.9932680 -30 -55 -55.8859502 600.5860840 621.9931060 ok 0.8237651 717.3206409 30.0343753 -30 -55 25 30.0343783 -30 -55 -55.8145131 600.5937850 621.8998130 19 ok 0.8242450 717.5248326 29.9771723 -30 -55 25 29.9771752 -30 -55 -55.9140102 600.7061010 622,1250300

Figure 21 – Associating each alias created in *Metacontrol* to each column of the \*.csv data.

Figure 22 – "Differential data" input screen: Reduced space model training, Differentiation method, and gradient/hessian evaluation.

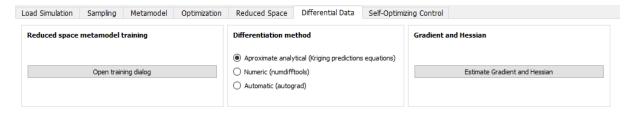
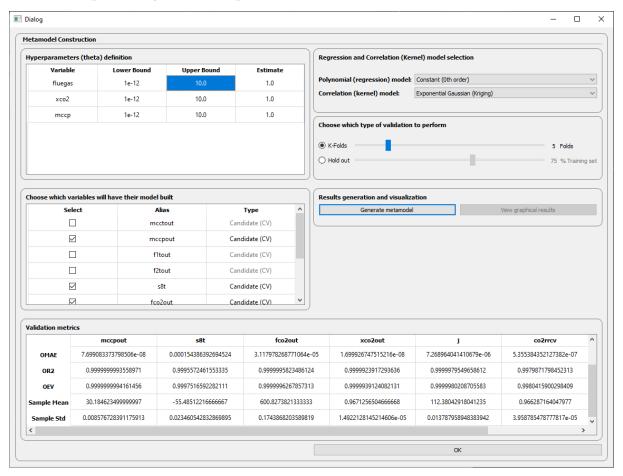


Table 6 – Best Self-Optimizing Control variables found by *Metacontrol* for a single measurement policy.

CV Candidate	Worst-Case	Average-Case
alias	Loss $(kWh/tCO_2)$	Loss $(kWh/tCO_2)$
mccpout	0.0097	0.0011
s8t	0.0125	0.0014
xco2out	0.0458	0.0051
co2rrcv	0.0549	0.0061
fco2out	15.5916	1.7324

Note: Description for the variables aliases present in Table 1.

Figure 23 – Generating reduced space metamodel for CPU process: to avoid redundancy, the variables "f1tout", "f2tout", and "mcctout" were not chosen in the reduced space problem since they correspond to the decision variables that were found as active constraints. In general, if the user decides to remove any variable previously set in the problem, he must uncheck the undesired variable.



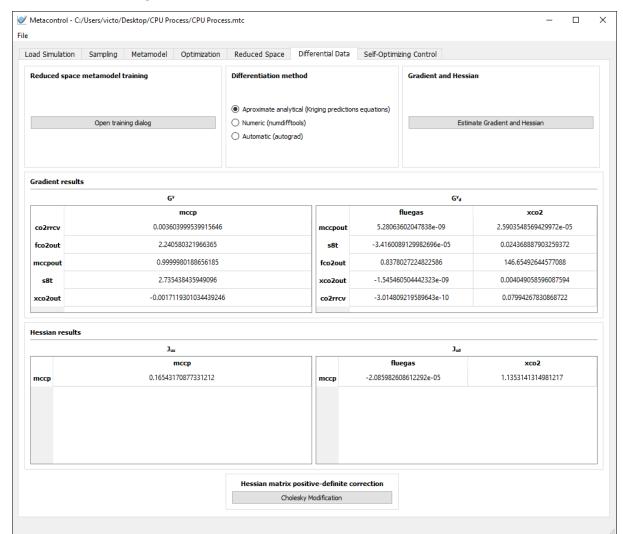


Figure 24 – Differential data estimated in Metacontrol

Metacontrol - C:/Users/victo/Desktop/CPU Process/CPU Process.mtc Load Simulation | Sampling | Metamodel | Optimization | Reduced Space | Differential Data | Self-Optimizing Control Disturbances magnitude Measurements error 35.8595 fluegas 0.001 co2rrcv 0.05 0.01 xco2 fco2out 0.01 mccpout 0.5 s8t 0.001 Subsets sizing options Size 1 Size 2 Size 3 Size 5 Subset number 5 10 Generate results

Figure 25 – Input screen in Metacontrol "Self-Optimizing Control "  ${\it tab}$  - CPU Process

Figure 26 – Best control structure in worst-case loss ascending order, for subsets of size 1 (single measurement policy)

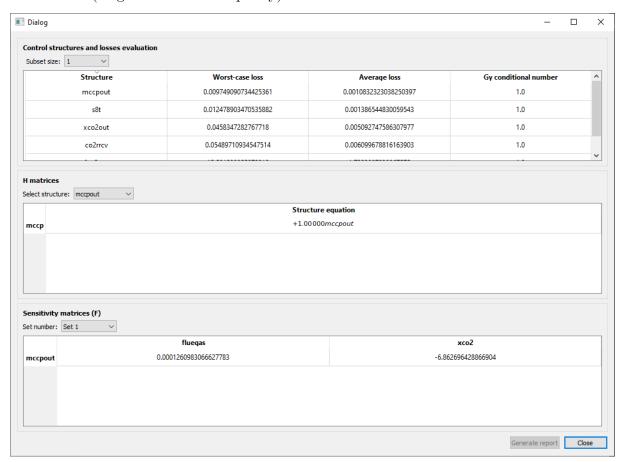
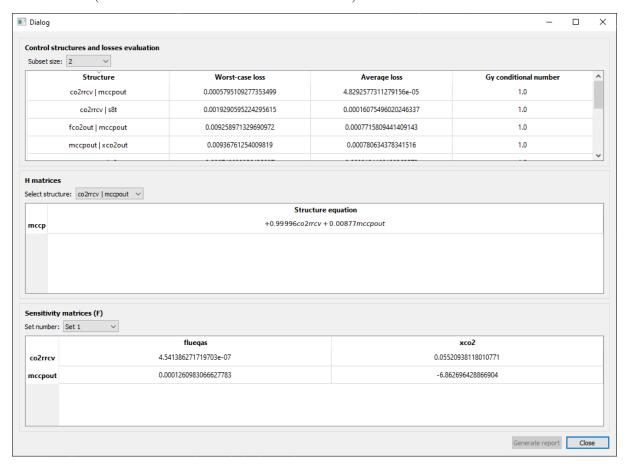


Figure 27 – Best control structure in worst-case loss ascending order, for subsets of size 2 (linear combinations of measurements)



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## APPENDIX A - Quisque libero justo

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# APPENDIX B – Nullam elementum urna vel imperdiet sodales elit ipsum pharetra ligula ac pretium ante justo a nulla curabitur tristique arcu eu metus

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## ANNEX A - Morbi ultrices rutrum lorem.

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## ANNEX B – Cras non urna sed feugiat cum sociis natoque penatibus et magnis dis parturient montes nascetur ridiculus mus

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### ANNEX C - Fusce facilisis lacinia dui

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