

# Advanced Control Systems: RPP manipulator

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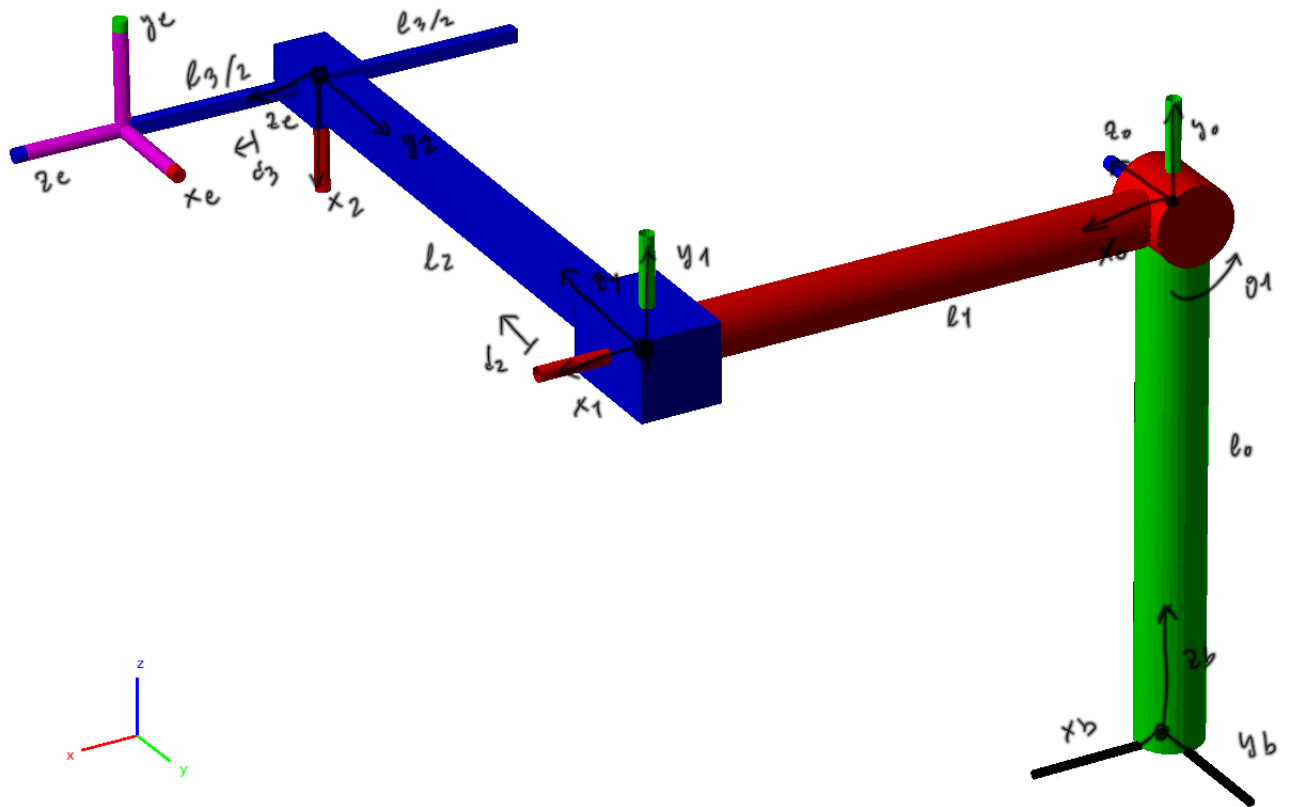
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# 1 Kinematics

## 1.1 Direct Kinematics



Lets define the DH table for our manipulator:

$\Sigma_i$	$d_i$	$\theta_i$	$a_i$	$\alpha_i$
$b - 0$	$\ell_0$	0	0	$\frac{\pi}{2}$
$0 - 1$	0	$\theta_1$	$\ell_1$	0
$1 - 2$	$\ell_2 + d_2$	$\frac{\pi}{2}$	0	$\frac{\pi}{2}$
$2 - 3$	$\ell_3 + d_3$	$\frac{\pi}{2}$	0	0
$3 - e$	0	0	0	0

The homogenous transformation is defined according to the following matrix and calculated for each row of the DH table. By multiplying  $H_0^b H_1^0 H_2^1 H_3^2 H_e^3$  we obtain the final transformation

$$H_i^{i-1}(q_i) = \begin{bmatrix} c_{\theta_i} & -s_{\theta_i}c_{\alpha_i} & s_{\theta_i}s_{\alpha_i} & a_i c_{\theta_i} \\ s_{\theta_i} & c_{\theta_i}c_{\alpha_i} & -c_{\theta_i}s_{\alpha_i} & a_i s_{\theta_i} \\ 0 & s_{\alpha_i} & c_{\alpha_i} & d_i \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$\begin{aligned}
H_0^b &= \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 0 & -1 & 0 \\ 0 & 1 & 0 & \ell_0 \\ 0 & 0 & 0 & 1 \end{bmatrix} & H_1^0(\theta_1) &= \begin{bmatrix} c_1 & -s_1 & 0 & \ell_1 c_1 \\ s_1 & c_1 & 0 & \ell_1 s_1 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} & H_2^1(d_2) &= \begin{bmatrix} 0 & 0 & 1 & 0 \\ 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & d_2 + \ell_2 \\ 0 & 0 & 0 & 1 \end{bmatrix} \\
H_3^2(d_3) &= \begin{bmatrix} 0 & -1 & 0 & 0 \\ 1 & 0 & 0 & 0 \\ 0 & 0 & 1 & d_3 + \ell_3 \\ 0 & 0 & 0 & 1 \end{bmatrix} & H_e^3 &= \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \\
H_e^b(\mathbf{q}) &= \begin{bmatrix} 0 & -s_1 & c_1 & c_1(\ell_1 + \ell_3 + d_3) \\ -1 & 0 & 0 & -\ell_2 - d_2 \\ 0 & -c_1 & s_1 & s_1(\ell_1 + \ell_3 + d_3) + \ell_0 \\ 0 & 0 & 0 & 1 \end{bmatrix}
\end{aligned}$$

## 1.2 Inverse Kinematics

Let's consider the position of ee with respect of the base frame to calculate the value of the joints.

$$p_e^b = \begin{bmatrix} x \\ y \\ z \end{bmatrix} = \begin{bmatrix} c_1(\ell_1 + \ell_3 + d_3) \\ -\ell_2 - d_2 \\ s_1(\ell_1 + \ell_3 + d_3) + \ell_0 \\ 1 \end{bmatrix}$$

It is easy to see that

$$d_2 = -\ell_2 - y$$

$$\theta_1 = \text{Atan2}(z - \ell_0, x)$$

For  $d_3$  we can apply sum of squares and the result is:

$$d_3 = -\ell_1 \pm \sqrt{x^2 + (z - \ell_0)^2} - \ell_3$$

## 2 Jacobians

### 2.1 Geometric Jacobians

The geometric jacobian is defined as follow with  $\mathbf{q} = [\theta_1, d_2, d_3]^\top$ . Note that the matlab robotic toolbox defines the angular velocities above the linear velocities:

$$\begin{bmatrix} \dot{x} \\ \dot{y} \\ \dot{z} \\ \dot{\omega}_x \\ \dot{\omega}_y \\ \dot{\omega}_z \end{bmatrix} = \begin{bmatrix} J_{P_1} & J_{P_2} & J_{P_3} \\ J_{O_1} & J_{O_2} & J_{O_3} \end{bmatrix} \begin{bmatrix} \dot{\theta}_1 \\ \dot{d}_2 \\ \dot{d}_3 \end{bmatrix}$$

$$\begin{aligned}
J_{P_1} = z_0 \times (d_e^0 - d_0^0) &= \begin{bmatrix} -s_1(\ell_1 + \ell_3 + d_3) \\ 0 \\ c_1(\ell_1 + \ell_3 + d_3) \end{bmatrix} & J_{O_1} = z_0 &= \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} \\
J_{P_2} = z_1 &= \begin{bmatrix} 0 \\ -1 \\ 0 \end{bmatrix} & J_{O_2} &= \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} \\
J_{P_3} = z_2 &= \begin{bmatrix} c_1 \\ 0 \\ s_1 \end{bmatrix} & J_{O_3} &= \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}
\end{aligned}$$

We can finally put all the pieces together and obtain the final geometric jacobian:

$$J(\mathbf{q}) = \begin{bmatrix} -s_1(\ell_1 + \ell_3 + d_3) & 0 & c_1 \\ 0 & -1 & 0 \\ c_1(\ell_1 + \ell_3 + d_3) & 0 & s_1 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \\ 1 & 0 & 0 \end{bmatrix}$$

## 2.2 Analytical Jacobian

The analytical jacobian can be easily calculated by using partial derivatives of  $p_e^b$

$$p_e^b = \begin{bmatrix} x \\ y \\ z \end{bmatrix} = \begin{bmatrix} c_1(\ell_1 + \ell_3 + d_3) \\ -\ell_2 - d_2 \\ s_1(\ell_1 + \ell_3 + d_3) + \ell_0 \\ 1 \end{bmatrix}$$

Finally we end up with the analytical jacobian

$$J_a(\mathbf{q}) = \begin{bmatrix} -s_1(\ell_1 + \ell_3 + d_3) & 0 & c_1 \\ 0 & -1 & 0 \\ c_1(\ell_1 + \ell_3 + d_3) & 0 & s_1 \\ 1 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix}$$

Another possibility is to use the relation between the geometric and analytical jacobian as follow using ZYZ:

$$\omega_e = T(\phi_e)\dot{\phi}_e \quad T(\phi_e) = \begin{bmatrix} 0 & -s_\varphi & c_\varphi s_\theta \\ 0 & c_\varphi & s_\varphi s_\theta \\ 1 & 0 & c_\theta \end{bmatrix}$$

$$J(\mathbf{q}) = T_A(\phi_e)J_A(\mathbf{q})$$

$$T_A(\phi_e) = \begin{bmatrix} \mathbb{I}_3 & \mathcal{O}_3 \\ \mathcal{O}_3 & T(\phi_e) \end{bmatrix}$$