Furuta Pendulum Virtual Laboratory Experiment

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May 21, 2021

This paper will follow the structure presented in the assignment. All the Matlab code and file used will be also provided through the following link: https://github.com/fil-bad/Furuta_pendulum.

Part II

Derivation of the model

1 From Lagrange equation to mechanical models

Without going much deeper, we have one main equation for the Lagrangian mechanics:

$$L\left(q\left(t\right),\dot{q}\left(t\right)\right)=T\left(q\left(t\right),\dot{q}\left(t\right)\right)-V\left(q\left(t\right)\right)$$

while the generalized coordinates in our case are: $(q, \dot{q}) = ([\theta(t) \quad \alpha(t)], [\dot{\theta}(t) \quad \dot{\alpha}(t)])$. In our case, the Lagrangian equation is:

$$L = \frac{1}{2}J_{arm}\dot{\theta}^2 + \frac{1}{2}J_p\dot{\alpha}^2 + \frac{1}{2}m_p\left(-\cos\left(\theta\right)\sin\left(\alpha\right)\dot{\theta}l_p - \sin\left(\theta\right)\cos\left(\alpha\right)\dot{\alpha}l_p - \sin\left(\theta\right)\dot{\theta}r\right)^2 + \frac{1}{2}m_p\left(-\sin\left(\theta\right)\sin\left(\alpha\right)\dot{\theta}l_p + \cos\left(\theta\right)\cos\left(\alpha\right)\dot{\alpha}l_p + \cos\left(\theta\right)\dot{\theta}r\right)^2 + \frac{1}{2}m_p\sin\left(\alpha\right)^2\dot{\alpha}^2l_p^2 + m_p\cos\left(\alpha\right)gl_p$$

Finally, the Euler-Lagrange equation can be expressed as:

$$\frac{d}{dt}\frac{\partial L}{\partial \dot{q}} - \frac{\partial L}{\partial q} = \tau$$

For this reason, we get two equations in column:

$$\begin{bmatrix} \frac{d}{dt} \frac{\partial L}{\partial \dot{\theta}} - \frac{\partial L}{\partial \theta} \\ \\ \frac{d}{dt} \frac{\partial L}{\partial \dot{\alpha}} - \frac{\partial L}{\partial \alpha} \end{bmatrix} = \tau$$

For this reason, we can calculate each partial derivative of the Lagrangian equation, that are:

$$\frac{\partial L}{\partial \theta} = m_p \left(-\cos(\theta)\sin(\alpha)\dot{\theta}l_p - \sin(\theta)\cos(\alpha)\dot{\alpha}l_p - \sin(\theta)\dot{\theta}r \right) \left(\sin(\theta)\sin(\alpha)\dot{\theta}l_p - \cos(\theta)\cos(\alpha)\dot{\alpha}l_p - \cos(\theta)\dot{\theta}r \right) + m_p \left(-\sin(\theta)\sin(\alpha)\dot{\theta}l_p + \cos(\theta)\cos(\alpha)\dot{\alpha}l_p + \cos(\theta)\dot{\theta}r \right) \left(-\cos(\theta)\sin(\alpha)\dot{\theta}l_p - \sin(\theta)\cos(\alpha)\dot{\alpha}l_p - \sin(\theta)\dot{\theta}r \right) = \dots = -2l_p m_p \sin(\alpha) \left(2\sin(\theta)^2 - 1 \right) \left(r\dot{\theta} + l_p \cos(\alpha)\dot{\alpha} \right) \dot{\theta}$$

$$\frac{\partial L}{\partial \dot{\theta}} = J_{\text{arm}} \dot{\theta} + m_p \left(r \cos \left(\theta \right) + l_p \sin \left(\alpha \right) \sin \left(\theta \right) \right) \left(r \cos \left(\theta \right) \dot{\theta} + l_p \sin \left(\alpha \right) \sin \left(\theta \right) \dot{\theta} + l_p \cos \left(\alpha \right) \cos \left(\theta \right) \dot{\alpha} \right) + \\ + m_p \left(r \sin \left(\theta \right) + l_p \sin \left(\alpha \right) \cos \left(\theta \right) \right) \left(r \sin \left(\theta \right) \dot{\theta} + l_p \cos \left(\alpha \right) \sin \left(\theta \right) \dot{\alpha} + l_p \sin \left(\alpha \right) \cos \left(\theta \right) \dot{\theta} \right) \\ \frac{d}{dt} \left(\frac{\partial L}{\partial \dot{\theta}} \right) = J_{\text{arm}} \ddot{\theta} + l_p^2 m_p \ddot{\theta} + m_p r^2 \ddot{\theta} - l_p^2 m_p \sin \left(2\theta \right) \dot{\alpha}^2 - l_p^2 m_p \cos \left(\alpha \right)^2 \ddot{\theta} - l_p m_p r \sin \left(\alpha \right) \dot{\alpha}^2 + l_p m_p r \cos \left(\alpha \right) \ddot{\alpha} - \\ - 4 l_p m_p r \sin \left(\alpha \right) \dot{\theta}^2 + 8 l_p m_p r \sin \left(\alpha \right) \cos \left(\theta \right)^2 \dot{\theta}^2 + 4 l_p^2 m_p \cos \left(\alpha \right)^2 \cos \left(\theta \right) \sin \left(\theta \right) \dot{\alpha}^2 + 4 l_p^2 m_p \cos \left(\alpha \right) \sin \left(\alpha \right) \cos \left(\theta \right) \dot{\theta} \dot{\alpha} \\ + 4 l_p m_p r \sin \left(\alpha \right) \cos \left(\theta \right) \sin \left(\theta \right) \ddot{\theta} + 2 l_p^2 m_p \cos \left(\alpha \right) \sin \left(\alpha \right) \cos \left(\theta \right) \sin \left(\theta \right) \ddot{\alpha} + 4 l_p m_p r \cos \left(\alpha \right) \cos \left(\theta \right) \sin \left(\theta \right) \dot{\theta} \dot{\alpha} \end{aligned}$$

Once calculated, we can assemble the two equations to get:

$$\begin{split} \frac{d}{dt}\frac{\partial L}{\partial \dot{\theta}} - \frac{\partial L}{\partial \theta} &= \qquad J_{\text{arm}}\ddot{\theta} + l_p^2 m_p \ddot{\theta} + m_p r^2 \ddot{\theta} - l_p^2 m_p \sin{(2\theta)}\,\dot{\alpha}^2 - l_p^2 m_p \cos{(\alpha)}^2 \,\ddot{\theta} - l_p m_p r \sin{(\alpha)}\,\dot{\alpha}^2 + l_p m_p r \cos{(\alpha)}\,\ddot{\alpha} - \\ &- \qquad \qquad - 2 l_p m_p r \sin{(\alpha)}\,\dot{\theta}^2 + l_p^2 m_p \sin{(2\alpha)}\,\dot{\theta}\dot{\alpha} + 4 l_p m_p r \sin{(\alpha)}\cos{(\theta)}^2 \,\dot{\theta}^2 + 4 l_p^2 m_p \cos{(\dot{\alpha})}^2 \cos{(\theta)}\sin{(\theta)}\,\dot{\alpha}^2 + \\ &+ \qquad 4 l_p m_p r \sin{(\alpha)}\cos{(\theta)}\sin{(\theta)}\,\ddot{\theta} + 2 l_p^2 m_p \cos{(\alpha)}\sin{(\alpha)}\cos{(\theta)}\sin{(\theta)}\,\ddot{\alpha} + 4 l_p m_p r \cos{(\alpha)}\cos{(\theta)}\sin{(\theta)}\,\dot{\theta}\dot{\alpha} \end{split}$$

The same can be done for the $\alpha(t)$ variable, leading to the equation:

$$\begin{split} \frac{\partial L}{\partial \alpha} &= m_p \sin{(\alpha)} \, l_p^2 \cos{(\alpha)} \, \dot{\theta}^2 + 2 m_p r \cos{(\theta)} \sin{(\theta)} \, l_p \cos{(\alpha)} \, \dot{\theta}^2 + 4 m_p \cos{(\theta)} \sin{(\theta)} \, l_p^2 \cos{(\alpha)}^2 \, \dot{\theta} \dot{\alpha} - \\ &- 2 m_p \cos{(\theta)} \sin{(\theta)} \, l_p^2 \dot{\theta} \dot{\alpha} - m_p r \sin{(\alpha)} \, l_p \dot{\theta} \dot{\alpha} - g m_p \sin{(\alpha)} \, l_p \\ \frac{\partial L}{\partial \dot{\alpha}} &= J_p \dot{\alpha} + l_p^2 m_p \dot{\alpha} + l_p m_p r \cos{(\alpha)} \, \dot{\theta} + \frac{1}{2} l_p^2 m_p \sin{(2\alpha)} \sin{(2\theta)} \, \dot{\theta} \\ \frac{d}{dt} \left(\frac{\partial L}{\partial \dot{\alpha}} \right) &= J_p \ddot{\alpha} + l_p^2 m_p \ddot{\alpha} + l_p m_p r \cos{(\alpha)} \, \ddot{\theta} + l_p^2 m_p \cos{(\alpha)} \sin{(\alpha)} \sin{(2\theta)} \, \ddot{\theta} + \\ &+ l_p^2 m_p \sin{(2\theta)} \left(2 \cos{(\alpha)}^2 - 1 \right) \dot{\theta} \dot{\alpha} - l_p m_p r \sin{(\alpha)} \, \dot{\theta} \dot{\alpha} + 2 l_p^2 m_p \cos{(\alpha)} \sin{(\alpha)} \cos{(2\theta)} \, \dot{\theta}^2 \\ \frac{d}{dt} \frac{\partial L}{\partial \dot{\alpha}} &- \frac{\partial L}{\partial \alpha} = J_p \ddot{\alpha} + l_p^2 m_p \ddot{\alpha} - \frac{1}{2} l_p^2 m_p \sin{(2\alpha)} \, \dot{\theta}^2 + g l_p m_p \sin{(\alpha)} + l_p^2 m_p \sin{(2\alpha)} \cos{(2\theta)} \, \dot{\theta}^2 + \\ &+ l_p m_p r \cos{(\alpha)} \, \ddot{\theta} + \frac{1}{2} l_p^2 m_p \sin{(2\alpha)} \sin{(2\theta)} \, \ddot{\theta} - l_p m_p r \cos{(\alpha)} \sin{(2\theta)} \, \dot{\theta}^2 \end{split}$$

If we equal the $\tau = \begin{bmatrix} \tau_m - B_{arm} \dot{\theta}(t) & -B_p \dot{\alpha}(t) \end{bmatrix}^T$ vector to the results found above, we finally get the non linear model expressed in the equations (7) and (8) of the assignment.

2 Matricial model

Our model can be rewritten in the form:

$$D\left(q\left(t\right)\right)\ddot{q}\left(t\right) + C\left(q\left(t\right),\dot{q}\left(t\right)\right)\dot{q}\left(t\right) + g\left(q\left(t\right)\right) = \tau$$

where the $C(q(t), \dot{q}(t))$ matrix is not uniquely defined due to mixed products in the equations; a possible representation is given by:

$$D = \begin{bmatrix} m_p r^2 + m_p l_p^2 - m_p l_p^2 \cos{(\alpha)}^2 + J_{arm} & m_p \cos{(\alpha)} l_p r \\ m_p \cos{(\alpha)} l_p r & J_p + m_p l_p^2 \end{bmatrix}$$

$$C = \begin{bmatrix} 2m_p \cos{(\alpha)} \dot{\alpha} l_p^2 \sin{(\alpha)} & -m_p \sin{(\alpha)} \dot{\alpha} l_p r \\ -m_p \cos{(\alpha)} \dot{\theta} l_p^2 \sin{(\alpha)} & 0 \end{bmatrix} \quad g = \begin{bmatrix} 0 \\ m_p g \sin{(\alpha)} l_p \end{bmatrix}$$

Part III

Linear System Analysis

1 Linearising the model

The matricial equation is not linear; in fact, each matrix depends from the coordinates q(t) (the angular position of each section of the pendulum) and/or from their derivative $\dot{q}(t)$ (the angular speed). For this reason, we can linearize the model in its two equilibrium points (as we will see from further analysis), the *downward* position and the *upward* position. The resulting system is a linear 2-DOF one that can be analysed through the classical approach for mechanical systems.

1.1 Downward position, $(\theta, \alpha) = (0, 0)$

Substituting the values in the matrices, they become:

$$D = \begin{bmatrix} m_p r^2 + J_{arm} & m_p l_p r \\ m_p l_p r & J_p + m_p l_p^2 \end{bmatrix} C = \begin{bmatrix} 0 & 0 \\ 0 & 0 \end{bmatrix} g = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$

1.2 Upward position, $(\theta, \alpha) = (0, \pi)$

Substituting the values in the matrices, they become:

$$D = \begin{bmatrix} m_p r^2 + J_{arm} & -m_p l_p r \\ -m_p l_p r & J_p + m_p l_p^2 \end{bmatrix} C = \begin{bmatrix} 0 & 0 \\ 0 & 0 \end{bmatrix} g = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$

2 State space representation

Due to the linearization around equilibrium points, both C and g matrices become null ones. In particular, the equations become:

$$D_{(0,0)}\ddot{q}(t) = \tau$$
 , $D_{(0,\pi)}\ddot{q}(t) = \tau$

For this reason, if the matrix D is invertible – that means $\det(D) \neq 0$ –, we can invert it and get an expression for the second order derivatives of q(t):

$$\begin{cases} \ddot{q}_{down}\left(t\right) = D_{(0,0)}^{-1}\tau = \begin{pmatrix} \frac{J_{p} + l_{p}^{2}m_{p}}{l_{p}^{2}J_{arm}m_{p} + r^{2}m_{p}J_{p} + J_{arm}J_{p}} & -\frac{rm_{p}l_{p}}{l_{p}^{2}J_{arm}m_{p} + r^{2}m_{p}J_{p} + J_{arm}J_{p}} \\ -\frac{rm_{p}l_{p}}{l_{p}^{2}J_{arm}m_{p} + r^{2}m_{p}J_{p} + J_{arm}J_{p}} & \frac{r^{2}m_{p} + J_{arm}}{l_{p}^{2}J_{arm}m_{p} + r^{2}m_{p}J_{p} + J_{arm}J_{p}} \end{pmatrix} \begin{pmatrix} \tau_{m} - B_{arm}\dot{\theta}\left(t\right) \\ -B_{p}\dot{\alpha}\left(t\right) \end{pmatrix} \\ \ddot{q}_{up}\left(t\right) = D_{(0,\pi)}^{-1}\tau = \begin{pmatrix} \frac{J_{p} + l_{p}^{2}m_{p}}{l_{p}^{2}J_{arm}m_{p} + r^{2}m_{p}J_{p} + J_{arm}J_{p}} & \frac{rm_{p}l_{p}}{l_{p}^{2}J_{arm}m_{p} + r^{2}m_{p}J_{p} + J_{arm}J_{p}} \\ \frac{rm_{p}l_{p}}{l_{p}^{2}J_{arm}m_{p} + r^{2}m_{p}J_{p} + J_{arm}J_{p}} & \frac{r^{2}m_{p} + J_{arm}J_{p}}{l_{p}^{2}J_{arm}m_{p} + r^{2}m_{p}J_{p} + J_{arm}J_{p}} \end{pmatrix} \begin{pmatrix} \tau_{m} - B_{arm}\dot{\theta}\left(t\right) \\ -B_{p}\dot{\alpha}\left(t\right) \end{pmatrix}$$

We can now introduce the state vectors $\begin{bmatrix} x_1(t) & x_2(t) & x_3(t) & x_4(t) \end{bmatrix}^T = \begin{bmatrix} \theta(t) & \alpha(t) & \dot{\theta}(t) & \dot{\alpha}(t) \end{bmatrix}^T$ and $\begin{bmatrix} x_1(t) & x_2(t) & x_3(t) & x_4(t) \end{bmatrix}^T = \begin{bmatrix} \theta(t) & \alpha(t) - \pi & \dot{\theta}(t) & \dot{\alpha}(t) \end{bmatrix}^T$ for downward and upward positions respectively.

In this case, the systems become (we keep the matrices D in the shortest form, since they have only constants):

$$down: \dot{x} = \begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \dot{x}_3 \\ \dot{x}_4 \end{bmatrix} = \begin{bmatrix} x_3 \\ x_4 \\ D_{(0,0)}^{-1} \begin{pmatrix} \tau_m - B_{arm} x_3 \\ -B_p x_4 \end{pmatrix} \end{bmatrix}, \quad \tau_m = \frac{\eta_g K_g \eta_m K_t \left(u - K_g K_m x_3 \right)}{R_m}$$

$$D^{-1}g = \begin{pmatrix} -\frac{rg \cos(\alpha) \sin(\alpha) m_p^2 l_p^2}{\left(l_p^2 m_p + J_p \right) \left(r^2 m_p + l_p^2 m_p - l_p^2 \cos^2(\alpha) m_p + J_{arm} \right) - r^2 \cos^2(\alpha) m_p^2 l_p^2} \\ \frac{g \sin(\alpha) m_p l_p \left(r^2 m_p + l_p^2 m_p - l_p^2 \cos^2(\alpha) m_p + J_{arm} \right)}{\left(l_p^2 m_p + J_p \right) \left(r^2 m_p + l_p^2 m_p - l_p^2 \cos^2(\alpha) m_p + J_{arm} \right) - r^2 \cos^2(\alpha) m_p^2 l_p^2} \end{pmatrix}$$