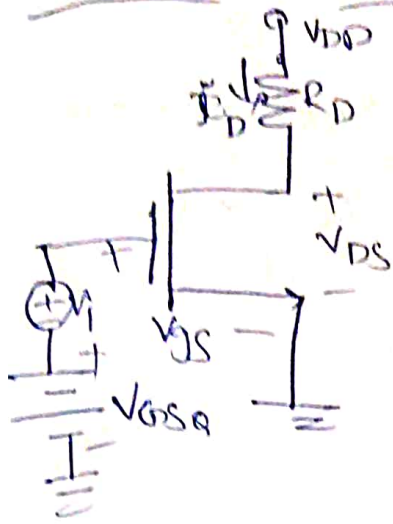


MOSFET Amplifier

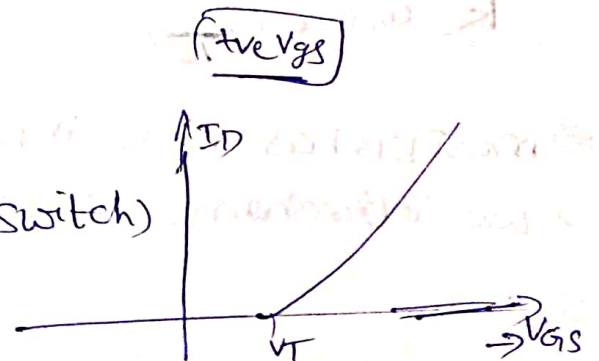
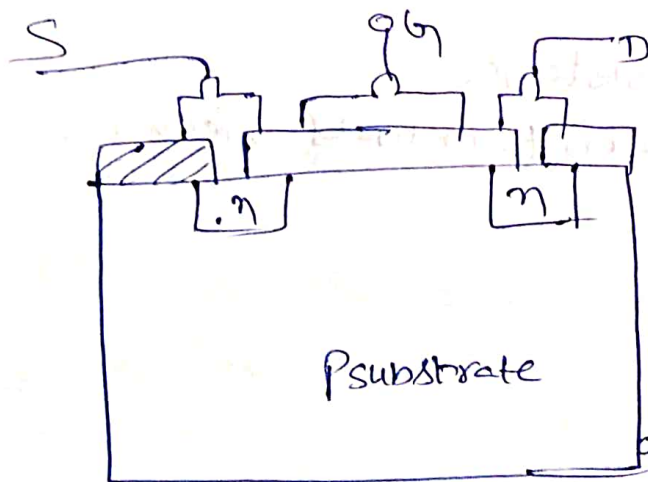
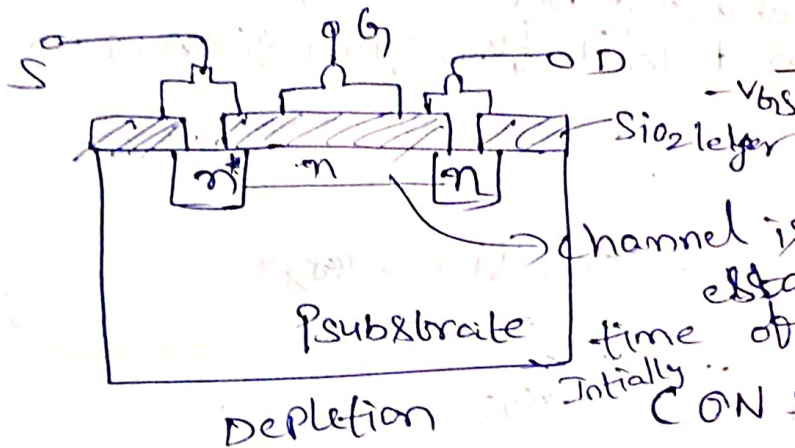
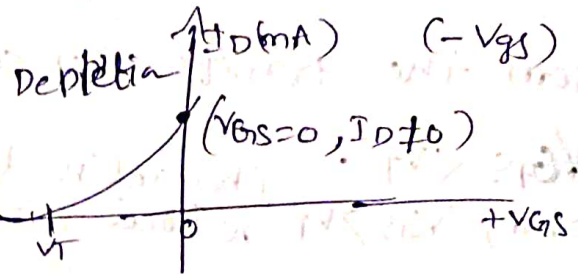


High input resistance due to oxide layer.

MOSFET

- (1) Depletion MOSFET
- (2) Enhancement MOSFET

Transfer characteristics

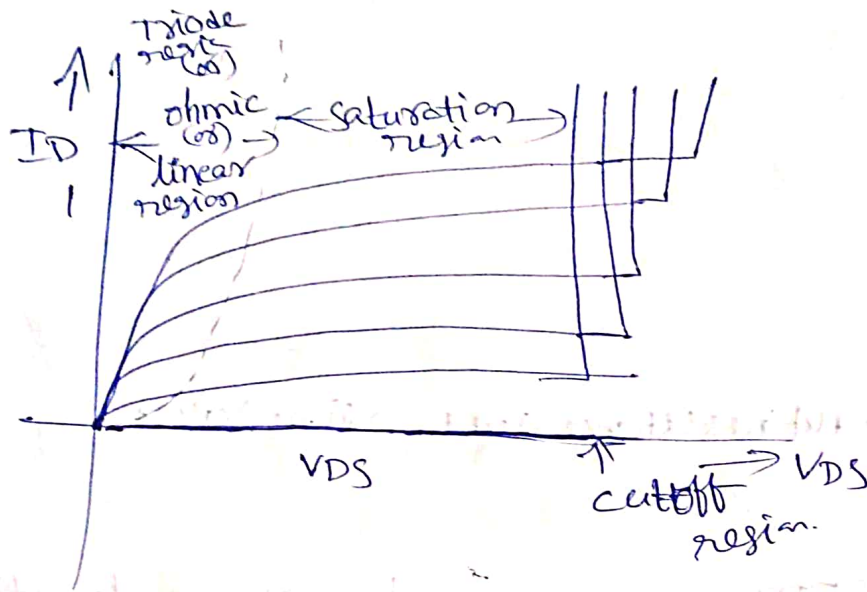


$$I_D = K (V_{GS} - V_T)^2$$

only enhancement mode
constant, it is depend on oxide & construction of MOSFET

Enhancement MOSFET. Initially "no channel" is present. channel is induced i.e. channel is developed by applying greater than ~~the~~ Threshold voltage $V_{GS} > V_T$

Drain characteristics (or) characteristics

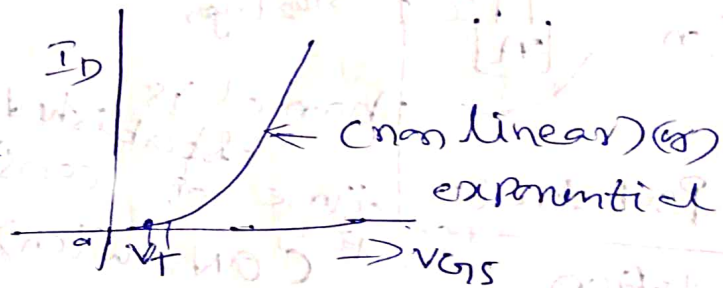


From the transfer characteristics Drain current is zero

When $V_{GS} < V_T$, channel is established between S & Drain.
 When $V_{GS} > V_T$, Drain current will flow from source to drain. Then I_D

$$I_D = K (V_{GS} - V_T)^2$$

$$K = \mu_n C_{ox} \left(\frac{W}{L} \right)$$



⇒ MOSFETs has high input resistance

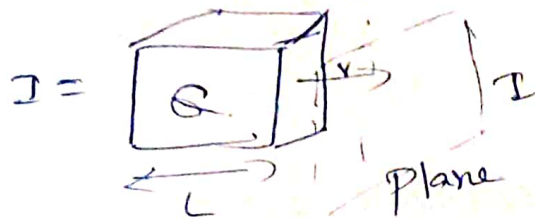
→ we interchange source & drain terminals vice versa

→

MOSFET Drain Current

or MOSFET acts like capacitor
Capacitor charge $Q = CV$

$$= C(V - V_t) \quad (\text{threshold voltage})$$



$$I = \frac{Q}{\Delta t} \quad \Delta t \text{ is time taken to cross the plane}$$

$$\Delta t = \frac{\text{length of cube}}{\text{velocity of charge}}$$

$$I = \frac{Q}{L} \vec{V}_a$$

$$\frac{1}{L} Q = CV = C(V - V_t)$$

$$I = \frac{C(V - V_t)}{L} \vec{V}_a$$

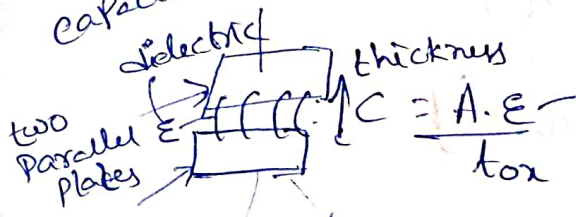
Semiconductor V_a =

$$\text{velocity of charge } V_a = \mu_q E \quad \begin{matrix} \text{mobility of charge particle} \\ \text{electric field} \end{matrix}$$

$$= I = \frac{C(V - V_t)}{L}$$

$$= \frac{\text{capacitance } C(V_{gc} - V_t) \mu E}{L}$$

capacitance



$$C = \frac{A \cdot \epsilon}{\text{thickness}} = \frac{\text{Area times the dielectric}}{\text{thickness of plates or distance between plates}}$$

$$\text{Area} = \text{width} \times \text{length} = W \cdot L$$

$$\text{then } C = \frac{W \cdot L \cdot \epsilon}{\text{tox}}$$

$$= \frac{WLE}{L \cdot C_{ox}} \mu_n$$

$$= \frac{WLE}{(L \cdot C_{ox})} \mu_n (V_{gs} - V_t)$$

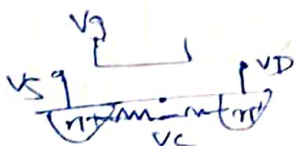
$$= \mu_n C_{ox}$$

$$I = W C_{ox} \mu_n (V_{gs} - V_t)$$

$$\text{Electric field} = E = \frac{V_{DS}}{L}$$

$$I = \mu_n C_{ox} \cdot \frac{W}{L} V_{DS} (V_{gs} - V_t)$$

V_{gs} = voltage between channel and gate.



$$V_c = \frac{V_s + V_d}{2}$$

$$V_c = \frac{V_s}{2} + \frac{V_d}{2} + \left(\frac{V_s}{2} - \frac{V_d}{2} \right)$$

$$I_{DS} = \mu_n C_{ox} \frac{W}{L} V_{DS} \left(V_{gs} - \left(\frac{V_s}{2} + \frac{V_d}{2} - \frac{V_d}{2} \right) - V_t \right)$$

$$= \mu_n C_{ox} \frac{W}{L} V_{DS} \left(V_{gs} - V_s - \frac{1}{2} V_{DS} - V_t \right)$$

$$= \mu_n C_{ox} \frac{W}{L} V_{DS} \left(V_{gs} - \frac{1}{2} V_{DS} - V_t \right)$$

$$I_{DS} = \mu_n C_{ox} \frac{W}{L} \left[(V_{gs} - V_t) V_{DS} - \frac{1}{2} V_{DS}^2 \right]$$

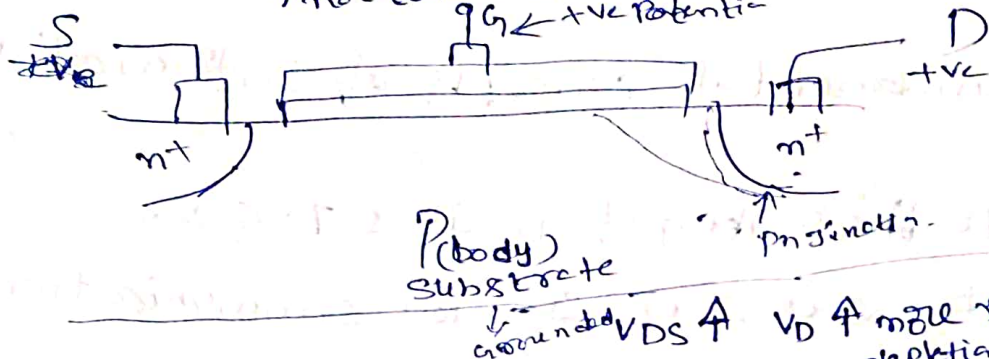
$$I_{DS} = K_n \left[(V_{gs} - V_t) V_{DS} - \frac{1}{2} V_{DS}^2 \right] \quad (\text{In saturation region})$$

$$\text{let } K_n = \mu_n C_{ox} \frac{W}{L}$$

Drain Current in channel length modulation

$$I_D = \frac{1}{2} \mu_n \text{cox} \frac{W}{L} (V_{GS} - V_t)^2$$

I_D is not dependent on V_{DS} . I_D is perfect current source.
 I_D is independent of V_{DS} . So it is perfect current source.
 $I_D = \text{constant}$ (Perfect current source)
 1 not ~~entirely~~ correct why means observe constant of MOSFET



$V_{DS} > V_t$
 $V_{DS} > V_t$ channel width form

$$L \downarrow I_D \uparrow$$

$V_D \uparrow$ more reverse bias \uparrow
 depletion region at J_n is thick
 so channel is going to reduce.
 channel length reduces \downarrow

channel length modulation

$$I_D = \frac{1}{2} \mu_n \text{cox} \frac{W}{L} (V_{GS} - V_t)^2$$

$$L \downarrow I_D \uparrow$$

$$I_D = \frac{1}{2} \mu_n \text{cox} \frac{W}{L - \Delta L} (V_{GS} - V_t)^2$$



$$= \frac{1}{2} \mu_n \text{cox} \frac{W}{L (1 - \frac{\Delta L}{L})} (V_{GS} - V_t)^2$$

$$= \frac{1}{2} \mu_n \text{cox} \frac{W}{L} (1 - \frac{\Delta L}{L})^{-1} (V_{GS} - V_t)^2$$

$$= \frac{1}{2} \mu_n \text{cox} \frac{W}{L} (1 + \frac{\Delta L}{L}) (V_{GS} - V_t)^2$$

$$= \frac{1}{2} \mu_n \text{cox} \frac{W}{L} (V_{GS} - V_t)^2 (1 + \lambda V_{DS})$$

$$I_D = \frac{1}{2} \mu_n \text{cox} \frac{W}{L} (V_{GS} - V_t)^2 (1 + \lambda V_{DS})$$

$$\Delta L \propto V_{DS}$$

$$\frac{\Delta L}{L} \propto \frac{V_{DS}}{L}$$

$$\frac{\Delta L}{L} = C \frac{V_{DS}}{L} \text{ constant}$$

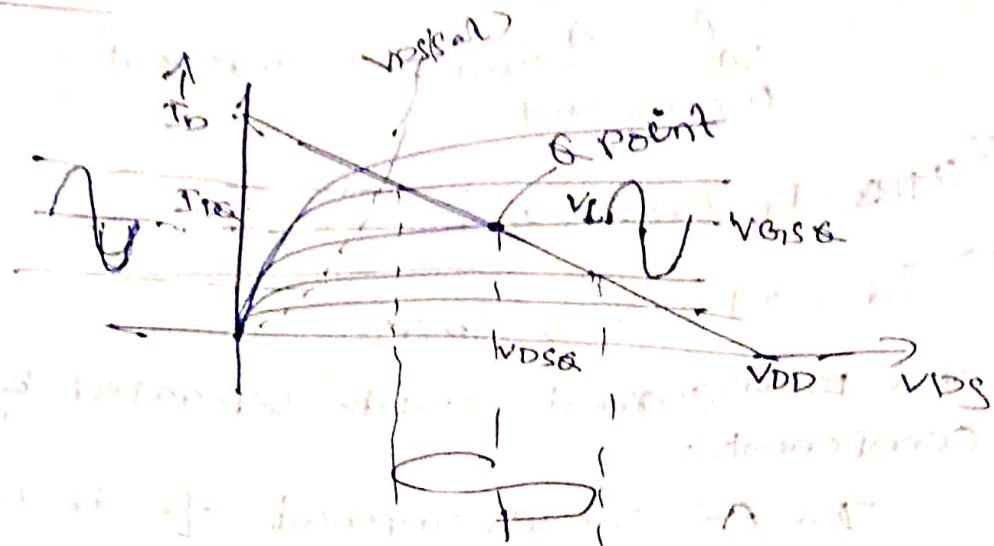
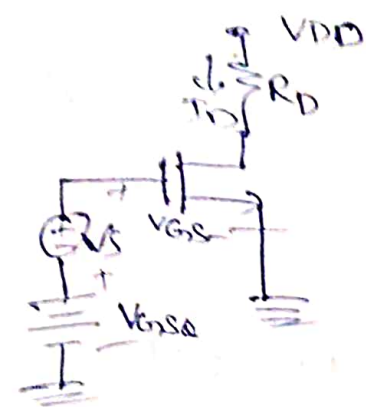
$$\frac{\Delta L}{L} = \lambda V_{DS}$$

$$\because \frac{C}{L} = \lambda$$

$$\lambda = V_t^{-1}$$

Graphical Analysis, Load lines and small signal parameters

common source amplifier characteristics



from

above figs

$$V_{GS} = V_{GSQ} + v_i = V_{GSQ} + v_{gs} \quad \rightarrow (1)$$

\downarrow DC component \downarrow AC component

$$I_D = K_n (V_{GS} - V_{TN})^2 \quad \rightarrow (2)$$

substitute eq(1) into eq(2) then

$$\begin{aligned}
 I_D &= K_n (V_{GSQ} + v_{gs} - V_{TN})^2 \\
 &= K_n (V_{GSQ} - V_{TN} + v_{gs})^2 \\
 &= K_n (V_{GSQ} - V_{TN})^2 + 2K_n (V_{GSQ} - V_{TN}) \cdot v_{gs} + K_n v_{gs}^2
 \end{aligned}$$

(1) (2) (3)

① term indicates DC (or) quiescent drain current I_{DQ} .

② term indicates time varying drain component that is linearly related to v_{gs} (AC component)

③ square of signal voltage, but it produces harmonics (or) nonlinear distortion.

To minimize nonlinear distortion we require

$$v_{gs} \ll 2(V_{GSQ} - V_{TN})$$

Then we neglecting v_{gs}^2 term hence it is small

Compared to $(V_{GSQ} - V_{TN})$

Then

$$i_D = I_{DQ} + i_d$$

\uparrow \uparrow
 I_{DQ} 2nd term (AC component)
DC component

$$I_{DQ} = K_n (V_{GSQ} - V_{TN})^2$$

$$i_d = 2K_n (V_{GSQ} - V_{TN}) v_{gs}$$

Total drain current can be separated into a DC & AC component.

The AC (or) AC component of drain current is

$$i_d = 2K_n (V_{GSQ} - V_{TN}) v_{gs}$$

$$\frac{i_d}{v_{gs}} = 2K_n (V_{GSQ} - V_{TN})$$

$$g_m = \frac{\text{output current}}{\text{input voltage}} = \text{transconductance}$$

$$= \frac{i_d}{v_{gs}} = 2K_n (V_{GSQ} - V_{TN})$$

(or) we can derive transconductance can be obtained from the derivative

$$g_m = \left. \frac{\partial i_D}{\partial V_{GS}} \right|_{V_{GS} = \text{Constant}}$$

$$= \frac{\partial}{\partial v_{gs}} (2K_n (V_{GSQ} - V_{TN}) v_{gs})$$

$$= 2K_n (V_{GSQ} - V_{TN})$$

$$g_m = 2\sqrt{K_n I_{DQ}}$$