

28th Nordic Seminar on Computational Mechanics

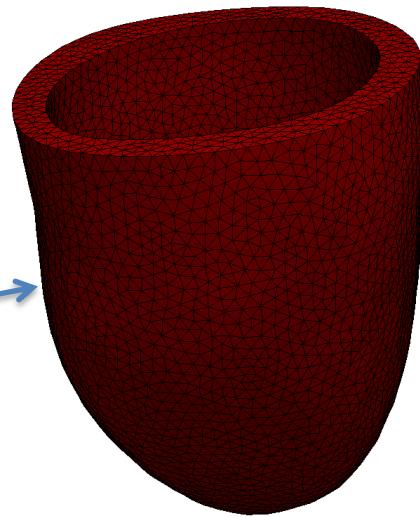
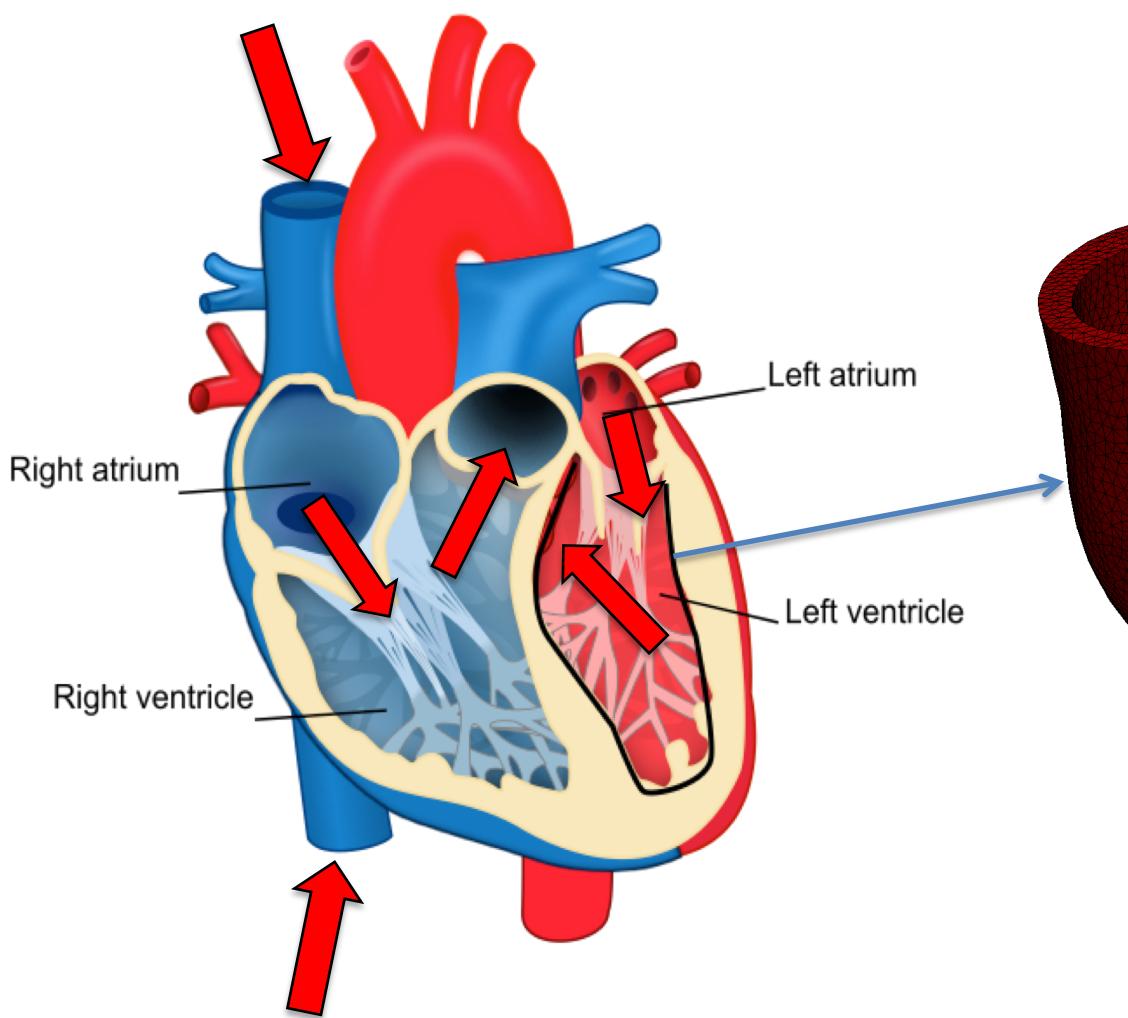
Personalization of a Cardiac Computational Model using Clinical Measurements

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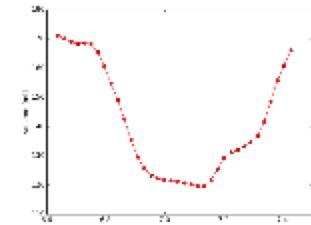
October 23, 2015



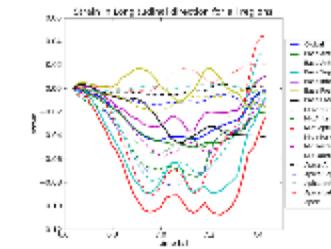
The heart is muscular organ that pumps blood through the blood vessels to the organs and the tissue in the body



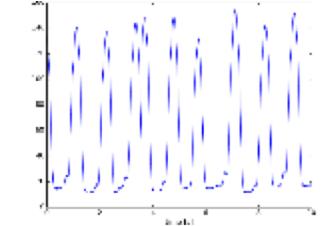
LV Volume



LV Strain

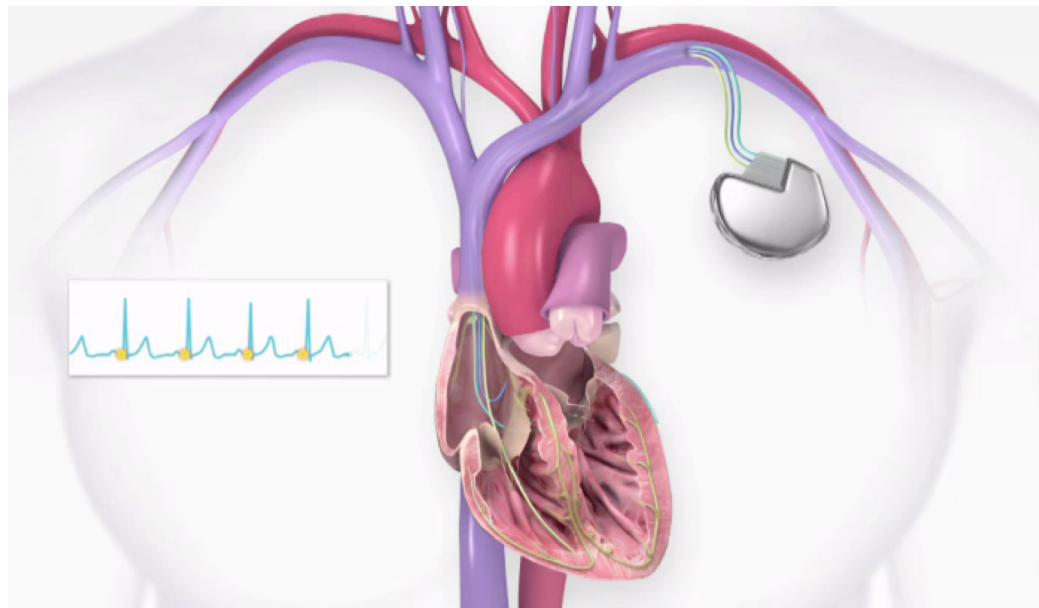
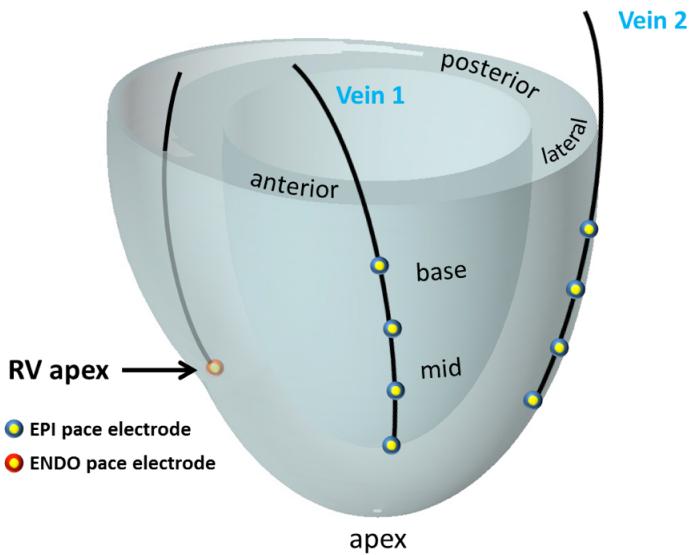


LV Pressure

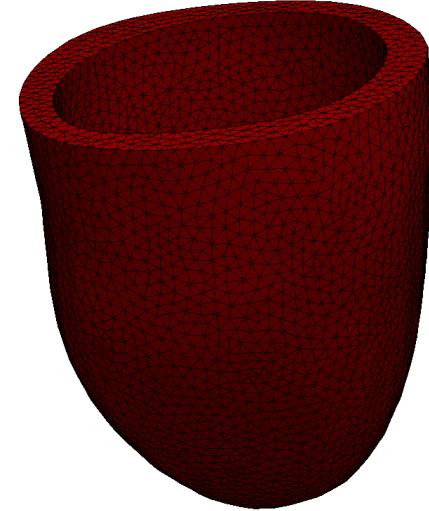


Clinicians want to improve response rates of cardiac resynchronization therapy (CRT)

Electrode positions



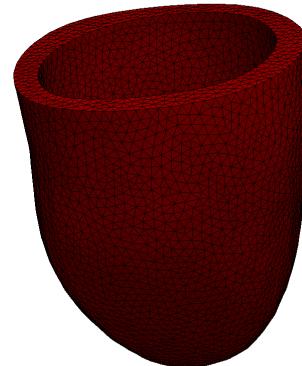
**Mechanical features that can not be measured in the clinic
can be computed using a cardiac computational model**



Myocardial stress can not be measured

Outline

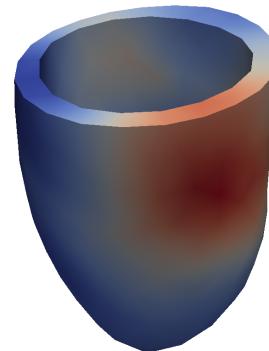
**1. Building a Cardiac
Computational Model**



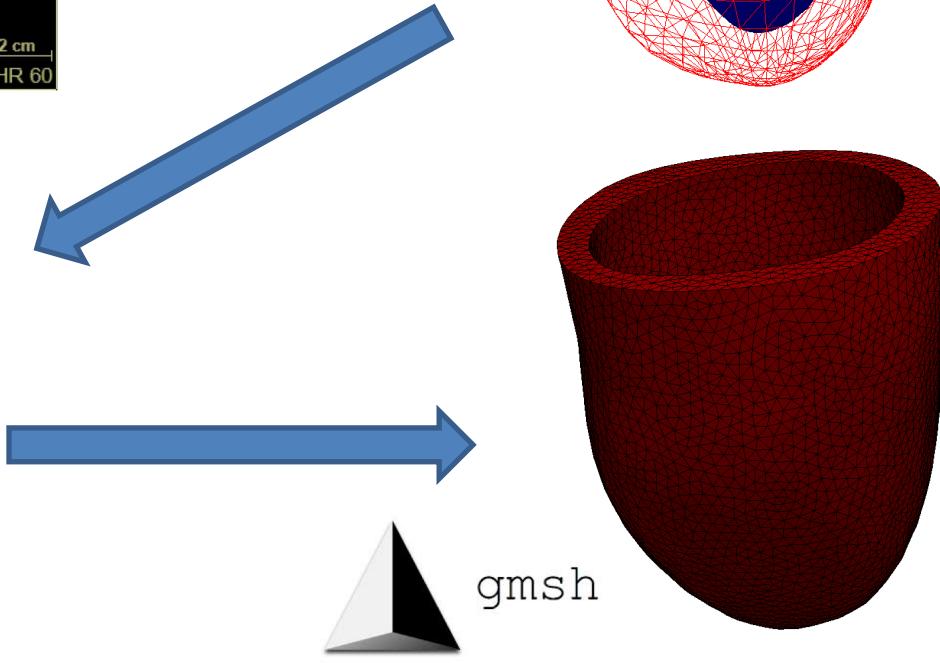
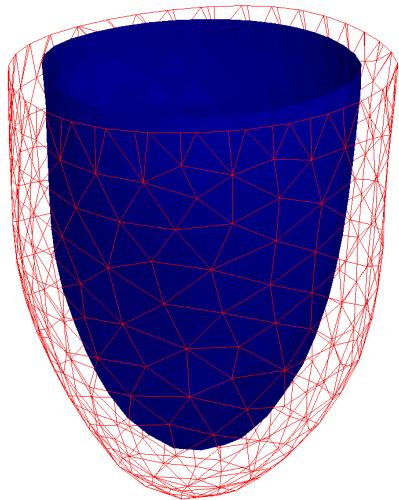
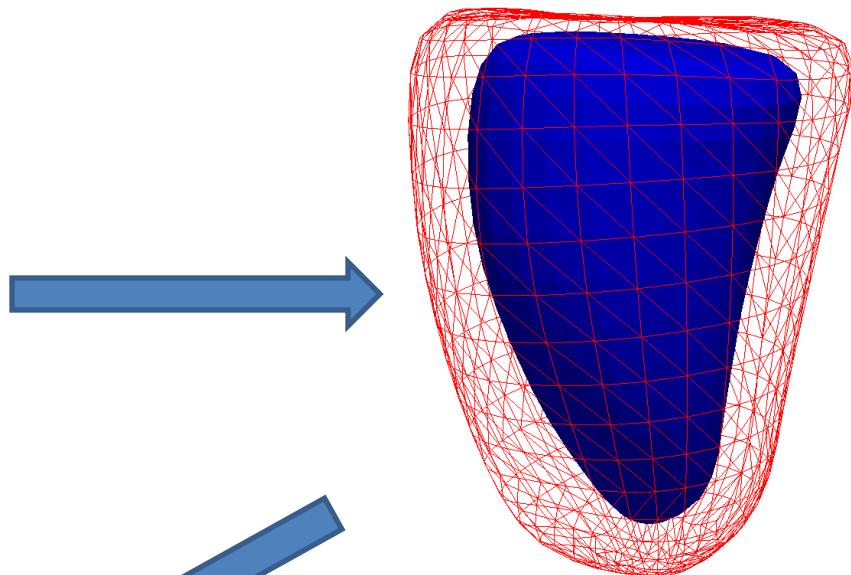
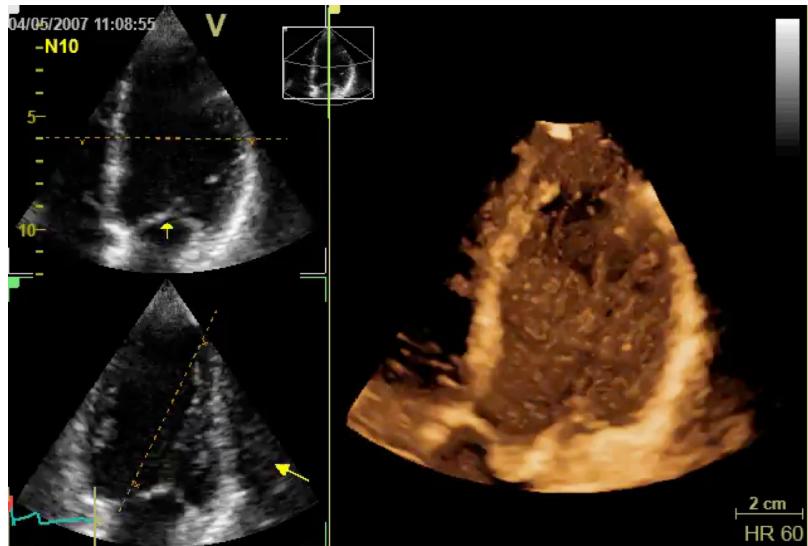
**2. Constraining the model
to clinical data**

$$I_{\alpha}^i = \alpha I_{\text{vol}}^i + (1 - \alpha) I_{\text{strain}}^i$$

**3. Verification and
preliminary results**



The geometry is extracted from 4D echocardiography

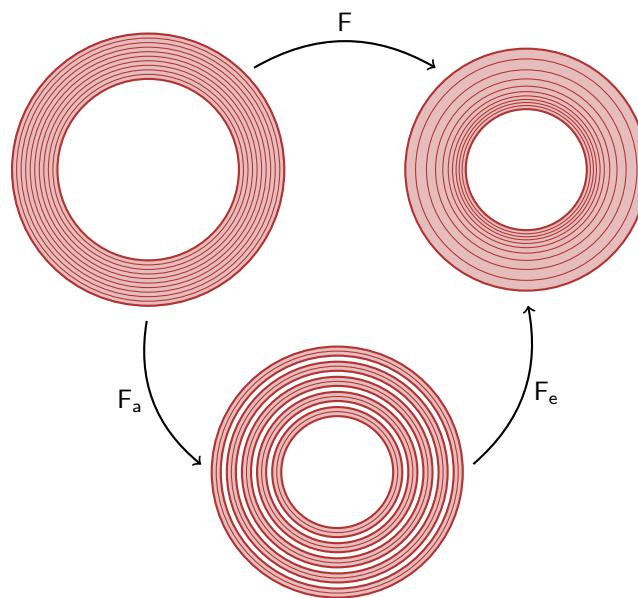


The mechanical model is based on the active strain approach

$$\mathbf{F} = \mathbf{F}_e \mathbf{F}_a$$

Elastic deformation: \mathbf{F}_e

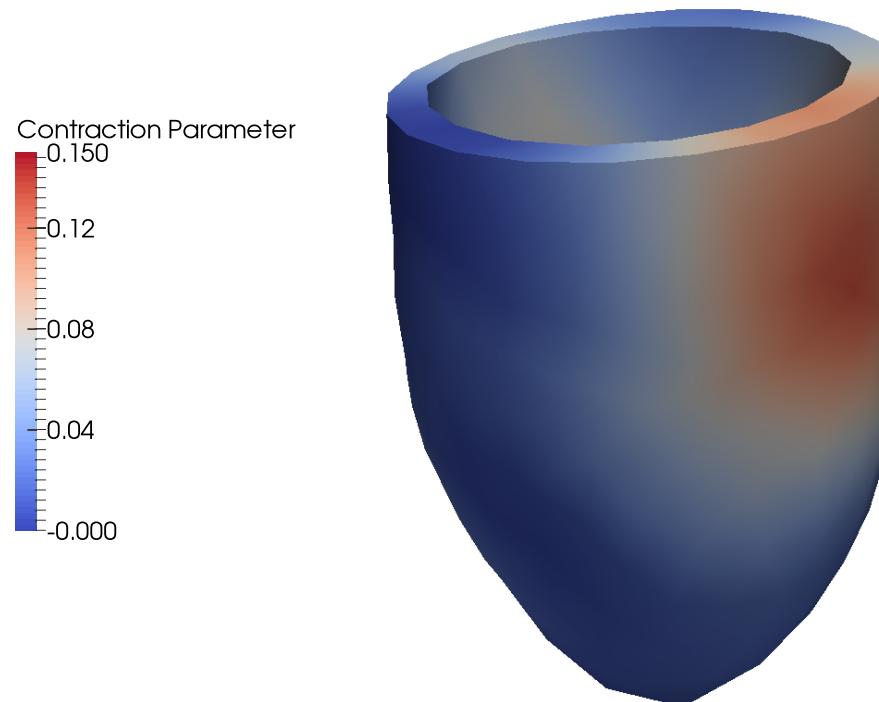
Active deformation: \mathbf{F}_a



The active contraction is modeled by introducing a parameter which represents the relative shortening in the fiber direction

$$\mathbf{F}_a = (1 - \gamma)\mathbf{f}_0 \otimes \mathbf{f}_0 + \frac{1}{\sqrt{1 - \gamma}}(\mathbf{I} - \mathbf{f}_0 \otimes \mathbf{f}_0)$$

\mathbf{f}_0 : fiber direction



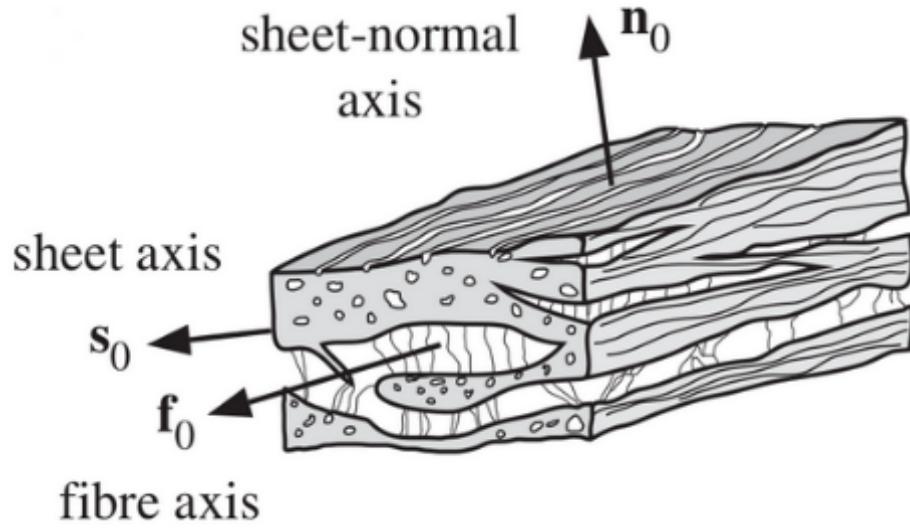
The myocardium is modelled as a hyperelastic, transversely isotropic material

$$\mathbf{F}_e = \mathbf{F}\mathbf{F}_a^{-1}$$

$$\mathbf{C}_e = \mathbf{F}_e^T \mathbf{F}_e$$

$$I_{4,\mathbf{f}_0} = \mathbf{f}_0 \cdot (\mathbf{C}_e \mathbf{f}_0)$$

$$I_1 = \text{tr}(\mathbf{C}_e)$$

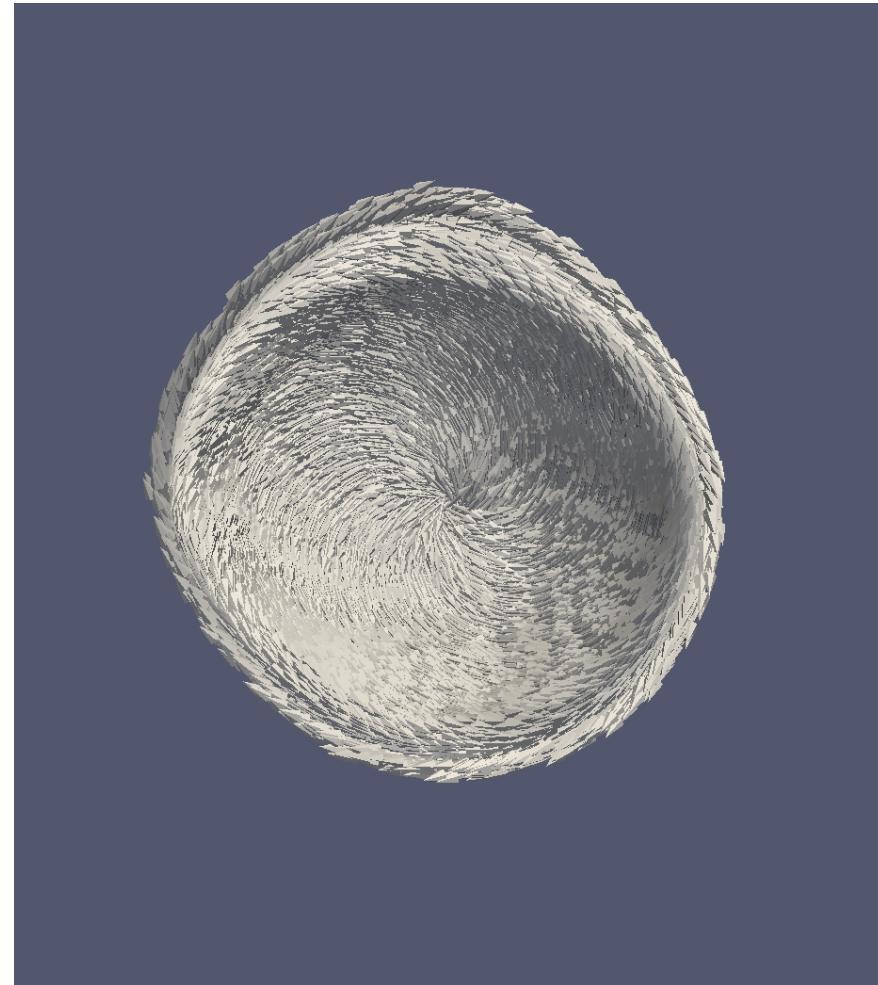
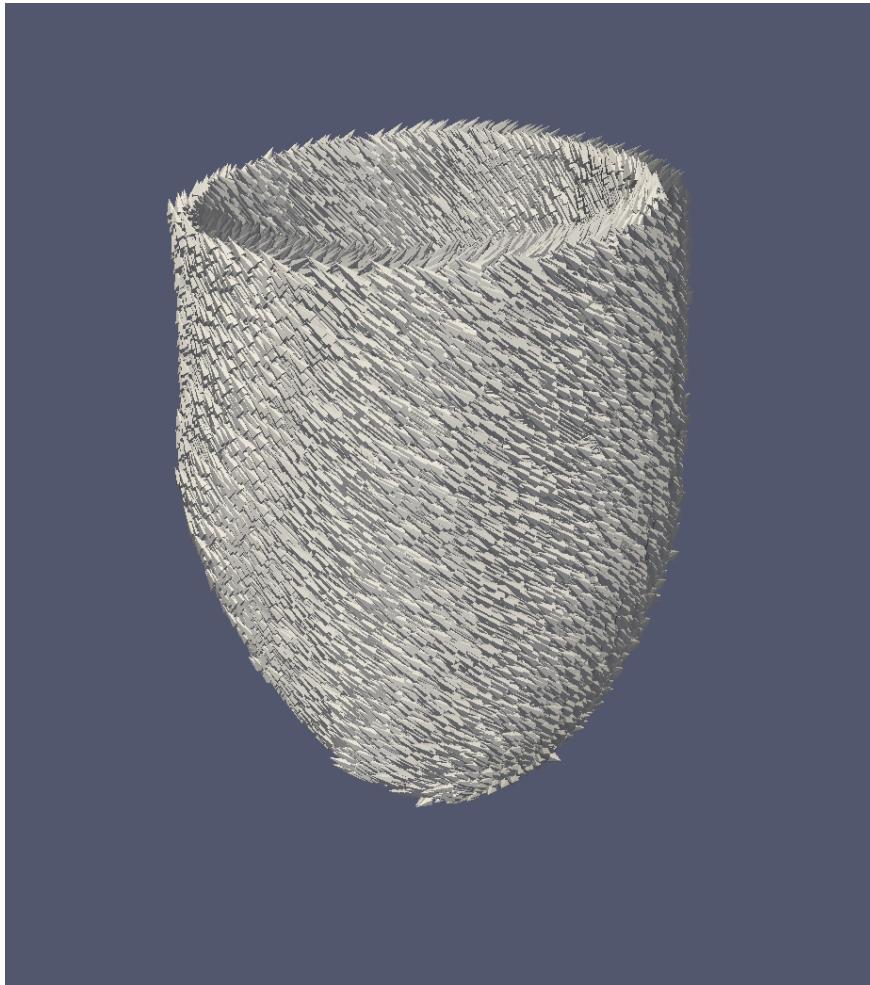


$$\mathcal{W}(\mathbf{C}_e) = \frac{a}{2b} \left(e^{b(I_1 - 3)} - 1 \right) + \frac{a_f}{2b_f} \left(e^{b_f(I_{4,\mathbf{f}_0} - 1)_+^2} - 1 \right)$$

Isotropic term

Transversely isotropic term (fibers)

Myocardial fiber orientation is assigned by using a rule-based algorithm



The mechanical model

Active Strain Decomposition:

$$\mathbf{F} = \mathbf{F}_e \mathbf{F}_a$$

Passive Mechanics:

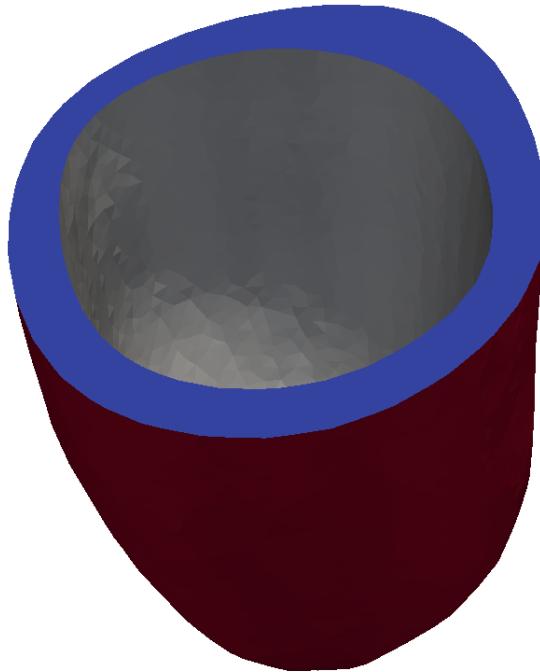
$$\mathcal{W}(\mathbf{C}_e) = \frac{a}{2b} \left(e^{b(I_1 - 3)} - 1 \right) + \frac{a_f}{2b_f} \left(e^{b_f(I_{4,\mathbf{f}_0} - 1)_+^2} - 1 \right)$$

$$\mathbf{C}_e = \mathbf{F}_e^T \mathbf{F}_e \quad I_{4,\mathbf{f}_0} = \mathbf{f}_0 \cdot (\mathbf{C}_e \mathbf{f}_0) \quad I_1 = \text{tr}(\mathbf{C}_e)$$

Active Mechanics:

$$\mathbf{F}_a = (1 - \gamma) \mathbf{f}_0 \otimes \mathbf{f}_0 + \frac{1}{\sqrt{1 - \gamma}} (\mathbf{I} - \mathbf{f}_0 \otimes \mathbf{f}_0)$$

The mechanical model (continue)



Boundary Conditions:

Endocardial pressure from
clinical data :

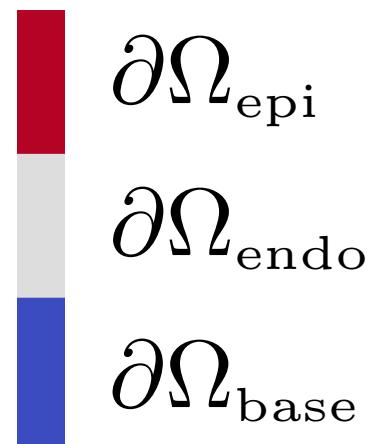
$$\mathbf{T} = J p_{LV} \mathbf{F}^{-T} \mathbf{N}, \quad \mathbf{x} \in \partial\Omega_{endo}$$

Fix base in vertical direction. Allow
some displacement in the base plane:

$$\mathbf{u} = (u_1, u_2, u_3)$$

$$u_1 = 0, \quad \mathbf{x} \in \partial\Omega_{base}$$

$$\mathbf{T} = -k\mathbf{u}, \quad \mathbf{x} \in \partial\Omega_{base}$$

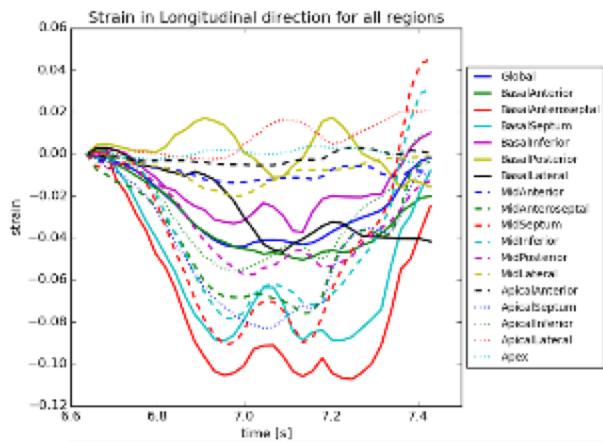


The total elastic energy functional is made specific to a patient by calibrating the 5 model parameters to clinical data

$$\Pi = \int_{\Omega} \mathcal{W}(\mathbf{C}_e) + p(J - 1)dV + \text{boundary conditions}$$

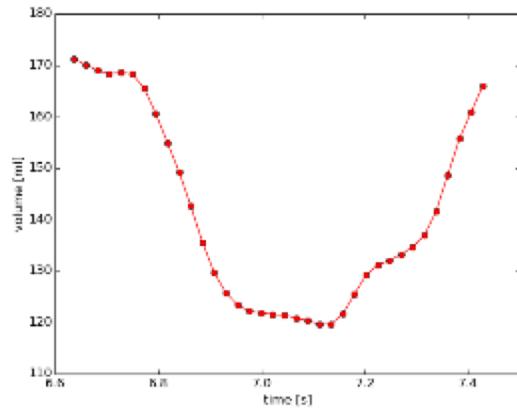
$$R(\mathbf{u}, p) = \begin{pmatrix} D_{\delta \mathbf{u}} \Pi \\ D_{\delta p} \Pi \end{pmatrix} = \mathbf{0} \quad \Pi = \Pi(\gamma, a, b, a_f, b_f)$$

LV Regional strain

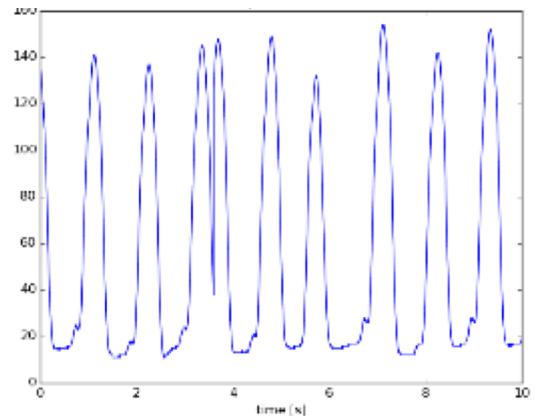


Minimize misfit

LV Volume



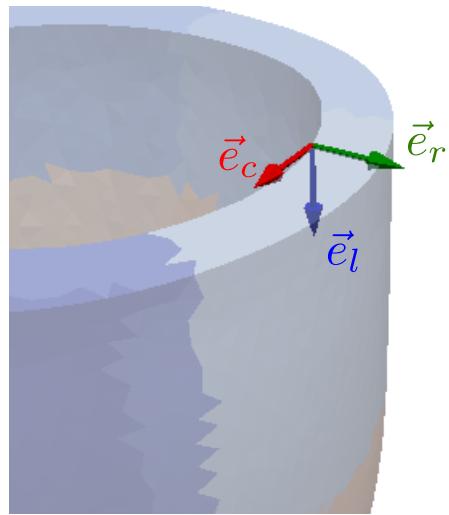
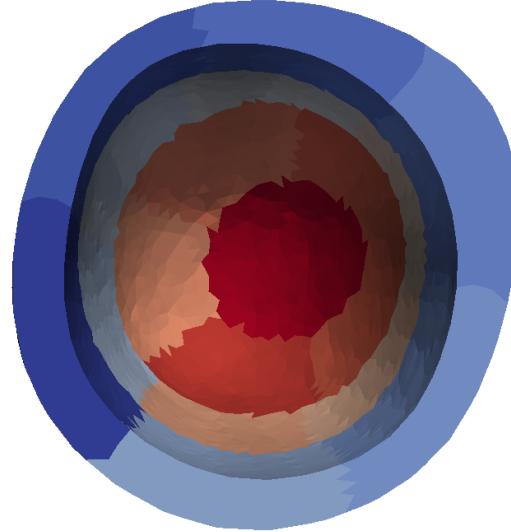
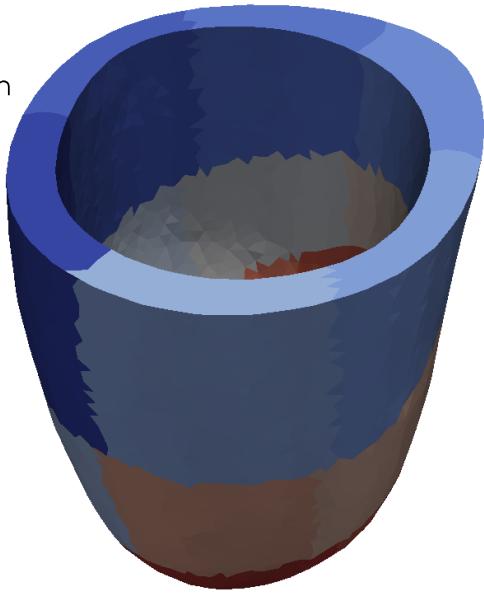
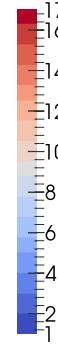
LV Pressure



Boundary condition

The average regional strain is computed in three directions in the left ventricle(LV)

AHA-zone representation



$$\Omega_{LV} = \bigcup_{j=1}^{17} \Omega^j$$

$$\tilde{\varepsilon}_{k,j} = \frac{1}{|\Omega^j|} \int_{\Omega^j} e_k^T \nabla \mathbf{u} \cdot e_k \, dx$$

We minimize the difference between measured and simulated strain and volume

Volume misfit functional:

$$I_{\text{vol}}^i = \frac{|V_i - \tilde{V}_i|}{V_i}, \quad \tilde{V}_i = \frac{1}{3} \int_{\partial\Omega_{\text{endo}}} (\mathbf{I} + \mathbf{u}) \cdot J \mathbf{F}^{-T} \mathbf{N} \, dS$$

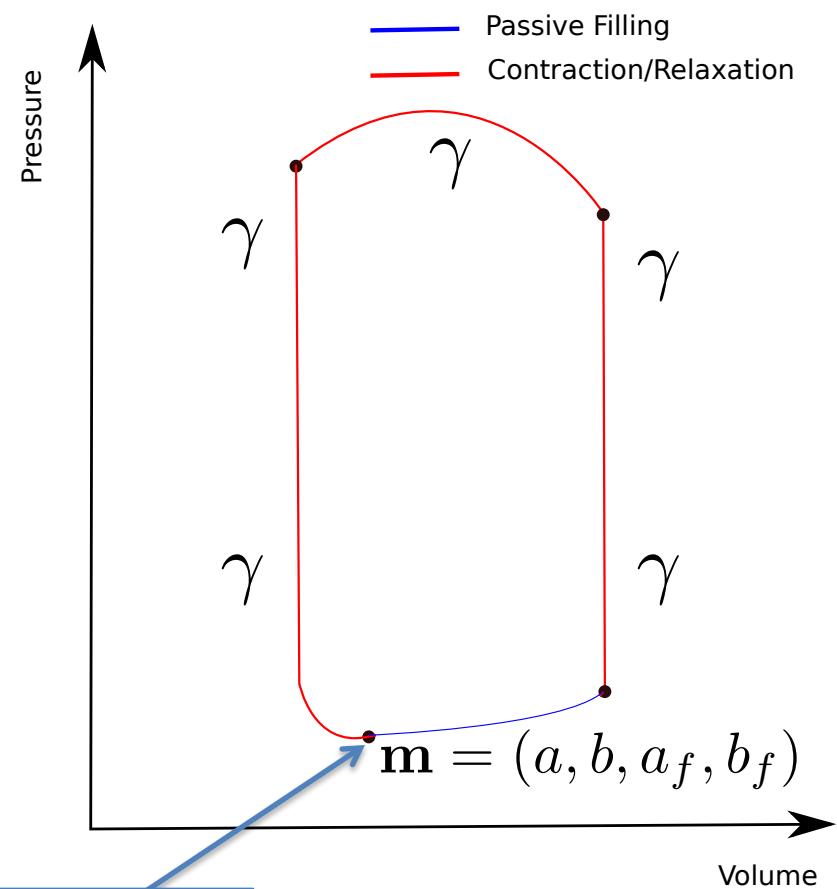
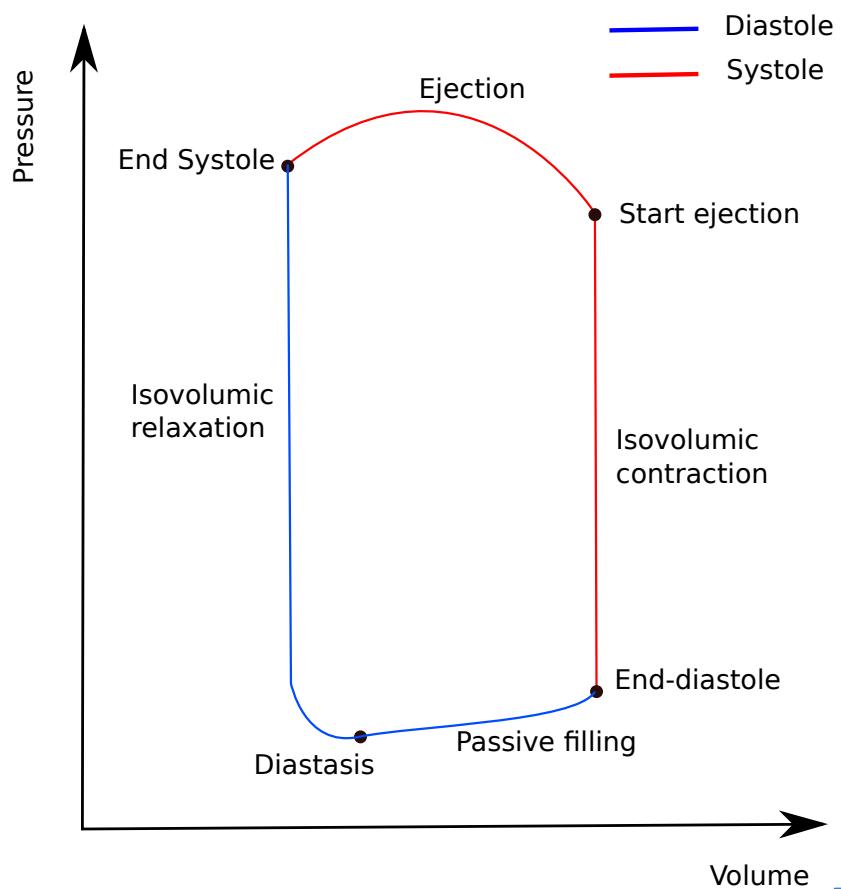
Strain misfit functional:

$$I_{\text{strain}}^i = \sum_{j=1}^{17} \left\| \mathbf{W}(\boldsymbol{\varepsilon}_j^i - \tilde{\boldsymbol{\varepsilon}}_j^i) \right\|_2, \quad \boldsymbol{\varepsilon}_j^i = \begin{bmatrix} \varepsilon_{c,j}^i \\ \varepsilon_{r,j}^i \\ \varepsilon_{l,j}^i \end{bmatrix}, \quad \mathbf{W} = \text{diag}(\omega_{c,j}, \omega_{r,j}, \omega_{l,j})$$

Total misfit functional (weighted):

$$I_\alpha^i = \alpha I_{\text{vol}}^i + (1 - \alpha) I_{\text{strain}}^i$$

Different part of the cardiac cycle is used to calibrate the different parameters



Parameters are estimated by solving a PDE-constrained optimization problem

Passive material parameters:

$$\begin{aligned} & \underset{\mathbf{m}}{\text{minimize}} && \sum_{i=0}^{N_{\text{ED}}} I_{\alpha}^i \\ & \text{subject to} && R(\mathbf{u}, p) = 0. \end{aligned}$$

N_{ED} = Number of points from beginning of passive filling to End-Diastole

Active contraction parameter:

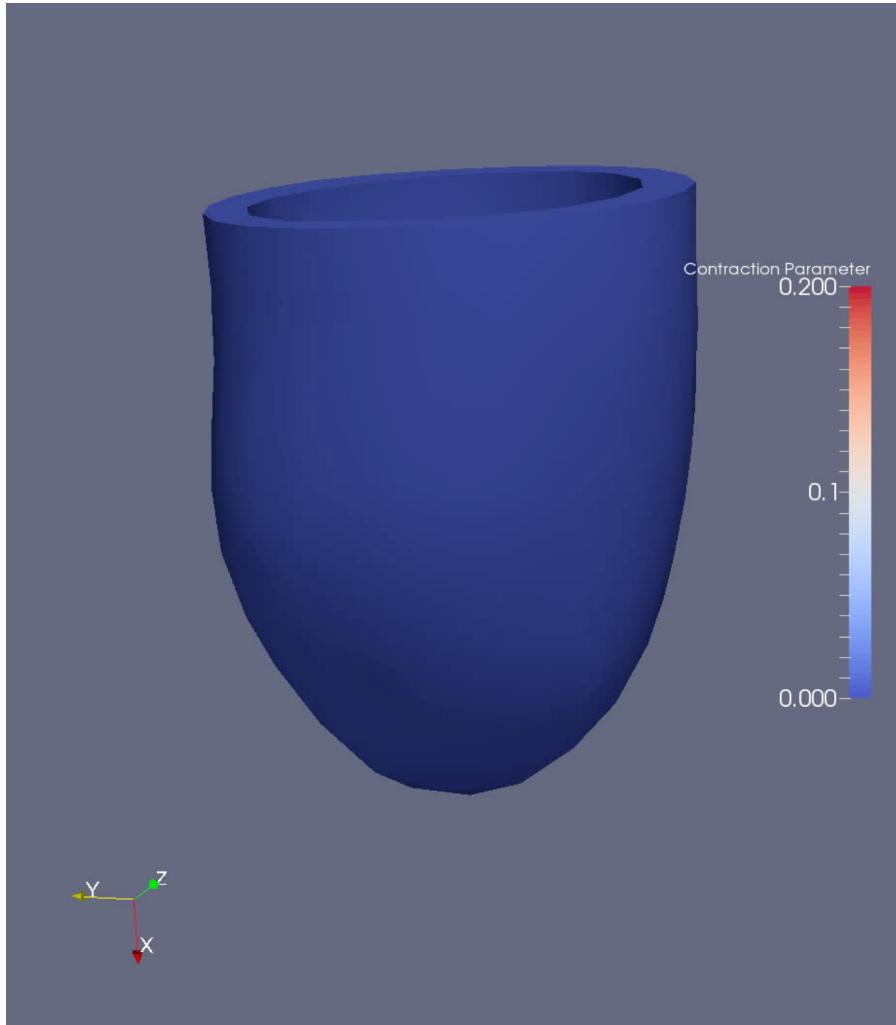
$$\begin{aligned} & \underset{\gamma(\mathbf{x}, i)}{\text{minimize}} && I_{\alpha}^i + \lambda \|\nabla \gamma\|_{L^2(\Omega)}^2 \\ & \text{subject to} && R(\mathbf{u}, p) = 0, \\ & && \gamma(\mathbf{x}, i) \in [0, 1], \quad \mathbf{x} \in \Omega, i = N_{\text{ED}} + 1, \dots, N. \end{aligned}$$



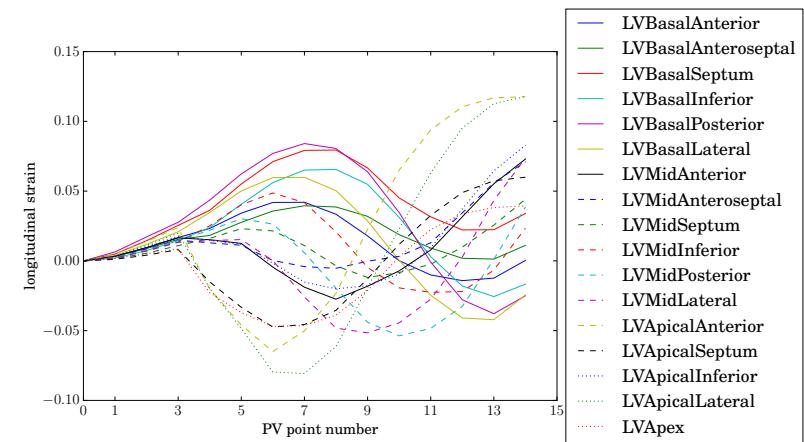
dolfin-adjoint



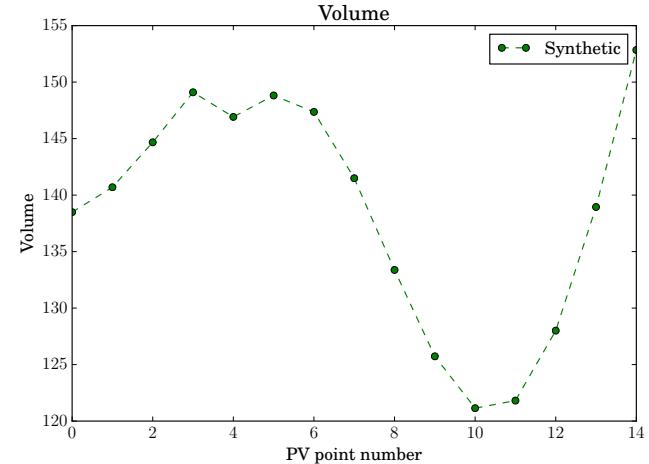
We test the model with a prescribed sequence of contraction parameters



Strain curves:



Volume:

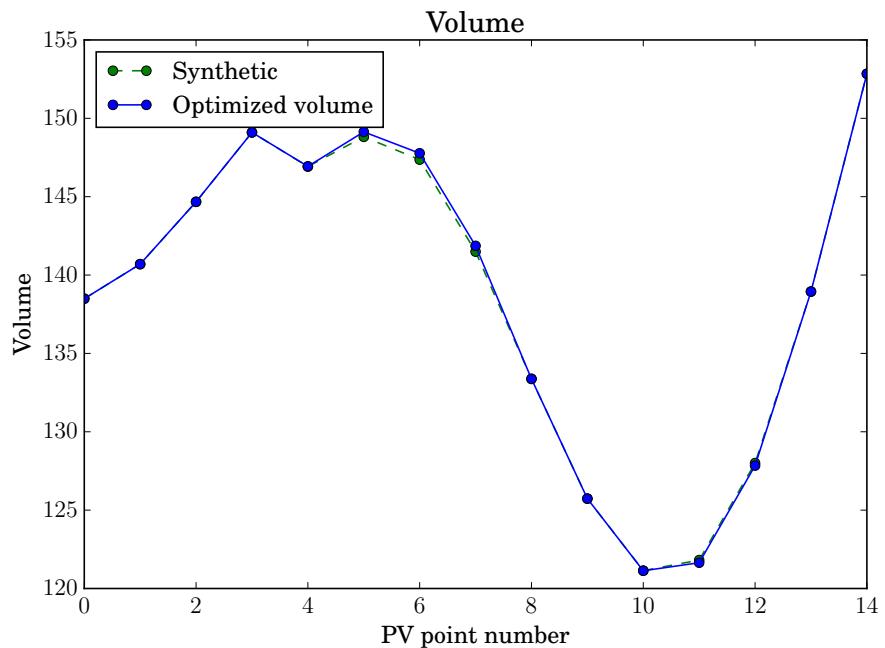


We are able to fit the volume and strain very well using synthetic data

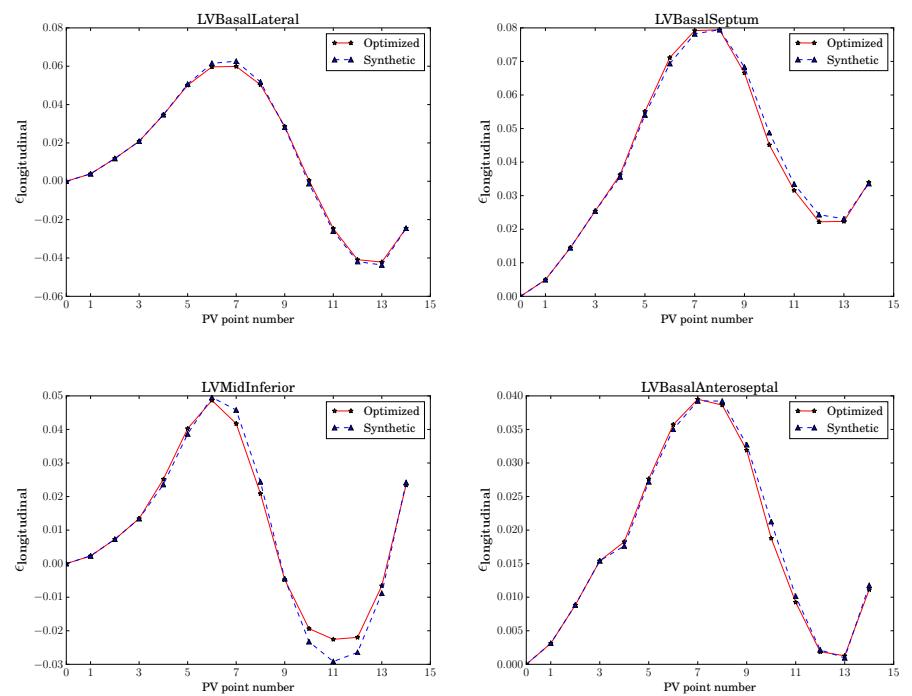
$$\alpha = 0.5$$

$$\lambda = 10.0$$

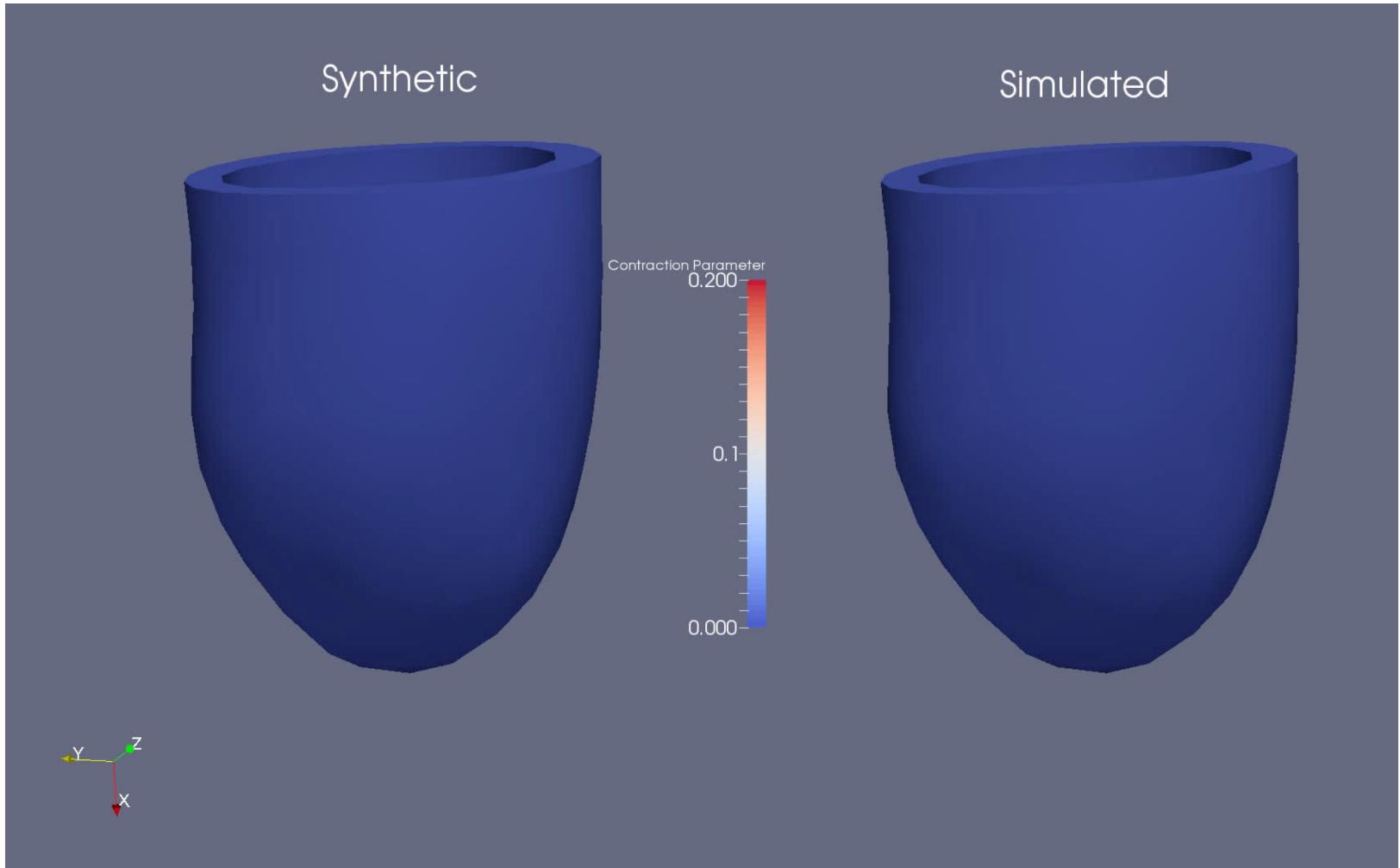
Volume match:



Strain match:

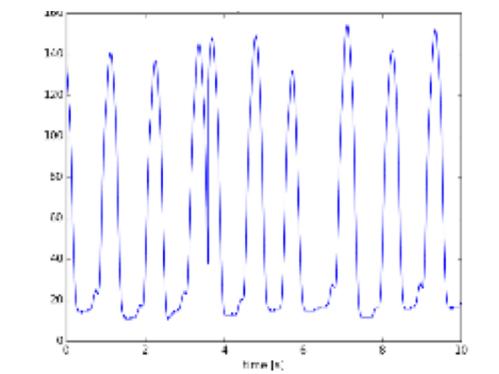


We test the model with a prescribed sequence of contraction parameters

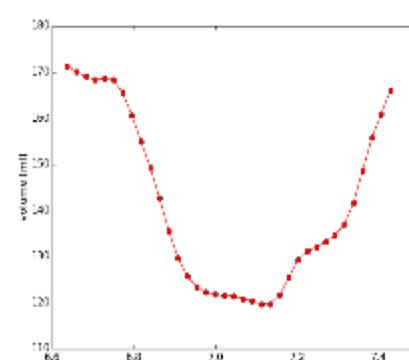


We test the model on real patient data

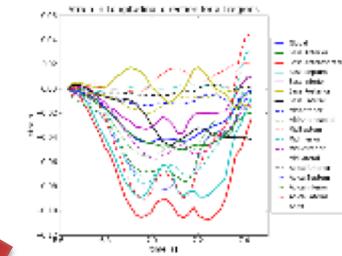
LV Pressure:



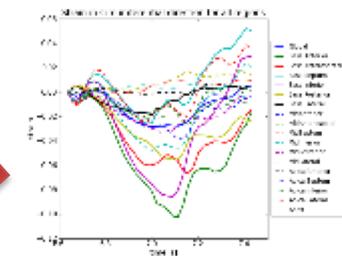
LV Volume:



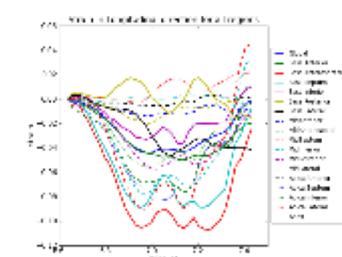
Longitudinal



Circumferential



Radial



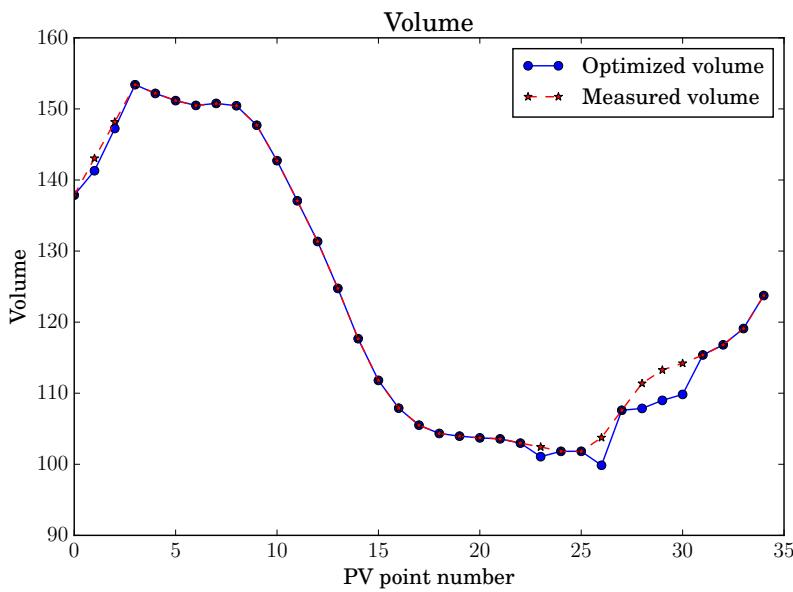
Model

Objective
function

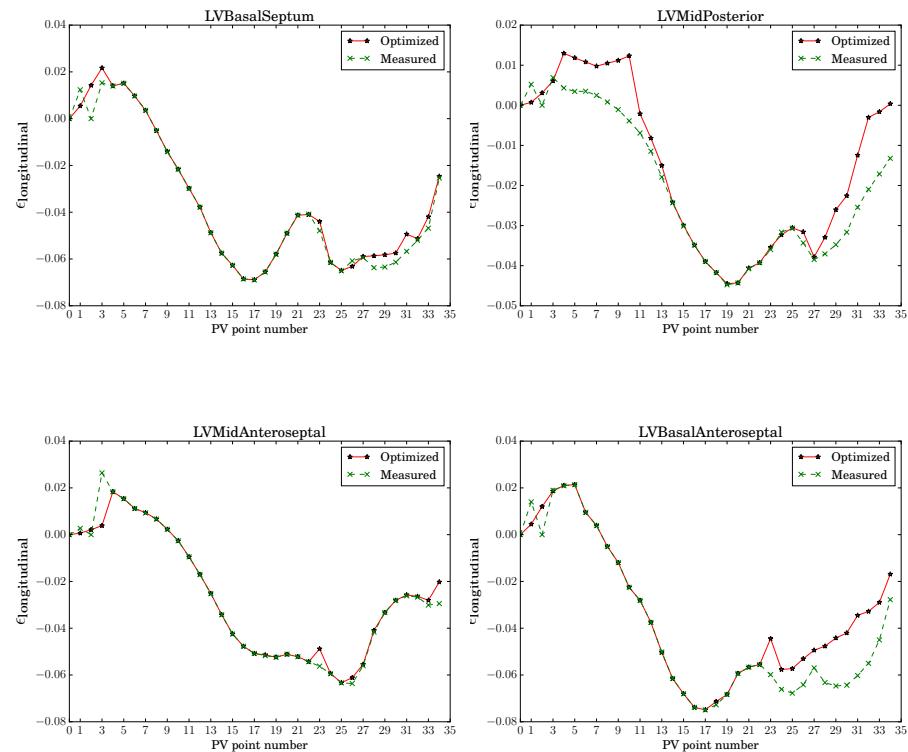
We are able to fit well the volume and strain in the regions with highest weight

$$\alpha = 0.5$$
$$\lambda = 50.0$$

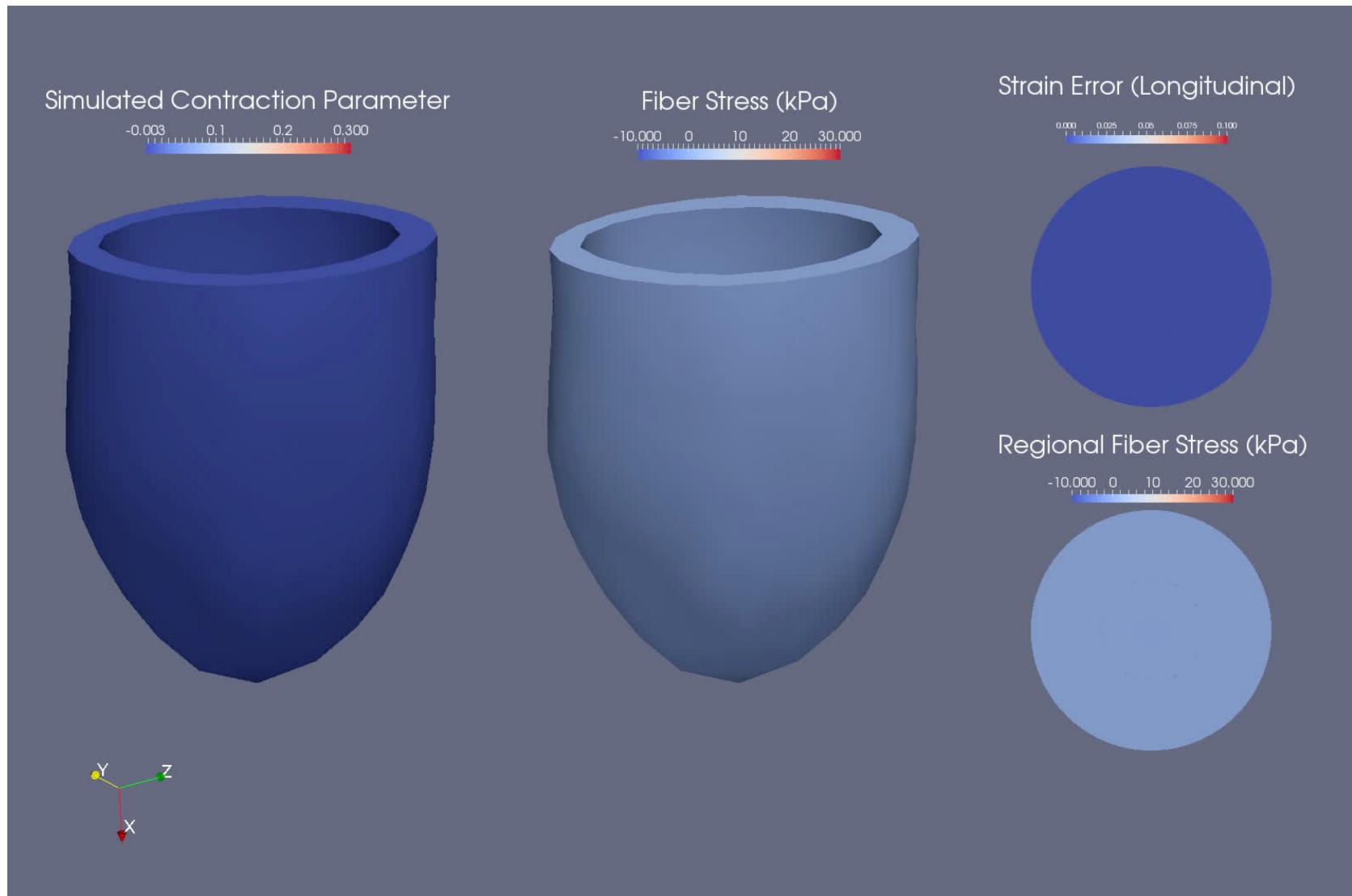
Volume match:



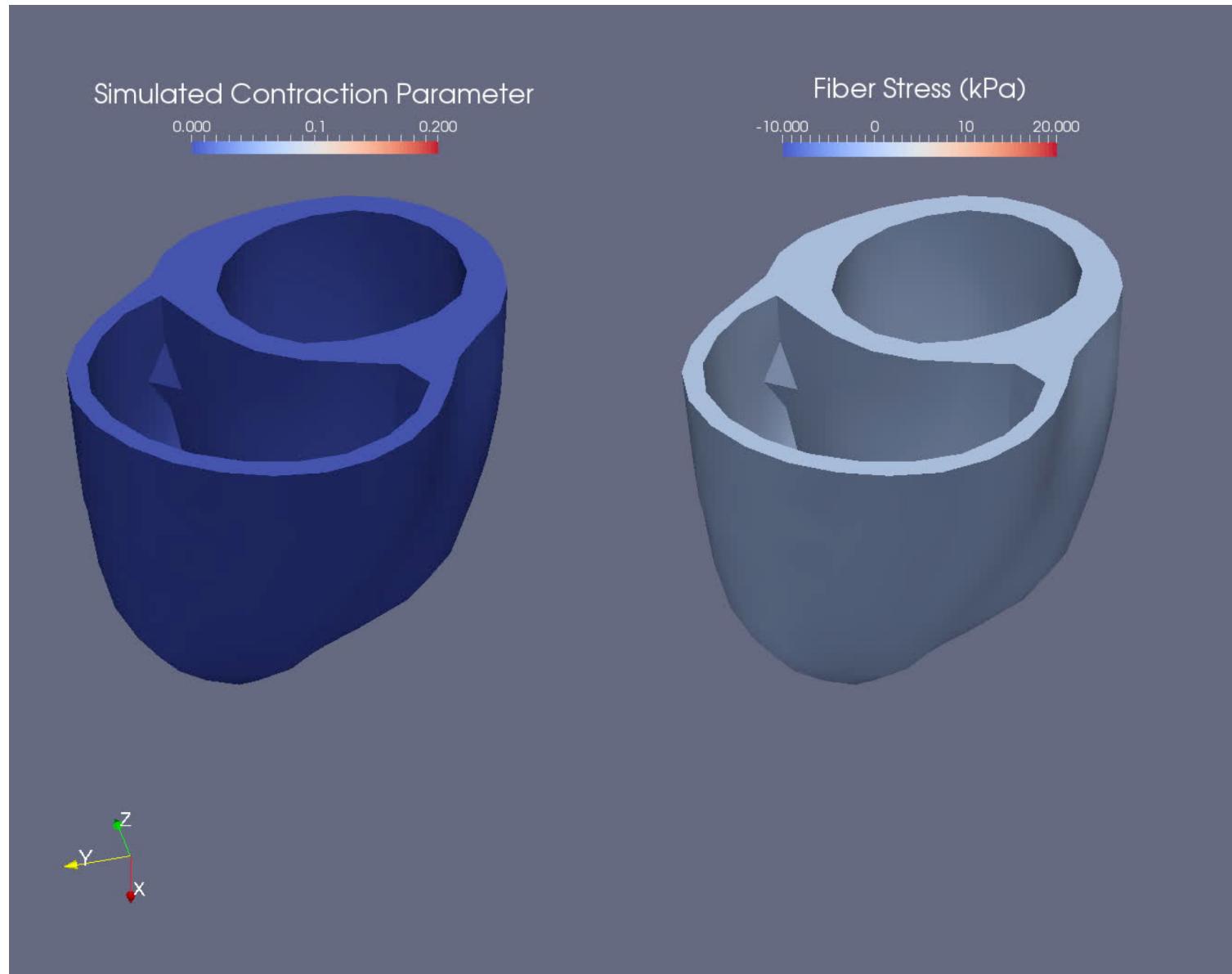
Strain match in regions with high weight:



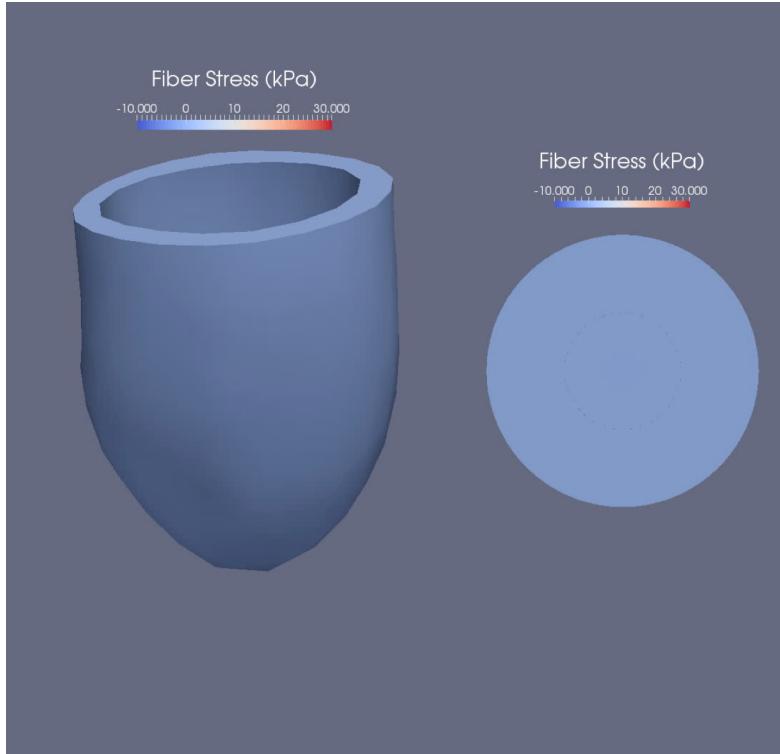
Results with equal weighting of strain and volume



We can also apply this method using a bi-ventricular mesh



In summary, we are able to calibrate a model using clinical measurement, and hence image patient specific stress maps



Acknowledgements

- **Gabriel Balaban**
- **Joakim Sundnes**
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- **Stian Ross**
- **Samuel Wall**

