

Chapter 5 Steady-State Sinusoidal Analysis

1. Sinusoidal signal.
2. Phasors and complex impedances.
3. Power for ac circuits.
4. AC circuits analysis: Ohm's law, KCL, KVL, Nodal voltage analysis, Mesh-current analysis, Thévenin and Norton equivalent circuits.
5. Load impedances for maximum power transfer.

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Sinusoidal Currents and Voltages

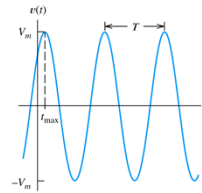


Figure 5.1 A sinusoidal voltage waveform given by $v(t) = V_m \cos(\omega t + \theta)$.
Note: Assuming that θ is in degrees, we have $t_{\max} = \frac{360}{\omega} \times T$.
For the waveform shown, θ is -45° .

V_m is the **peak value**
 ω is the **angular frequency**
 θ is the **phase angle**
 T is the **period**

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Relationships

Frequency $f = \frac{1}{T}$

Angular frequency $\omega = \frac{2\pi}{T}$

$$\omega = 2\pi f$$

$$\sin(z) = \cos(z - 90^\circ)$$

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Root-Mean-Square Values

$$V_{\text{rms}} = \sqrt{\frac{1}{T} \int_0^T v^2(t) dt} \quad I_{\text{rms}} = \sqrt{\frac{1}{T} \int_0^T i^2(t) dt}$$

$$P_{\text{avg}} = \frac{\int_0^T p dt}{T} = \frac{\frac{1}{T} \int_0^T v^2 dt}{R} = \frac{V_{\text{rms}}^2}{R}$$

$$P_{\text{avg}} = I_{\text{rms}}^2 R$$

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RMS Value of a Sinusoid

$$V_{\text{rms}} = \frac{V_m}{\sqrt{2}}$$

This is **NOT** true for other periodic waveforms such as square waves or triangular waves.

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Example 5.1: Find rms value and average power

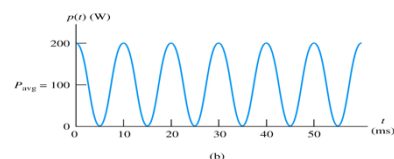
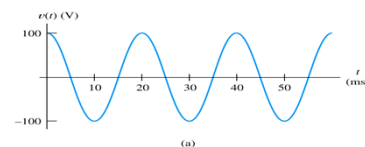


Figure 5.2 Voltage and power versus time for Example 5.1.

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Phasor Definition

Time function : $v_1(t) = V_1 \cos(\omega t + \theta_1)$

Phasor : $\mathbf{V}_1 = V_1 \angle \theta_1$

- ω always in radians/sec, θ always in degrees
- **Phasor**: a complex number that represents the magnitude and phase of a sinusoid
- We will use $j = \sqrt{-1}$

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Complex numbers review

Three representations of complex numbers :

$$z = x + jy \quad z = r \angle \phi \quad z = r e^{j\phi}$$

where

$$r = \sqrt{x^2 + y^2} \quad \phi = \arctan\left(\frac{y}{x}\right)$$

Eular's identity :

$$e^{\pm j\phi} = \cos \phi \pm j \sin \phi$$

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Adding Sinusoids Using Phasors

Step 1: Determine the **phasor** for each term.

Step 2: Add the **phasors** using complex arithmetic.

Step 3: Convert the sum to polar form.

Step 4: Write the result as a time function.

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Example 5.3

$$v_1(t) = 20 \cos(\omega t - 45^\circ)$$

$$v_2(t) = 10 \sin(\omega t + 60^\circ)$$

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$$\begin{aligned} \mathbf{V}_s &= \mathbf{V}_1 + \mathbf{V}_2 \\ &= 20 \angle -45^\circ + 10 \angle -30^\circ \\ &= 14.14 - j14.14 + 8.660 - j5 \\ &= 23.06 - j19.14 \\ &= 29.97 \angle -39.7^\circ \end{aligned}$$

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Phase Relationships

To determine phase relationships from a phasor diagram, consider the phasors to rotate **counterclockwise**. Then when standing at a fixed point, if \mathbf{V}_1 arrives first followed by \mathbf{V}_2 after a rotation of θ , we say that \mathbf{V}_1 leads \mathbf{V}_2 by θ . Alternatively, we could say that \mathbf{V}_2 lags \mathbf{V}_1 by θ .

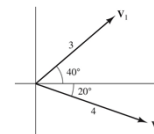


Figure 5.6 Because the vectors rotate counterclockwise, \mathbf{V}_1 leads \mathbf{V}_2 by 60° (or, equivalently, \mathbf{V}_2 lags \mathbf{V}_1 by 60°).

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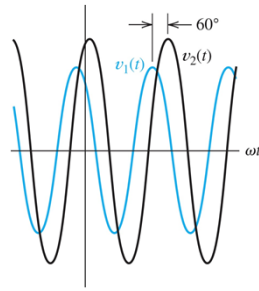


Figure 5.7 The peaks of $v_1(t)$ occur 60° before the peaks of $v_2(t)$. In other words, $v_1(t)$ leads $v_2(t)$ by 60° .

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Circuit Analysis

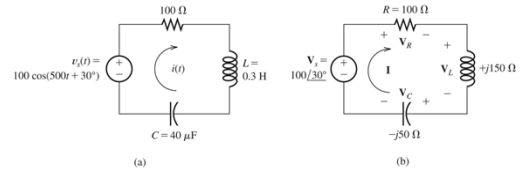


Figure 5.13 Circuit for Example 5.5.

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Complex impedance: Inductor

$$i_L = I_m \sin(\omega t + \theta) \quad v_L = L \frac{di_L}{dt} = \omega L I_m \cos(\omega t + \theta)$$

$$\mathbf{I}_L = I_m \angle \theta - 90^\circ \quad \mathbf{V}_L = \omega L I_m \angle \theta = V_m \angle \theta$$

$$\mathbf{V}_L = (\omega L \angle 90^\circ) \times \mathbf{I}_L \quad \mathbf{V}_L = j\omega L \times \mathbf{I}_L$$

$$Z_L = j\omega L = \omega L \angle 90^\circ$$

$$\mathbf{V}_L = Z_L \mathbf{I}_L$$

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Complex impedance: Inductor

$$Z_L = j\omega L = \omega L \angle 90^\circ$$

$$\mathbf{V}_L = Z_L \mathbf{I}_L$$

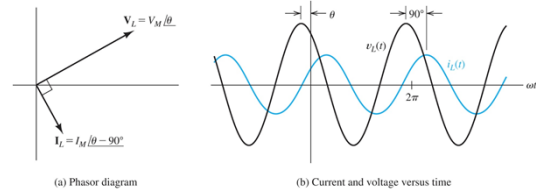


Figure 5.8 Current lags voltage by 90° in a pure inductance.

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Complex impedance: Capacitor

$$v_C = V_m \sin(\omega t + \theta)$$

$$i_C = C \frac{dv_C}{dt} = \omega C V_m \cos(\omega t + \theta)$$

$$\mathbf{V}_C = V_m \angle \theta - 90^\circ, \quad \mathbf{I}_C = \omega C V_m \angle \theta = I_m \angle \theta$$

$$\mathbf{I}_C = (\omega C \angle 90^\circ) \times \mathbf{V}_C \quad \mathbf{V}_C = \frac{1}{\omega C} \angle -90^\circ \times \mathbf{I}_C$$

$$Z_C = \frac{1}{\omega C} \angle -90^\circ = -j \frac{1}{\omega C} = \frac{1}{j\omega C}$$

$$\mathbf{V}_C = Z_C \mathbf{I}_C$$

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Complex impedance: Capacitor

$$Z_C = \frac{1}{j\omega C} = \frac{1}{\omega C} \angle -90^\circ$$

$$\mathbf{V}_C = Z_C \mathbf{I}_C$$

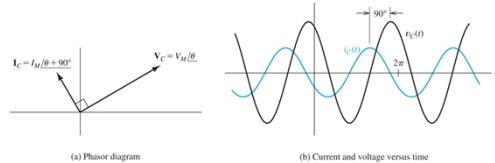


Figure 5.9 Current leads voltage by 90° in a pure capacitance.

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Complex impedance: Resistor

$$Z = R \quad \mathbf{V}_R = R\mathbf{I}_R$$

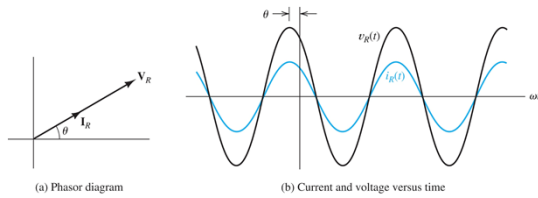


Figure 5.10 For a pure resistance, current and voltage are in phase.

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Exercises 5.6-5.8

5.6

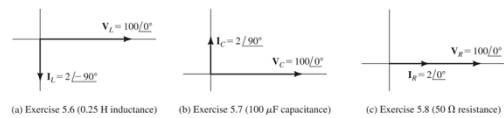


Figure 5.12 Answers for Exercises 5.6, 5.7, and 5.8. The scale has been expanded for the currents compared with the voltages so the current phasors can be easily seen.

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Kirchhoff's Laws in Phasor Form

We can apply **KVL** directly to phasors. The sum of the phasor voltages equals zero for any closed path.

The sum of the phasor currents entering a node must equal the sum of the phasor currents leaving. (**KCL**)

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Circuit Analysis Using Phasors and Impedances

1. Replace the time descriptions of the voltage and current sources with the corresponding phasors. **(All of the sources must have the same frequency.)**
2. Replace inductances by their complex impedances $Z_L = j\omega L$. Replace capacitances by their complex impedances $Z_C = 1/(j\omega C)$. Resistances have impedances equal to their resistances.
3. Analyze the circuit using any of the techniques studied earlier in Chapter 2, performing the calculations with **complex arithmetic**.

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Example 5.5

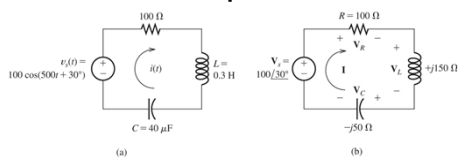


Figure 5.13 Circuit for Example 5.5.

$$Z_L = j\omega L = j150\Omega \quad Z_C = -j\frac{1}{\omega C} = -j50\Omega$$

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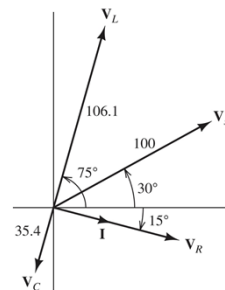


Figure 5.14 Phasor diagram for Example 5.5.

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Example 5.6: Series/parallel combination

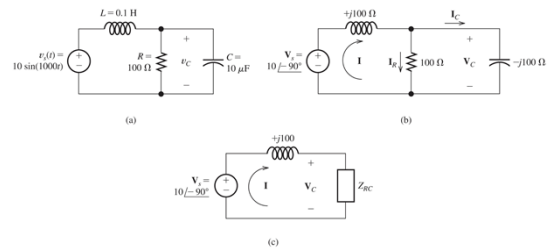


Figure 5.15 Circuit for Example 5.6.

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$$Z_{RC} = R // Z_C = \frac{1}{1/R + 1/Z_C} = \frac{1}{1/100 + 1/(-j100)}$$

$$= \frac{1}{0.01 + j0.01} = \frac{1 \angle 0^\circ}{0.01414 \angle 45^\circ} = 70.7 \angle -45^\circ = 50 - j50$$

$$V_C = V_s \frac{Z_{RC}}{Z_L + Z_{RC}}$$

$$= 10 \angle -90^\circ \frac{70.71 \angle -45^\circ}{j100 + 50 - j50}$$

$$= 10 \angle -90^\circ \frac{70.71 \angle -45^\circ}{50 + j50}$$

$$= 10 \angle -90^\circ \frac{70.71 \angle -45^\circ}{70.71 \angle 45^\circ}$$

$$= 10 \angle -180^\circ$$

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$$I_R = \frac{V_C}{R} = 0.1 \angle -180^\circ$$

$$I_C = \frac{V_C}{Z_C} = \frac{10 \angle -180^\circ}{-j100} = \frac{10 \angle -180^\circ}{100 \angle -90^\circ} = 0.1 \angle -90^\circ$$

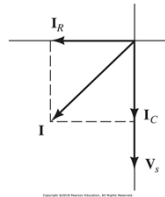


Figure 5.16 Phasor diagram for Example 5.6.

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Example 5.7: Node voltage analysis

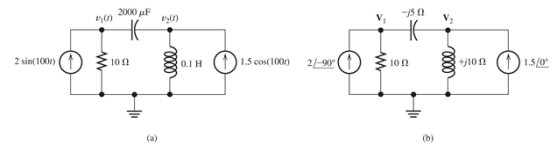


Figure 5.17 Circuit for Example 5.7.

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$$(0.1 + j0.2)V_1 - j0.2V_2 = -j2$$

$$-j0.2V_1 + j0.1V_2 = 1.5$$

$$(0.1 - j0.2)V_1 = 3 - j2$$

$$V_1 = \frac{3 - j2}{0.1 - j0.2} = 16.1 \angle 29.7^\circ$$

$$v_1(t) = 16.1 \cos(1000t + 29.7^\circ)$$

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Exercise 5.11: Mesh Current analysis

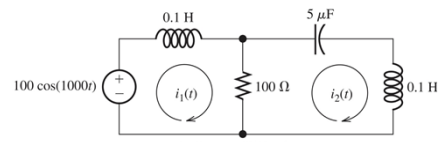


Figure 5.21 Circuit for Exercise 5.11.

$$\mathbf{I}_1 = 1.414 \angle -45^\circ \text{ A} \quad \text{and} \quad \mathbf{I}_2 = 1 \angle 0^\circ \text{ A}$$

$$i_1(t) = 1.414 \cos(1000t - 45^\circ) \text{ A} \quad \text{and} \quad i_2(t) = \cos(1000t) \text{ A}$$

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Power in AC Circuits

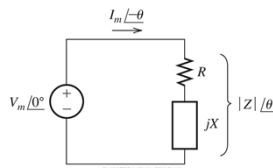


Figure 5.22 A voltage source delivering power to a load impedance $Z = R + jX$.

$$I = \frac{V}{Z} = \frac{V_m \angle 0^\circ}{|Z| \angle \theta^\circ} = I_m \angle -\theta^\circ \quad I_m = \frac{V_m}{|Z|}$$

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Purely resistive circuits

$$p(t) = v(t)i(t) = V_m I_m \cos^2(\omega t)$$

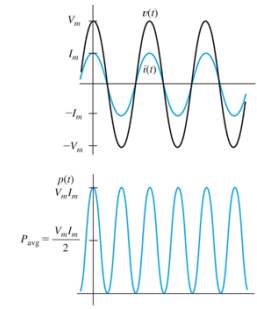


Figure 5.23 Current, voltage, and power versus time for a purely resistive load.

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Pure energy-storage elements

$$p(t) = v(t)i(t) = \pm V_m I_m \cos(\omega t) \sin(\omega t)$$

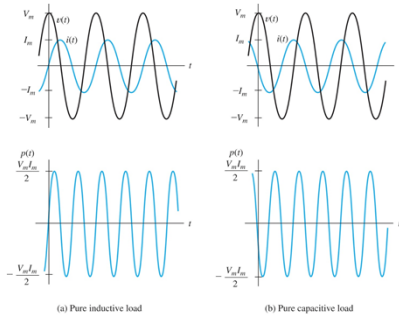


Figure 5.24 Current, voltage, and power versus time for pure energy-storage elements.

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AC Power Calculations

Average power $P = V_{\text{rms}} I_{\text{rms}} \cos(\theta) \quad W$

Power factor $\text{PF} = \cos(\theta)$

Power angle $\theta = \theta_v - \theta_i$

Reactive power $Q = V_{\text{rms}} I_{\text{rms}} \sin(\theta) \quad \text{VAR}$

Apparent power $P_a = V_{\text{rms}} I_{\text{rms}} \quad \text{VA}$

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Relationships

$$P^2 + Q^2 = P_a^2 = (V_{\text{rms}} I_{\text{rms}})^2$$

$$P = I_{\text{rms}}^2 R \quad P = \frac{V_{\text{rms}}^2}{R}$$

$$Q = I_{\text{rms}}^2 X \quad Q = \frac{V_{\text{rms}}^2}{X}$$

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Power Triangle

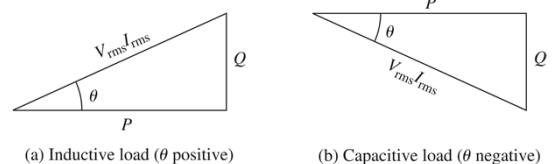


Figure 5.25 Power triangles for inductive and capacitive loads.

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Impedance Triangle

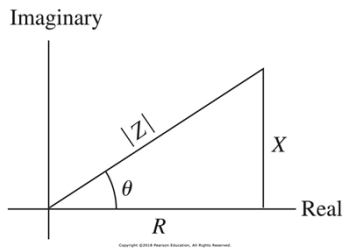


Figure 5.26 The load impedance in the complex plane.

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Example 5.9

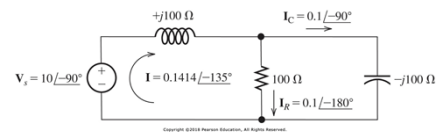


Figure 5.28 Circuit and currents for Example 5.9.

$$\theta = \theta_v - \theta_i = -90^\circ - (-135^\circ) = 45^\circ$$

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Example 5.9 - continued

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Example 5.10

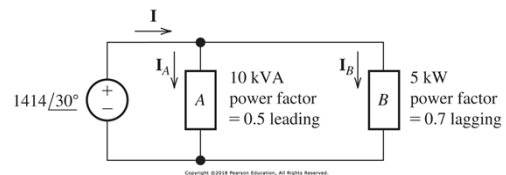


Figure 5.29 Circuit for Example 5.10.

Leading or Lagging: **Current versus voltage**

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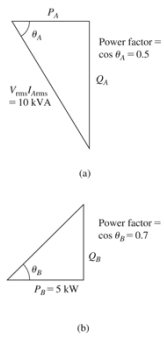


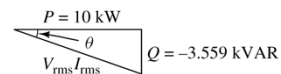
Figure 5.30 Power triangles for loads A and B of Example 5.10.

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$$P = P_A + P_B = 10 \text{ kW}$$

$$Q = Q_A + Q_B = -3.559 \text{ kVAR}$$

$$\theta = \arctan\left(\frac{Q}{P}\right) = -19.59^\circ$$



Power triangle for the source of Example 5.10

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$$P_a = \sqrt{P^2 + Q^2} = 10.61 \text{ kVA}$$

$$I_{rms} = \frac{P_a}{V_{rms}} = \frac{10.61 \text{ kVA}}{1 \text{ kV}} = 10.61 \text{ A}$$

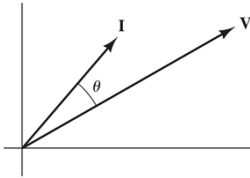


Figure 5.31 Phasor diagram for Example 5.10.

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Example 5.11 Power factor correction

$$P = 50 \text{ kW}, \quad f = 60 \text{ Hz}, \quad V_{rms} = 10 \text{ kV}$$

$$PF = 0.6 \quad \Rightarrow \quad \theta_L = \arccos(0.6) = 53.13^\circ$$

$$Q_L = P \tan(\theta_L) = 66.67 \text{ kVAR}$$

C=? (in Parallel) to make PF=0.9

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Example 5.11 Power factor correction

After adding the capacitor

$$\theta_{new} = \arccos(0.9) = 25.84^\circ$$

$$Q_{new} = P \tan(\theta_{new}) = 24.22 \text{ kVAR}$$

$$Q_C = Q_{new} - Q_L = -42.45 \text{ kVAR}$$

$$X_C = \frac{V_{rms}^2}{Q_C} = \frac{(10^4)^2}{-42450} = -2356$$

$$C = \frac{1}{\omega |X_C|} = 1.126 \mu\text{F}$$

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Thevenin equivalent circuits

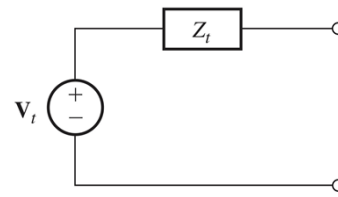


Figure 5.32 The Thévenin equivalent for an ac circuit consists of a phasor voltage source V_t in series with a complex impedance Z_t .

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The Thévenin voltage is equal to the **open-circuit** phasor voltage of the original circuit.

$$V_t = V_{oc}$$

We can find the **Thévenin impedance** by zeroing the independent sources and determining the impedance looking into the circuit terminals.

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The Thévenin impedance equals the open-circuit voltage divided by the short-circuit current.

$$Z_t = \frac{V_{oc}}{I_{sc}} = \frac{V_t}{I_{sc}}$$

$$I_n = I_{sc}$$

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Norton equivalent circuits

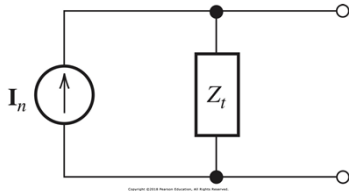


Figure 5.33 The Norton equivalent circuit consists of a phasor current source I_n in parallel with the complex impedance Z_t .

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Example 5.12

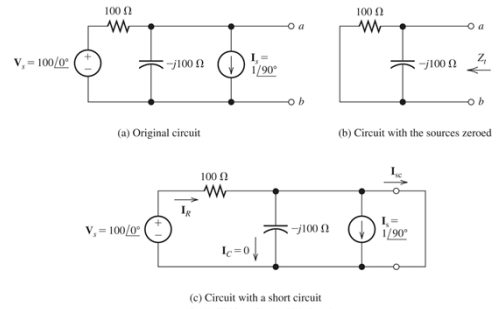


Figure 5.34 Circuit of Example 5.12.

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$$Z_t = (100) // (-j100) = \frac{1}{0.01 + j0.01} = 50 - j50 \Omega$$

$$I_{sc} = I_R - I_s = \frac{V_s}{100} - I_s = 1 - 1 \angle 90^\circ = 1 - j = 1.414 \angle -45^\circ$$

$$V_t = I_{sc} Z_t = 1.414 \angle -45^\circ \times 70.71 \angle -45^\circ = 100 \angle -90^\circ$$

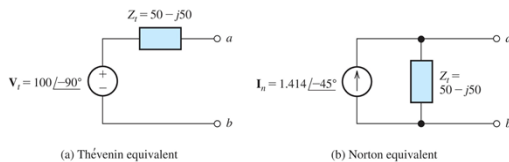


Figure 5.35 Thévenin and Norton equivalents for the circuit of Figure 5.34(a).

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Maximum Power Transfer

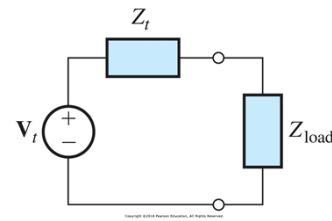


Figure 5.36 The Thévenin equivalent of a two-terminal circuit delivering power to a load impedance.

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Maximum Power Transfer Conditions

If the load can take on any complex value, maximum power transfer is attained for a load impedance equal to the **complex conjugate** of the Thévenin impedance.

Why?

If the load is required to be a **pure** resistance, maximum power transfer is attained for a load resistance equal to the **magnitude** of the Thévenin impedance.

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Example 5.13

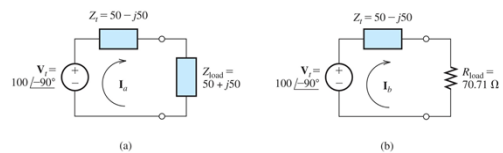


Figure 5.37 Thévenin equivalent circuit and loads of Example 5.13.

$$I = \frac{V_t}{Z_t + Z_{load}} = 1 \angle -90^\circ$$

$$P = I_{rms}^2 R_{load} = \left(\frac{1}{\sqrt{2}}\right)^2 (50) = 25W$$

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Example 5.13 (b)

$$R_{load} = |Z_t| = 70.71 \Omega$$

$$I = \frac{V_t}{Z_t + Z_{load}} = \frac{100 \angle -90^\circ}{50 - j50 + 70.71} = 0.76541 \angle -67.5^\circ$$

$$P = I_{rms}^2 R_{load} = \left(\frac{0.7654}{\sqrt{2}}\right)^2 (70.71) = 20.71 W$$

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Exercise 5.14: find equivalent circuit

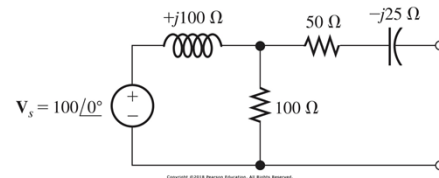


Figure 5.38 Circuit of Exercises 5.14 and 5.15.

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