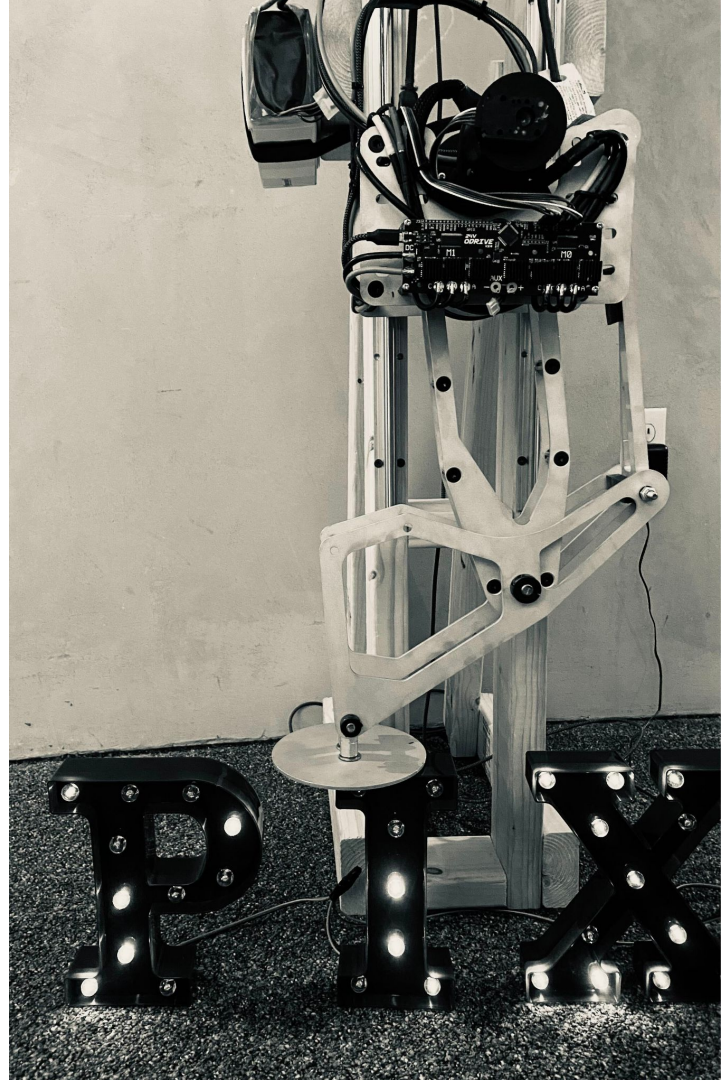


P I X A R

luxo jr. (the pixar lamp)

Analyzing the effects of soft ground contact on the ability of a real system to reach a steady-state jump height.

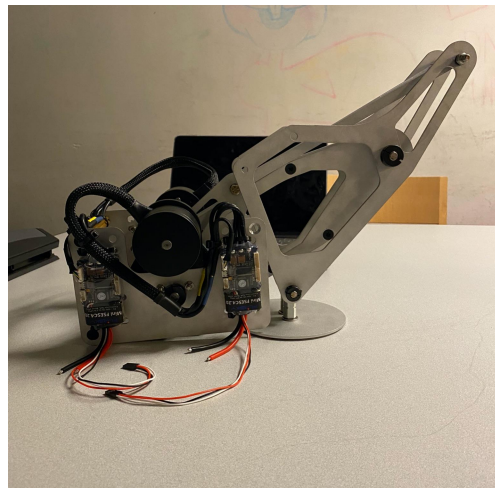
Adi Mehrotra, Fischer Moseley, Alexander Tsao



Introduction

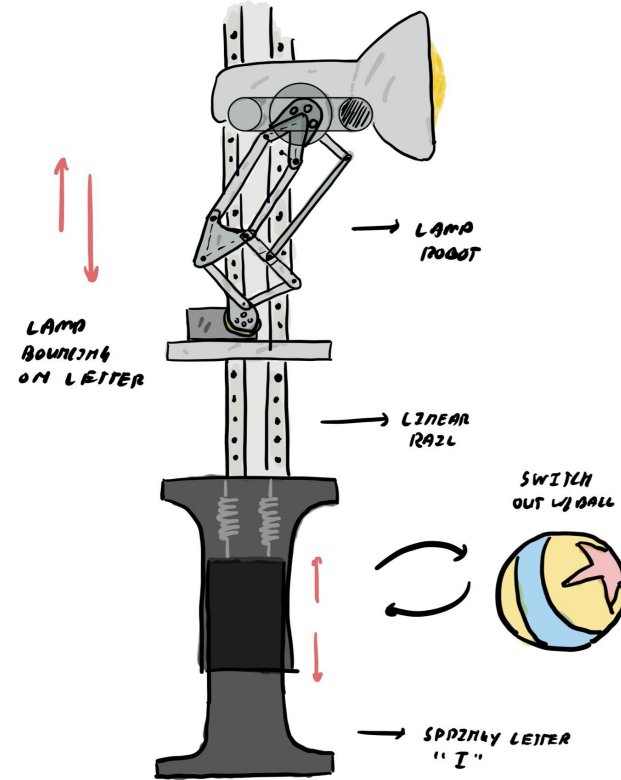
The Pixar lamp jumps on an elastic “I”

Goal: Replicate this soft ground contact and optimize a controller to achieve a stable jump height oscillation.

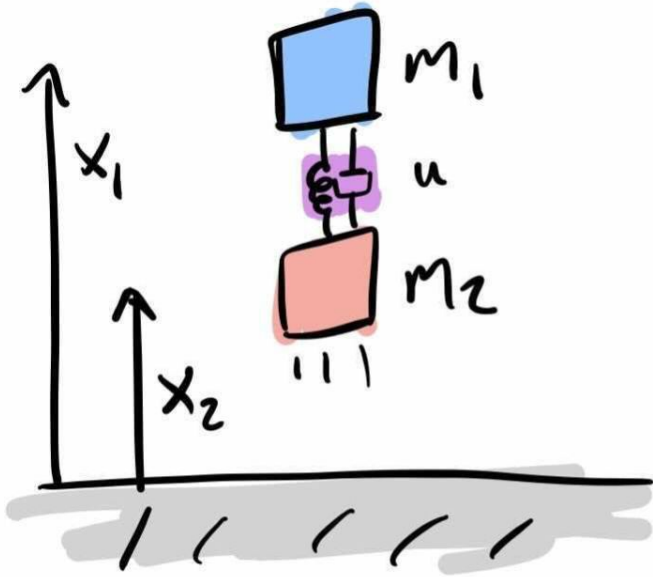


Basic System Model

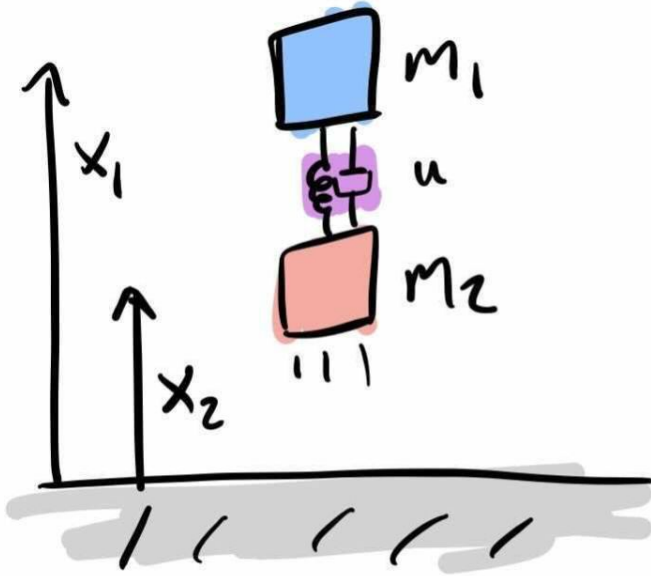
- 2-DOF leg
- hip is constrained to a vertical slider
- foot is unconstrained



Simulation Methods



Simulation Methods



$$m_1 \ddot{x}_1 = -m_1 g + u$$

$$m_2 \ddot{x}_2 = -m_2 g - u + F_g$$

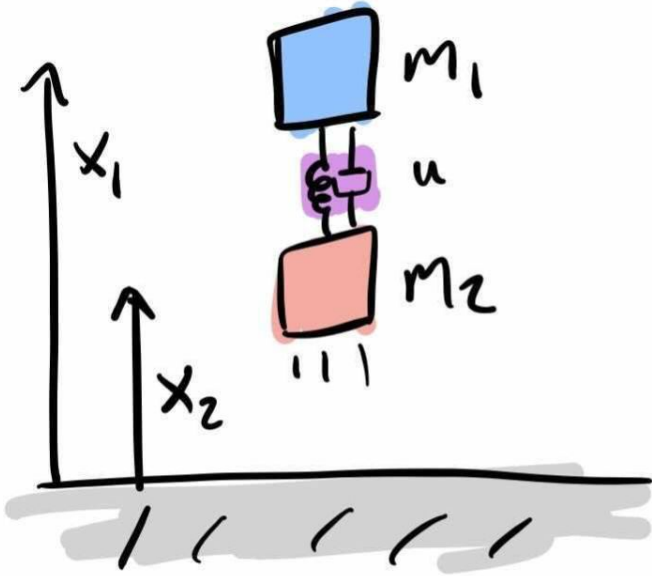
$$F_g = \underbrace{\left(\frac{1}{\pi} \arctan(\epsilon x_2) + \frac{1}{2} \right)}_{\text{smoothing term}} \cdot (-k x_2 - d \dot{x}_2)$$

smoothing term



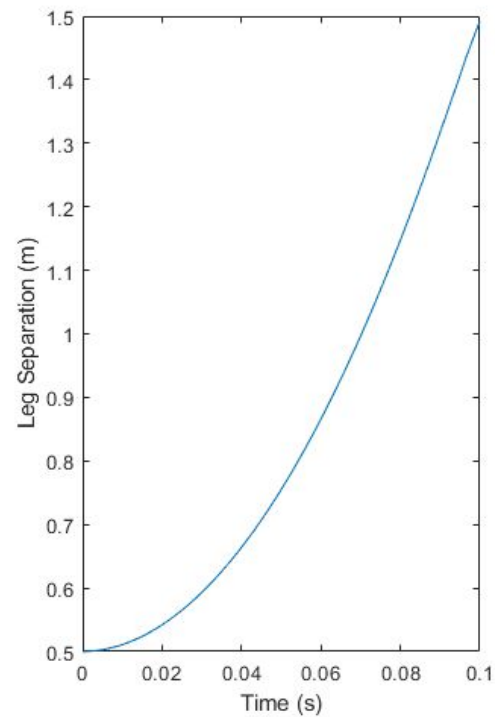
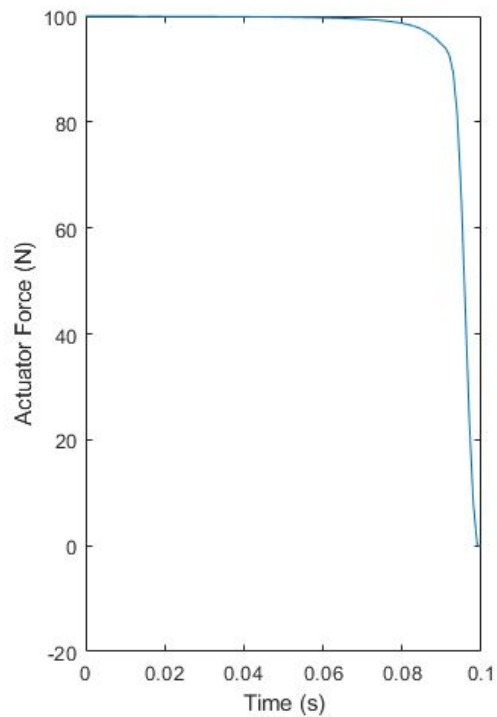
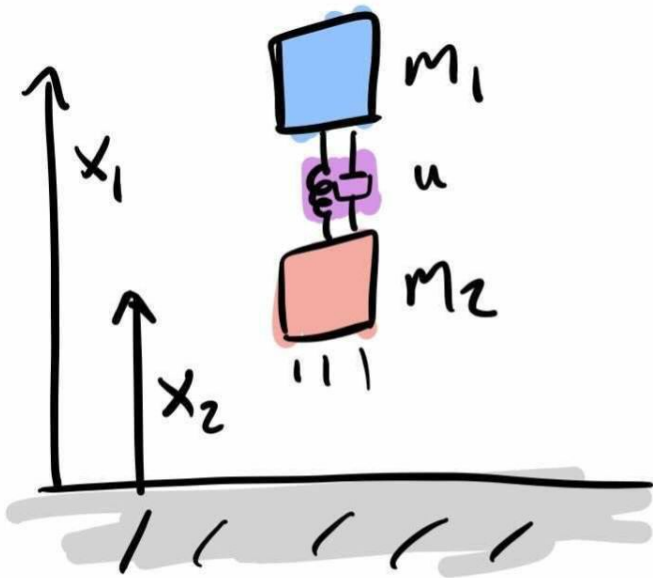
A small red graph showing a smooth, S-shaped curve that transitions from 0 to 1, representing the smoothing function used in the equation above.

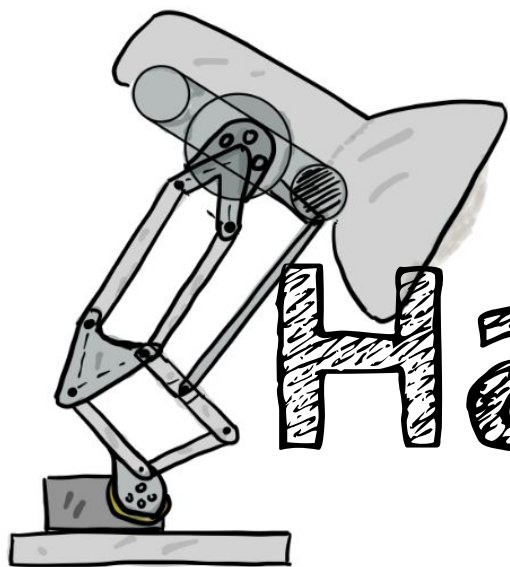
Simulation Methods



- Direct shooting optimization (IPOPT)
- Decision variables: duration and trajectory of control
- Subject to:
 - Bounding box constraint on separation between hip and foot
 - Actuator limit
 - Springy ground dynamics

Simulation Results





Hardware



Hardware

(is hard...)

General Overview

Mechanical:

- Linear rail and carriage
- Waterjet aluminum frame
- ~~Spring loaded 'I'~~

→ **very heavy hip, used a bungee**

Actuators:

- 2x brushless motors

Control:

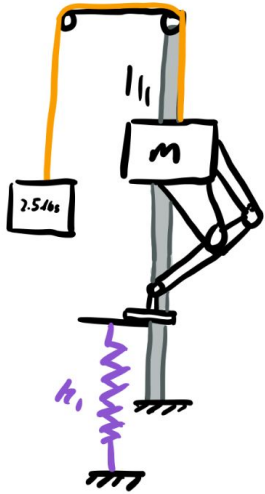
- ~~Teensy microcontroller~~
- ~~VESCs~~

**too much torque ripple, added encoders
for FOC**

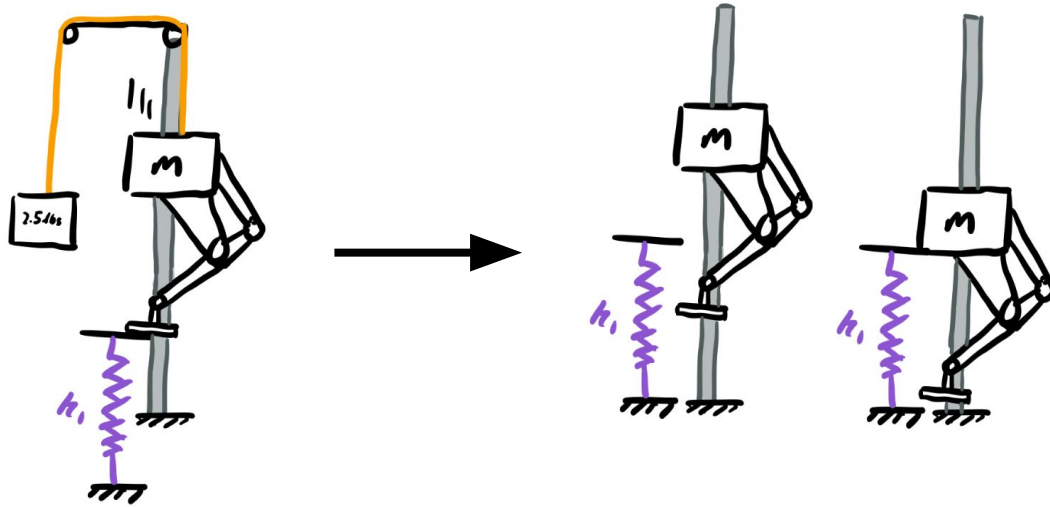
Used an ODrive instead!



Counterweight vs Bungee



Counterweight vs Bungee



(bungee cords in
orange)

Initial Control Strategy

TYPICAL IMPEDANCE
CONTROLLER



$$\tau = k[\theta_e] + d[\dot{\theta}_e]$$

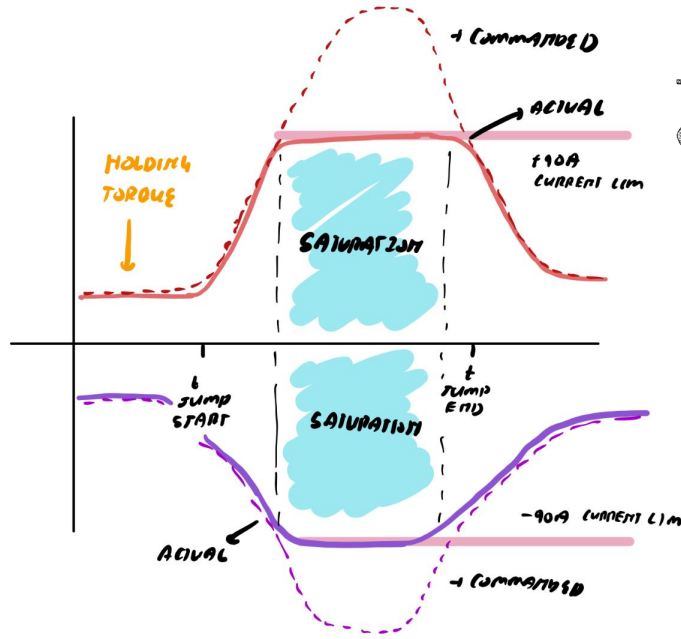
The "Full-Send"
Controller

Impedance Controller:

- Basic impedance controller
- Used this to track a recorded trajectory

Process:

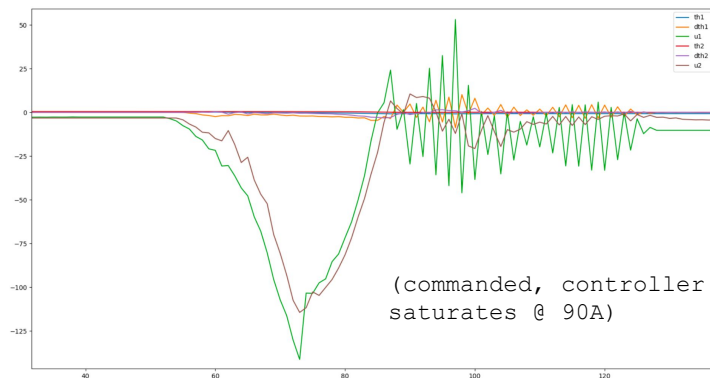
- Recorded a "jump" trajectory with desired positions and velocities
- Tried to maximize joint torques to jump as high as possible



Intermediate Results

- 2.5 lbs counterweight
- controller attempts to optimize for jump height

It learned bang-bang control!!!, like the sim showed!!!



Control Strategy - Energy Pumping

ENERGY ABSORBED

PROP

$$mgh = \frac{1}{2} kx^2 + E_{\text{FOOT}} + E_{\text{IMPACT}}$$

ENERGY
LOST TO
IMPACT

SEND

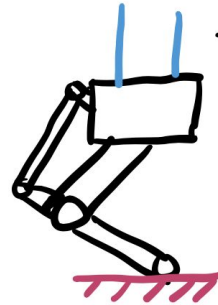
$$mgh = \frac{1}{2} kx^2 + E_{\text{FOOT}}$$

$$mgh = E_{\text{FOOT}} + E_{\text{IMPACT}}$$

MEASURING
w/ SLOW-MO
CAMERA

CSV DATA
FROM
MOTORS &
SUCH

DIFF IS
LOST TO
ENV



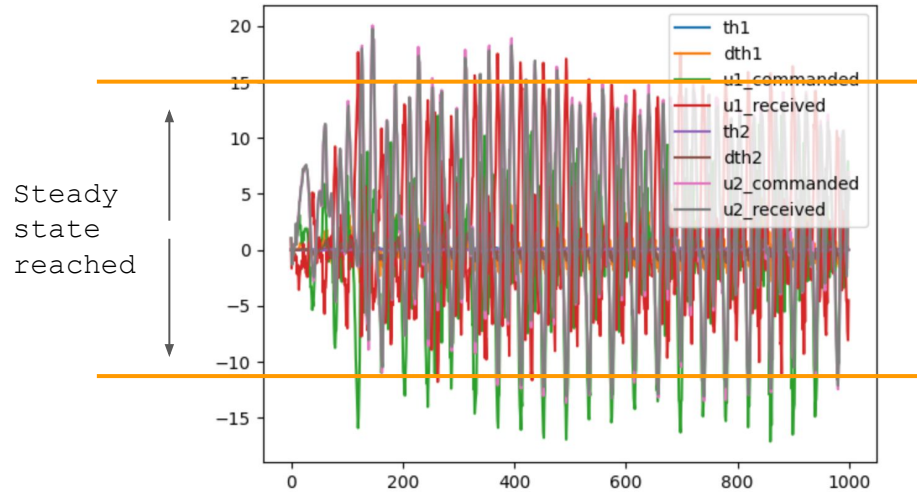
→ NOMINAL
POSE

→ BOUNCE LAMP UP &
DOWN & WATCH
CURRENT RISE



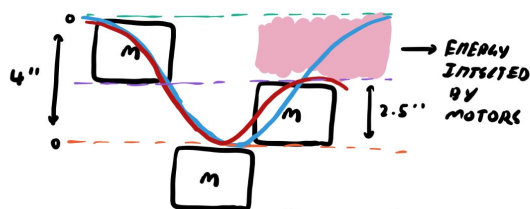
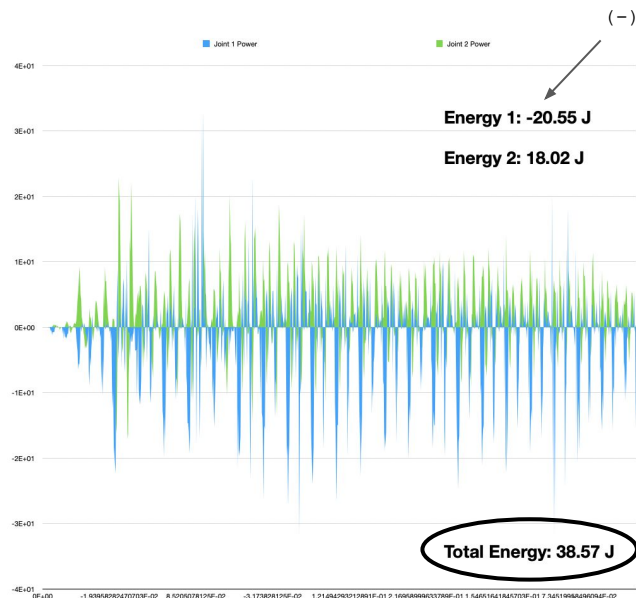
→ THEN DO A FULL
SEND FROM HERE

Final Results - IT JUMPS!!!!



So basically, it's putting any energy lost back into the spring each cycle... let's prove that!

Final Results - Energy Analysis



DRIVEN

UN DRIVEN

$4 \text{ in} = 0.1016 \text{ m}$

$2.5 \text{ in} = 0.0635 \text{ m}$

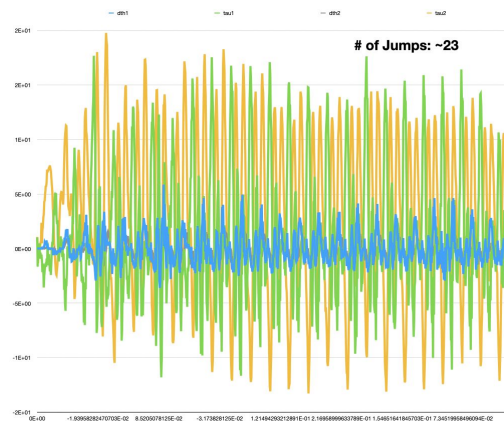
$m \approx 5 \text{ kg}$ $g \approx 9.8 \text{ m/s}^2$

$\Delta E = 5 \text{ kg} \cdot (9.8 \text{ m/s}^2) \cdot (0.1016 \text{ m} - 0.0635 \text{ m})$

$\Delta E = 1.8669 \text{ J} \cdot 23 = 42.9237 \text{ J}$

23 CYCLES

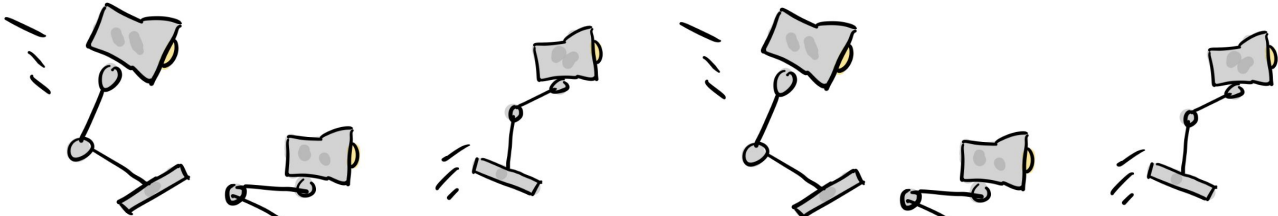
only 4 J difference!



Possible Discrepancies:

- We **assumed 23 complete jump cycles** but the first few were "pumping" and the last was "deceleration"
- assumed energy was the same each cycle**

**mass est. not measured,
+ got heights by recreating
video by hand



This supports the theory...

On its own, the lamp would lose energy.

The motors pump any lost energy back into the system to maintain a stable limit cycle.

Takeaways

- Hall effect sensors give poor position estimates at low speed
- The unconstrained foot was a disaster
 - Added a spring to provide a rest position
- Key Takeaway:
 - Intuitively, the leg must inject enough energy into the spring-mass system to maintain stable oscillation
 - But to write an optimizer we'd need to know the spring position, contact detection, CoM position...
 - all difficult to measure in real life

References

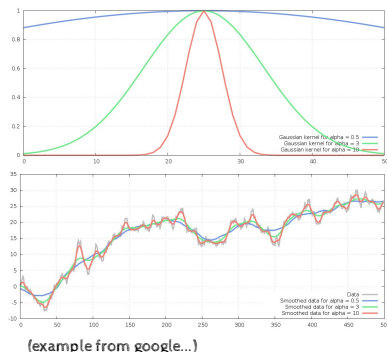
- MIT 6.832/843 notes
- Matt Chignoli's HW5 optimization code
- ODrive references
- Thanks to:
 - Professor Russ Tedrake for advice on trajectory optimization
 - Elijah for teaching Adi about motors
 - Andrew for advice on research question
 - All the course staff + Professor Sangbae Kim
- Special thanks to Pixar for letting us completely violate copyright law

Come talk to us after!

Integration Pains (Appendix)

VESC Problems:

- VESC motors do 6-step commutation
- This causes large amounts of torque ripple
- Which shows up as velocity “noise”

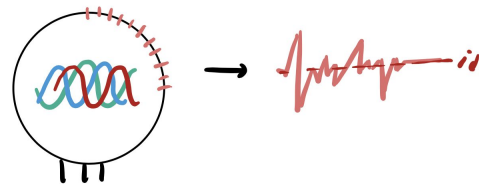


Key Takeaway:

- Made it incredibly difficult to tune a stable impedance controller

**moving average filter doesn't work b/c this filters out useful data we need to control (not noise)

Came up w/ a control strategy that uses gaussian filters on velocity term



$$\tau = k(\theta_d - \theta_c) + d(\dot{\theta}_d - \dot{\theta}_c)$$

↓
NOW THERE'S TWO PROBLEMS w/ THIS

GAUSSIAN DIST. $G(\dot{\theta}_e) = e^{-\frac{\dot{\theta}_e^2}{\sigma^2}}$ $\dot{\theta}_e = \dot{\theta}_d - \dot{\theta}_c$

$$\therefore \tau = k\theta_e + d \cdot e^{-\frac{\dot{\theta}_e^2}{\sigma^2}}$$

