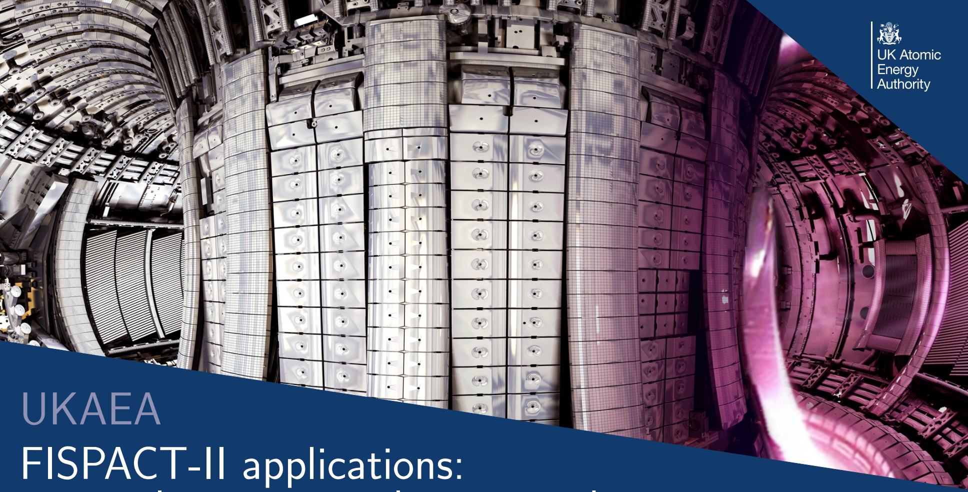

UK Atomic Energy Authority

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FISPACT-II applications: material activation, damage and waste

Mark Gilbert
United Kingdom Atomic Energy Authority

FISPACT-II workshop

June 13-15, 2018, OECD/NEA, Paris

This work was funded by the RCUK Energy Programme
[Grant number EP/P012450/1]

Energy — For a Low Carbon Future

CCFE — CULHAM CENTRE FOR FUSION ENERGY

Applications

- Integrated assessment of helium embrittlement
- DEMO fusion power plant activation and waste analysis
- Material response database
- Primary damage spectra (& emitted particle spectra)

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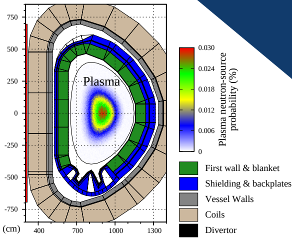
Integrated assessment: Outline

UK Atomic Energy Authority

- Neutron transport modelling results for DEMO (MCNP)
- Neutron-induced transmutation (FISPACT-II)
    - helium production
- Helium embrittlement model and critical lifetimes



DEMO model with defined 3D plasma source

Gilbert, Dudarev, Nguyen-Manh, Zheng, Packer, Sublet
J. Nucl. Mater. **442** (2013) S755
Gilbert, Dudarev, Zheng, Packer, Sublet
Nucl. Fus. **52** (2012) 083019

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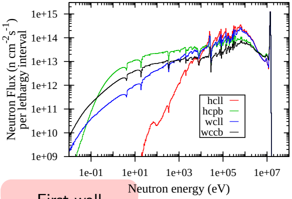

First wall neutron spectra as a function of DEMO concept

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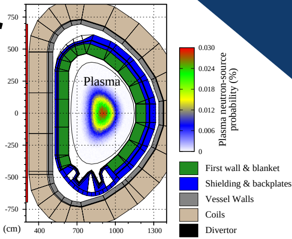

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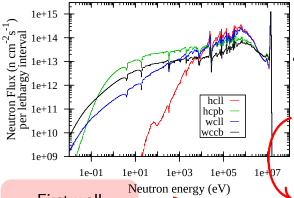

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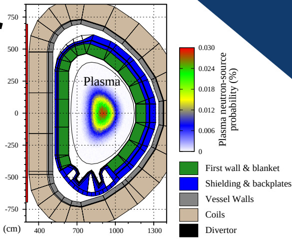

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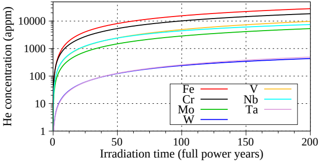
He production rates in materials



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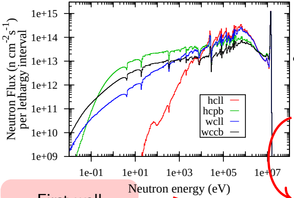

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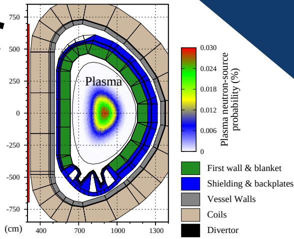

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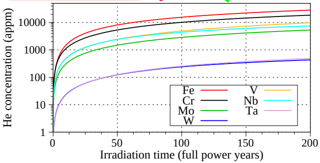

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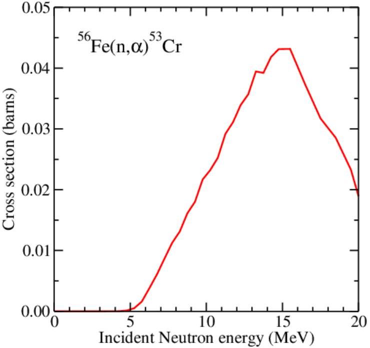
Helium production

- Helium production is a particular problem for fusion because of the generally higher neutron energies – many of the He producing reactions have thresholds
- Material comparison under identical DEMO hcpb conditions
- 3 fpy under outboard equatorial FW armour irradiation:



- FISPACT-II inventory calculations:
- Helium production highest in Be ($\sim$ 710 appm/fpy)
- More than an order of magnitude lower in Fe ($\sim$ 120 appm/fpy)
- Only $\sim$ 2 appm/fpy in W

appm=atomic parts per million; fpy - full power years

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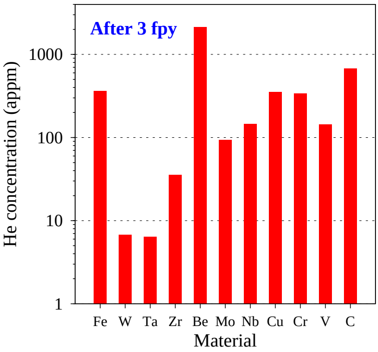

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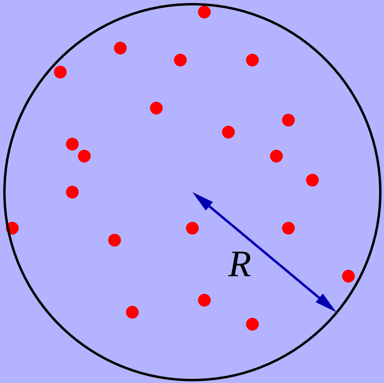
Simple modelling of grain boundary (GB) failure

1. Number of He atoms in spherical grain:

$$\boxed{N_{\mathrm{He}} \approx \frac{4}{3}\pi R^3 n G_{\mathrm{He}}}$$



Assumptions:

- All helium atoms produced migrate to grain boundary
  - traps neglected
  - most valid for small grains

G_{He} = bulk concentration (time evolution from inventory calcs.)

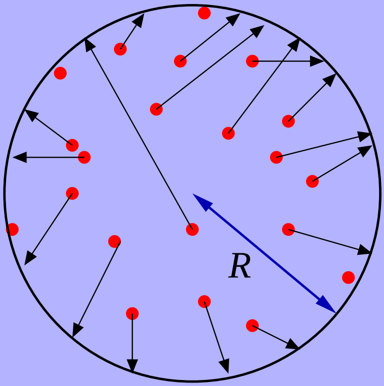
n = atom density

Modelling: He embrittlement of GBs

Simple modelling of grain boundary (GB) failure

2. All He atoms move to GB: – $\therefore$ surface total $\equiv$ bulk total

$$\boxed{4\pi R^2 \nu_{\mathrm{He}} = \frac{4}{3}\pi R^3 n G_{\mathrm{He}}} \quad \Rightarrow \quad \boxed{\nu_{\mathrm{He}} = \frac{R}{3} n G_{\mathrm{He}}}$$



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ν_{He} = surface density

Modelling: He embrittlement of GBs

UK Atomic Energy Authority

Simple modelling of grain boundary (GB) failure

3. GB destabilize when E of inserted He equals E of surfaces:

$$\boxed{E_{\text{He}}^{\text{insrt}} \nu_{\text{He}}^{c} \approx 2\varepsilon_{\text{surf}}}$$

Material	He insert. energy (eV)† – $E_{\text{He}}^{\text{insrt}}$	Surf. energy $(\text{Jm}^{-2})^{*}$ – $\varepsilon_{\text{surf}}$	Critical He conc. at GBs (cm^{-2}) – ν_{He}^{c}
Fe	2.77	2.4	1.08×10^{15}
Cr	2.68	2.3	1.07×10^{15}
Mo	1.91	3.0	1.96×10^{15}
Nb	1.60	2.7	2.11×10^{15}
W	1.61	3.5	2.71×10^{15}
V	2.30	2.6	1.41×10^{15}

* Averages of experimental data reported in: L. Vitos *et al.*, 1998, *Surf. Sci.*, **411** 186–202

† DFT values – Gilbert *et al. J. Nucl. Mater.* **442** (2013) S755

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Simple modelling of grain boundary (GB) failure

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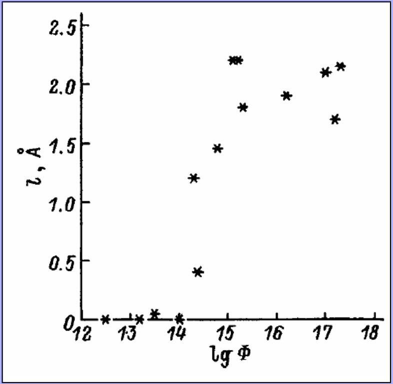

- Experimental confirmation:
  - Helium irradiated W bicrystals
  - Expansion of grain boundaries at He fluence of 10^{14}–10^{15} ions cm^{-2}
  - our ν_{He}^{c} value: 2.71×10^{15}

Gerasimenko, Mikhaĭlovskiĭ, Neklyudov, Parkhomenko, and Velikodnaya
Tech. Phys. **43** (1998) 803

Modelling: He embrittlement of GBs

UK Atomic Energy Authority

Simple modelling of grain boundary (GB) failure

4. Critical bulk He concentration:

$$\boxed{G^c_{\mathrm{He}} = \frac{3}{Rn}\nu^c_{\mathrm{He}}}$$

Material	ν^c_{He} (cm^{-2})	n (cm^{-3})	G^c_{He} (appm)
Fe	1.08×10^{15}	8.5×10^{22}	764.6
Cr	1.07×10^{15}	6.4×10^{22}	771.9
Mo	1.96×10^{15}	5.5×10^{22}	1833.8
Nb	2.11×10^{15}	6.3×10^{22}	2275.2
W	2.71×10^{15}	1.2×10^{23}	2582.1
V	1.41×10^{15}	4.7×10^{22}	1172.2

- Assumed Grain size of $R = 0.5\mu m$
- G^c_{He} varies with $1/R$

appm – atomic parts per million

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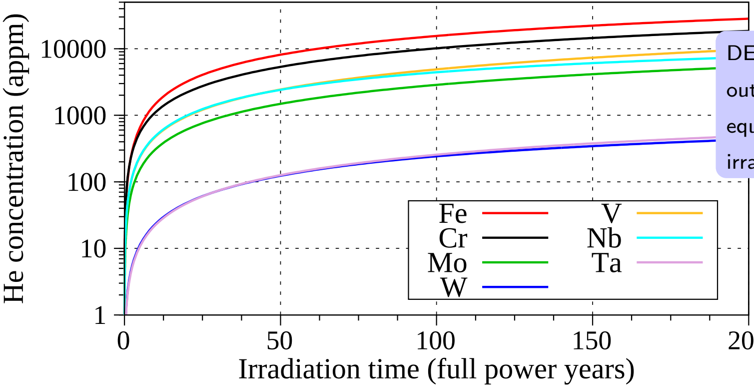
FISPACT-II results: helium production rates

- standard output during irradiation in FISPACT-II simulation

- Estimated “time to destabilize” t^c_{He} based on inventory calculations



DEMO hcpb outboard equatorial FW irradiation

appm = atomic parts per million

He embrittlement: Critical times

- t^c_{He} for irradiations in outboard equatorial DEMO FW armour position assuming linear grain size of 0.5 μm

Element	ν^c_{He} (cm^{-2})	G^c_{He} (appm)	t^c_{He} (fpy)			
			hcll	hcpb	wcll	wccb
Fe	1.08×10^{15}	764.6	9	6	8	7
Cr	1.07×10^{15}	771.9	7	7	7	7
Mo	1.96×10^{15}	1833.8	58	63	59	62
Nb	2.11×10^{15}	2275.2	45	47	46	46
W	2.71×10^{15}	2582.1	700+	597	700+	700+
V	1.41×10^{15}	1172.2	25	25	25	25

- For some elements, such as W, the He production rates are so low, and/or the ν^c_{He} is so great that the critical lifetimes are many hundreds of years
- only for $t^c_{\mathrm{He}} \lessapprox 10$ is this failure mechanism likely to be of concern

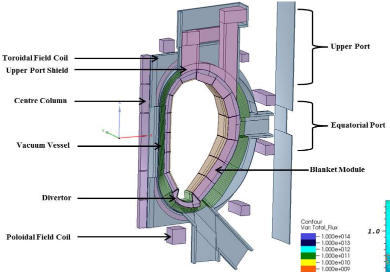
appm = atomic parts per million, fpy = full power year

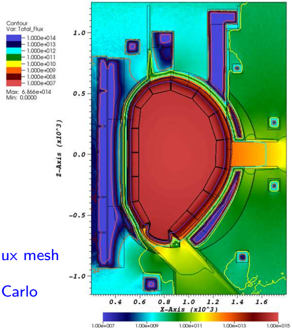
Applications

- Integrated assessment of helium embrittlement
- DEMO fusion power plant activation and waste analysis
- Material response database
- Primary damage spectra (& emitted particle spectra)

Application: DEMO activation & waste predictions

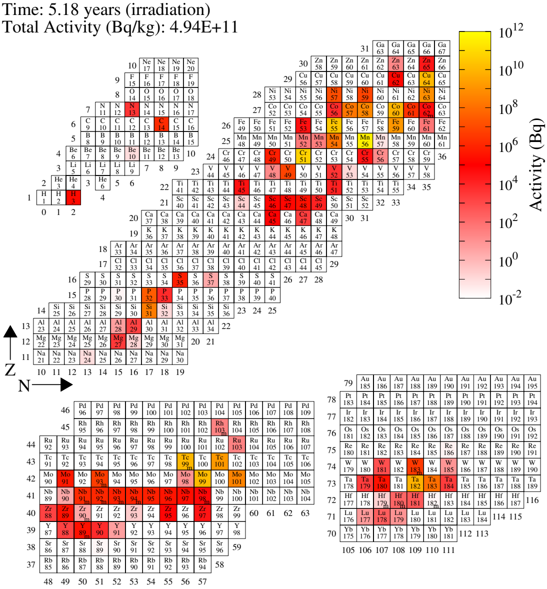
- (European) designs for a demonstration fusion power plant (DEMO) are still conceptual
- But inventory calculations have a role to play in guiding choices relating to
  - shielding requirements
  - maintenance schedules
  - radioactive waste generation
  - (active) cooling needs
- FISPACT-II is well-suited to such analyses
  - easily script-able for 1000s of simulations
  - fast (using binary data files)
  - standardized output formats for easy post-processing





Input neutron flux mesh from Monte Carlo

- Material composition (& hence activity) of each cell evolved in time according to a DEMO operational scenario
  - 22-year, 2-phase plan
  - one blanket replacement – 1-year shutdown
  - 3 divertor replacements – 8-month shutdowns



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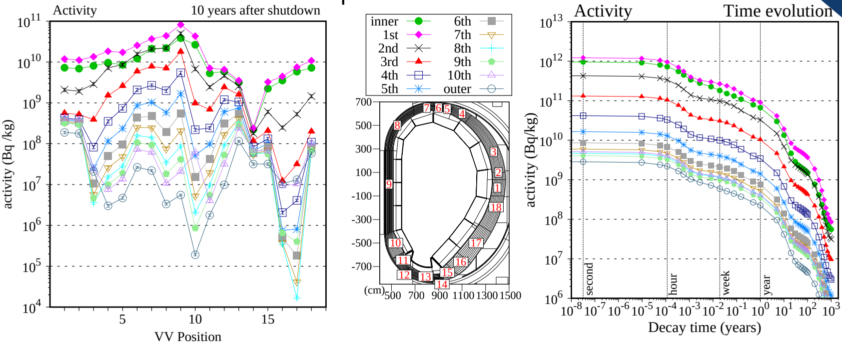
FISPACT-II automation

- e.g. for the vacuum vessel (VV) at end-of-life
- variation with time and depth in VV



- Output used to define waste (& recycling) class of component as a function of time

Waste classification

UK Atomic Energy Authority

- Preliminary waste classes based on IAEA structure and UK limits*:
  1) **NAW** – (non-active waste)
     - IAEA clearance index less than 1
  2) **LLW** – (low-level waste)
     - α activity less than 4 MBq kg^{-1} and combined β and γ activity of less than 12 MBq kg^{-1}
  3) **ILW** – (intermediate-level waste)
     - activities above LLW limits [high-level waste assumed to be zero]
- Recycling assessment:
  - component considered as being Potentially Recyclable Material (PRM) if contact γ dose is below 2 mSv hr^{-1}
    - (contact dose is a standard result, but also a conservative overestimate)
- replaced components (i.e. blankets and divertor) included in waste assessment
- 100% tritium removal assumed for blanket components

§HLW (high-level waste) assumed to be zero

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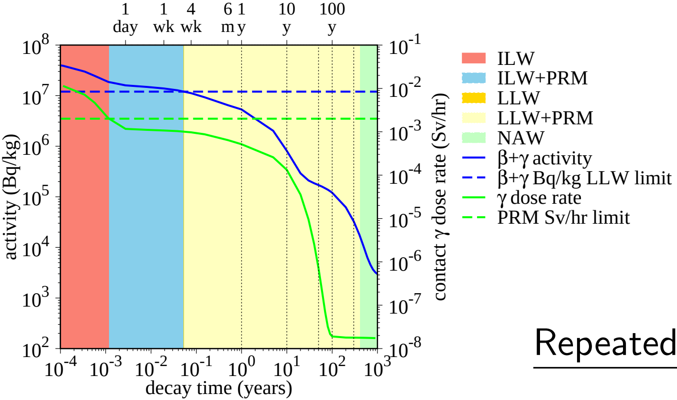
Typical evolution

- For a cell/region in the outboard Vacuum Vessel



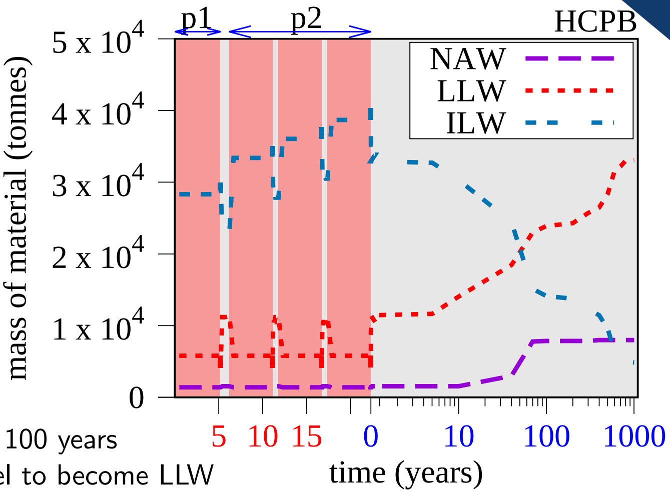
Repeated for all cells

- Never exceeds α-activity limit for LLW (true in general in fusion)
- Satisfies the $\beta + \gamma$-activity LLW limit after 20 days of decay cooling
- Meets the PRM limit sooner (after $\sim$ 10 hours)

Total reactor waste results

UK Atomic Energy Authority

- jumps in waste masses due to new components
- mainly ILW in first few decades after shutdown
- & very little NAW at any time



- takes more than 100 years for most of vessel to become LLW (dominated by blanket module masses)

blue time labels are post final shutdown;
red during operational life;
red shading is for periods of irradiation;
grey shading during shutdown.

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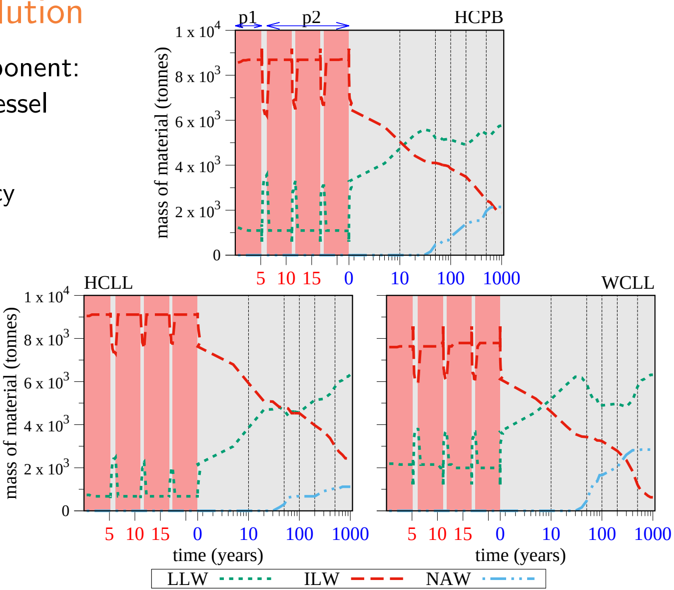
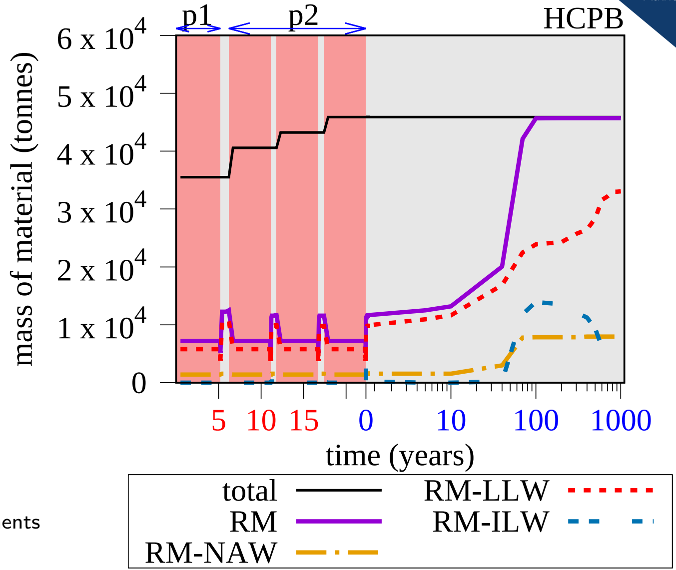
Waste Evolution

- For whole component: e.g. Vacuum Vessel
- slightly lower shielding efficiency in HCLL design
  - no water/Be moderation
- ⇒ higher neutron fluxes in VV
- ⇒ later cross-over to majority LLW



Total reactor recycling results

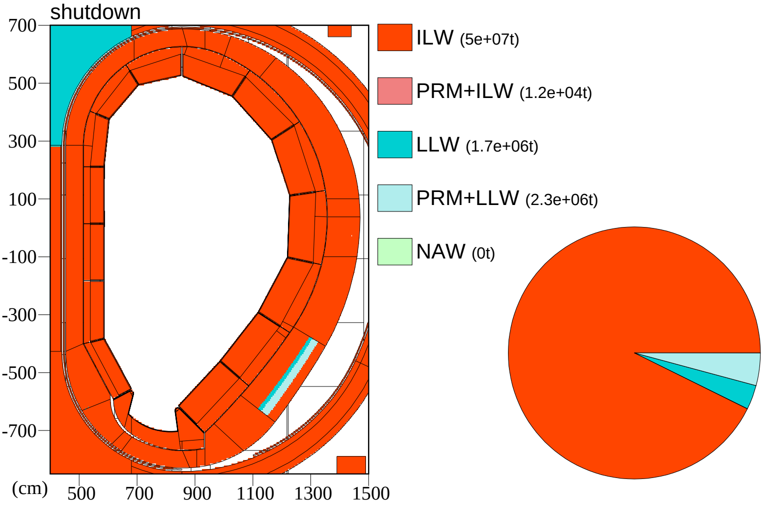
- entire design (including VV+IVCs) becomes potentially recyclable within 100 years despite waste classification



IVCs – in-vessel components

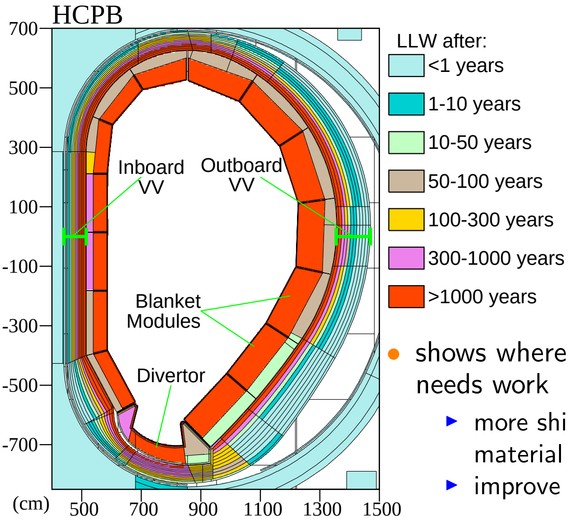
Time variation in class - entire DEMO reactor

- including pie-chart showing waste distribution)



Time to LLW plot

- re-processing of results to predict disposal criteria time-limits



- shows where design and modelling still needs work
  - more shielding, change to starting material compositions ...
  - improve detail (resolution) in model

Applications

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Application: material response database

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CULHAM CENTRE FOR FUSION ENERGY

CCFE-R(16)36
August 2016

Mark R. Gilbert
Jean-Christophe Sublet

Handbook of activation, transmutation, and radiation damage properties of the elements simulated using FISPACT-II & TENDL-2015; Magnetic Fusion Plants

785 pages
∼60000 calculations

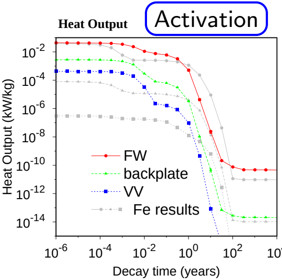
www.ccfe.ac.uk

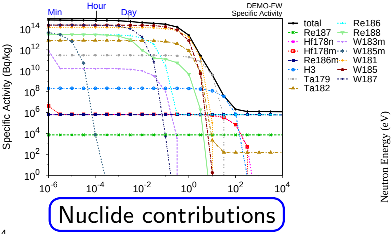
- Reference document of typical activity and burn-up responses of the elements to neutron irradiation is a useful tool during material selection exercises for nuclear components
- Results for all naturally occurring elements from H to Bi, with separate reports for:
  - predicted DEMO and ITER conditions
  - fission conditions (PWR, FBR, HFR)
- Available to download from http://fispact.ukaea.uk

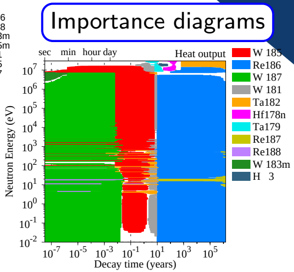
Scoping calculations for each element:

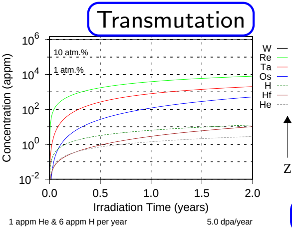
1. Tabulated activation response
   - % contributions of important radionuclides to various radiological quantities as a function of cooling time after irradiation
2. Graphs of activation response after irradiation
   - decay evolution of total activity, heat, and γ-dose under three different spectra & compared to Fe + indicative dominant nuclide contributions
   - nuclide contributions as a function of time
3. Importance diagrams
   - spectrum independent mapping of important radionuclides in the neutron-energy vs. decay time phase-space
4. Transmutation response
   - time evolution under irradiation of initially-pure elemental composition
   - nuclide concentration maps
5. Primary knock-on atom (PKA) distributions
   - $t_{irr} = 0$ spectra plotted as both elemental and isotopic sums
6. Reaction pathways
   - major production pathways for important radionuclides at four characteristic neutron-energy ranges

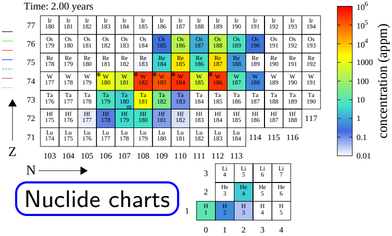
Example outputs: W

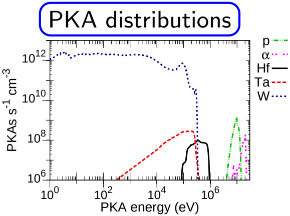






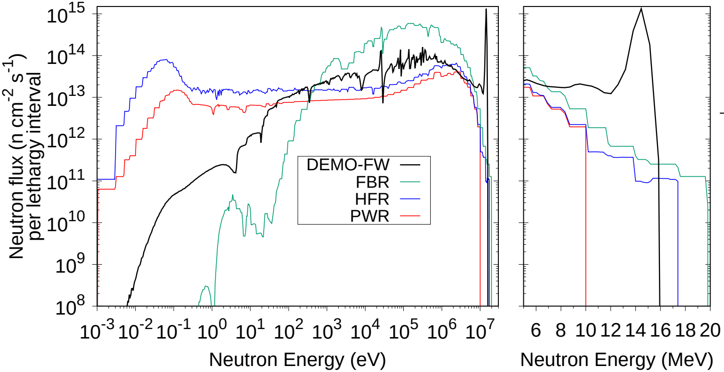






Neutron irradiation fields

- Monte Carlo simulations of a fusion DEMOnstration power plant & typical fission reactors



total fluxes ϕ: ($\times 10^{14}$ n cm^{-2} s^{-1})

DEMO	6
FBR	24
HFR	5
PWR	3

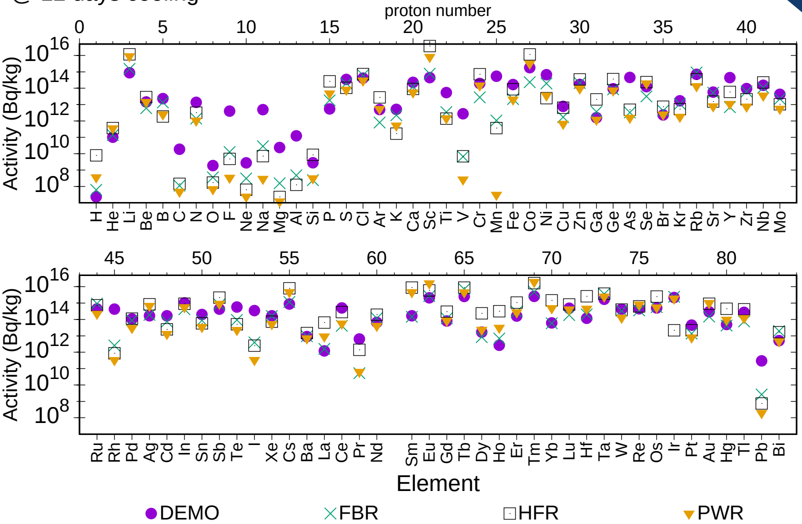
- fusion spectrum in first wall (FW) dominated by 14 MeV peak
- well-moderated (averaged) fission spectra don't have such dominant peaks but can have tails that explore the 14 MeV region of fusion

FBR – superphenix Fast Breeder Reactor
HFR – High Flux Reactor, Petten
PWR – Pressurized Water-cooled Reactor

Activation – fusion vs. fission

- time snapshot of activity during decay cooling§:

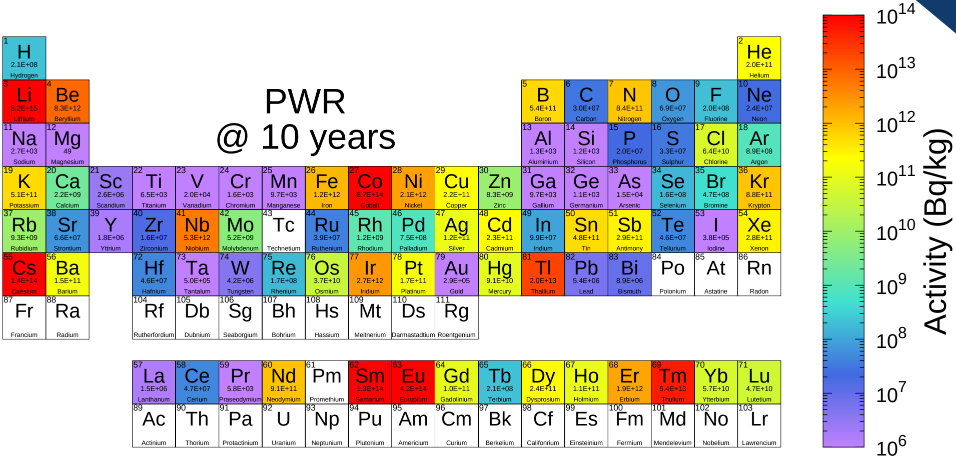
@ 12 days cooling



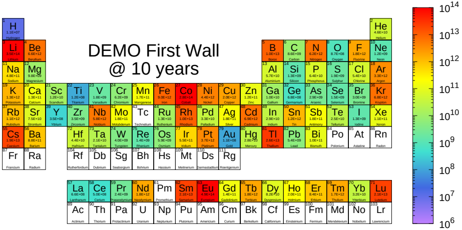
§after 2 years of continuous irradiation

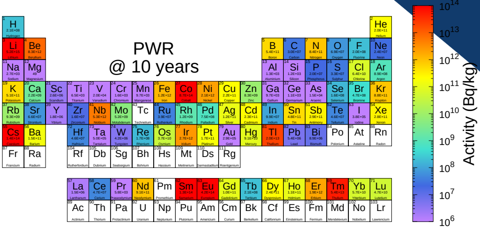
Activation summary – periodic table plot

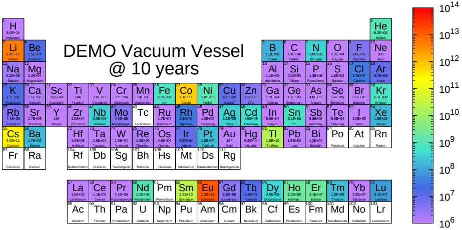
- total becquerel/kg activity from each element at 10-years following a 2-year PWR irradiation:

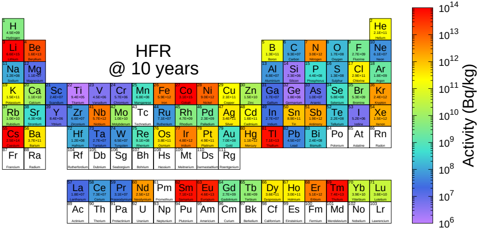


Activation summary – periodic table



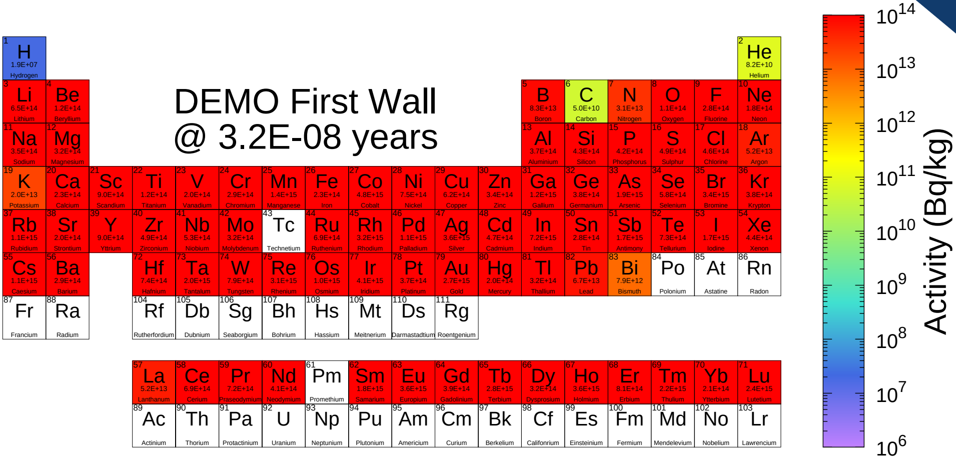






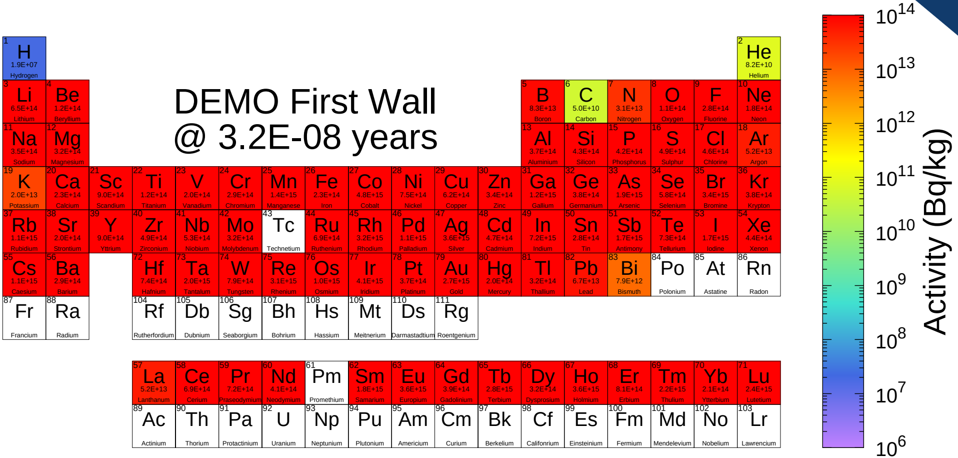
Activation summary – animated

- total becquerel/kg activity from each element as a function of time following 2-year irradiation



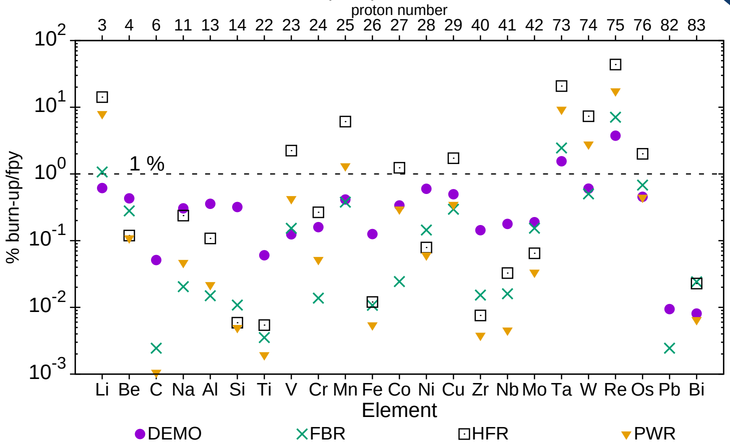
Activation summary – animated

- total becquerel/kg activity from each element as a function of time following 2-year irradiation



Transmutation – fusion vs. fission

- % burn-up per full-power year (fpy) for selected elements:

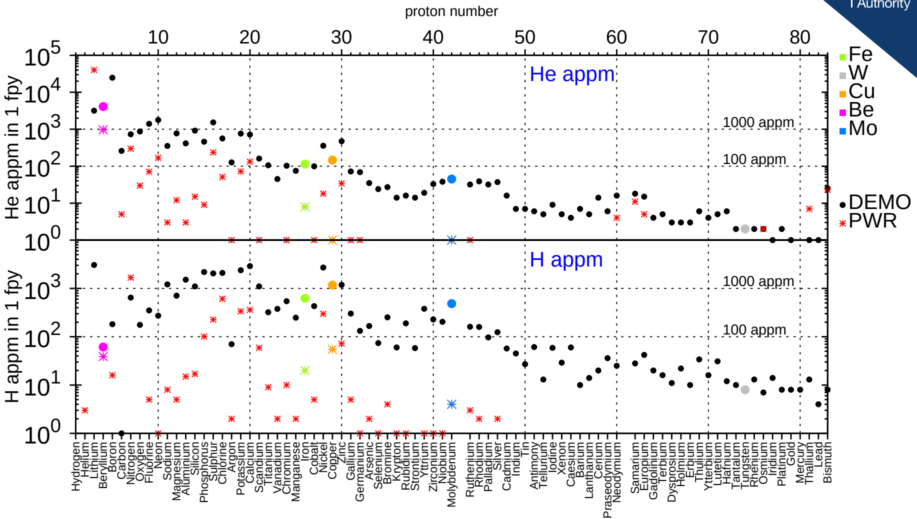


- Fission spectra are more-moderated ("softer") than fusion & combined with high-flux in HFR produces greater burn-up rates in many elements[§] ⇒ spectrum modification (via shielding) required to match fusion in experimental campaigns

[§] due to higher neutron capture rates

Gas production – fusion vs. fission

- Gas appm after 1 fpy in DEMO first wall and PWR:



- gas production is significantly higher under fusion neutrons
  - ▶

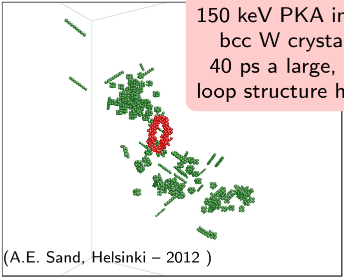
Applications

- Integrated assessment of helium embrittlement
- DEMO fusion power plant activation and waste analysis
- Material response database
- Primary damage spectra (& emitted particle spectra)

Application: PKA distributions

- Motivation: a full description of the initial damage events (the primary knock-on atoms or PKAs) under irradiation is a necessary input to modelling and simulation of radiation damage
  - PKA energy.vs.flux distributions provide more information than simpler damage-dose measures (e.g. dpa)

- Complete evaluation requires all possible nuclear reaction channels to be considered:
  - elastic & inelastic scattering, and non-elastic reactions ($(n, p), (n, 2n)$, etc.)
  - including secondary emitted (light) gas particles - α (^{4}He), protons (^{1}H), etc, as PKAs



150 keV PKA in a perfect bcc W crystal - after 40 ps a large, coherent loop structure has formed

(A.E. Sand, Helsinki – 2012)

PKA – primary knock-on atom

Additional need

- emitted particle spectra for α, protons, neutrons, γ, etc.
- could be used in FISPACT-II to compute transmutation from secondary particles

PKA – primary knock-on atom

PKA distributions

Calculation method (1)

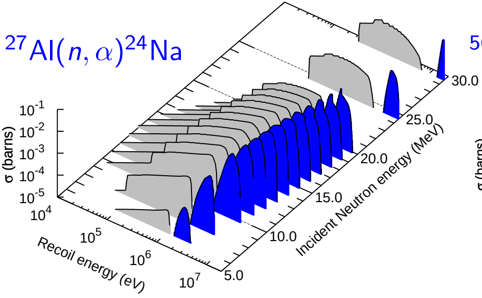
- From raw pointwise nuclear data (TENDL)
- Neutron interaction recoil matrices $M^{x\rightarrow y} \equiv \{m_{ij}^{x\rightarrow y}\}$ calculated using NJOY[§] (via GROUPR)
  - $m_{ij}^{x\rightarrow y}$ is the recoil cross section (in barns) for a recoil energy E_i of daughter y resulting from an incident neutron energy E_j on parent x
- for each target (parent) isotope x there will be a set of $M^{x\rightarrow y}$
  - (at least) one for each reaction channel
- & each reaction may have more than one associated matrix
  - for example, (n,α) will produce a heavy recoil and an α-particle (^{4}He nucleus)
- recoil matrices can also be produced for charged particle interactions

[§]the nuclear data processing system developed at LANL

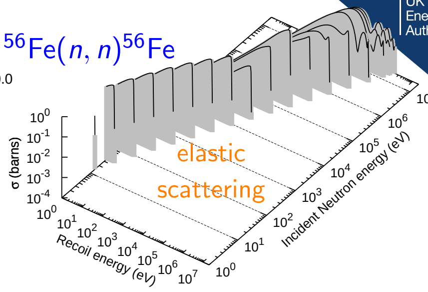
$M^{x \to y}$ matrices & vectors

UK Atomic Energy Authority

$^{27}Al(n,\alpha)^{24}Na$



$^{56}Fe(n,n)^{56}Fe$

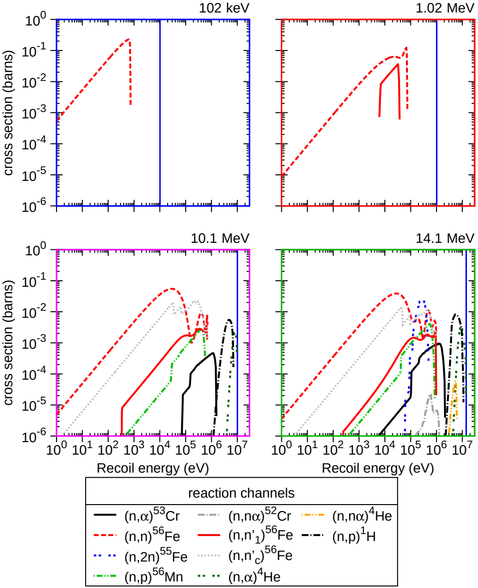


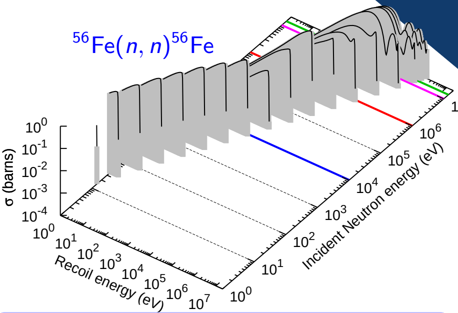
- Non-elastic nuclear reactions can produce two recoiling species
- The main (heavy) residual and a higher energy light (gas) particle
- On ^{27}Al the threshold (n,α) reaction produces ^{24}Na (grey) recoils and ^{4}He particles (blue)

- The primary reaction channel is normally simple elastic scattering
- Produces recoils for all incident neutron energies
- Other channels only become important at higher energy...

CCFE CULHAM CENTRE FOR FUSION ENERGY

$M^{x\rightarrow y}$ matrices & vectors – ^{56}Fe





- In ^{56}Fe, at low incident energy only elastic and inelastic channels are open
- Number of contributing channels increases at higher energies (MeV range)

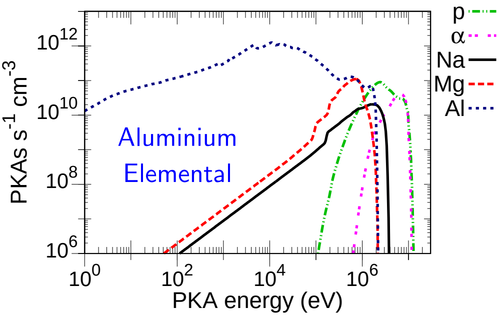
Calculation method (2)

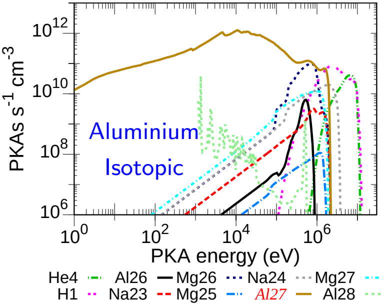
UK Atomic Energy Authority

- Collapsing each recoil matrix with a neutron irradiation spectrum $\{\phi_j\}$ gives the recoil-energy spectrum $R^{x\rightarrow y}(E)$:

$$\text{"PKA-spectrum" under neutron irradiation} \equiv R^{x\rightarrow y}(E) \equiv \{r_i^{x\rightarrow y}\} = \left\{\sum_j m_{ij}^{x\rightarrow y}\phi_j\right\}$$

- processing (& summing) done with `SPECTRA-PKA`[§] utility





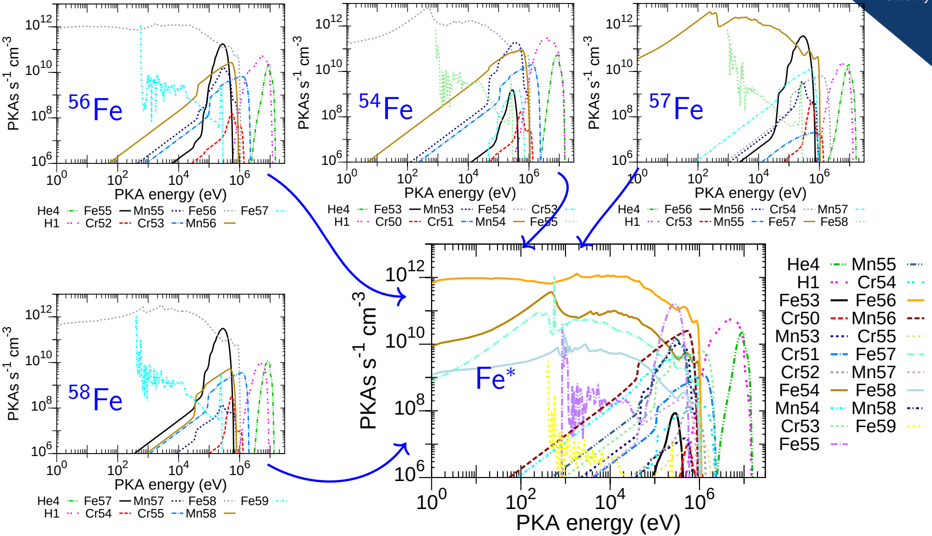
- PKA spectra of pure Al under DEMO conditions
- many different recoil species (even with just Al27 target)

§ Gilbert *et al.*, *JNM* **467** (2015) 121-134

CCFE CULHAM CENTRE FOR FUSION ENERGY

PKA results – e.g. Fe

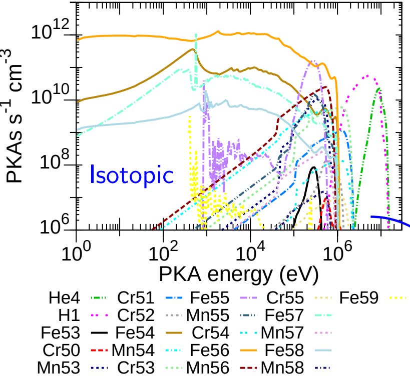
- Isotopic results for each nuclide in the material must be merged:

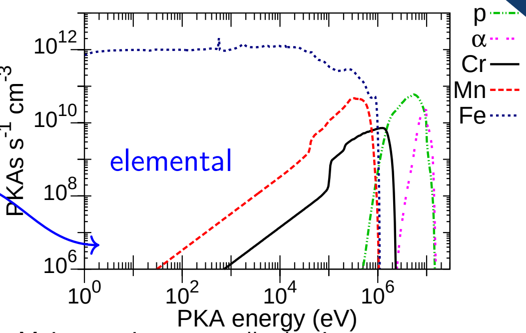


*5.845% ^{54}Fe, 91.754% ^{56}Fe, 2.119% ^{57}Fe, 0.282% ^{58}Fe (atomic percentages)

PKA results – e.g. Fe

- For modelling it is more useful to sum the isotopic spectra:

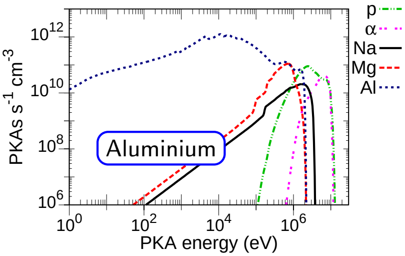


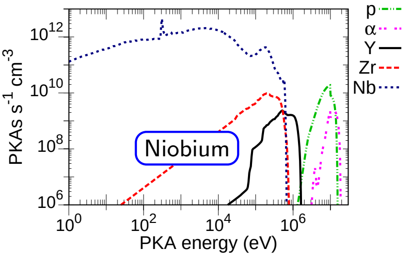


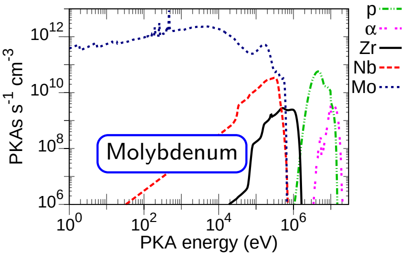
- Main constituent usually dominates

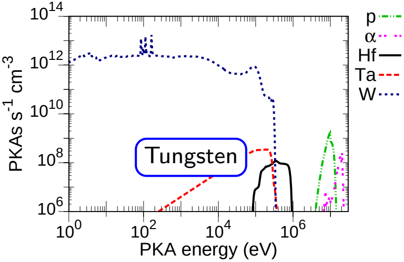
- Total PKAs (s^{-1}cm^{-3}) in material can be calculated by summing (& integrating over) all elemental distributions
- here there are 4.33E+14 PKAs s^{-1}cm^{-3} above 1eV (light particles excluded)
- the average PKA energy above 10 eV for the Fe+Mn+Cr spectrum is 18.8 keV

PKA distributions – elemental





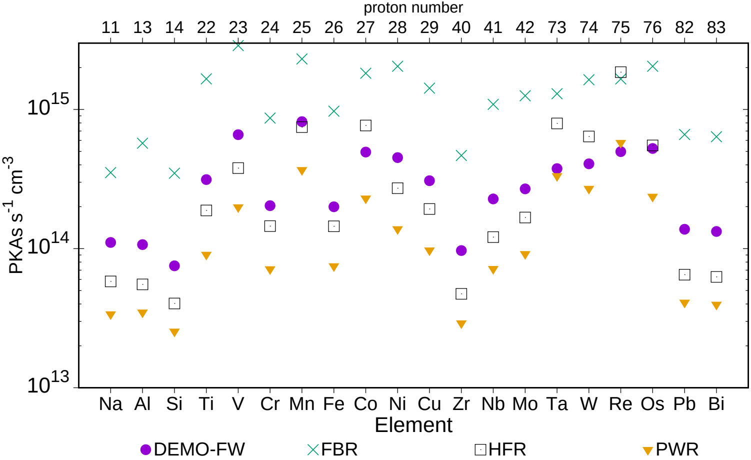




- Under DEMO FW conditions

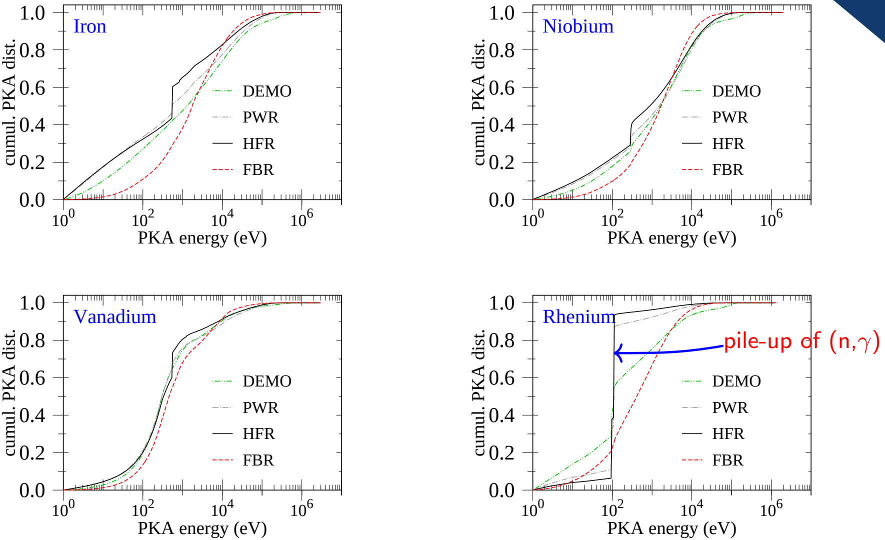
Total PKA rates – fusion vs. fission

- total heavy PKAs (H/He excluded) for selected materials



- FBR spectrum produces highest rates due to high, fast flux
- PWR the lowest

Cumulative (PKA) probability distributions



- FPR missing low and high energy parts due to peaked spectrum

Damage energy & dpa from SPECTRA-PKA

- The displacement energy in the NRT-dpa formula is normally calculated using the total damage kerma cross section
- However, with SPECTRA-PKA, it is possible to calculate the damage contribution as a function of reaction channel
  – a new & novel capability
- Standard LSS[§] formula to account for electronic loss and convert PKA energy into damage energy – including correct treatment of parent and daughter mass
- displacement-energy rate accumulated and summed using PKA rate at each damage energy. NRT formula can be applied to the total
- For a given reaction channel, the total displacement energy is:

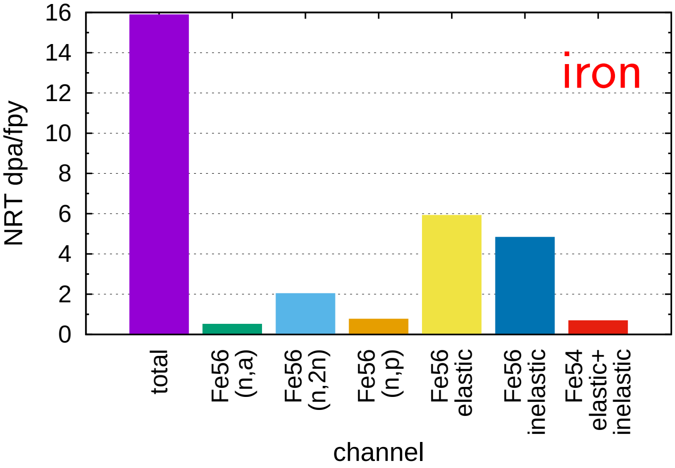
$$\sum_i T^{LSS}(E_i^{pka})R_i^{pka},$$

where $T^{LSS}(E^{pka})$ is the LSS equivalent energy for PKA energy E^{pka}, and R_i^{pka} is number of PKAs at energy E_i^{pka}

[§] Lindhard, Scharff, Schiøtt, *Mat. Fys. Medd. Dan. Vid. Selsk.* **33** (1963) 1–42

Damage energy from SPECTRA-PKA

- Channel contributions to NRT dpa/fpy* for Fe[§] under DEMO FW conditions:



TENDL results

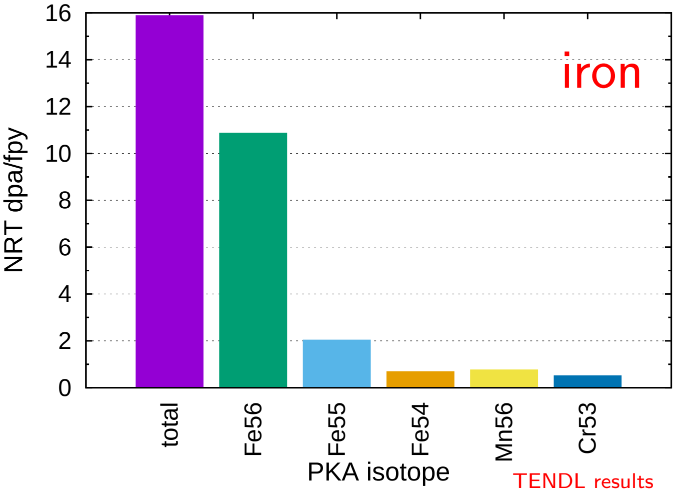
- Largest contributions are from scattering of ^{56}Fe (91.2 atm.%)
- ^{56}Fe(n,2n) also important (13%)
- total agrees with value obtained from standard approach – FISPACT-II & total damage kerma

Gilbert and Sublet, JNM **504** (2018) 101-108

*fpy – full power years
§ $E_d = 40$ eV

Damage energy from SPECTRA-PKA

- Nuclide contributions to NRT dpa/fpy* for Fe§ under DEMO FW conditions:



TENDL results

- the per-channel dpas summed by daughter indicate the proportion of damage from different recoiling species
- dominated by Fe nuclides, but with a contribution from ^{56}Mn & ^{53}Cr

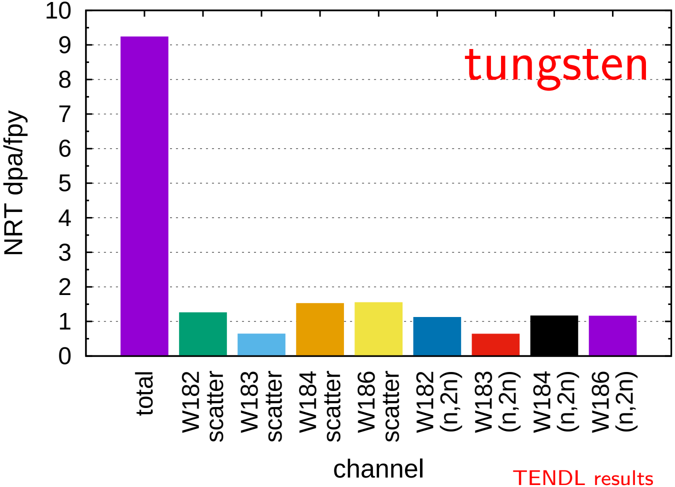
Gilbert and Sublet, JNM **504** (2018) 101-108

*fpy – full power years

§ $E_d = 40$ eV

Damage energy from SPECTRA-PKA

- Channel contributions to NRT dpa/fpy for W§ under DEMO FW conditions:



TENDL results

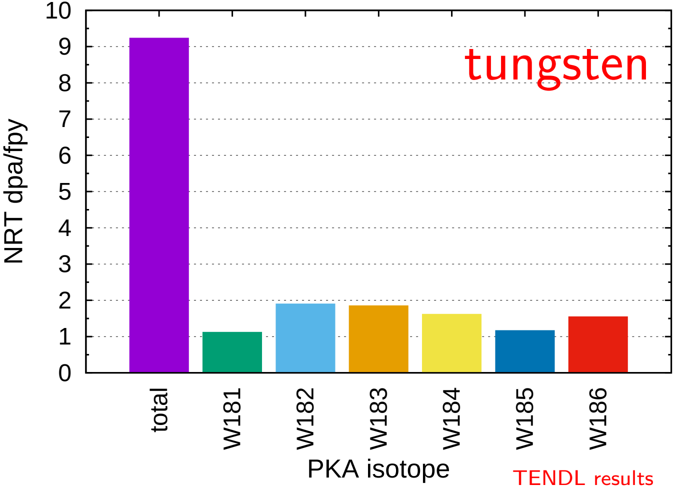
- In W, (n,2n) contributes as much as elastic/inelastic scattering

Gilbert and Sublet, JNM **504** (2018) 101-108

§ $E_d = 55$ eV

Damage energy from SPECTRA-PKA

- Nuclide contributions to NRT dpa/fpy for W§ under DEMO FW conditions:



TENDL results

- no significant contributions from reactions that produce isotopes of other elements

Gilbert and Sublet, JNM **504** (2018) 101-108

§ $E_d = 55$ eV

Running SPECTRA-PKA

- SPECTRA-PKA is now open-source and downloadable from: https://github.com/fispact/SPECTRA-PKA
- code is command-line driven
- execution controlled by an input file of code words and values (similar to FISPACT-II, but order does not matter)

  `<location of SPECTRA-PKA>SPECTRA-PKA input.in`
- manual on the github explains use of all code-words & provide there is an example calculation...
  - including example plotting script to visualize results (with gnuplot)
- ...this is a good place to start
  - & example input can be easily modified to a specific material/spectrum of interest
  - if not already compiled on your system, the executable for SPECTRA-PKA can be easily created
    - navigate to `fispact/source/spectra-pka` and type `make`

Gilbert and Sublet, JNM **504** (2018) 101-108