Dates	(Ma)													Cor	nposition								otopic Ratios													Coefficients										
206Pt raction 238U	o/ '-2"   206 2 <u>3</u> 8	SPb/ BU '-2" 2	207Pb/ ´-2*	207Pb/	´-2ˇ Cor	ŗ	208 <u>Pb</u> / ′-	207Pb/ 2 <u>0</u> 6Pb	2071 2351	Pb/ U ~2 2	207Pb/ 206Pb ´-2ˇ	207Pb/ 2 <u>0</u> 6Pb	´–2ˇ be	est ´–2´ Mas	ss mass	conc (	Ţh ,	Ţh/ Pb*	total co	nc c	onc conc	Pb*/ 20	96Pb/ 208Pb/ 20	6Pb/	07Pb/	207Pb/	208 <u>P</u> b/	206l 2 <u>38</u> l	Pb/ 207P J. 235U	b/ 20 20	7Pb/ 6Pb	207Pb/ 206Pb	207Pb/ 206Pb	Corr.	206Pb/238U	J 206Pb/238U <th>-</th> <th>206Pb/238U -207Pb/</th> <th>206Pb/238U <th>&gt;-207Pb/</th><th>207Pb/206Pb</th><th>207Pb/206Pb 2</th><th>207Pb/206Pb 2 <th>-238U/ &lt;</th><th>07Pb/206Pb ThPa&gt;-238U/ 06Pb <th> Fraction</th></th></th></th>	-	206Pb/238U -207Pb/	206Pb/238U <th>&gt;-207Pb/</th> <th>207Pb/206Pb</th> <th>207Pb/206Pb 2</th> <th>207Pb/206Pb 2 <th>-238U/ &lt;</th><th>07Pb/206Pb ThPa&gt;-238U/ 06Pb <th> Fraction</th></th></th>	>-207Pb/	207Pb/206Pb	207Pb/206Pb 2	207Pb/206Pb 2 <th>-238U/ &lt;</th> <th>07Pb/206Pb ThPa&gt;-238U/ 06Pb <th> Fraction</th></th>	-238U/ <	07Pb/206Pb ThPa>-238U/ 06Pb <th> Fraction</th>	Fraction
raction 2380• 56-99::R56-99		n≯  abs  2	2350⁴ ∣abs	206Pb	abs coet	f.  % disc <sup>c</sup>	<sup>?</sup> ∣2321㎡ ∣a	abs∣ <ih≯< th=""><th>abs <pa< th=""><th>a≯  abs  ∢</th><th><pa≯ abs<="" th=""><th>s  <ihpa9e< th=""><th>abs da</th><th>ate  abs  (g)</th><th>U(ˌg</th><th>U(ppm)</th><th>(ppm)<sup>r</sup></th><th>U (pg) <sup>g</sup></th><th>(pg) <sup>n</sup> Pb(pg) (p</th><th>pm) ((</th><th>opm) (ppm)</th><th> Pbc  20</th><th>14Pb   206Pb   23</th><th>8U   -2 %2</th><th>35U   -2</th><th>2°%206Pb   -</th><th>-2° %2321ff</th><th><math>\frac{1}{2}</math> % &lt; 1 h:</th><th><sup>⊀°</sup>   '–2' %<pa≯< th=""><th>e   '-2' %&lt; </th><th>h≯<sup>to</sup>   '-2' %</th><th>&gt;<pa≯<sup>e   ~-2</pa≯<sup></th><th>%<thpa≸<sup>©</thpa≸<sup></th><th>–2* % coef.</th><th>207Pb/2350</th><th>J 207Pb/235U</th><th>235U <pa></pa></th><th>235U <pa></pa></th><th>238U/206Pb</th><th>238U/206Pb   2</th><th>207Pb &lt;1h&gt; 2</th><th>06Pb &lt;1h&gt;   Fraction</th></pa≯<></th></ihpa9e<></th></pa≯></th></pa<></th></ih≯<>	abs <pa< th=""><th>a≯  abs  ∢</th><th><pa≯ abs<="" th=""><th>s  <ihpa9e< th=""><th>abs da</th><th>ate  abs  (g)</th><th>U(ˌg</th><th>U(ppm)</th><th>(ppm)<sup>r</sup></th><th>U (pg) <sup>g</sup></th><th>(pg) <sup>n</sup> Pb(pg) (p</th><th>pm) ((</th><th>opm) (ppm)</th><th> Pbc  20</th><th>14Pb   206Pb   23</th><th>8U   -2 %2</th><th>35U   -2</th><th>2°%206Pb   -</th><th>-2° %2321ff</th><th><math>\frac{1}{2}</math> % &lt; 1 h:</th><th><sup>⊀°</sup>   '–2' %<pa≯< th=""><th>e   '-2' %&lt; </th><th>h≯<sup>to</sup>   '-2' %</th><th>&gt;<pa≯<sup>e   ~-2</pa≯<sup></th><th>%<thpa≸<sup>©</thpa≸<sup></th><th>–2* % coef.</th><th>207Pb/2350</th><th>J 207Pb/235U</th><th>235U <pa></pa></th><th>235U <pa></pa></th><th>238U/206Pb</th><th>238U/206Pb   2</th><th>207Pb &lt;1h&gt; 2</th><th>06Pb &lt;1h&gt;   Fraction</th></pa≯<></th></ihpa9e<></th></pa≯></th></pa<>	a≯  abs  ∢	<pa≯ abs<="" th=""><th>s  <ihpa9e< th=""><th>abs da</th><th>ate  abs  (g)</th><th>U(ˌg</th><th>U(ppm)</th><th>(ppm)<sup>r</sup></th><th>U (pg) <sup>g</sup></th><th>(pg) <sup>n</sup> Pb(pg) (p</th><th>pm) ((</th><th>opm) (ppm)</th><th> Pbc  20</th><th>14Pb   206Pb   23</th><th>8U   -2 %2</th><th>35U   -2</th><th>2°%206Pb   -</th><th>-2° %2321ff</th><th><math>\frac{1}{2}</math> % &lt; 1 h:</th><th><sup>⊀°</sup>   '–2' %<pa≯< th=""><th>e   '-2' %&lt; </th><th>h≯<sup>to</sup>   '-2' %</th><th>&gt;<pa≯<sup>e   ~-2</pa≯<sup></th><th>%<thpa≸<sup>©</thpa≸<sup></th><th>–2* % coef.</th><th>207Pb/2350</th><th>J 207Pb/235U</th><th>235U <pa></pa></th><th>235U <pa></pa></th><th>238U/206Pb</th><th>238U/206Pb   2</th><th>207Pb &lt;1h&gt; 2</th><th>06Pb &lt;1h&gt;   Fraction</th></pa≯<></th></ihpa9e<></th></pa≯>	s   <ihpa9e< th=""><th>abs da</th><th>ate  abs  (g)</th><th>U(ˌg</th><th>U(ppm)</th><th>(ppm)<sup>r</sup></th><th>U (pg) <sup>g</sup></th><th>(pg) <sup>n</sup> Pb(pg) (p</th><th>pm) ((</th><th>opm) (ppm)</th><th> Pbc  20</th><th>14Pb   206Pb   23</th><th>8U   -2 %2</th><th>35U   -2</th><th>2°%206Pb   -</th><th>-2° %2321ff</th><th><math>\frac{1}{2}</math> % &lt; 1 h:</th><th><sup>⊀°</sup>   '–2' %<pa≯< th=""><th>e   '-2' %&lt; </th><th>h≯<sup>to</sup>   '-2' %</th><th>&gt;<pa≯<sup>e   ~-2</pa≯<sup></th><th>%<thpa≸<sup>©</thpa≸<sup></th><th>–2* % coef.</th><th>207Pb/2350</th><th>J 207Pb/235U</th><th>235U <pa></pa></th><th>235U <pa></pa></th><th>238U/206Pb</th><th>238U/206Pb   2</th><th>207Pb &lt;1h&gt; 2</th><th>06Pb &lt;1h&gt;   Fraction</th></pa≯<></th></ihpa9e<>	abs da	ate  abs  (g)	U(ˌg	U(ppm)	(ppm) <sup>r</sup>	U (pg) <sup>g</sup>	(pg) <sup>n</sup> Pb(pg) (p	pm) ((	opm) (ppm)	Pbc  20	14Pb   206Pb   23	8U   -2 %2	35U   -2	2°%206Pb   -	-2° %2321ff	$\frac{1}{2}$ % < 1 h:	<sup>⊀°</sup>   '–2' % <pa≯< th=""><th>e   '-2' %&lt; </th><th>h≯<sup>to</sup>   '-2' %</th><th>&gt;<pa≯<sup>e   ~-2</pa≯<sup></th><th>%<thpa≸<sup>©</thpa≸<sup></th><th>–2* % coef.</th><th>207Pb/2350</th><th>J 207Pb/235U</th><th>235U <pa></pa></th><th>235U <pa></pa></th><th>238U/206Pb</th><th>238U/206Pb   2</th><th>207Pb &lt;1h&gt; 2</th><th>06Pb &lt;1h&gt;   Fraction</th></pa≯<>	e   '-2' %<	h≯ <sup>to</sup>   '-2' %	> <pa≯<sup>e   ~-2</pa≯<sup>	% <thpa≸<sup>©</thpa≸<sup>	–2* % coef.	207Pb/2350	J 207Pb/235U	235U <pa></pa>	235U <pa></pa>	238U/206Pb	238U/206Pb   2	207Pb <1h> 2	06Pb <1h>   Fraction				
	1.2 180	13 12 1	185 14	240	180 0.70	24 87	. 0	0 239	180 185	14	240 180	239	180 0	0 0 0	0010 0 0001	83475   1 8347	5 0	0.83 5.89	4 37 10 2560 0	0588742	0 102560	1 (	93 0 264 0 0	02835 0 68	199 8:	3 0 0510 7	7.8 0	0 002	8363 0.68 0.199	266 83 0	050955 7.8	0.050978 7.8	3 0.050953	7.8 0.700	0.70	0.70	0.70	0.70	-0.65	-0.65	-0.65	-0.65 71				
3 180.8	8 0.37 180	0.96 0.37 1	182.0 4.5	197	59 0.71	12 8.30	0 0	0 196	59 182	2.0 4.5	197 59	196	59 0	0.00	0.0001	44474 1.4447	4 0	1.03 4.88	0.84 5.71570 0.	0487701	0 0.057157	0 6 3	325 0.327 0.0	028456 0.21	0.1964 2.	7 0.0500 2	2.5 0	0 0.02	8468 0.21 0.196	3361 2.7 0.	050027 2.5	0.050047 2.5	0.050935	2.5 0.712	0.70	0.71	0.71	0.71	-0.67	-0.67	-0.67	-0.67 z3				
4 180.0	8 0.51 180	0.16 0.51 1	182.4 4.5	213	58 0.68	15.50	0 (	0 212	58 182	2.4 4.5	213 58	212	58 0	0.00	0.0001	74678 1.7467	8 0	0.75 5.49	1.14 6.63661 0.	0549479	0 0.066366	1 5 2	289 0.240 0.0	028328 0.28	.1968 2.	7 0.0504 2	2.5 0	0 0.02	8342 0.28 0.196	8821 2.7 0.	050367 2.5	0.050390 2.5	0.050366	2.5 0.687	7 0.69	0.69	0.69	0.69	-0.62	-0.62	-0.62	-0.62 z4				
13 186.9	1.4 187	7.0   1.4   1	190 17	227	210 0.80	06 17.76	0 0	0 226	210 190	17	227 210	226	210 0	0  0  0.00	0.0000	282345 0.2823	45 0	0.90 0.956	0.80 1.75403 0	00956251	0 0.017540	3 1 8	0.286 0.0	02942 0.74	0.206 9.8	8 0.0507 9	9.2 0	0 0.02	9429 0.74 0.205	5629 9.8 0.	050678 9.2	0.050699 9.2	0.050677	9.2 0.806	0.81	0.81	0.81	0.81	-0.78	-0.78	-0.78	-0.78 z13				
19 180.6	1.0 181 5 0.71 180	1.2 1.0 1 0.74 0.71 1	184.4 9.3	233	120 0.77	73 22.32	0 0	0 250	120 184	4 9.3	232 120	) 231	120 0	0.00	0.0000	0.742773 0.7427	3 0	0.71 2.32	1.60 3.92021 0.	0232382	0.039202	6 2 1	0.224 0.0  36	02842 0.40	0.201 7.0 0.199 5.3	5 0.0508 5	7.2 0 5.2 0	0 0.02	88434 0.40 0.199	0122 5.5 0.	051203 7.2 050791 5.2	0.051227 7.2 0.050816 5.2	2 0.051202 2 0.050790	7.2 0.783 5.2 0.773	3 0.78	0.78	0.78	0.78	-0.75 -0.74	-0.75 -0.74	-0.75 -0.74	-0.75 216 -0.74 719				
20 180.7	4 0.57 180	0.83 0.57 1	182.6 7.5	206	99 0.78	32 12.36	0	0 205	99 182	2.6 7.5	206 99	205	99 0	0.00	0.0000	682598 0.6825	98 0	0.63 2.09	0.85 2.93693 0	0208739	0 0.029369	3 2 1	61 0.199 0.0	028435 0.32	0.1970 4.5	5 0.0502	4.2 0	0 0.02	8449 0.32 0.196	6975 4.5 0.	050217 4.2	0.050241 4.2	2 0.050216	4.3 0.782	0.78	0.78	0.78	0.78	-0.75	-0.75	-0.75	-0.75 z20				
56-28::R56-28																																														
	4 0.66 182	2.83 0.66 1	183.2 5.5	189	72 0.54	3.35	0 0	0 188	72 183	5.2 5.5	189 72	188	72 0	0.00	0.0001	94848 1.9484	8 0	0.58 5.95	1.63 7.57754 0.	0595167	0 0.075775	4 4 2	234 0.185 0.0	02875 0.37	0.1977 3.3	3 0.0499 3	3.1 0	0 0.02	8768 0.37 0.197	7718 3.3 0.	049848 3.1	0.049872 3.1	0.049847	3.1 0.549	0.55	0.55	0.55	0.55	-0.46	-0.46	-0.46	-0.46 z4				
6 182.1 7 181.8	9   0.93   182 9   0.62   181	2.28 0.93 1 1.97 0.62 1	188 12 183 4 6 4	203	150 0.78 84 0.65	32 31.68 50 10.30	0 0	0 266	150 188 84 183	34 64	267 150 203 84	200	84 0	0.00	0.0002	20457 2.2045 62240 1.6224	0 0	0.74 7.00	4.82 11.8110 0. 1.76 6.97318 0.	0520821	0.118110	8 3 1	83 0.253 0.0	028617 0.34	7.204 1979 3	8 0.0502 3	0.8	0 0.02	28680 0.52 0.203 28631 0.34 0.197	7944 38 0	051552 6.8 050144 3.6	0.051576 6.8	0.051551 0.050143	3.6 0.782	0.78	0.78	0.78	0.78	-0.75 -0.59	-0.75 -0.59	-0.75 -0.59	-0.75 Z6 -0.59 z7				
8 182.0	1 0.29 182	2.10 0.29 1	179.4 3.6	145	50 0.57	71 -25.94	0 0	0 143	50 179	0.4 3.6	144 50	143	50 0	0 0.00	0.0001	79366 1.7936	6 0	0.70 5.62	1.00 6.62230 0.	0561921	0 0.066223	0 6 3	0.222 0.0	028637 0.16	0.1932 2.5	2 0.0489 2	2.1 0	0 0.02	8651 0.16 0.193	3195 2.2 0.	048907 2.1	0.048930 2.3	0.048906	2.1 0.571	0.57	0.57	0.57	0.57	-0.52	-0.52	-0.52	-0.52 z8				
9 182.2	8 0.28 182	2.37 0.28 1	184.0 3.4	206	45 0.73	32 11.72	0 0	0 205	45 184	.0 3.4	206 45	205	45 0	0.00	0.0003	22312 3.2231	2 0	0.58 9.82	1.90 11.7136 0	0981620	0 0.117136	5 3	323 0.184 0.0	028679 0.16	.1987 2.	0 0.05025	1.9 0	0 0.02	8694 0.16 0.198	3692 2.0 0.	050223 1.9	0.050247 1.9	0.050221	1.9 0.732	0.73	0.73	0.73	0.73	-0.69	-0.69	-0.69	-0.69 z9				
10 182.0	4 0.14 182 4 0.67 195	2.13   0.14   1	182.7   1.5	192	19 0.70	02 4.94	0 0	0 190	19 182	2.7 1.5	191 19 174 110	190	19 0	0  0  0.00	0.0020	0832 20.0832	2 0	0.43 58.6	5.17 63.8126 0.	586391	0 0.638126	11 7	714 0.135 0.0	028641 0.076	0.1972 0.5	88 0.04993 0	0.83 0	0 0.02	$0.076 \mid 0.197 \mid 0.19$	7153 0.88 0.	049899 0.83	0.049924 0.8	33 0.049897	0.83   0.702	0.70	0.70	0.70	0.70	-0.65	-0.65	-0.65	-0.65 z10				
112 182.3	3 0.34 182	2.43 0.34 1	182.59 0.91	1 186	11 0.77	11 1.98	0 0	0 173	11 182	2.59 0.91	186 11	185	110 0	0.00	0.0000	7826 14.7826	65 0	0.34 42.2	1.99 44.2191 0.	422244	0.026217	21 13	348 0.108 0.0	028688 0.19	0.1900 0.5	54 0.04981 (	0.48	0 0.02	28703 0.19 0.197	7006 0.54 0.	049321 4.7	0.049806 0.4	48 0.049779	0.48 0.511	0.77	0.77	0.77	0.77	-0.74	-0.74	-0.74	-0.74 Z11 z12				
13 182.0	0 0.12 182	2.09 0.12 1	182.7 1.2	192	15 0.65	51 5.14	0	0 191	15 182	2.7 1.2	192 15	191	15 0	0.00	0.0009	06389 9.0638	9 0	0.45 26.7	1.83 28.4846 0	266579	0 0.284846	15 9	0.144 0.0	028634 0.067	0.1971 0.1	70 0.04993 0	0.65 0	0 0.02	8649 0.067 0.197	7134 0.70 0.	049906 0.65	0.049931 0.6	0.049905	0.65 0.651	0.65	0.65	0.65	0.65	-0.59	-0.59	-0.59	-0.59 z13				
56-22::R56-22																																														
1b 182.4	1 0.34 182	2.50 0.34 1	183.4 2.8	196	36 0.53	6.84	0 (	0 195	36 183	3.4 2.8	196 36	195	36 0	0.00	0.0003	17953 3.1795	3 0	0.45 9.36	1.47 10.8308 0	0936425	0 0.108308	6 4	0.143 0.0	028700 0.19	0.1979 1.	7 0.05002	1.6 0	0 0.02	8715 0.19 0.197	7921 1.7 0.	049991 1.6	0.050016 1.6	0.049990	1.6 0.539	0.54	0.54	0.54	0.54	-0.45	-0.45	-0.45	-0.45 z1b				
11t 184.5	1.1   184 0   0.64   185	1.6   1.1   1 5.20   0.64   1	184.7 1.9	188	21 0.57	72 1.73	0 0	0 187	74 186	4.7 1.9 1.5 S	188 21 202 74	18 <i>/</i>	21 0	0 0.00	0.0006	89565 6.8956	5 0	0.50 20.8	1.63 22.4656 0. 2.60 11.8495 0.	208345	0 0.224656	13 /	786 0.160 0.0	02903 0.59 0	0.1995   1. 0.2016   3.	1 0.04984 0	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	0 0.02	9050 0.59 0.199	9540 1.1 0.	049819 0.92	0.049844 0.9	0.049818	0.92 0.572	0.57	0.57	0.57	0.57	-0.05 <i>/</i>	-0.05 <i>/</i>	-0.05 <i>/</i>	-0.05/ Z1t				
3t 181.8	9 0.14 181	1.98 0.14 1	182.20 0.68	8 186.3	8.7 0.47	71 2.35	0	0 185.0	8.7 182	2.20 0.68	186.2 8.7	7 185.0	8.7	0.00	0.0002	49772 9.4977	2 0	0.43 27.8	1.00 28.7709 0	277740	0 0.287709	28 17	723 0.138 0.0	028618 0.079	0.19655 0.4	40 0.04981 0	0.37	0 0.02	8633 0.079 0.196	5545 0.41 0.	049786 0.37	0.030138 3.2	0.030135	0.37 0.471	0.03	0.47	0.03	0.03	-0.30	-0.30	-0.30	-0.30 z3t				
6b 184.2	1 0.61 184	1.29 0.61 1	184.3 7.5	186	99 0.67	71 0.78	0 (	0 185	99 184	.3 7.5	186 99	184	99 0	0.00	0.0001	38905 1.3890	5 0	0.67 4.37	1.68 6.05170 0	0437288	0 0.060517	0 3 1	68 0.212 0.0	028987 0.34	0.1990 4.5	5 0.0498 4	4.3 0	0 0.02	9001 0.34 0.199		049776 4.3			4.3 0.671	0.67	0.67	0.67	0.67	-0.63	-0.63	-0.63	-0.63 z6b				
		2.31 0.15 1			18 0.65	55 1.77	0 0	0 184	18 182		185 18	184	18 0	0.00	0.000	33412 6.3341	_   _	0.10	1.50 19.8938 0.	100011	0 0.198938	12 7	776 0.128 0.0	028670 0.082		83 0.04980 0		0 0.02			049770 0.78				0.00	0.65	0.65	0.65	-0.59	-0.59	-0.59	-0.59 z7t				
		1.99   0.36   1 2.34   0.29   1			32 0.45 19 0.59		0 0	0 190 0 190	32 182 19 182		191 32 192 19	190 190	19 0	0  0  0.00		96088   1.9608 04694   4.0469			0.74   6.62578   0. 0.92   12.8819   0.		0 0.066257 0 0.128819		192   0.169   0.0	028618   0.20   0	0.1970 1.9 0.1974 0.9	5 0.04991 <i>2</i> 91 0.04993 (			8633 0.20 0.196 8689 0.16 0.197							0.45	0.45	0.45	-0.33 -0.46	-0.33 -0.46	-0.33 -0.46	-0.33 Z8b				
		2.11 0.68 1			76 0.61	19 -61.73		0 111	76 177		112 76	111	76 0	0.00	0.000	04613 1.0461		0.60 3.20	0.89 4.08769 0	0319542	0 0.040876	9 4 2	228 0.191 0.0		0.1906 3.4	4 0.0483	3.2 0					0.048269 3.2				0.62	0.62	0.62	-0.54	-0.54	-0.54	-0.54 z9b				
.9t 184.5	9 0.14 184	1.68 0.14 1	185.24 0.96	6 194	12 0.63	39 4.60	0 (	0 192	12 185	5.24 0.96	193 12	192	12 0	0.00	0.0006	96550 6.9655	0 0			229863	0 0.240263	22 12	235 0.269 0.0	029049 0.078	0.2001 0.5	56 0.04997 0	0.52 0	0 0.02	9062 0.078 0.200	0.56 0.	049945 0.52	0.049967 0.5	0.049944	0.52 0.639	0.64	0.64	0.64	0.64	-0.55	-0.55	-0.55	-0.55 z9t				
	5   0.22   186	5.34   0.22   1	186.5   1.7	190	22 0.59	94 1.95	0 (	0   189	22   186	5.5   1.7	190   22	189	22 0	0.00	0.0004	87510   4.8751	0 0	0.77   15.9	1.21   17.1224   0	159109	0 0.171224	13 7	756   0.243   0.0	029314   0.12   (	).2017   1.0	0   0.04989   0	0.94   0	0 0.02	9327   0.12   0.201	646 1.0 0.	049869   0.94	0.049891   0.9	94   0.049867	0.94   0.594	1 0.59	0.59	0.59	0.59	-0.51	-0.51	-0.51	-0.51 z13b				
56-2::R56-2	1.3 182	2 2 1 3 1	1826 77	181	100 0.46	-0.80	0 (	0 180	100 182	6 77	181 100	180	100 0	0 0 0	0.000	967824 0.9678	24 0	0.61 2.08	1.04 4.01779 0	0207802	0 0.040177	0 3 1	86 0.194 0.0	02875 0.70	1071 /	6 0.0497 4	4.3 0	0 000	8767 0.70 0.197	7051 46 0	049682 4.3	0.049705 4.3	3 0.049680	13 0.468	0.47	0.47	0.47	0.47	-0.34	-0.34	-0.33	-0.33				
3 183.0			179.4 6.6	133	88 0.53	32 -37.85		0 132	88 179	0.4 6.6	133 88	132	88 0			51283 1.5128			1.40 6.22745 0		0 0.062274		212 0.238 0.0		0.1932 4.0	0 0.0487	3.7 0		8801 0.66 0.193			0.048685 3.7		3.7 0.532	2 0.53	0.53	0.53	0.53	-0.40	-0.40	-0.40	-0.40 z3				
		3.15 0.47 1		238	67 0.69	23.16	0 (	0 237	67 187	7.1 5.3	238 67	237	67 0	0.00	0.0002	97666 2.9766				0925024	0 0.119302			028805 0.26			2.9 0		8819 0.26 0.202			0.050942 2.9		2.9 0.690		0.69	0.69	0.69	-0.64	-0.64	-0.64	-0.64 z6				
183.9	1 0.68 184	1.00 0.68 1	186.5 8.5	220	110 0.68	16.27	0 0	0 218	110 186		220 110	218	110 0	0.00		744094 0.7440		0.60 2.30		0229763	0 0.033087		3		.202 5.	0 0.0505	4.7 0					0.050533 4.7			0.00	0.69	0.69	0.69	-0.64	-0.64	-0.64	-0.64 z9				
:15		3.29   0.32   1	182.5   4.0	1/3	52 0.75	50 -6.06	0 (	0   172	52   182	2.4 4.0	173   52	172	52   0	0.00	0.0001	03882   1.0388	2   0	0.60   3.20	0.68   3.87551   0.	0319694	0 0.038755	1 5 2	294   0.191   0.0	028827   0.18   (	).1968   2. <sub>4</sub>	4   0.0495   2	2.2   0	0 0.02	8842 0.18 0.196	8839   2.4   0.	049500   2.2	0.049523   2.2	2   0.049498	2.2 0.750	0.75	0.75	0.75	0.75	-0.71	-0.71	-0.71	-0.71 z15				
		9.81 0.33 1	181 1 4 3	200	57 0.75	51 10.02	0 0	0 199	57 181	1 43	200 57	199	57 0	0 0	0.0002	37573 2.3757	3 0	0.74 7.44	1.74 9.18111 0	0743695	0 0.091811	1 4 2	259 0.236 0.0	028272 0 19	0.1953 2.0	6 0.0501 3	2.5 0	0 002	8286 0.19 0.195	302 26 0	050078 2.5	0.050101 2.5	5 0.050077	2.5 0.751	0.75	0.75	0.75	0.75	-0.72	-0.72	-0.72	-0.72				
		0.39 0.29 1		194	48 0.65	7.54	0 0	0 193	48 180	0.3 3.6	194 48	193	48 0			17380 2.1738				0676801	0 0.080498				0.1944 2.5	2 0.0500 2	2.1 0		8219 0.16 0.194			0.049976 2.3		2.1 0.652	2 0.65	0.65	0.65	0.65	-0.61	-0.61	-0.60	-0.60 z6				
179.8	1 0.46 179	9.90 0.46 1	182.1 5.6	211	73 0.79	98 14.94	0 (	0 210	73 182	2.1 5.6	211 73	210	73 0	0.00	0.0001	21039 1.2103	9 0	0.70 3.75	1.02 4.77070 0	0375337	0 0.047707	0 4 2	229 0.223 0.0	028286 0.26	0.1964 3.5	3 0.0504 3	3.1 0	0 0.02	8300 0.26 0.196	3383 3.3 0.		0.050353 3.1	. 0.0000		0.00	0.80	0.80	0.80	-0.77	-0.77	-0.77	-0.77 z10				
		0.54   0.77   1		217	130 0.78	35 16.88	$\begin{bmatrix} 0 & 0 \\ 0 & 0 \end{bmatrix}$	0 216	130 183		217   130		130 0	0 0.00	0.0000	870276 0.8702	-		1.48 4.33131 0	0285222	0 0.043313	-   -	0.200	32000 0.11	0.198 6.0		5.7 0		8402 0.43 0.197			0.050477 5.7				0.78	0.78	0.78	-0.75	-0.75	-0.75	-0.75 z11				
		0.20   0.96   1 9 22   0.27   1		_		31 -2952.62 67 -21.69	0 0		190   168 44   176		6 190 147 44	146	190 0	0.0		298249 0.2982 87587 1.8758			0.00 1.07001 0	00940522 0564329	0.015753		0.247 0.0 374 0.192 0.0	02833   0.54   0		2 0.0462 7 0 0.04899 7	7.8 0 1.9 0		.8348 0.54 0.180 .8191 0.15 0.190			0.048157 7.8				0.78	0.78	0.78 0.57	-0.75 -0.51	-0.75 -0.51	-0.75 -0.51	-0.75 z15 -0.51 z18				
A39::SA39	0,21   170	).LL   0.L1   1	170.0 0.2		11   0.00	21.00				0.2		110		0.00	3010   0.000	7.007		0.00   0.01	0.00   0.01220   0.	0001020	0.000722		0.102	320111   3.13	2.1000	0.01000	1.0	0 0.02	.0101  0.10	, o , o , o ,	0 10002	0.010000   1.0	0.010001	1.0   0.001	0.01	0.07	0.01	0.01	0.01	0.01	0.01	0.01				
181.1	8 0.56 181	1.26 0.56 1	171.0 6.0	33	86 0.82	20 -453.72	2 0 0	0 32	86 171	.0 6.0	33 86	32	86 0	0.00	0.0001	09893   10.9893	3 0	0.87 3.57	0.95 4.52127 0	356818	0 0.452127	4 2	224 0.276 0.0	028504 0.31	0.1834 3.6	8 0.0467 3	3.6 0	0 0.02	8518 0.31 0.183	3444 3.8 0.	046655 3.6	0.046676 3.6	0.046654	3.6 0.820	0.82	0.82	0.82	0.82	-0.79	-0.79	-0.79	-0.79 z1				
		1.80 0.11 1			11 0.62	23 2.47	0 (	0 185	11 182	2.05 0.84	186 11	185	11 0	0.00	0.0009	82049 98.2049	0	1.38 36.0		60252	0 3.74032	26 12	293 0.439 0.0	028591 0.062	0.19638 0.5	50 0.04981 0	0.47 0				049795 0.47					0.62	0.62	0.62	-0.54	-0.54	-0.54	-0.54 z2				
		3.04   0.89   1 1.2   1.1   1			150 0.78	35 10.43		0 203	150 184 170 185		204 150	203	150 0	0 0.00	3.333	304558 3.0455		0.84 0.995	0.59   1.58/// 0. 0.83   2.18428   0.	135350	0 0.158///	2 1		02879   0.49   0			6.3 0		8800 0.49 0.199 8505 0.62 0.200			0.050199 6.3				0.78	0.78	0.78	-0.75 -0.76	-0.75 -0.76	-0.75 -0.76	-0.75 z3 -0.76 z4				
		1.6 1.0 1				90 -232.01		0 240	200 173		55 200		200 0			228493 2.2849			0.51 1.23121 0.		0 0.123121		99 0.241 0.0						8571 0.58 0.185							0.79	0.79	0.79	-0.76	-0.76	-0.76	-0.76 Z4 -0.76 Z6				
							2 0 0	0 159					120 0				7 0	0.87 1.16	0.53   1.69043   0.	116202			39 0.277 0.0				I		8666 0.39 0.194						0.78	0.78	0.78	0.78	-0.75	-0.75	-0.75	-0.75 z7				
		1.87 0.91 1			150 0.76			0 212	150 184	. —	213 150		150 0	0.00		233683 2.3368			0.45 1.19117 0.		0 0.119117		0.242 0.0						8615 0.51 0.198			0.050384 6.5				0.76	0.76	0.76	-0.73	-0.73	-0.73	-0.73 z8				
9 182.8 :10 181.6		2.89 0.75 1 1.72 0.19 1							130 185 30 182		219   130 193   30	) 218 193	130 0	0  0  0.00		276448 2.7644 862811 8.6281			0.46     1.34811     0.       0.32     3.59243     0.		0 0.134811		0.244 0.0						8777 0.41 0.200 8591 0.11 0.196							0.77 0.77	0.77 0.77	0.77 0.77	-0.74 -0.74	-0.74 -0.74	-0.74 -0.73	-0.74 z9 -0.73 z10				
		1.88 0.60 1						0 248			249 98	248	98 0	0.00		321003 3.2100			0.37 1.37353 0.				73 0.216 0.0						8615 0.33 0.201							0.75	0.75	0.75	-0.71	-0.71	-0.71	-0.73 Z10				
12 181.8	1.5 181	1.9 1.5 1	186 19	237	240 0.79	23.15	0 (	0 235	240 186	19	236 240	235	240 0		0.0000	227721 2.2772	1 0	0.76 0.724	0.66 1.38018 0	0723728	0 0.138018	1 8	80 0.240 0.0	02860 0.82	.201 11	0.0509 1	0 0	0 0.02	8614 0.82 0.200	0734 11 0.	050881 10	0.050904 10	0.050879	10 0.796	0.80	0.80	0.80	0.80	-0.77	-0.77	-0.77	-0.77 z12				
		1.10 0.30 1			40 0.66			0 158	40 179		159 40	158	40 0	$\begin{array}{c cccc} 0 & 0 & 0.00 \\ 0 & 0 & 0.00 \\ \end{array}$		12406 11.2406			0.48 4.01803 0		0 0.401803								8491 0.17 0.193							0.66	0.66	0.66	-0.60	-0.60	-0.60	-0.60 z15				
16 182.3 18 181.4					78 0.76 38 0.67			0 219	78 185 38 180		220 78 171 38	219 170	38 0	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		446591 4.4659 10372 11.0372			0.41     1.76777     0.50       4.00798     0.50		0 0.176777 0 0.400798		213   0.179   0.0 114   0.245   0.0			6 0.0506 3 7 0.04949			8712 0.28 0.200 8554 0.15 0.194		050526 3.4 049467 1.6					0.77 0.68	0.77 0.68	0.77 0.68	-0.73 -0.63	-0.73 -0.63	-0.73 -0.63	-0.73 z16 -0.63 z18				
aroo152::Karoo			2.0		0.07	5, 5.00		- 110				110		3 0.00	233. 73.000	. 30. 2   1110012		57			5 , 0. 100100		0.210   0.0			. 0.0 10 10		3 0.02			2 .0 .07	5.5 15 155 110	0.010100	0.070	0.00	0.00	3.00	3.00	3.00	3.00	5.55	2.33				
		0.68 0.34 1				6.44		0 191	58 180	0.5 4.3		191							1.75 9.17953 0										8265 0.19 0.194							0.74	0.74	0.74	-0.71	-0.71	-0.71	-0.71 z2				
179.3							0 0				194 48		48 0						1.28 8.04986 0		I															0.65	0.65	0.65	-0.61	-0.61	-0.60	-0.60 z6				
		9.72   0.44   1 9.54   0.77   1			75 0.80			0 198 0 216			199 75 217 130	198	130 0			21044 1.2104 870276 0.8702			1.02 4.76906 0. 1.48 4.33131 0.				228 0.223 0.0				3.2 0		8272 0.25 0.195							0.80 0.78	0.80	0.80	-0.77 -0.75	-0.77 -0.75	-0.77 -0.75	-0.77 z10 -0.75 z11				

0.78

0.44

-0.74 -0.75 -0.74 z14

-0.75 z15

a Isotopic dates calculated using the decay constants <code>.»238 = 1.55125E-10</code> and <code>.»235 = 9.8485E-10</code> (Jaffey et al. 1971).

b Corrected for initial Th/U disequilibrium using radiogenic 208Pb and Th/U[magma] = 4.00000.

c % discordance = 100 - (100 \* (206Pb/238U date) / (207Pb/206Pb date))
d Isotopic date calculated using the decay constant [»232 = 4.93343E-11 (Holden 1990)

e Corrected for initial Pa/U disequilibrium using initial fraction activity ratio [231Pa]/[235U] = 1.10000.

f Th contents calculated from radiogenic 208Pb and the 207Pb/206Pb date of the sample, assuming concordance between U-Th and Pb systems.

g Total mass of radiogenic Pb.

h Total mass of common Pb.

i Ratio of radiogenic Pb (including 208Pb) to common Pb.j Measured ratio corrected for fractionation and spike contribution only.

k Measured ratios corrected for fractionation, tracer and blank.