i i	tes (Ma)													osition						Isotopic Ra											lation Coefficients	}									
206	SPb/ Â+2Ïf 2	06Pb/ 38U Â+2Ïf 20	07Pb/ Â+2Ï <i>t</i>	f 207Pb/ Â-	+2Ïf Corr	208	8Pb/ Â+2Ï <i>Ð</i>	07Pb/ 06Pb	207Pb/ f 235U Â+	±2Ï <i>f</i> 207Pb/ 206Pb Â s <pa≯ a<="" th="" =""><th>207Pb/ A+2Ïf 206Pb</th><th>$\hat{A}+2\hat{I}f$ bes</th><th>st Â+2IfMass</th><th>mass</th><th>conc</th><th>Th Th/ Ph*</th><th>total con</th><th>c conc</th><th>conc Pb P</th><th>Pb*/ 206Pb/ 20</th><th>08Pb/ 206Pb/</th><th>207Pb/</th><th>207Pb/</th><th>208Pb/</th><th>206Pb/ 238U</th><th>207Pb/ 235U</th><th>207Pb/ 206Pb</th><th>207Pb/ 206Pb</th><th>207Pb/ 206Pb</th><th>Corr -</th><th>o/238U 206Pb/23 <th>-</th><th>8U 206Pb/238 -207Pb/</th><th>U 206Pb/238U <th>-207Pb/</th><th>207Pb/206Pb</th><th>207Pb/206Pb 2</th><th>207Pb/206Pb 2 <th>-238U/ <</th><th>07Pb/206Pb ThPa>-238U/ 06Pb <th> Fraction</th></th></th></th></th></pa≯>	207Pb/ A+2Ïf 206Pb	$\hat{A}+2\hat{I}f$ bes	st Â+2I f Mass	mass	conc	Th Th/ Ph*	total con	c conc	conc Pb P	Pb*/ 206Pb/ 20	08Pb/ 206Pb/	207Pb/	207Pb/	208Pb/	206Pb/ 238U	207Pb/ 235U	207Pb/ 206Pb	207Pb/ 206Pb	207Pb/ 206Pb	Corr -	o/238U 206Pb/23 <th>-</th> <th>8U 206Pb/238 -207Pb/</th> <th>U 206Pb/238U <th>-207Pb/</th><th>207Pb/206Pb</th><th>207Pb/206Pb 2</th><th>207Pb/206Pb 2 <th>-238U/ <</th><th>07Pb/206Pb ThPa>-238U/ 06Pb <th> Fraction</th></th></th></th>	-	8U 206Pb/238 -207Pb/	U 206Pb/238U <th>-207Pb/</th> <th>207Pb/206Pb</th> <th>207Pb/206Pb 2</th> <th>207Pb/206Pb 2 <th>-238U/ <</th><th>07Pb/206Pb ThPa>-238U/ 06Pb <th> Fraction</th></th></th>	-207Pb/	207Pb/206Pb	207Pb/206Pb 2	207Pb/206Pb 2 <th>-238U/ <</th> <th>07Pb/206Pb ThPa>-238U/ 06Pb <th> Fraction</th></th>	-238U/ <	07Pb/206Pb ThPa>-238U/ 06Pb <th> Fraction</th>	Fraction
		Th≯ abs 2	350° abs	206Pb al	bs coef. 9	% disc [□] 232	2Th abs <	Th≯ abs	<pa> ab</pa>	bs <pa> a</pa>	abs <thpa< th=""><th>≯ abs dat</th><th>te abs (g)</th><th>Ü(μg)</th><th>Ü(ppm)</th><th>(pg) g</th><th>(pg) h Pb(pg) (pp</th><th>n) (ppm</th><th>) (ppm) P</th><th></th><th>Ď6Pb 238U –</th><th>±2Ïf ⁄235U ~</th><th>±2Ïf ŶĀŎĠÞĔ Â</th><th>À±2Ïf ÞZZŽŤŘ Â:</th><th>x±2Ïf %kTh≯b</th><th>±2Ïf % Pa≯e</th><th>±2Ïf %ĸTḧÞĎ</th><th>±2Ïf % Pa≯ ±</th><th>2Ïf %ThPa≯be ±2Ï</th><th>f %oef. 207P</th><th>o/235U 207Pb/23</th><th>5U 235U <pa< th=""><th>> 235Ú <pa></pa></th><th>238U/206Pb</th><th>238Ú/206Pb 2</th><th>207Pb < Th> 2</th><th>06Pb <th> Fraction</th></th></pa<></th></thpa<>	≯ abs dat	te abs (g)	Ü(μg)	Ü(ppm)	(pg) g	(pg) h Pb(pg) (pp	n) (ppm) (ppm) P		Ď6Pb 238U –	±2Ïf ⁄235U ~	±2Ïf ŶĀŎĠÞĔ Â	À±2Ïf ÞZZŽŤŘ Â:	x±2Ïf %kTh≯b	±2Ïf % Pa≯e	±2Ïf %ĸTḧÞĎ	±2Ïf % Pa≯ ±	2Ïf %ThPa≯be ±2Ï	f %oef. 207P	o/235U 207Pb/23	5U 235U <pa< th=""><th>> 235Ú <pa></pa></th><th>238U/206Pb</th><th>238Ú/206Pb 2</th><th>207Pb < Th> 2</th><th>06Pb <th> Fraction</th></th></pa<>	> 235Ú <pa></pa>	238U/206Pb	238Ú/206Pb 2	207Pb < Th> 2	06Pb <th> Fraction</th>	Fraction			
56-99::R56-9																				.																					
	0.2 1.2 1 0.88 0.37 1	80.3 1.2 1	85 14	240 18	80 0.700	24.87 ($\begin{bmatrix} 0 & 0 & 2 \\ 0 & 0 & 1 \end{bmatrix}$	239 180 106 50	185 14	4 240 1	180 239	180 0	0 0.000	0.0001834	75 1.83475	0 0.83 5.89	4.37 10.2560 0.0	588742 0	0.102560	1 93 0	0.02835	0.68 0.199	8.3 0.0510	7.8 0	0 0.028363	0.68 0.199266 0.21 0.196361	8.3 0.050955	7.8 0.050978 7. 2.5 0.050047 2.	8 0.050953 7.8	0.700 0	70 0.70	0.70	0.70	-0.65	-0.65 0.67	-0.65 0.67	-0.65 z1				
4 180	0.08 0.51 1	80.16 0.51 1	82.4 4.5	213 5	58 0.687	15.50	$\begin{bmatrix} 0 & 0 & 1 \\ 0 & 0 & 2 \end{bmatrix}$	212 58	182.4 4.	1.5 197 3 1.5 213 5	58 212	58 0	0.000	0.0001444	78 1.74678	0 0.75 5.49	1.14 6.63661 0.0	549479 0	0.0663661	5 289 0	0.028328	0.21 0.1964 0.1968	2.7 0.0500 2	2.5 0	0.028342	0.21	2.7 0.050027	2.5 0.050047 2.	- 0.00000	0.712 0	69 0.69	0.71	0.71	-0.62	-0.62	-0.62	-0.67 z3 -0.62 z4				
13 186	6.9 1.4 1	87.0 1.4 1	90 17	227 2	10 0.806	17.76	0 0 2	226 210	190 17	7 227 2	210 226	210 0	0.000	0.0000282	345 0.282345	0 0.90 0.956	0.80 1.75403 0.0	0956251 0	0.0175403	1 83 0	0.286 0.02942	0.74 0.206	9.8 0.0507	9.2 0	0 0.029429	0.74 0.205629	9.8 0.050678	9.2 0.050699 9.	2 0.050677 9.2	0.806 0	81 0.81	0.81	0.81	-0.78	-0.78	-0.78	-0.78 z13				
16 181	1.2 1.0 1	81.2 1.0 1	86 13	251 17	70 0.783	27.86	0 0 2	250 170	186 13	3 251 1	170 250	170 0	0.000	0.0000742	773 0.742773	0 0.71 2.32	1.60 3.92021 0.0	232382 0	0.0392021	1 101 0	0.224 0.02850	0.56 0.201	7.6 0.0512	7.2 0	0 0.028514	0.56 0.201303	7.6 0.051203	7.2 0.051227 7.	2 0.051202 7.2	0.783 0	78 0.78	0.78	0.78	-0.75	-0.75	-0.75	-0.75 z16				
19 180	0.65 0.71 1	80.74 0.71 1	84.4 9.3	233 12	20 0.773	22.32 (0 0 2	231 120	184.4 9.	9.3 232 1	120 231	120 0	0 0 0.000	0.0001090	13 1.09013	0 0.52 3.24	1.64 4.88366 0.0	324228 0	0.0488366	2 136 0	0.165 0.02842	0.40 0.199	5.5 0.0508	5.2 0	0 0.028434	0.40 0.199122	5.5 0.050791	5.2 0.050816 5.	2 0.050790 5.2	0.773 0	77 0.77	0.77	0.77	-0.74	-0.74	-0.74	-0.74 z19				
56-28::R56-2	0.74 0.57 1 28	80.83 0.57 1	82.0 7.5	206 9	99 0.782	12.30	0 0 2	205 99	182.0 /	7.5 200 8	99 205	99 0	0.000	0.0000682	598 0.682598	0 0.63 2.09	0.85 2.93693 0.0	208739 0	0.0293693	2 161 0	0.199 0.028435	0.32 0.1970	4.5 0.0502 4	4.2 0	0 0.028449	0.32 0.196975	4.5 0.050217	4.2 0.050241 4.	2 0.050216 4.3	0.782 0	78 0.78	0.78	0.78	-0.75	-0.75	-0.75	-0.75 ZZU				
	2.74 0.66 1	82 83 0 66 1	83 2 5 5	189 7	72 0.549	3.35	0 0 1	188 72	183.2 5	5.5 189 7	72 188	72 0	0 000	010 0 0001948	48 1 94848	0 0.58 5.95	1 63 7 57754 0 0	595167 0	0.0757754	4 234 (185 0 02875	0.37 0.1977	3.3 0.0499	3.1 0	0 0.028768	0.37 0.197718	3.3 0.049848	3.1 0.049872 3.	1 0.049847 3.1	0.549	55 0.55	0.55	0.55	-0.46	-0.46	-0.46	-0.46				
6 182	2.19 0.93 1	82.28 0.93 1	88 12	267 15	50 0.782	31.68	$\begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & 2 \end{bmatrix}$	266 150	188 12	2 267 1	150 266	150 0	0.000	0.0002204	57 2.20457	0 0.74 7.00	4.82 11.8110 0.0	699594 0	0.118110	1 100 0	0.234 0.02867	0.52 0.204	7.1 0.0516	6.8 0	0 0.028680	0.52 0.203852	7.1 0.051552	6.8 0.051576 6.	8 0.051551 6.8	0.782 0	78 0.78	0.78	0.78	-0.75	-0.75	-0.75	-0.75 z6				
7 181	1.89 0.62 1	81.97 0.62 1	83.4 6.4	203 8	0.650	10.30	0 0 2	202 84	183.4 6.	6.4 203 8	84 202	84 0	0.000	0.0001622	40 1.62240	0 0.80 5.21	1.76 6.97318 0.0	520821 0	0.0697318	3 183 0	0.253 0.028617	0.34 0.1979	3.8 0.0502	3.6 0	0 0.028631	0.34 0.197944	3.8 0.050144	3.6 0.050167 3.	6 0.050143 3.6	0.650 0	65 0.65	0.65	0.65	-0.59	-0.59	-0.59	-0.59 z7				
		82.10 0.29 1	79.4 3.6	145 5	0.571	-25.94	0 0 1	143 50	179.4 3.	3.6 144 5	50 143	50 0	0.000	0.0001793	66 1.79366	0 0.70 5.62	1.00 6.62230 0.0	561921 0	0.0662230	6 339 0	0.222 0.028637	0.16 0.1932	2.2 0.0489	2.1 0	0 0.028651	0.16 0.193195	2.2 0.048907	2.1 0.048930 2.	1 0.048906 2.1	0.571 0	57 0.57	0.57	0.57	-0.52	-0.52	-0.52	-0.52 z8				
9 182	2.28 0.28 1	82.37 0.28 1	84.0 3.4	206 4	15 0.732	11.72	$\begin{bmatrix} 0 & 0 & 2 \\ 0 & 0 & 4 \end{bmatrix}$	205 45	184.0 3.	3.4 206 4	45 205	45 0	0 0 0.000	0.0003223	12 3.22312	0 0.58 9.82	1.90 11.7136 0.0	981620 0	0.117136	5 323 0	0.028679	0.16 0.1987	2.0 0.05025	1.9 0 0.83 0	0 0.028694	0.16 0.198692	2.0 0.050223	1.9 0.050247 1.	9 0.050221 1.9 83 0.049897 0.83	0.732 0	73 0.73	0.73	0.73	-0.69	-0.69	-0.69 0.65	-0.69 Z9				
10 102	4 94 0.14 1	85 02 0 67 1	84 1 8 3	174 1	10 0.702	-6.48	$\begin{bmatrix} 0 & 0 & 1 \\ 0 & 0 & 1 \end{bmatrix}$	173 110	184 1 8	3 3 174 1	110 173	110 0	0 0.000	0.0020083	663 0.577663	0 0.43 36.6	0.79 2.62173 0.0	183436 0	0.036120	2 152 0	0.028041	0.076 0.1972	5.0 0.04995	4.7	0.028030	0.076 0.197153	5.0 0.049521	4.7 0.049543 4	7 0.049520 4.7	0.702	77 0.70	0.70	0.70	-0.03	-0.65	-0.03	-0.05 210				
12 182	2.33 0.34 1	82.43 0.34 1	82.59 0.91	186 1	11 0.511	1.98	0 0 1	185 11	182.59 0.	0.91 186	11 185	11 0	0 0.000	010 0.0014782	6 14.7826	0 0.34 42.2	1.99 44.2191 0.4	22244 0	0.442191 2	21 1348 0	0.108 0.028688	0.19 0.1970	0.54 0.04981	0.48 0	0 0.028703	0.19 0.197006	0.54 0.049780	0.48 0.049806 0.	48 0.049779 0.48	0.511 0	51 0.51	0.51	0.51	-0.19	-0.19	-0.19	-0.19 z12				
		82.09 0.12 1	82.7 1.2	192 1	15 0.651	5.14	0 0 1	191 15	182.7 1.	1.2 192 <i>°</i>	15 191	15 0	0.000	0.0009063	89 9.06389	0 0.45 26.7	1.83 28.4846 0.2	66579 0	0.284846	15 907 C	0.144 0.028634	0.067 0.1971	0.70 0.04993	0.65 0	0 0.028649	0.067 0.197134	0.70 0.049906	0.65 0.049931 0.	65 0.049905 0.65	0.651 0	65 0.65	0.65	0.65	-0.59	-0.59	-0.59	-0.59 z13				
56-22::R56-2	.2																																								
1b 182	2.41 0.34 1	82.50 0.34 1	83.4 2.8	196 3	36 0.539	6.84	0 0 1	195 36	183.4 2.	2.8 196 3	36 195	36 0	0.000	0.0003179	53 3.17953	0 0.45 9.36	1.47 10.8308 0.0	036425 0	0.108308	6 407 0	0.143 0.028700	0.19 0.1979	1.7 0.05002	1.6 0	0 0.028715	0.19 0.197921	1.7 0.049991	1.6 0.050016 1.	6 0.049990 1.6	0.539 0	54 0.54	0.54	0.54	-0.45	-0.45	-0.45	-0.45 z1b				
1t 184	4.5 1.1 1 5.20 0.64 1	84.6 1.1 1	84.7 1.9	188 2	21 0.572	1.73	0 0 1	187 21	184.7 1.	1.9 188 2	21 187	21 0	0.000	0.0006895	65 6.89565	0 0.50 20.8	1.63 22.4656 0.2	08345 0	0.224656	13 /86 0	0.160 0.02903	0.59 0.1995	1.1 0.04984 0	0.92 0	0 0.029050	0.59 0.199540	1.1 0.049819	0.92 0.049844 0.	$92 \mid 0.049818 \mid 0.92$	0.572 0	5/ 0.5/	0.57	0.57	-0.057	-0.057	-0.057	-0.05/ Z1t				
3t 181	1.89 0.14 1	81.98 0.14 1	82.20 0.68	186.3	8.7 0.471	2.35	$\begin{bmatrix} 0 & 0 & 2 \\ 0 & 0 & 1 \end{bmatrix}$	185.0 8.7	182.20 0.	0.68 186.2	8.7 185.0	8.7	0.000	0.0002804	72 9.49772	0 0.63 9.23	1.00 28.7709 0.2	77740 0	0.118493	28 1723 0	0.138 0.028618	0.079 0.19655	0.40 0.04981	0.37	0.029100	0.079 0.196545	0.41 0.049786	0.37 0.049811 0.	37 0.049785 0.37	0.631 0	47 0.47	0.63	0.63	-0.30	-0.30	-0.30	-0.30 z3t				
6b 184	4.21 0.61 1	84.29 0.61 1	84.3 7.5	186 9	99 0.671	0.78	0 0 1	185 99	184.3 7.	7.5 186 9	99 184	99 0	0.000	0.0001389	05 1.38905	0 0.67 4.37	1.68 6.05170 0.0	137288 0	0.0605170	3 168 0	0.212 0.028987	0.34 0.1990	4.5 0.0498	4.3 0	0 0.029001	0.34 0.199032	4.5 0.049776	4.3 0.049799 4.	3 0.049774 4.3	0.671 0	67 0.67	0.67	0.67	-0.63	-0.63	-0.63	-0.63 z6b				
7t 182	2.22 0.15 1	82.31 0.15 1	82.5 1.4	185 1	18 0.655	1.77	0 0 1	184 18	182.4 1.	1.4 185 <i>°</i>	18 184	18 0	0.000	0.0006334	12 6.33412	0 0.40 18.4	1.50 19.8938 0.1	33941 0	0.198938	12 776 C	0.028670	0.082 0.1968	0.83 0.04980	0.78 0	0 0.028685	0.082 0.196838	0.83 0.049770	0.78 0.049795 0.			65 0.65	0.65	0.65	-0.59	-0.59	-0.59	-0.59 z7t				
		81.99 0.36 1			0.455	4.77	0 0 1	190 32	182.5 2.	2.4 191 3	32 190	32 0	0.000	0.0001960		0 0.53 5.89		588509 0	0.0662578	8 492 0	0.169 0.028618	0.20 0.1970	1.5 0.04991	1.4 0		0.20 0.196952			4 0.049888 1.4		45 0.45	0.45	0.45	-0.33	-0.33	-0.33	-0.33 z8b				
3t 182 3h 183	2.25 0.29 1	82.34 0.29 1 82.11 0.68 1	77.1 5.6	192 1 113 7	76 0.593	4.92 ($\begin{bmatrix} 0 & 0 & 1 \\ 0 & 0 & 1 \end{bmatrix}$	190 19 111 76	182.9 1.	1.5 192 7 5.6 112 7	19 190 76 111	76 0	0.000	0.0004046	94 4.04694	0 0.47 12.0	0.92 12.8819 0.1	19659 0	0.128819	13 811 0	0.149 0.028674	0.16 0.1974	0.91 0.04993 0	0.82 0	0 0.028652	0.16 0.197395		0.82 0.049928 0. 3.2 0.048269 3.			59 0.59 62 0.62	0.59 0.62	0.59	-0.46 -0.54	-0.46 -0.54	-0.46 -0.54	-0.46 28t -0.54 z9b				
9t 184	4.59 0.14 1	84.68 0.14 1			12 0.639	4.60	0 0 1	192 12	185.24 0	0.96 193	12 192	12 0	0.000	0.0006965	50 6.96550	0 0.85 23.0	1.04 24.0263 0.2	29863 0	0.240263	22 1235 0	0.269 0.029049	0.078 0.2001	0.56 0.04997	0.52 0	0 0.029062	0.078 0.200132	0.56 0.049945				64 0.64	0.64	0.64	-0.55	-0.55	-0.55	-0.55 z9t				
13b 186	6.25 0.22 1	86.34 0.22 1	86.5 1.7	190 2	0.594	1.95	0 0 1	189 22	186.5	1.7 190 2	22 189	22 0	0.000	0.0004875	10 4.87510	0 0.77 15.9	1.21 17.1224 0.1	59109 0	0.171224	13 756 0	0.243 0.029314	0.12 0.2017	1.0 0.04989	0.94 0	0 0.029327	0.12 0.201646	1.0 0.049869	0.94 0.049891 0.	94 0.049867 0.94	0.594 0	59 0.59	0.59	0.59	-0.51	-0.51	-0.51	-0.51 z13b				
56-2::R56-2														_								_									_										
2 182	2.7 1.3 1	82.8 1.3 1	82.6 7.7	181 10	00 0.468	-0.80	0 0 1	180 100	182.6 7.		100 180	100 0	0.000	0.0000967			1.04 4.01779 0.0		0.0401779	3 186 0	0.194 0.02875	0.70 0.1971	4.6 0.0497	4.3 0				4.3 0.049705 4.			47 0.47	0.47	0.47	-0.34	-0.34	-0.33	-0.33 z2				
	3.0 1.2 1		79.4 6.6	133 8	38 0.532	-37.85	0 0 1	132 88	179.4 6.	6.6 133 8	88 132	88 0	0.000	0.0001512	83 1.51283		1.40 6.22745 0.0		0.0622745	3 212 0	0.02879	0.66 0.1932	4.0 0.0487	3.7 0	0 0.028801	0.66 0.193236		3.7 0.048685 3.	7 0.048661 3.7		53 0.53	0.53	0.53	-0.40	-0.40	-0.40	-0.40 z3				
		83.15 0.47 1 84.00 0.68 1		238 6	10 0.690	16 27	$\begin{bmatrix} 0 & 0 & 2 \\ 0 & 0 & 2 \end{bmatrix}$	237 67	187.1 5.	5.3 238 6 3.5 220 1	110 218	110 0	0.000		66 2.97666 094 0.744094			925024 0 229763 0	0.119302 0.0330870		0.02000	0.26 0.2023 0.37 0.202		2.9 0 4.7 0		0.26 0.202320 0.37 0.201640		2.9 0.050942 2. 4.7 0.050533 4.	9 0.050916 2.9 7 0.050508 4.7			0.69 0.69	0.69 0.69	-0.64 -0.64	-0.64 -0.64	-0.64 -0.64	-0.64 z6 -0.64 z9				
				173 5	52 0.750	-6.06	0 0 1	172 52			52 172		0.000	0.0001038		0 0.60 3.20		319694 0	0.0387551	5 294 0		0.18 0.1968		2.2 0								0.75	0.75	-0.71	-0.71	-0.71	-0.71 z15				
z15 183.20 0.32 183.29 0.32 183.29 0.32 183.29 0.32 182.5 4.0 173 52 0.750 -6.06 0 0 0.00103882 0.049593 2.2 0.049593 2.2 0.049593 2.2 0.049593 2.2 0.049593 2.2 0.049593 2.2 0.049498 2.2 0.750 -0.71 -0.71 z 2.2 0 0 0.000103882 0.049593 2.2 0.049																																									
2 179	9.72 0.33 1	79.81 0.33 1	81.1 4.3	200 5	0.751	10.02	0 0 1	199 57	181.1 4.	1.3 200 5	57 199	57 0	0.000	0.0002375	73 2.37573	0 0.74 7.44	1.74 9.18111 0.0	743695 0	0.0918111	4 259 0	0.236 0.028272	0.19 0.1953	2.6 0.0501	2.5 0	0 0.028286	0.19 0.195302	2.6 0.050078	2.5 0.050101 2.	5 0.050077 2.5	0.751 0	75 0.75	0.75	0.75	-0.72	-0.72	-0.72	-0.72 z2				
		79.39 0.29 1		194 4	18 0.652	7.54	0 0 1	193 48	180.3	3.6 194 4	48 193	48 0	0.000	0.0002173	80 2.17380		1120 0101000 010	676801 0	0.0804986	5 317 0		0.16 0.1944		2.1 0			2.2 0.049952				65 0.65	0.65	0.65	-0.61	-0.61	-0.60	-0.60 z6				
		79.90 0.46 1		211 7	73 0.798	14.94	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	210 73	182.1 5.	5.6 211 7	73 210	73 0	0.000	0.0001210		00			0.0477070			0.26 0.1964	3.3 0.0504				3.3 0.050330					0.80	0.80	-0.77	-0.77	-0.77	-0.77 z10				
		80.54 0.77 1 80.20 0.96 1		217 13	90 0.781 -	·2952.62 (0 0 2	5 130	183 10 168 13	$egin{array}{c cccc} 0 & 217 & 1 \\ 3 & 6 & 1 \\ \end{array}$	130 216 190 5	130 0	0 0 0.000		276		1.48 4.33131 0.0 0.63 1.57531 0.0	285222 U 1940522 0	0.0433131	2 123 0 1 102 0		0.44 0.198 0.54 0.180	0.0	5.7 0 7.8 0			6.0 0.050455 8.2 0.046136		7 0.050454 5.7 8 0.046135 7.8		78 0.78 78 0.78	0.78	0.78	-0.75 -0.75	-0.75 -0.75	-0.75 -0.75	-0.75 z11 -0.75 z15				
		79.22 0.27 1		147 4		-21.69	0 0 1	146 44	176.9	3.2 147 4	44 146	44 0	0.000			0 0.60 5.64		564329 0	0.0657228		0.192 0.028177						2.0 0.048962		9 0.048961 1.9			0.57	0.57	-0.51	-0.51	-0.51	-0.51 z18				
A39::SA39																																									
1 181	1.18 0.56 1	81.26 0.56 1	71.0 6.0	33 8	36 0.820	-453.72	0 0	32 86	171.0 6.	6.0 33 8	86 32	86 0	0.000	0.0001098	93 10.9893	0 0.87 3.57	0.95 4.52127 0.3	66818 0	0.452127	4 224 0	0.028504	0.31 0.1834	3.8 0.0467	3.6 0	0 0.028518	0.31 0.183444	3.8 0.046655	3.6 0.046676 3.	6 0.046654 3.6	0.820 0	82 0.82	0.82	0.82	-0.79	-0.79	-0.79	-0.79 z1				
		81.80 0.11 1			11 0.623	2.47	0 0 1	185 11	182.05 0.	0.84 186	11 185	11 0	0 0.000	0.0009820	49 98.2049	0 1.38 36.0	1.38 37.4032 3.6	0252 0	3.74032	26 1293 0	0.020001	0.062 0.19638	0.00 0.01001	0.47 0	0 0.028603	0.062 0.196373	0.50 0.049795		47 0.049794 0.47	0.623 0	62 0.62	0.62	0.62	-0.54	-0.54	-0.54	-0.54 z2				
		83.04 0.89 1		204 15	50 0.783	10.43	$\begin{bmatrix} 0 & 0 & 2 \\ 0 & 0 & 3 \end{bmatrix}$	203 150	184 11	1 204 1	150 203	150 0	0.000	0.0000304	0.0 1000	0 0.84 0.995		995040 0	0.158777	2 111 0		0.49 0.199		6.3 0	0 0.028800	0.49 0.199248	6.7 0.050177			0.783 0	78 0.78	0.78	0.78	-0.75	-0.75	-0.75 0.76	-0.75 z3				
		81.2 1.1 1 81.6 1.0 1				-232.01	0 0 2	54 200	173 14		200 53	200 0	0.000				0.83 2.18428 0.1 0.51 1.23121 0.0						8.9 0.0471 8					8.4 0.047106 8.				0.79	0.79	-0.76 -0.76	-0.76 -0.76	-0.76 -0.76	-0.76 Z4 -0.76 Z6				
	1	82.19 0.71 1				1	0 0 1	159 120	180.5 9			120 0	0.000	1			0.53 1.69043 0.1											5.3 0.049257 5.					0.78	-0.75	-0.75	-0.75	-0.75 z7				
3 181	1.79 0.91 1	81.87 0.91 1	84 12	213 1	50 0.763	14.57	0 0 2	212 150	184 12		1			0.0000233			0.45 1.19117 0.0	743433 0	0.119117	2 112 0	0.242 0.02860	0.51 0.199	6.9 0.0504	6.5 0	0 0.028615	0.51 0.198686	6.9 0.050361	6.5 0.050384 6.	5 0.050359 6.5	0.763 0	76 0.76	0.76	0.76	-0.73	-0.73	-0.73	-0.73 z8				
										9.8 219 1							0.46 1.34811 0.0											5.5 0.050525 5.				0.77	0.77	-0.74	-0.74	-0.74	-0.74 z9				
		81.72 0.19 1 81.88 0.60 1					0 0 1		182.5 2. 186.7 7.		30 193 98 248		0.000				0.32 3.59243 0.3 0.37 1.37353 0.1						1.4 0.04997 4.5 0.0512 4					1.3 0.049966 1. 4.3 0.051183 4.				0.77	0.77	-0.74 -0.71	-0.74 -0.71	-0.73 -0.71	-0.73 Z10 -0.71 z11				
		81.9 1.5 1					0 0 2	235 240	186.7			240 0	0.000				0.66 1.38018 0.0				0.240 0.02860		11 0.0509 1				11 0.050881					0.73	0.80	-0.77	-0.77	-0.77	-0.77 z12				
15 181	1.01 0.30 1	81.10 0.30 1	79.4 3.0	159 4	40 0.661	-14.03			179.4 3.	3.0 159 4	40 158	40 0	0.000	0.0001124	06 11.2406	0 0.74 3.54	0.48 4.01803 0.3	53921 0	0.401803	7 436 0	0.235 0.028477	0.17 0.1933	1.8 0.04923	1.7 0	0 0.028491	0.17 0.193290	1.8 0.049205	1.7 0.049228 1.	7 0.049204 1.7	0.661 0	66 0.66	0.66	0.66	-0.60	-0.60	-0.60	-0.60 z15				
16 182	2.39 0.50 1	82.48 0.50 1	85.1 6.1	220 7	78 0.767	17.26	0 0 2	219 78	185.1 6.	5.1 220 7	78 219	78 0	0.000	0.0000446	591 4.46591	0 0.56 1.36	0.41 1.76777 0.1	35570 0	0.176777	3 213 0	0.179 0.028698	0.28 0.2000	3.6 0.0506	3.4 0	0 0.028712	0.28 0.200020	3.6 0.050526	3.4 0.050550 3.	4 0.050525 3.4	0.767 0	77 0.77	0.77	0.77	-0.73 -0.63	-0.73	-0.73	-0.73 z16				
y 101	1 40 0 07 4	U1 10 0 77 1	U/1 7 7 0	1/1		E (1)(1)		7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	1007		.,0 170	00 0		U UUUAAOO'	44 0070	0 0 77 0 FA	1010 100700 000	4 () () 4	0.400700		$A \cap A \cap$	0.4047	0.04040				4 / 1 / 1 / 1 / 1 / 1 / 1	4 (\sim \sim \sim \sim \sim \sim \sim \sim	10 C 70 \	0.00	$\Lambda \Lambda \Lambda$	$\alpha \alpha \alpha$	$\alpha \alpha \alpha$	(1 (2)	() () ()	() (()				

180.7 | 2.8 | 171 | 38 | 170 | 38 | 0 | 0 | 0.00001 | 0.000110372 | 11.0372 | 0 | 0.77 | 3.51 | 0.50 | 4.00798 | 0.351021 | 0 | 0.400798 | 7 | 414 | 0.245 | 0.049467 | 1.6 | 0.049467 | 1.6 | 0.049469 | 1.6 | 0.049466 | 1.6 | 0.679 | 0.68

0 0.0476906 4 228

0 | 0.51 | 2.33 | 0.72 | 3.04280 | 0.0232695 | 0 | 0.0304280 | 3

-0.63 z18

-0.75 z11

-0.75 z15

-0.39 z18

-0.77

-0.74

z10

z14

-0.63

-0.74

0.80

0.78

0.78

0.78

0.44

0.80

0.78

0.78

0.44

-0.75

-0.74

-0.75

-0.39

-0.75

a Isotopic dates calculated using the decay constants \hat{l} »238 = 1.55125E-10 and \hat{l} »235 = 9.8485E-10 (Jaffey et al. 1971).

b Corrected for initial Th/U disequilibrium using radiogenic 208Pb and Th/U[magma] = 4.00000.

c % discordance = 100 - (100 * (206Pb/238U date) / (207Pb/206Pb date))
d Isotopic date calculated using the decay constant λ232 = 4.93343E-11 (Holden 1990)

e Corrected for initial Pa/U disequilibrium using initial fraction activity ratio [231Pa]/[235U] = 1.10000.

f Th contents calculated from radiogenic 208Pb and the 207Pb/206Pb date of the sample, assuming concordance between U-Th and Pb systems.

g Total mass of radiogenic Pb.

h Total mass of common Pb.

i Ratio of radiogenic Pb (including 208Pb) to common Pb.j Measured ratio corrected for fractionation and spike contribution only.

k Measured ratios corrected for fractionation, tracer and blank.

z12

Karoo152::Karoo152