

**Table 1.** Band-integrated flux densities at 728, 1382 and 3100 MHz, the spectral classification, the frequency range  $\Delta\nu$  the classification was performed over and an eventual spectral index was determined for, the spectral index  $\alpha$  for the pulsars that have simple power-law spectra and the robust modulation index  $m_r$  at all three centre frequencies for pulsars of which we have at least six measurement epochs. The flux density uncertainties include scintillation and a systematic contribution, in addition to the statistical uncertainty. Upper limits are reported at the  $3\sigma$  level and all other uncertainties at the  $1\sigma$  level.

PSRJ	$S_{728}$ (mJy)	$S_{1382}$ (mJy)	$S_{3100}$ (mJy)	Class	$\Delta\nu$ (GHz)	$\alpha$	$m_r$ , 728	$m_r$ , 1382	$m_r$ , 3100
J0401–7608	$4 \pm 2$	–	$0.8 \pm 0.5$	pl	$0.4 - 3.4$	$-1.5 \pm 0.5$	–	–	–
J0437–4715	$300 \pm 200$	$160 \pm 20$	$30 \pm 30$	broken pl	$0.08 - 17.0$	–	–	–	–
J0511–6508	$1.3 \pm 0.7$	$0.6 \pm 0.2$	$< 0.1$	–	$0.7 - 1.4$	–	–	–	–
J0519–6932	–	$0.14 \pm 0.04$	–	–	$1.4 - 1.4$	–	–	–	–
J0536–7543	$11 \pm 7$	–	$3 \pm 2$	pl	$0.4 - 3.5$	$-1.8 \pm 0.4$	–	–	–
J0543+2329	$25 \pm 2$	$10.7 \pm 0.7$	$3.0 \pm 0.2$	broken pl	$0.1 - 32.0$	–	$0.18^{+0.2}_{-0.08}$	$0.41^{+0.09}_{-0.04}$	$0.23^{+0.3}_{-0.07}$
J0601–0527	$6 \pm 2$	–	$0.6 \pm 0.2$	pl	$0.1 - 4.9$	$-1.74 \pm 0.08$	–	–	–
J0614+2229	$8.8 \pm 0.8$	$3.3 \pm 0.2$	$0.76 \pm 0.06$	pl	$0.09 - 3.5$	$-1.77 \pm 0.05$	$0.25^{+0.07}_{-0.2}$	$0.18^{+0.01}_{-0.03}$	$0.22^{+0.1}_{-0.08}$
J0624–0424	$3.0 \pm 1.0$	–	$< 0.05$	pl	$0.1 - 1.4$	$-1.0 \pm 0.5$	–	–	–
J0627+0706	$3.8 \pm 0.2$	$1.39 \pm 0.08$	$0.31 \pm 0.05$	pl	$0.4 - 3.1$	$-1.6 \pm 0.2$	$0.11^{+0.03}_{-0.05}$	$0.27^{+0.02}_{-0.06}$	$0.39^{+0.04}_{-0.1}$
J0630–2834	$180 \pm 90$	–	$1.6 \pm 0.8$	low turn-over	$0.04 - 10.6$	–	–	–	–
J0656–2228	$0.9 \pm 0.4$	$3.0 \pm 1.0$	$0.3 \pm 0.2$	pl	$0.7 - 3.1$	$-1.0 \pm 1.0$	–	–	–
J0659+1414	$3.9 \pm 0.8$	$2.7 \pm 0.2$	$1.6 \pm 0.3$	lps	$0.09 - 8.4$	–	$0.6^{+0.4}_{-0.4}$	$0.55^{+0.09}_{-0.07}$	$0.6^{+0.2}_{-0.2}$
J0711–6830	$7 \pm 4$	$5 \pm 3$	$1.0 \pm 0.7$	lps	$0.4 - 3.4$	–	–	–	–
J0721–2038	$0.5 \pm 0.2$	$0.21 \pm 0.07$	–	–	$0.7 - 1.4$	–	–	–	–
J0729–1448	$2.1 \pm 0.2$	$0.83 \pm 0.06$	$0.19 \pm 0.02$	pl	$0.7 - 3.1$	$-1.7 \pm 0.3$	$0.25^{+0.2}_{-0.09}$	$0.53^{+0.06}_{-0.07}$	$0.3^{+0.4}_{-0.2}$
J0729–1836	$4.0 \pm 1.0$	$1.9 \pm 0.5$	$0.5 \pm 0.2$	pl	$0.4 - 3.1$	$-1.7 \pm 0.2$	–	–	–
J0737–3039B	–	$< 0.1$	–	–	$1.4 - 1.4$	–	–	–	–
J0742–2822	$90 \pm 30$	$26 \pm 2$	$6.8 \pm 0.5$	broken pl	$0.1 - 10.6$	–	–	$0.28^{+0.05}_{-0.06}$	$0.22^{+0.1}_{-0.07}$
J0745–5353	$12.0 \pm 0.7$	$5.0 \pm 0.2$	$1.21 \pm 0.07$	pl	$0.4 - 3.5$	$-1.6 \pm 0.06$	$0.07^{+0.04}_{-0.03}$	$0.055^{+0.006}_{-0.007}$	$0.14^{+0.04}_{-0.04}$
J0751+1807	–	–	$< 0.06$	pl	$0.1 - 3.0$	$-1.6 \pm 0.3$	–	–	–
J0758–1528	$4.0 \pm 1.0$	$2.6 \pm 0.8$	$1.4 \pm 0.5$	pl	$0.1 - 4.9$	$-1.1 \pm 0.2$	–	–	–
J0809–4753	$21 \pm 9$	$2.6 \pm 0.6$	$0.46 \pm 0.07$	low turn-over	$0.08 - 3.4$	–	–	–	–
J0812–3905	$1.6 \pm 0.2$	$0.38 \pm 0.09$	$< 0.1$	–	$0.7 - 1.4$	–	–	–	–
J0818–3049	$1.3 \pm 0.3$	$0.33 \pm 0.09$	$< 5.0$	–	$0.7 - 1.4$	–	–	–	–
J0818–3232	$2.4 \pm 0.4$	$1.4 \pm 0.4$	$0.18 \pm 0.04$	pl	$0.7 - 3.3$	$-1.7 \pm 0.2$	–	–	–
J0820–1350	$27 \pm 8$	$6 \pm 2$	$1.4 \pm 0.7$	broken pl	$0.06 - 4.9$	–	–	–	–
J0820–3826	$1.27 \pm 0.08$	$0.49 \pm 0.03$	$0.093 \pm 0.007$	pl	$0.7 - 3.1$	$-1.8 \pm 0.2$	$0.14^{+0.08}_{-0.06}$	$0.24^{+0.05}_{-0.02}$	–
J0820–4114	$20 \pm 10$	$5.0 \pm 1.0$	$1.0 \pm 0.4$	lps	$0.08 - 3.4$	–	–	–	–
J0823+0159	$4 \pm 3$	$4 \pm 2$	$0.4 \pm 0.3$	lps	$0.1 - 4.9$	–	–	–	–
J0834–4159	$0.82 \pm 0.08$	$0.28 \pm 0.02$	$0.08 \pm 0.01$	pl	$0.7 - 3.1$	$-1.6 \pm 0.3$	$0.2^{+0.2}_{-0.2}$	$0.28^{+0.04}_{-0.04}$	–
J0835–4510	$3100 \pm 200$	$1050 \pm 60$	$170 \pm 20$	broken pl	$0.08 - 24.0$	–	$0.13^{+0.03}_{-0.08}$	$0.19^{+0.03}_{-0.03}$	$0.32^{+0.04}_{-0.09}$
J0837+0610	$13 \pm 6$	$5.0 \pm 1.0$	$0.2 \pm 0.1$	low turn-over	$0.02 - 4.9$	–	–	–	–
J0837–4135	$110 \pm 30$	$35 \pm 9$	$8 \pm 2$	broken pl	$0.1 - 8.4$	–	–	–	–
J0840–5332	$23 \pm 9$	$1.7 \pm 0.5$	$0.26 \pm 0.07$	broken pl	$0.1 - 3.1$	–	–	–	–
J0846–3533	$12 \pm 2$	$5.0 \pm 1.0$	$0.7 \pm 0.1$	pl	$0.4 - 3.4$	$-2.0 \pm 0.2$	–	–	–
J0855–3331	$3.5 \pm 0.7$	–	$0.11 \pm 0.02$	pl	$0.1 - 3.1$	$-2.0 \pm 0.1$	–	–	–
J0855–4644	$0.57 \pm 0.05$	$0.28 \pm 0.02$	$0.105 \pm 0.006$	pl	$0.7 - 3.1$	$-1.2 \pm 0.2$	–	$0.18^{+0.03}_{-0.02}$	–
J0856–6137	$3.1 \pm 0.6$	$3.3 \pm 0.7$	$0.11 \pm 0.02$	broken pl	$0.08 - 3.1$	–	–	–	–
J0857–4424	$3.3 \pm 0.2$	$0.98 \pm 0.05$	$0.23 \pm 0.02$	pl	$0.4 - 3.1$	$-1.9 \pm 0.1$	$0.09^{+0.02}_{-0.05}$	$0.15^{+0.02}_{-0.02}$	$0.24^{+0.1}_{-0.07}$
J0900–3144	$6.0 \pm 1.0$	$3.0 \pm 1.0$	$0.9 \pm 0.2$	pl	$0.7 - 3.4$	$-1.3 \pm 0.3$	–	–	–
J0901–4624	$0.7 \pm 0.1$	$0.51 \pm 0.03$	$0.18 \pm 0.02$	pl	$0.7 - 3.1$	$-1.1 \pm 0.3$	$0.5^{+0.1}_{-0.2}$	$0.43^{+0.07}_{-0.05}$	$0.36^{+0.09}_{-0.1}$
J0904–7459	$8 \pm 2$	$2.0 \pm 0.7$	$0.3 \pm 0.1$	pl	$0.4 - 3.1$	$-1.9 \pm 0.5$	–	–	–
J0905–5127	$3.4 \pm 0.5$	$1.05 \pm 0.06$	$0.22 \pm 0.03$	pl	$0.09 - 3.1$	$-2.09 \pm 0.07$	$0.48^{+0.09}_{-0.2}$	$0.27^{+0.05}_{-0.03}$	$0.4^{+0.2}_{-0.2}$
J0907–5157	$30 \pm 6$	$17 \pm 5$	$5.8 \pm 0.9$	lps	$0.08 - 3.5$	–	–	–	–
J0908–1739	$10 \pm 4$	$4 \pm 2$	$0.7 \pm 0.4$	pl	$0.05 - 3.3$	$-1.5 \pm 0.2$	–	–	–
J0908–4913	$33 \pm 5$	$20.0 \pm 1.0$	$7.8 \pm 0.6$	lps	$0.4 - 17.0$	–	$0.5^{+0.1}_{-0.2}$	$0.25^{+0.06}_{-0.01}$	$0.2^{+0.1}_{-0.03}$
J0909–7212	$3.0 \pm 1.0$	$1.9 \pm 0.5$	$< 0.3$	pl	$0.4 - 1.5$	$-1.0 \pm 0.6$	–	–	–
J0922+0638	$17 \pm 9$	$10 \pm 3$	$1.3 \pm 0.6$	low turn-over	$0.02 - 10.6$	–	–	–	–
J0922–4949	$1.5 \pm 0.2$	–	$0.32 \pm 0.04$	pl	$0.7 - 3.4$	$-1.0 \pm 0.2$	–	–	–
J0924–5302	$9 \pm 9$	$1.1 \pm 0.3$	$0.2 \pm 0.1$	pl	$0.10 - 3.1$	$-2.16 \pm 0.09$	–	–	–
J0924–5814	$11 \pm 3$	$6 \pm 2$	$1.5 \pm 0.5$	pl	$0.4 - 3.4$	$-1.4 \pm 0.3$	–	–	–
J0934–5249	$22 \pm 9$	$3.2 \pm 0.9$	$0.2 \pm 0.04$	lps	$0.3 - 3.1$	–	–	–	–
J0940–5428	$1.5 \pm 0.2$	$0.66 \pm 0.04$	$0.3 \pm 0.02$	pl	$0.7 - 3.1$	$-1.0 \pm 0.2$	$0.41^{+0.09}_{-0.2}$	$0.3^{+0.05}_{-0.05}$	$0.1^{+0.05}_{-0.05}$
J0942–5552	$26 \pm 7$	$11 \pm 3$	$2.0 \pm 0.3$	broken pl	$0.2 - 3.5$	–	–	–	–
J0942–5657	$2.6 \pm 0.4$	$1.0 \pm 0.3$	$0.3 \pm 0.09$	low turn-over	$0.08 - 3.3$	–	–	–	–
J0943+1631	$5 \pm 3$	$1.3 \pm 0.6$	$0.3 \pm 0.2$	pl	$0.03 - 3.1$	$-1.0 \pm 0.4$	–	–	–
J0952–3839	$1.3 \pm 0.3$	$4.0 \pm 1.0$	$< 0.01$	pl	$0.4 - 1.5$	$-2.5 \pm 0.6$	–	–	–

Table 1 – *continued*

PSRJ	$S_{728}$ (mJy)	$S_{1382}$ (mJy)	$S_{3100}$ (mJy)	Class	$\Delta\nu$ (GHz)	$\alpha$	$m_r, 728$	$m_r, 1382$	$m_r, 3100$
J0953+0755	600 ± 600	100 ± 40	20 ± 20	low turn-over	0.02 – 10.6	–	–	–	–
J0954–5430	0.7 ± 0.1	0.51 ± 0.03	0.38 ± 0.04	pl	0.7 – 3.4	–0.3 ± 0.2	–	0.43 <sup>+0.04</sup> <sub>–0.07</sub>	0.29 <sup>+0.2</sup> <sub>–0.08</sub>
J0959–4809	13 ± 3	4.0 ± 0.8	0.5 ± 0.2	lps	0.2 – 3.3	–	–	–	–
J1001–5507	41 ± 5	10 ± 3	2.7 ± 0.4	broken pl	0.1 – 3.5	–	–	–	–
J1001–5559	3.4 ± 0.8	1.4 ± 0.4	0.11 ± 0.03	pl	0.7 – 3.1	–2.4 ± 0.4	–	–	–
J1003–4747	4.8 ± 0.9	1.43 ± 0.08	0.3 ± 0.04	pl	0.3 – 3.1	–1.4 ± 0.1	0.5 <sup>+0.2</sup> <sub>–0.3</sub>	0.32 <sup>+0.07</sup> <sub>–0.03</sub>	0.29 <sup>+0.2</sup> <sub>–0.07</sub>
J1012–5857	13 ± 5	1.8 ± 0.3	0.41 ± 0.04	pl	0.4 – 3.3	–1.8 ± 0.1	–	–	–
J1013–5934	3.4 ± 0.4	2.6 ± 0.6	0.9 ± 0.2	pl	0.7 – 3.5	–0.9 ± 0.1	–	–	–
J1015–5719	2.7 ± 0.4	3.0 ± 0.2	1.7 ± 0.1	pl	0.7 – 3.5	–0.62 ± 0.09	–	0.16 <sup>+0.02</sup> <sub>–0.02</sub>	0.18 <sup>+0.04</sup> <sub>–0.06</sub>
J1016–5345	2.2 ± 0.6	1.1 ± 0.4	0.14 ± 0.04	pl	0.4 – 3.1	–1.6 ± 0.4	–	–	–
J1016–5819	1.18 ± 0.06	0.36 ± 0.02	0.053 ± 0.008	pl	0.7 – 3.1	–2.0 ± 0.2	0.06 <sup>+0.2</sup> <sub>–0.01</sub>	0.29 <sup>+0.02</sup> <sub>–0.05</sub>	–
J1016–5857	1.8 ± 0.2	0.9 ± 0.05	0.29 ± 0.02	pl	0.7 – 3.1	–1.3 ± 0.2	–	0.26 <sup>+0.02</sup> <sub>–0.04</sub>	0.2 <sup>+0.1</sup> <sub>–0.07</sub>
J1017–5621	6.4 ± 0.7	1.8 ± 0.4	0.37 ± 0.04	pl	0.4 – 3.3	–2.0 ± 0.1	–	–	–
J1017–7156	3.1 ± 0.7	1.1 ± 0.2	0.14 ± 0.05	pl	0.7 – 3.1	–1.73 ± 0.09	–	–	–
J1018–1642	1.3 ± 0.5	0.7 ± 0.2	< 0.3	pl	0.1 – 1.4	–2.0 ± 0.4	–	–	–
J1019–5749	< 0.6	3.8 ± 0.2	2.4 ± 0.1	lps	1.3 – 3.5	–	–	0.41 <sup>+0.03</sup> <sub>–0.03</sub>	0.053 <sup>+0.007</sup> <sub>–0.01</sub>
J1020–5921	–	< 5.0	–	–	1.4 – 1.4	–	–	–	–
J1020–6026	< 0.06	0.25 ± 0.01	0.16 ± 0.01	–	1.4 – 3.1	–	–	0.24 <sup>+0.04</sup> <sub>–0.05</sub>	0.16 <sup>+0.07</sup> <sub>–0.05</sub>
J1024–0719	–	0.3 ± 0.2	–	lps	0.1 – 5.0	–	–	–	–
J1028–5819	< 0.2	0.24 ± 0.02	0.13 ± 0.06	pl	1.4 – 3.1	1.3 ± 0.8	–	0.5 <sup>+0.1</sup> <sub>–0.1</sub>	0.8 <sup>+1.0</sup> <sub>–0.3</sub>
J1032–5911	3.7 ± 0.6	1.1 ± 0.2	< 0.3	pl	0.4 – 1.5	–2.5 ± 0.4	–	–	–
J1034–3224	18 ± 6	8 ± 3	1.4 ± 0.6	pl	0.4 – 3.3	–1.6 ± 0.4	–	–	–
J1036–4926	2.2 ± 0.5	0.8 ± 0.2	< 0.02	pl	0.3 – 1.5	–1.5 ± 0.5	–	–	–
J1038–5831	3.0 ± 1.0	2.3 ± 0.9	0.5 ± 0.2	pl	0.6 – 3.1	–1.3 ± 0.6	–	–	–
J1041–1942	–	2.3 ± 0.9	–	pl	0.4 – 1.5	–2.0 ± 0.4	–	–	–
J1043–6116	2.6 ± 0.2	1.39 ± 0.07	0.49 ± 0.03	pl	0.7 – 3.4	–1.2 ± 0.1	0.14 <sup>+0.08</sup> <sub>–0.05</sub>	0.16 <sup>+0.01</sup> <sub>–0.02</sub>	0.19 <sup>+0.1</sup> <sub>–0.09</sub>
J1045–4509	7.0 ± 1.0	1.9 ± 0.4	0.33 ± 0.09	broken pl	0.3 – 3.1	–	–	–	–
J1046–5813	4.1 ± 0.8	1.4 ± 0.3	0.24 ± 0.05	pl	0.4 – 3.1	–1.9 ± 0.3	–	–	–
J1047–6709	3.9 ± 0.9	3.1 ± 0.9	1.4 ± 0.3	pl	0.4 – 3.5	–0.7 ± 0.2	–	–	–
J1048–5832	12.0 ± 1.0	9.1 ± 0.5	6.2 ± 0.5	pl	0.6 – 17.0	–0.52 ± 0.08	0.3 <sup>+0.1</sup> <sub>–0.1</sub>	0.34 <sup>+0.07</sup> <sub>–0.02</sub>	0.31 <sup>+0.08</sup> <sub>–0.1</sub>
J1049–5833	–	–	0.07 ± 0.01	–	1.4 – 3.1	–	–	–	–
J1052–5954	< 0.2	0.147 ± 0.009	0.071 ± 0.005	–	1.4 – 3.1	–	–	0.45 <sup>+0.02</sup> <sub>–0.2</sub>	0.12 <sup>+0.06</sup> <sub>–0.06</sub>
J1055–6028	1.2 ± 0.2	0.95 ± 0.05	0.13 ± 0.01	lps	0.7 – 3.1	–	0.11 <sup>+0.08</sup> <sub>–0.05</sub>	0.22 <sup>+0.02</sup> <sub>–0.03</sub>	0.24 <sup>+0.08</sup> <sub>–0.2</sub>
J1056–6258	54 ± 6	34 ± 8	11.0 ± 1.0	pl	0.4 – 8.4	–1.1 ± 0.1	–	–	–
J1057–5226	22 ± 5	4.4 ± 0.6	1.4 ± 0.3	lps	0.08 – 3.1	–	0.6 <sup>+0.3</sup> <sub>–0.4</sub>	1.0 <sup>+0.1</sup> <sub>–0.2</sub>	0.8 <sup>+0.2</sup> <sub>–0.3</sub>
J1057–7914	2.4 ± 0.9	–	< 0.1	–	0.4 – 0.7	–	–	–	–
J1058–5957	–	0.6 ± 0.1	–	–	1.2 – 1.5	–	–	–	–
J1059–5742	30 ± 10	2.0 ± 0.6	0.21 ± 0.05	pl	0.4 – 3.1	–3.3 ± 0.4	–	–	–
J1105–6107	2.4 ± 0.2	1.2 ± 0.07	0.46 ± 0.04	pl	0.7 – 3.4	–1.1 ± 0.1	0.18 <sup>+0.03</sup> <sub>–0.1</sub>	0.36 <sup>+0.06</sup> <sub>–0.02</sub>	0.28 <sup>+0.09</sup> <sub>–0.06</sub>
J1110–5637	4.7 ± 0.7	3.3 ± 0.8	0.9 ± 0.2	pl	0.6 – 3.5	–1.2 ± 0.1	–	–	–
J1112–6103	< 0.08	2.3 ± 0.1	1.03 ± 0.07	pl	1.3 – 3.5	–1.0 ± 0.1	–	0.22 <sup>+0.04</sup> <sub>–0.02</sub>	0.18 <sup>+0.05</sup> <sub>–0.05</sub>
J1112–6613	12 ± 4	1.7 ± 0.4	0.32 ± 0.05	pl	0.4 – 3.3	–2.1 ± 0.2	–	–	–
J1112–6926	4.0 ± 1.0	0.6 ± 0.2	0.4 ± 0.1	pl	0.4 – 3.1	–2.2 ± 0.5	–	–	–
J1114–6100	–	4.7 ± 0.9	1.8 ± 0.7	pl	0.6 – 3.5	–0.9 ± 0.4	–	–	–
J1115–6052	1.9 ± 0.5	0.48 ± 0.03	0.2 ± 0.01	pl	0.7 – 3.1	–1.2 ± 0.2	–	0.22 <sup>+0.03</sup> <sub>–0.01</sub>	0.17 <sup>+0.06</sup> <sub>–0.08</sub>
J1116–4122	6 ± 7	6 ± 2	0.3 ± 0.1	pl	0.09 – 3.1	–1.2 ± 0.1	–	–	–
J1117–6154	–	1.6 ± 0.3	–	–	1.2 – 1.5	–	–	–	–
J1119–6127	3.0 ± 0.4	1.09 ± 0.06	0.36 ± 0.03	pl	0.7 – 3.4	–1.4 ± 0.2	–	0.11 <sup>+0.01</sup> <sub>–0.01</sub>	0.24 <sup>+0.07</sup> <sub>–0.08</sub>
J1119–7936	3.0 ± 1.0	–	< 0.06	–	0.4 – 0.7	–	–	–	–
J1121–5444	4.3 ± 0.9	1.5 ± 0.4	0.22 ± 0.05	pl	0.1 – 3.1	–2.2 ± 0.1	–	–	–
J1123–4844	2.5 ± 0.5	1.0 ± 0.3	0.4 ± 0.1	pl	0.4 – 3.4	–1.4 ± 0.3	–	–	–
J1123–6102	–	1.1 ± 0.2	–	–	1.2 – 1.5	–	–	–	–
J1123–6259	2.0 ± 0.2	0.51 ± 0.03	0.1 ± 0.006	pl	0.4 – 3.1	–2.1 ± 0.1	0.2 <sup>+0.1</sup> <sub>–0.07</sub>	0.29 <sup>+0.04</sup> <sub>–0.03</sub>	–
J1126–6942	3.0 ± 1.0	–	< 0.05	–	0.4 – 0.7	–	–	–	–
J1133–6250	22 ± 3	7.0 ± 1.0	1.6 ± 0.3	pl	0.6 – 3.5	–1.8 ± 0.1	–	–	–
J1136+1551	–	20 ± 10	–	broken pl	0.02 – 32.0	–	–	–	–
J1136–5525	–	6.0 ± 1.0	–	pl	0.4 – 1.5	–1.2 ± 0.8	–	–	–
J1138–6207	< 0.3	0.57 ± 0.03	0.27 ± 0.02	pl	1.4 – 3.4	–0.9 ± 0.2	–	0.22 <sup>+0.04</sup> <sub>–0.05</sub>	0.24 <sup>+0.05</sup> <sub>–0.1</sub>
J1141–3322	–	1.6 ± 0.5	–	pl	0.4 – 1.5	–1.2 ± 0.8	–	–	–
J1141–6545	15 ± 4	2.4 ± 0.7	0.28 ± 0.08	pl	0.7 – 3.1	–2.7 ± 0.4	–	–	–
J1144–6146	–	< 0.6	–	–	1.4 – 1.4	–	–	–	–
J1146–6030	10 ± 3	3.2 ± 0.6	1.1 ± 0.3	pl	0.4 – 3.4	–1.6 ± 0.3	–	–	–
J1156–5707	0.5 ± 0.1	0.27 ± 0.02	0.12 ± 0.01	pl	0.7 – 3.1	–1.2 ± 0.3	–	0.34 <sup>+0.06</sup> <sub>–0.06</sub>	–

Table 1 – *continued*

PSRJ	$S_{728}$ (mJy)	$S_{1382}$ (mJy)	$S_{3100}$ (mJy)	Class	$\Delta\nu$ (GHz)	$\alpha$	$m_r, 728$	$m_r, 1382$	$m_r, 3100$
J1156–5909	< 40.0	–	< 0.01	–	0.4 – 0.4	–	–	–	–
J1157–6224	54 ± 9	14 ± 3	1.8 ± 0.4	pl	0.4 – 3.5	–2.4 ± 0.1	–	–	–
J1159–7910	–	0.7 ± 0.2	–	pl	0.4 – 1.5	–2.0 ± 1.0	–	–	–
J1202–5820	9 ± 2	3.0 ± 0.8	0.7 ± 0.2	pl	0.4 – 3.3	–1.8 ± 0.3	–	–	–
J1210–5559	10 ± 2	2.3 ± 0.6	0.27 ± 0.07	pl	0.4 – 3.3	–2.4 ± 0.3	–	–	–
J1216–6223	< 0.4	0.23 ± 0.01	0.061 ± 0.006	–	1.4 – 3.1	–	–	0.19 <sup>+0.05</sup> <sub>–0.04</sub>	–
J1224–6407	20 ± 2	8.9 ± 0.5	3.0 ± 0.4	pl	0.4 – 3.5	–1.36 ± 0.08	0.22 <sup>+0.04</sup> <sub>–0.1</sub>	0.32 <sup>+0.04</sup> <sub>–0.04</sub>	0.4 <sup>+0.2</sup> <sub>–0.2</sub>
J1227–6208	–	–	< 0.01	–	1.4 – 1.4	–	–	–	–
J1231–6303	9 ± 2	–	0.5 ± 0.1	pl	0.7 – 3.3	–2.0 ± 0.3	–	–	–
J1235–5516	–	–	< 0.1	–	0.4 – 1.4	–	–	–	–
J1239–6832	5.0 ± 1.0	–	0.15 ± 0.05	pl	0.4 – 3.1	–2.3 ± 0.4	–	–	–
J1243–6423	140 ± 30	–	4.1 ± 0.8	broken pl	0.4 – 8.4	–	–	–	–
J1248–6344	1.1 ± 0.2	0.2 ± 0.01	< 0.02	–	0.7 – 1.4	–	–	0.31 <sup>+0.05</sup> <sub>–0.07</sub>	–
J1253–5820	25 ± 7	–	1.6 ± 0.5	pl	0.4 – 3.5	–1.8 ± 0.2	–	–	–
J1259–6741	8 ± 2	–	0.3 ± 0.1	pl	0.4 – 3.3	–2.1 ± 0.4	–	–	–
J1301–6305	0.7 ± 0.1	0.49 ± 0.03	0.21 ± 0.02	pl	0.7 – 3.1	–0.9 ± 0.2	–	0.24 <sup>+0.05</sup> <sub>–0.02</sub>	0.24 <sup>+0.04</sup> <sub>–0.09</sub>
J1302–6350	1.3 ± 0.5	4.5 ± 0.3	2.7 ± 0.3	pl	0.6 – 8.4	–0.5 ± 0.1	0.5 <sup>+0.4</sup> <sub>–0.2</sub>	0.34 <sup>+0.06</sup> <sub>–0.03</sub>	0.42 <sup>+0.09</sup> <sub>–0.1</sub>
J1305–6203	8 ± 3	0.67 ± 0.04	0.23 ± 0.02	pl	0.7 – 3.1	–1.4 ± 0.3	–	0.16 <sup>+0.02</sup> <sub>–0.02</sub>	0.23 <sup>+0.05</sup> <sub>–0.07</sub>
J1305–6455	12 ± 2	–	0.44 ± 0.07	pl	0.4 – 3.4	–2.3 ± 0.2	–	–	–
J1312–5402	5.0 ± 1.0	–	0.13 ± 0.04	pl	0.3 – 3.1	–2.4 ± 0.2	–	–	–
J1312–5516	12 ± 3	–	0.6 ± 0.2	pl	0.4 – 3.4	–2.1 ± 0.3	–	–	–
J1312–6400	3.0 ± 1.0	–	< 0.08	–	0.7 – 1.4	–	–	–	–
J1317–6302	4.2 ± 0.5	–	0.24 ± 0.03	pl	0.7 – 3.3	–2.0 ± 0.2	–	–	–
J1319–6056	7.0 ± 1.0	–	0.29 ± 0.05	pl	0.6 – 3.3	–2.2 ± 0.2	–	–	–
J1319–6105	2.3 ± 0.3	–	0.42 ± 0.07	pl	0.7 – 3.4	–1.4 ± 0.2	–	–	–
J1320–5359	8.0 ± 1.0	2.1 ± 0.1	0.51 ± 0.05	pl	0.3 – 3.1	–1.7 ± 0.2	0.4 <sup>+0.3</sup> <sub>–0.2</sub>	0.3 <sup>+0.06</sup> <sub>–0.03</sub>	0.3 <sup>+0.2</sup> <sub>–0.06</sub>
J1326–5859	45 ± 8	–	3.6 ± 0.7	pl	0.4 – 8.4	–1.8 ± 0.1	–	–	–
J1326–6408	11 ± 2	–	0.32 ± 0.05	pl	0.4 – 3.3	–2.5 ± 0.1	–	–	–
J1326–6700	–	–	4.0 ± 1.0	pl	0.4 – 3.5	–1.1 ± 0.3	–	–	–
J1327–6222	160 ± 30	–	5.0 ± 1.0	broken pl	0.1 – 6.5	–	–	–	–
J1327–6301	13 ± 2	–	1.1 ± 0.2	pl	0.6 – 3.5	–1.7 ± 0.2	–	–	–
J1327–6400	0.5 ± 0.2	0.21 ± 0.02	0.081 ± 0.008	pl	0.7 – 3.1	–1.3 ± 0.3	–	0.3 <sup>+0.08</sup> <sub>–0.05</sub>	0.3 <sup>+0.1</sup> <sub>–0.2</sub>
J1338–6204	–	–	1.1 ± 0.2	pl	0.6 – 3.4	–1.4 ± 0.3	–	–	–
J1341–6023	1.6 ± 0.3	–	< 0.02	–	0.7 – 1.4	–	–	–	–
J1341–6220	< 0.9	2.7 ± 0.1	1.24 ± 0.09	pl	1.3 – 8.4	–0.92 ± 0.09	–	0.16 <sup>+0.01</sup> <sub>–0.02</sub>	0.21 <sup>+0.04</sup> <sub>–0.09</sub>
J1345–6115	2.5 ± 0.5	–	0.2 ± 0.04	pl	0.7 – 3.1	–1.8 ± 0.4	–	–	–
J1347–5947	2.7 ± 0.5	–	0.14 ± 0.03	pl	0.7 – 3.1	–2.1 ± 0.4	–	–	–
J1349–6130	< 1.0	0.76 ± 0.04	0.32 ± 0.02	pl	1.3 – 3.1	–1.0 ± 0.2	–	0.15 <sup>+0.01</sup> <sub>–0.02</sub>	0.15 <sup>+0.04</sup> <sub>–0.05</sub>
J1355–5153	< 200.0	–	< 0.3	–	0.3 – 0.4	–	–	–	–
J1356–5521	< 100.0	–	< 0.2	–	0.4 – 1.4	–	–	–	–
J1357–62	31 ± 5	–	2.5 ± 0.4	pl	0.7 – 3.5	–1.8 ± 0.1	–	–	–
J1357–6429	1.0 ± 0.3	0.52 ± 0.03	0.15 ± 0.02	pl	0.7 – 3.1	–1.4 ± 0.4	–	0.34 <sup>+0.05</sup> <sub>–0.05</sub>	0.4 <sup>+0.1</sup> <sub>–0.2</sub>
J1359–6038	57 ± 3	12.5 ± 0.6	2.1 ± 0.1	broken pl	0.1 – 8.4	–	0.03 <sup>+0.02</sup> <sub>–0.01</sub>	0.091 <sup>+0.05</sup> <sub>–0.01</sub>	0.1 <sup>+0.05</sup> <sub>–0.03</sub>
J1401–6357	20 ± 6	–	1.9 ± 0.6	pl	0.4 – 3.5	–1.8 ± 0.2	–	–	–
J1406–6121	< 0.3	0.44 ± 0.03	0.31 ± 0.02	pl	1.4 – 6.5	–0.5 ± 0.2	–	0.24 <sup>+0.04</sup> <sub>–0.05</sub>	0.24 <sup>+0.02</sup> <sub>–0.1</sub>
J1410–6132	< 0.2	1.9 ± 0.1	1.79 ± 0.09	lps	1.3 – 6.5	–	–	0.5 <sup>+0.05</sup> <sub>–0.05</sub>	0.038 <sup>+0.03</sup> <sub>–0.007</sub>
J1412–6145	< 0.3	0.69 ± 0.04	0.2 ± 0.01	pl	1.4 – 3.1	–1.5 ± 0.2	–	0.17 <sup>+0.02</sup> <sub>–0.02</sub>	0.21 <sup>+0.08</sup> <sub>–0.07</sub>
J1413–6141	< 0.4	0.82 ± 0.04	0.49 ± 0.03	pl	1.4 – 3.5	–0.5 ± 0.2	–	0.22 <sup>+0.02</sup> <sub>–0.03</sub>	0.1 <sup>+0.04</sup> <sub>–0.03</sub>
J1413–6222	< 0.2	–	0.45 ± 0.06	–	1.4 – 3.1	–	–	–	–
J1413–6307	3.0 ± 0.8	–	0.5 ± 0.1	pl	0.6 – 3.3	–1.4 ± 0.4	–	–	–
J1415–6621	1.3 ± 0.2	–	< 0.2	–	0.7 – 1.5	–	–	–	–
J1420–5416	< 200.0	–	< 6.0	–	0.4 – 0.4	–	–	–	–
J1420–6048	< 1.0	1.19 ± 0.06	0.9 ± 0.05	pl	1.3 – 3.5	–0.3 ± 0.1	–	0.16 <sup>+0.01</sup> <sub>–0.02</sub>	0.1 <sup>+0.05</sup> <sub>–0.02</sub>
J1424–5822	4.3 ± 0.7	–	0.29 ± 0.06	pl	0.7 – 3.3	–1.9 ± 0.2	–	–	–
J1452–5851	0.6 ± 0.3	0.33 ± 0.02	0.123 ± 0.008	pl	0.7 – 3.1	–1.2 ± 0.2	–	0.23 <sup>+0.04</sup> <sub>–0.04</sub>	0.14 <sup>+0.05</sup> <sub>–0.07</sub>
J1452–6036	1.8 ± 0.2	1.9 ± 0.1	0.76 ± 0.05	pl	0.7 – 3.5	–1.1 ± 0.1	–	0.13 <sup>+0.02</sup> <sub>–0.02</sub>	0.19 <sup>+0.1</sup> <sub>–0.08</sub>
J1453–6413	80 ± 10	18.0 ± 1.0	2.4 ± 0.5	broken pl	0.08 – 8.4	–	0.46 <sup>+0.07</sup> <sub>–0.2</sub>	0.47 <sup>+0.05</sup> <sub>–0.05</sub>	0.7 <sup>+0.5</sup> <sub>–0.3</sub>
J1507–6640	< 20.0	–	< 2.0	pl	0.4 – 1.5	–2.8 ± 0.4	–	–	–
J1509–5850	–	0.21 ± 0.01	< 0.05	–	1.4 – 1.4	–	–	0.21 <sup>+0.07</sup> <sub>–0.04</sub>	–
J1512–5759	16.8 ± 0.9	7.8 ± 0.4	1.24 ± 0.06	lps	0.6 – 3.5	–	0.07 <sup>+0.05</sup> <sub>–0.02</sub>	0.056 <sup>+0.009</sup> <sub>–0.008</sub>	0.06 <sup>+0.02</sup> <sub>–0.02</sub>
J1513–5739	0.07 ± 0.06	–	< 10.0	–	0.7 – 1.4	–	–	–	–
J1513–5908	3.3 ± 0.3	1.43 ± 0.07	0.35 ± 0.03	pl	0.4 – 3.1	–1.5 ± 0.2	0.4 <sup>+0.1</sup> <sub>–0.1</sub>	0.139 <sup>+0.02</sup> <sub>–0.008</sub>	0.3 <sup>+0.03</sup> <sub>–0.04</sub>
J1514–5925	< 0.4	0.29 ± 0.02	0.16 ± 0.01	–	1.4 – 3.1	–	–	0.29 <sup>+0.02</sup> <sub>–0.06</sub>	0.2 <sup>+0.04</sup> <sub>–0.09</sub>

Table 1 – *continued*

PSRJ	$S_{728}$ (mJy)	$S_{1382}$ (mJy)	$S_{3100}$ (mJy)	Class	$\Delta\nu$ (GHz)	$\alpha$	$m_r, 728$	$m_r, 1382$	$m_r, 3100$
J1515–5720	$1.04 \pm 0.07$	$0.25 \pm 0.01$	$0.08 \pm 0.01$	pl	0.7 – 3.1	$-2.0 \pm 0.2$	$0.13^{+0.2}_{-0.03}$	$0.25^{+0.04}_{-0.04}$	–
J1522–5829	$30 \pm 6$	–	$5.0 \pm 1.0$	broken pl	0.6 – 8.4	–	–	–	–
J1524–5625	$1.8 \pm 0.5$	$1.28 \pm 0.07$	$0.55 \pm 0.03$	pl	0.7 – 3.4	$-0.9 \pm 0.2$	–	$0.18^{+0.02}_{-0.01}$	$0.13^{+0.04}_{-0.05}$
J1524–5706	$0.17 \pm 0.04$	$0.45 \pm 0.02$	$0.14 \pm 0.02$	pl	0.7 – 3.1	$-1.3 \pm 0.4$	–	$0.21^{+0.04}_{-0.02}$	$0.4^{+0.2}_{-0.2}$
J1527–5552	$< 200.0$	–	$< 8.0$	–	0.4 – 1.4	–	–	–	–
J1530–5327	$1.6 \pm 0.4$	$0.92 \pm 0.06$	$0.41 \pm 0.06$	pl	0.7 – 3.1	$-0.9 \pm 0.4$	–	$0.47^{+0.05}_{-0.04}$	$0.5^{+0.2}_{-0.2}$
J1531–5610	$< 0.4$	$0.87 \pm 0.05$	$0.6 \pm 0.04$	pl	1.4 – 6.5	$-0.4 \pm 0.2$	–	$0.19^{+0.03}_{-0.03}$	$0.13^{+0.1}_{-0.03}$
J1534–5405	$6.0 \pm 1.0$	–	$0.21 \pm 0.05$	pl	0.6 – 3.1	$-2.3 \pm 0.2$	–	–	–
J1536–5433	$< 80.0$	–	$1.3 \pm 0.4$	–	1.4 – 3.3	–	–	–	–
J1538–5551	$< 0.7$	$0.33 \pm 0.02$	$0.1 \pm 0.01$	–	1.4 – 3.1	–	–	$0.26^{+0.03}_{-0.04}$	–
J1539–5626	$7.6 \pm 0.8$	$5.0 \pm 0.3$	$2.1 \pm 0.1$	pl	0.6 – 8.4	$-1.04 \pm 0.07$	$0.23^{+0.05}_{-0.1}$	$0.09^{+0.01}_{-0.02}$	$0.1^{+0.05}_{-0.04}$
J1541–5535	$< 0.1$	$0.3 \pm 0.02$	$0.17 \pm 0.01$	–	1.4 – 3.1	–	–	$0.2^{+0.02}_{-0.02}$	$0.23^{+0.1}_{-0.08}$
J1543–5459	$< 0.3$	$0.81 \pm 0.04$	$0.21 \pm 0.02$	–	1.4 – 3.1	–	–	$0.22^{+0.02}_{-0.04}$	$0.2^{+0.2}_{-0.1}$
J1548–4927	$2.2 \pm 0.5$	–	$0.2 \pm 0.06$	pl	0.7 – 3.1	$-1.9 \pm 0.5$	–	–	–
J1548–5607	$3.1 \pm 0.4$	$1.39 \pm 0.07$	$0.3 \pm 0.02$	pl	0.7 – 3.1	$-1.8 \pm 0.2$	–	$0.1^{+0.02}_{-0.02}$	$0.22^{+0.05}_{-0.09}$
J1549–4848	$4.1 \pm 0.7$	$1.6 \pm 0.1$	$0.25 \pm 0.04$	pl	0.4 – 3.1	$-1.9 \pm 0.3$	$0.5^{+0.1}_{-0.3}$	$0.44^{+0.09}_{-0.05}$	$0.4^{+0.2}_{-0.2}$
J1551–5310	$< 0.9$	$0.72 \pm 0.04$	$0.24 \pm 0.01$	–	1.4 – 3.1	–	–	$0.29^{+0.03}_{-0.04}$	$0.14^{+0.02}_{-0.05}$
J1600–5044	$84 \pm 5$	$21.0 \pm 1.0$	$3.6 \pm 0.2$	pl	0.3 – 8.4	$-2.16 \pm 0.05$	$0.1^{+0.01}_{-0.06}$	$0.045^{+0.006}_{-0.008}$	$0.08^{+0.03}_{-0.02}$
J1600–5751	$9.2 \pm 0.5$	$2.5 \pm 0.1$	$0.54 \pm 0.07$	pl	0.4 – 3.4	$-2.1 \pm 0.1$	$0.1^{+0.08}_{-0.04}$	$0.18^{+0.03}_{-0.02}$	$0.4^{+0.1}_{-0.1}$
J1601–5335	$0.5 \pm 0.1$	$0.25 \pm 0.02$	$0.06 \pm 0.01$	pl	0.7 – 3.1	$-1.5 \pm 0.5$	–	$0.43^{+0.02}_{-0.2}$	–
J1604–4909	$23 \pm 6$	–	$2.7 \pm 0.8$	pl	0.4 – 3.4	$-1.6 \pm 0.3$	–	–	–
J1610–5303	$2.6 \pm 0.4$	–	$< 0.01$	–	0.7 – 1.4	–	–	–	–
J1611–4949	$< 1.0$	–	$0.34 \pm 0.05$	–	1.4 – 3.1	–	–	–	–
J1611–5209	$2.6 \pm 0.2$	$1.45 \pm 0.09$	$0.49 \pm 0.07$	pl	0.6 – 3.4	$-1.1 \pm 0.2$	$0.13^{+0.2}_{-0.06}$	$0.37^{+0.04}_{-0.05}$	$0.5^{+0.1}_{-0.2}$
J1613–4714	$8 \pm 2$	–	$0.36 \pm 0.09$	pl	0.4 – 3.3	$-2.2 \pm 0.3$	–	–	–
J1614–5048	$6.0 \pm 1.0$	$4.1 \pm 0.2$	$0.67 \pm 0.04$	pl	0.7 – 3.5	$-2.16 \pm 0.09$	–	$0.09^{+0.01}_{-0.01}$	$0.089^{+0.005}_{-0.03}$
J1617–5055	$< 0.1$	$0.27 \pm 0.02$	$0.24 \pm 0.01$	–	1.4 – 3.4	–	–	$0.39^{+0.06}_{-0.08}$	$0.11^{+0.04}_{-0.01}$
J1618–4723	$2.2 \pm 0.5$	–	$< 0.03$	–	0.7 – 1.4	–	–	–	–
J1622–4802	–	–	$0.32 \pm 0.06$	pl	1.3 – 3.3	$-1.1 \pm 0.3$	–	–	–
J1625–4048	$3.3 \pm 0.8$	–	$< 1.0$	–	0.4 – 0.7	–	–	–	–
J1626–4537	$4.4 \pm 0.9$	–	$0.29 \pm 0.06$	pl	0.7 – 3.1	$-2.0 \pm 0.2$	–	–	–
J1626–4807	$< 0.3$	$0.37 \pm 0.02$	$0.26 \pm 0.02$	–	1.4 – 3.1	–	–	$0.32^{+0.08}_{-0.03}$	$0.18^{+0.08}_{-0.06}$
J1627–4706	$< 0.09$	$0.18 \pm 0.01$	$0.061 \pm 0.005$	–	1.4 – 3.1	–	–	$0.2^{+0.04}_{-0.04}$	–
J1630–4733	$< 1.0$	–	$3.4 \pm 0.4$	pl	1.4 – 8.4	$-0.3 \pm 0.3$	–	–	–
J1632–4621	–	–	$0.21 \pm 0.02$	pl	1.3 – 3.1	$-1.8 \pm 0.3$	–	–	–
J1632–4757	$< 0.3$	$0.51 \pm 0.03$	$0.2 \pm 0.01$	–	1.4 – 3.1	–	–	$0.22^{+0.05}_{-0.03}$	$0.2^{+0.2}_{-0.09}$
J1632–4818	$< 0.1$	$0.48 \pm 0.03$	$0.101 \pm 0.006$	–	1.4 – 3.1	–	–	$0.23^{+0.02}_{-0.04}$	$0.06^{+0.3}_{-0.03}$
J1633–5015	$27 \pm 4$	–	$1.2 \pm 0.2$	pl	0.6 – 3.3	$-2.2 \pm 0.2$	–	–	–
J1635–5954	$3.4 \pm 0.8$	–	$0.4 \pm 0.1$	lps	0.4 – 3.3	–	–	–	–
J1636–4440	$< 0.2$	$0.29 \pm 0.02$	$0.16 \pm 0.02$	–	1.4 – 3.1	–	–	$0.28^{+0.09}_{-0.05}$	–
J1636–4803	–	–	$0.37 \pm 0.04$	pl	1.3 – 3.4	$-2.0 \pm 0.2$	–	–	–
J1637–4553	$3.0 \pm 0.4$	$1.5 \pm 0.09$	$0.37 \pm 0.03$	pl	0.4 – 3.4	$-1.6 \pm 0.2$	$0.33^{+0.07}_{-0.2}$	$0.32^{+0.04}_{-0.05}$	$0.2^{+0.1}_{-0.1}$
J1637–4642	$< 0.2$	$0.93 \pm 0.05$	$0.53 \pm 0.03$	pl	1.4 – 3.4	$-0.6 \pm 0.2$	–	$0.22^{+0.02}_{-0.04}$	$0.13^{+0.04}_{-0.06}$
J1638–4417	$< 0.08$	$0.3 \pm 0.02$	$0.07 \pm 0.02$	–	1.4 – 3.1	–	–	$0.22^{+0.03}_{-0.03}$	–
J1638–4608	$< 0.3$	$0.45 \pm 0.02$	$0.121 \pm 0.009$	–	1.4 – 3.1	–	–	$0.21^{+0.02}_{-0.03}$	$0.13^{+0.07}_{-0.04}$
J1639–4359	$4.9 \pm 0.9$	–	$0.19 \pm 0.04$	pl	0.7 – 3.1	$-2.3 \pm 0.3$	–	–	–
J1639–4604	$4.9 \pm 0.9$	–	$0.15 \pm 0.03$	pl	0.4 – 3.1	$-2.4 \pm 0.4$	–	–	–
J1640–4715	$4 \pm 2$	$1.56 \pm 0.08$	$0.6 \pm 0.03$	pl	0.7 – 3.4	$-1.1 \pm 0.1$	–	$0.13^{+0.01}_{-0.02}$	$0.11^{+0.05}_{-0.07}$
J1643–4505	$< 0.4$	$0.45 \pm 0.02$	$0.27 \pm 0.02$	pl	1.4 – 3.4	$-0.5 \pm 0.2$	–	$0.16^{+0.04}_{-0.02}$	$0.14^{+0.07}_{-0.04}$
J1644–4559	$1200 \pm 60$	$300 \pm 60$	$61 \pm 3$	low turn-over	0.3 – 17.0	–	–	–	$0.04^{+0.5}_{-0.02}$
J1646–4346	$< 0.4$	$1.25 \pm 0.08$	$0.39 \pm 0.04$	pl	1.3 – 3.1	$-1.4 \pm 0.3$	–	$0.39^{+0.04}_{-0.04}$	$0.4^{+0.06}_{-0.1}$
J1646–6831	$8 \pm 2$	–	$0.7 \pm 0.4$	pl	0.4 – 3.4	$-1.9 \pm 0.4$	–	–	–
J1648–4611	$< 0.07$	$0.61 \pm 0.03$	$0.46 \pm 0.03$	–	1.4 – 3.1	–	–	$0.23^{+0.03}_{-0.04}$	$0.14^{+0.03}_{-0.05}$
J1649–4349	–	–	$< 0.07$	–	1.4 – 1.4	–	–	–	–
J1649–4653	$< 0.1$	$0.37 \pm 0.02$	$0.13 \pm 0.01$	pl	1.3 – 3.1	$-1.2 \pm 0.3$	–	$0.21^{+0.06}_{-0.03}$	$0.19^{+0.1}_{-0.08}$
J1650–4502	$< 2.0$	$0.61 \pm 0.04$	$0.27 \pm 0.03$	–	1.4 – 3.1	–	–	$0.29^{+0.02}_{-0.06}$	$0.3^{+0.1}_{-0.2}$
J1650–4921	$< 0.3$	$0.29 \pm 0.02$	$0.31 \pm 0.03$	pl	1.4 – 3.4	$0.1 \pm 0.2$	–	$0.25^{+0.06}_{-0.04}$	$0.22^{+0.05}_{-0.1}$
J1651–4246	$80 \pm 8$	–	$2.8 \pm 0.3$	low turn-over	0.08 – 3.5	–	–	–	–
J1651–5222	$11 \pm 3$	–	$1.7 \pm 0.4$	pl	0.4 – 3.5	$-1.4 \pm 0.2$	–	–	–
J1651–5255	$9 \pm 2$	–	$0.7 \pm 0.2$	broken pl	0.4 – 3.4	–	–	–	–
J1653–3838	$2.6 \pm 0.5$	–	$0.9 \pm 0.2$	pl	0.6 – 3.5	$-0.7 \pm 0.2$	–	–	–
J1653–4249	$0.28 \pm 0.06$	–	$2.0 \pm 1.0$	pl	0.7 – 3.4	$1.0 \pm 0.6$	–	–	–
J1654–4140	$< 5.0$	–	$0.1 \pm 0.02$	–	1.4 – 3.1	–	–	–	–

Table 1 – *continued*

PSRJ	$S_{728}$ (mJy)	$S_{1382}$ (mJy)	$S_{3100}$ (mJy)	Class	$\Delta\nu$ (GHz)	$\alpha$	$m_{\text{r}, 728}$	$m_{\text{r}, 1382}$	$m_{\text{r}, 3100}$
J1658–4958	$3.7 \pm 0.8$	–	$0.23 \pm 0.06$	lps	0.7 – 3.3	–	–	–	–
J1700–3312	$3.9 \pm 0.9$	–	$0.31 \pm 0.08$	pl	0.4 – 3.1	$-1.8 \pm 0.3$	–	–	–
J1701–3726	$14 \pm 2$	–	$0.9 \pm 0.2$	pl	0.6 – 3.4	$-2.0 \pm 0.2$	–	–	–
J1701–4533	$5.2 \pm 0.7$	–	$0.6 \pm 0.1$	pl	0.6 – 3.3	$-1.4 \pm 0.2$	–	–	–
J1702–4128	$< 1.0$	$1.17 \pm 0.07$	$0.94 \pm 0.06$	pl	1.4 – 6.5	$-0.2 \pm 0.2$	–	$0.27^{+0.04}_{-0.02}$	$0.14^{+0.03}_{-0.04}$
J1702–4306	–	$0.46 \pm 0.04$	–	–	1.3 – 1.4	–	–	–	–
J1702–4310	–	$0.92 \pm 0.06$	$0.42 \pm 0.07$	pl	1.3 – 3.3	$-1.1 \pm 0.3$	–	$0.13^{+0.04}_{-0.03}$	–
J1703–3241	$30 \pm 8$	–	$1.9 \pm 0.6$	lps	0.4 – 3.5	–	–	–	–
J1703–4851	$5.0 \pm 1.0$	–	$< 0.09$	pl	0.4 – 1.4	$-2.3 \pm 0.5$	–	–	–
J1704–6016	$< 0.1$	–	–	–	0.4 – 0.6	–	–	–	–
J1705–3423	$15 \pm 4$	–	$1.6 \pm 0.4$	pl	0.4 – 3.4	$-1.6 \pm 0.2$	–	–	–
J1705–3950	–	$1.6 \pm 0.1$	$1.1 \pm 0.2$	lps	0.6 – 3.4	–	–	$0.11^{+0.1}_{-0.04}$	–
J1705–4108	–	–	$1.0 \pm 0.1$	pl	1.4 – 3.4	$-0.4 \pm 0.5$	–	–	–
J1707–4053	$22 \pm 4$	–	$1.5 \pm 0.3$	hard cut-off	0.2 – 6.5	–	–	–	–
J1707–4729	$< 2.0$	–	$0.8 \pm 0.2$	pl	1.3 – 3.4	$-1.4 \pm 0.3$	–	–	–
J1708–3426	$9 \pm 2$	–	$0.24 \pm 0.06$	pl	0.4 – 3.1	$-2.6 \pm 0.3$	–	–	–
J1709–4429	–	$12.1 \pm 0.7$	$5.0 \pm 1.0$	pl	0.4 – 8.4	$-0.8 \pm 0.2$	–	$0.11^{+0.04}_{-0.05}$	–
J1711–5350	$4.0 \pm 1.0$	–	$0.19 \pm 0.06$	pl	0.4 – 3.1	$-2.0 \pm 0.5$	–	–	–
J1715–3903	–	$0.66 \pm 0.05$	$0.33 \pm 0.04$	–	1.4 – 3.1	–	–	$0.2^{+0.05}_{-0.07}$	–
J1715–4034	$6.0 \pm 1.0$	–	$0.26 \pm 0.06$	pl	0.7 – 3.1	$-2.2 \pm 0.2$	–	–	–
J1717–3425	$19 \pm 2$	–	$0.6 \pm 0.09$	pl	0.6 – 3.4	$-2.4 \pm 0.1$	–	–	–
J1717–4054	$20 \pm 3$	$< 0.06$	$1.0 \pm 0.2$	pl	0.4 – 3.4	$-1.4 \pm 0.5$	–	–	–
J1718–3825	–	$1.7 \pm 0.1$	$1.1 \pm 0.2$	pl	1.3 – 3.5	$-0.5 \pm 0.2$	–	$0.15^{+0.02}_{-0.08}$	–
J1719–4006	$3.6 \pm 0.6$	–	$0.41 \pm 0.07$	pl	0.6 – 3.4	$-1.5 \pm 0.2$	–	–	–
J1720–1633	$5 \pm 2$	–	$< 0.1$	pl	0.4 – 4.9	$-2.1 \pm 0.4$	–	–	–
J1721–3532	–	$16.8 \pm 0.9$	$8.0 \pm 0.7$	pl	1.3 – 17.0	$-0.8 \pm 0.1$	–	$0.06^{+0.02}_{-0.02}$	–
J1722–3207	$17 \pm 4$	–	$1.1 \pm 0.3$	pl	0.08 – 3.4	$-2.01 \pm 0.06$	–	–	–
J1722–3712	–	$3.8 \pm 0.3$	$0.6 \pm 0.2$	pl	0.4 – 3.5	$-2.2 \pm 0.2$	–	$0.23^{+0.04}_{-0.08}$	–
J1723–3659	–	$2.1 \pm 0.1$	$0.71 \pm 0.09$	lps	0.3 – 3.4	–	–	$0.16^{+0.09}_{-0.04}$	–
J1726–3530	–	$0.39 \pm 0.03$	$0.18 \pm 0.06$	–	1.4 – 3.1	–	–	$0.14^{+0.09}_{-0.07}$	–
J1727–2739	$7 \pm 2$	–	$0.7 \pm 0.2$	lps	0.7 – 3.1	–	–	–	–
J1730–2304	$6 \pm 3$	$3.0 \pm 1.0$	$0.1 \pm 0.1$	pl	0.1 – 3.1	$-1.6 \pm 0.2$	–	–	–
J1730–3350	–	$4.3 \pm 0.2$	$0.9 \pm 0.1$	pl	1.3 – 8.4	$-1.8 \pm 0.1$	–	$0.06^{+0.02}_{-0.03}$	–
J1731–4744	–	$27 \pm 3$	$7 \pm 2$	lps	0.08 – 3.5	–	–	$0.36^{+0.07}_{-0.1}$	–
J1733–3322	$< 0.2$	–	$0.35 \pm 0.06$	pl	1.3 – 3.1	$-1.8 \pm 0.4$	–	–	–
J1733–3716	–	$3.6 \pm 0.2$	$2.1 \pm 0.3$	pl	0.6 – 3.5	$-0.6 \pm 0.2$	–	$0.13^{+0.04}_{-0.08}$	–
J1734–3333	–	$0.49 \pm 0.06$	$0.37 \pm 0.08$	pl	1.4 – 3.5	$-0.5 \pm 0.4$	–	$0.45^{+0.5}_{-0.06}$	–
J1735–3258	–	$0.35 \pm 0.06$	$0.39 \pm 0.05$	pl	1.4 – 3.4	$-0.1 \pm 0.4$	–	$0.4^{+0.2}_{-0.2}$	–
J1737–3137	–	$0.88 \pm 0.06$	$0.2 \pm 0.02$	pl	1.3 – 3.1	$-2.0 \pm 0.3$	–	$0.23^{+0.04}_{-0.06}$	–
J1737–3555	$2.5 \pm 0.8$	–	$0.28 \pm 0.09$	pl	0.6 – 3.1	$-1.2 \pm 0.4$	–	–	–
J1738–2955	–	$0.24 \pm 0.02$	$0.04 \pm 0.01$	–	1.4 – 3.1	–	–	$0.25^{+0.05}_{-0.1}$	–
J1738–3211	$5 \pm 2$	–	$0.8 \pm 0.4$	pl	0.6 – 3.5	$-0.9 \pm 0.2$	–	–	–
J1739–2903	–	$4.5 \pm 0.3$	$1.4 \pm 0.3$	pl	0.6 – 3.4	$-1.3 \pm 0.3$	–	$0.11^{+0.04}_{-0.04}$	–
J1739–3023	–	$1.01 \pm 0.07$	$0.16 \pm 0.03$	pl	0.6 – 3.1	$-1.5 \pm 0.2$	–	$0.18^{+0.1}_{-0.02}$	–
J1740–3015	$18 \pm 2$	$8.9 \pm 0.5$	$3.4 \pm 0.2$	pl	0.6 – 17.0	$-1.11 \pm 0.06$	$0.22^{+0.07}_{-0.1}$	$0.19^{+0.02}_{-0.02}$	$0.14^{+0.04}_{-0.05}$
J1741–2733	$6 \pm 2$	–	$< 0.2$	pl	0.7 – 1.5	$-2.2 \pm 0.4$	–	–	–
J1741–3016	–	–	$0.29 \pm 0.05$	pl	1.3 – 3.1	$-2.4 \pm 0.4$	–	–	–
J1741–3927	$19 \pm 3$	–	$2.0 \pm 0.4$	pl	0.4 – 3.5	$-1.6 \pm 0.1$	–	–	–
J1743–3150	$9 \pm 2$	–	$0.31 \pm 0.08$	broken pl	0.3 – 3.1	–	–	–	–
J1744–1134	$12 \pm 9$	$13 \pm 8$	$0.3 \pm 0.3$	pl	0.1 – 5.0	$-1.7 \pm 0.1$	–	–	–
J1744–3130	$1.8 \pm 0.4$	–	$0.35 \pm 0.08$	pl	0.6 – 3.3	$-1.1 \pm 0.3$	–	–	–
J1745–3040	–	$21.0 \pm 1.0$	$4.2 \pm 0.7$	lps	0.4 – 4.9	–	–	$0.19^{+0.03}_{-0.09}$	–
J1748–1300	$11 \pm 2$	–	$0.3 \pm 0.2$	pl	0.1 – 3.3	$-1.8 \pm 0.2$	–	–	–
J1749–3002	$11 \pm 2$	–	$1.0 \pm 0.2$	pl	0.6 – 3.4	$-1.6 \pm 0.2$	–	–	–
J1751–3323	$1.5 \pm 0.2$	–	$0.9 \pm 0.1$	broken pl	0.6 – 3.4	–	–	–	–
J1751–4657	$30 \pm 10$	–	$0.4 \pm 0.2$	hard cut-off	0.4 – 3.4	–	–	–	–
J1752–2806	$350 \pm 50$	–	$5 \pm 2$	lps	0.06 – 10.7	–	–	–	–
J1755–2521	$< 1.0$	–	–	–	1.4 – 1.4	–	–	–	–
J1756–2435	$6.0 \pm 1.0$	–	$0.4 \pm 0.07$	pl	0.6 – 3.3	$-1.5 \pm 0.3$	–	–	–
J1757–2223	–	–	$0.34 \pm 0.08$	pl	1.3 – 3.3	$-1.5 \pm 0.4$	–	–	–
J1757–2421	–	$7.2 \pm 0.4$	$2.2 \pm 0.3$	pl	0.4 – 6.5	$-1.27 \pm 0.08$	–	$0.1^{+0.03}_{-0.03}$	–
J1758–2630	–	–	$< 0.03$	–	1.3 – 1.5	–	–	–	–
J1759–1956	$1.7 \pm 0.3$	–	$0.1 \pm 0.02$	pl	0.7 – 3.1	$-2.0 \pm 0.4$	–	–	–

Table 1 – *continued*

PSRJ	$S_{728}$ (mJy)	$S_{1382}$ (mJy)	$S_{3100}$ (mJy)	Class	$\Delta\nu$ (GHz)	$\alpha$	$m_{\text{r}, 728}$	$m_{\text{r}, 1382}$	$m_{\text{r}, 3100}$
J1759–2205	–	–	$0.5 \pm 0.1$	pl	$0.4 - 4.9$	$-1.8 \pm 0.2$	–	–	–
J1759–3107	$4.0 \pm 0.7$	–	$0.38 \pm 0.09$	pl	$0.7 - 3.3$	$-1.6 \pm 0.2$	–	–	–
J1801–2154	–	$0.21 \pm 0.02$	$0.069 \pm 0.009$	–	$1.4 - 3.1$	–	–	–	–
J1801–2304	–	$7.0 \pm 0.5$	$1.6 \pm 0.1$	pl	$1.3 - 6.5$	$-1.7 \pm 0.1$	–	$0.19^{+0.05}_{-0.03}$	–
J1801–2451	–	$1.46 \pm 0.09$	$0.22 \pm 0.03$	pl	$0.6 - 3.1$	$-0.8 \pm 0.2$	–	$0.14^{+0.05}_{-0.05}$	–
J1801–2920	$7.0 \pm 1.0$	–	$0.42 \pm 0.08$	pl	$0.6 - 3.3$	$-2.0 \pm 0.2$	–	–	–
J1803–1857	$< 5.0$	–	$< 0.3$	–	$1.3 - 1.5$	–	–	–	–
J1803–2137	–	$15.0 \pm 1.0$	$8.0 \pm 1.0$	low turn-over	$0.3 - 6.5$	–	–	$0.17^{+0.03}_{-0.04}$	–
J1805–1504	$14 \pm 3$	–	–	pl	$0.7 - 1.5$	$-1.8 \pm 0.2$	–	–	–
J1806–1154	$8 \pm 2$	–	$0.4 \pm 0.1$	broken pl	$0.4 - 3.3$	–	–	–	–
J1806–2125	–	$0.8 \pm 0.04$	$0.16 \pm 0.02$	pl	$1.2 - 3.3$	$-2.1 \pm 0.3$	–	$0.11^{+0.07}_{-0.05}$	–
J1807–0847	$34 \pm 6$	–	$4.0 \pm 1.0$	pl	$0.1 - 4.9$	$-1.4 \pm 0.1$	–	–	–
J1807–2459A	$< 0.2$	–	$0.3 \pm 0.1$	–	$1.4 - 3.1$	–	–	–	–
J1808–0813	$7.0 \pm 1.0$	–	$0.23 \pm 0.04$	pl	$0.1 - 3.1$	$-2.1 \pm 0.2$	–	–	–
J1808–2057	$16 \pm 2$	–	$1.0 \pm 0.1$	pl	$0.6 - 4.9$	$-2.0 \pm 0.2$	–	–	–
J1809–1429	$3.5 \pm 0.5$	–	$0.24 \pm 0.04$	pl	$0.7 - 3.1$	$-2.1 \pm 0.2$	–	–	–
J1809–1917	–	$2.8 \pm 0.2$	$2.1 \pm 0.3$	pl	$1.2 - 6.5$	$-0.4 \pm 0.2$	–	$0.26^{+0.02}_{-0.07}$	–
J1809–2109	–	–	$0.28 \pm 0.05$	pl	$0.6 - 3.3$	$-1.8 \pm 0.3$	–	–	–
J1809–3547	$20 \pm 10$	–	–	–	$0.4 - 0.8$	–	–	–	–
J1810–5338	$12 \pm 3$	–	$0.5 \pm 0.2$	pl	$0.4 - 3.3$	$-2.1 \pm 0.4$	–	–	–
J1812–1718	–	–	$0.2 \pm 0.04$	pl	$1.3 - 3.1$	$-2.2 \pm 0.4$	–	–	–
J1812–1733	$11 \pm 2$	–	$1.0 \pm 0.1$	lps	$0.7 - 3.5$	–	–	–	–
J1812–1910	–	$0.28 \pm 0.02$	$0.076 \pm 0.009$	–	$1.4 - 3.1$	–	–	$0.21^{+0.1}_{-0.08}$	–
J1812–2102	–	–	$0.51 \pm 0.08$	pl	$1.3 - 4.9$	$-1.8 \pm 0.2$	–	–	–
J1815–1738	–	$0.4 \pm 0.03$	$0.14 \pm 0.02$	pl	$1.4 - 3.3$	$-1.2 \pm 0.4$	–	$0.18^{+0.1}_{-0.07}$	–
J1817–3618	$7 \pm 4$	–	$0.4 \pm 0.2$	pl	$0.4 - 3.4$	$-2.0 \pm 0.4$	–	–	–
J1817–3837	$9 \pm 4$	–	$0.6 \pm 0.1$	pl	$0.4 - 3.4$	$-1.7 \pm 0.4$	–	–	–
J1818–1519	$< 0.2$	–	$< 0.02$	–	$1.4 - 1.4$	–	–	–	–
J1820–1529	–	$0.83 \pm 0.08$	$0.23 \pm 0.02$	pl	$1.3 - 3.4$	$-1.7 \pm 0.2$	–	$0.3^{+0.1}_{-0.1}$	–
J1822–2256	$16 \pm 4$	–	$1.0 \pm 0.3$	pl	$0.4 - 3.4$	$-1.8 \pm 0.1$	–	–	–
J1822–4209	$2.3 \pm 0.8$	–	$0.3 \pm 0.1$	pl	$0.4 - 3.1$	$-1.4 \pm 0.6$	–	–	–
J1823–1115	$11.0 \pm 1.0$	–	$1.0 \pm 0.1$	pl	$0.4 - 4.9$	$-1.52 \pm 0.09$	–	–	–
J1823–3106	$11 \pm 3$	–	$1.2 \pm 0.4$	pl	$0.4 - 3.3$	$-1.8 \pm 0.2$	–	–	–
J1824–1118	$6.2 \pm 0.8$	–	$0.44 \pm 0.07$	pl	$0.6 - 4.9$	$-2.1 \pm 0.2$	–	–	–
J1824–1945	–	$7.8 \pm 0.4$	$1.3 \pm 0.2$	lps	$0.08 - 4.9$	–	–	$0.12^{+0.02}_{-0.04}$	–
J1825–1446	–	$2.9 \pm 0.2$	$1.9 \pm 0.3$	lps	$0.3 - 4.9$	–	–	$0.22^{+0.06}_{-0.07}$	–
J1826–1334	–	$4.7 \pm 0.2$	$3.0 \pm 0.4$	lps	$0.3 - 3.5$	–	–	$0.05^{+0.04}_{-0.02}$	–
J1827–0750	$7.0 \pm 1.0$	–	$0.7 \pm 0.1$	pl	$0.7 - 3.4$	$-1.6 \pm 0.2$	–	–	–
J1828–0611	$3.6 \pm 0.6$	–	$0.43 \pm 0.08$	pl	$0.7 - 3.4$	$-1.5 \pm 0.2$	–	–	–
J1828–1057	–	$0.33 \pm 0.04$	$0.17 \pm 0.03$	–	$1.4 - 3.1$	–	–	$0.27^{+0.05}_{-0.1}$	–
J1828–1101	–	$2.3 \pm 0.2$	$1.4 \pm 0.2$	pl	$1.3 - 4.9$	$-0.6 \pm 0.3$	–	$0.22^{+0.05}_{-0.1}$	–
J1829–1751	$28 \pm 6$	–	$3.0 \pm 0.7$	pl	$0.4 - 4.9$	$-1.7 \pm 0.1$	–	–	–
J1830–1059	–	$1.5 \pm 0.1$	$0.6 \pm 0.1$	lps	$0.6 - 4.9$	–	–	$0.32^{+0.09}_{-0.1}$	–
J1831–0823	$3.4 \pm 0.7$	–	$0.21 \pm 0.05$	pl	$0.7 - 3.1$	$-1.9 \pm 0.3$	–	–	–
J1831–0952	–	$0.35 \pm 0.04$	–	–	$1.4 - 1.4$	–	–	–	–
J1831–1223	$3.7 \pm 0.6$	–	$0.24 \pm 0.05$	pl	$0.7 - 3.1$	$-1.9 \pm 0.3$	–	–	–
J1832–0644	$< 0.1$	–	$1.5 \pm 0.2$	pl	$1.4 - 3.4$	$1.0 \pm 0.5$	–	–	–
J1832–0827	–	$4.0 \pm 0.3$	$1.5 \pm 0.2$	lps	$0.4 - 6.5$	–	–	$0.17^{+0.1}_{-0.05}$	–
J1833–0338	$14 \pm 3$	–	$0.35 \pm 0.05$	pl	$0.1 - 3.3$	$-2.8 \pm 0.1$	–	–	–
J1833–0827	–	$6.9 \pm 0.4$	$1.9 \pm 0.2$	pl	$0.6 - 4.9$	$-1.5 \pm 0.1$	–	$0.15^{+0.02}_{-0.04}$	–
J1834–0731	–	$1.3 \pm 0.1$	$0.37 \pm 0.05$	pl	$0.6 - 4.9$	$-1.6 \pm 0.1$	–	$0.22^{+0.06}_{-0.08}$	–
J1834–1710	$4.0 \pm 1.0$	–	$0.17 \pm 0.05$	pl	$0.7 - 3.1$	$-2.2 \pm 0.4$	–	–	–
J1835–0643	–	$2.3 \pm 0.2$	$0.6 \pm 0.2$	lps	$0.3 - 4.9$	–	–	$0.26^{+0.01}_{-0.1}$	–
J1835–1020	–	–	$0.9 \pm 0.3$	lps	$0.3 - 4.9$	–	–	–	–
J1835–1106	–	$2.5 \pm 0.2$	$0.5 \pm 0.1$	pl	$0.4 - 3.3$	$-2.1 \pm 0.2$	–	$0.18^{+0.06}_{-0.06}$	–
J1836–0436	$3.3 \pm 0.7$	–	$0.7 \pm 0.2$	pl	$0.6 - 3.4$	$-1.4 \pm 0.2$	–	–	–
J1836–1008	–	–	$0.5 \pm 0.1$	lps	$0.4 - 3.4$	–	–	–	–
J1837–0559	–	$0.58 \pm 0.04$	$0.13 \pm 0.02$	pl	$1.3 - 3.1$	$-1.9 \pm 0.4$	–	$0.2^{+0.1}_{-0.05}$	–
J1837–0604	–	$0.75 \pm 0.06$	$0.38 \pm 0.04$	pl	$1.4 - 3.3$	$-0.8 \pm 0.4$	–	$0.17^{+0.2}_{-0.06}$	–
J1837–0653	$13 \pm 2$	–	$0.8 \pm 0.2$	pl	$0.1 - 3.4$	$-1.7 \pm 0.2$	–	–	–
J1838–0453	–	$0.4 \pm 0.05$	$0.09 \pm 0.01$	–	$1.4 - 3.1$	–	–	$0.3^{+0.1}_{-0.1}$	–
J1838–0549	–	$0.42 \pm 0.04$	$0.14 \pm 0.02$	–	$1.4 - 3.1$	–	–	$0.19^{+0.05}_{-0.1}$	–
J1839–0321	–	$0.27 \pm 0.03$	$0.066 \pm 0.009$	–	$1.4 - 3.1$	–	–	–	–

Table 1 – *continued*

PSRJ	$S_{728}$ (mJy)	$S_{1382}$ (mJy)	$S_{3100}$ (mJy)	Class	$\Delta\nu$ (GHz)	$\alpha$	$m_r, 728$	$m_r, 1382$	$m_r, 3100$
J1839–0643	< 2.0	–	$0.56 \pm 0.09$	pl	1.3 – 3.3	$-1.5 \pm 0.3$	–	–	–
J1839–0905	–	$0.22 \pm 0.02$	$0.11 \pm 0.02$	–	1.4 – 3.1	–	–	$0.15^{+0.08}_{-0.07}$	–
J1840–0809	$5.0 \pm 0.8$	–	$0.8 \pm 0.1$	pl	0.7 – 3.5	$-1.5 \pm 0.1$	–	–	–
J1840–0815	$9 \pm 2$	–	$0.5 \pm 0.1$	pl	0.7 – 3.3	$-2.3 \pm 0.2$	–	–	–
J1841–0425	–	$3.3 \pm 0.2$	$0.72 \pm 0.09$	pl	0.6 – 3.4	$-1.7 \pm 0.1$	–	$0.04^{+0.01}_{-0.01}$	–
J1841–0524	–	$0.2 \pm 0.04$	$0.048 \pm 0.007$	–	1.4 – 3.1	–	–	$0.43^{+0.04}_{-0.3}$	–
J1842–0153	$1.4 \pm 0.2$	–	$0.15 \pm 0.03$	pl	0.7 – 3.1	$-1.7 \pm 0.4$	–	–	–
J1842–0359	$36 \pm 8$	–	$3.4 \pm 0.8$	pl	0.1 – 3.5	$-1.5 \pm 0.1$	–	–	–
J1842–0905	–	$1.04 \pm 0.07$	$0.32 \pm 0.05$	pl	0.6 – 3.3	$-1.4 \pm 0.2$	–	$0.18^{+0.04}_{-0.07}$	–
J1843–0000	$10 \pm 3$	–	$1.2 \pm 0.4$	pl	0.7 – 3.3	$-1.5 \pm 0.2$	–	–	–
J1843–0211	$2.0 \pm 0.3$	–	$0.31 \pm 0.05$	lps	0.7 – 3.4	–	–	–	–
J1843–0355	–	$0.89 \pm 0.07$	$0.54 \pm 0.05$	pl	1.4 – 3.4	$-0.3 \pm 0.3$	–	$0.16^{+0.1}_{-0.07}$	–
J1843–0459	$4.1 \pm 0.6$	–	$0.21 \pm 0.04$	pl	0.7 – 3.1	$-2.4 \pm 0.4$	–	–	–
J1843–0702	–	$0.27 \pm 0.04$	< 0.06	–	1.4 – 1.4	–	–	$0.3^{+0.2}_{-0.1}$	–
J1844–0256	–	$0.59 \pm 0.06$	$0.35 \pm 0.03$	–	1.4 – 3.3	–	–	$0.3^{+0.2}_{-0.1}$	–
J1844–0433	$16 \pm 4$	–	$0.24 \pm 0.07$	pl	0.4 – 3.4	$-1.8 \pm 0.1$	–	–	–
J1844–0538	–	$3.2 \pm 0.2$	$0.55 \pm 0.07$	pl	0.6 – 4.9	$-1.9 \pm 0.1$	–	$0.1^{+0.01}_{-0.04}$	–
J1845–0743	–	$3.7 \pm 0.2$	$0.9 \pm 0.1$	pl	1.3 – 3.4	$-1.7 \pm 0.2$	–	$0.12^{+0.02}_{-0.04}$	–
J1845–1114	$0.8 \pm 0.2$	–	$0.3 \pm 0.07$	–	0.7 – 3.1	–	–	–	–
J1847–0402	–	$4.9 \pm 0.3$	$1.4 \pm 0.2$	lps	0.1 – 4.9	–	–	$0.13^{+0.03}_{-0.05}$	–
J1847–0438	< 0.2	–	$0.15 \pm 0.03$	pl	1.3 – 3.1	$-1.7 \pm 0.5$	–	–	–
J1847–0605	< 3.0	–	< 0.2	–	1.3 – 1.5	–	–	–	–
J1848–0123	$40 \pm 10$	–	$3.1 \pm 0.8$	pl	0.1 – 10.6	$-1.64 \pm 0.09$	–	–	–
J1848–1414	$1.7 \pm 0.4$	–	$0.07 \pm 0.02$	pl	0.4 – 3.1	$-2.2 \pm 0.4$	–	–	–
J1849–0636	$7 \pm 2$	–	$0.23 \pm 0.06$	pl	0.1 – 3.3	$-2.3 \pm 0.1$	–	–	–
J1850–0026	< 0.1	–	$0.6 \pm 0.08$	–	1.4 – 3.3	–	–	–	–
J1852–0635	$11 \pm 2$	–	$10 \pm 2$	broken pl	0.3 – 8.3	–	–	–	–
J1852–2610	$1.9 \pm 0.7$	–	–	–	0.4 – 1.4	–	–	–	–
J1853+0545	< 0.3	–	$1.1 \pm 0.3$	pl	1.3 – 3.5	$-1.2 \pm 0.2$	–	–	–
J1853–0004	–	$0.7 \pm 0.1$	$0.17 \pm 0.02$	pl	1.3 – 3.1	$-2.3 \pm 0.3$	–	$0.58^{+0.04}_{-0.3}$	–
J1854–1421	$9 \pm 2$	–	$0.5 \pm 0.1$	pl	0.4 – 3.3	$-1.4 \pm 0.3$	–	–	–
J1855+0307	$1.9 \pm 0.2$	–	$0.23 \pm 0.05$	pl	0.7 – 3.1	$-1.6 \pm 0.3$	–	–	–
J1856+0404	–	–	< 1.0	–	1.3 – 1.5	–	–	–	–
J1857+0212	$5.6 \pm 0.8$	–	$0.8 \pm 0.1$	lps	0.1 – 4.9	–	–	–	–
J1900–2600	$50 \pm 20$	–	$2.1 \pm 0.7$	broken pl	0.08 – 10.7	–	–	–	–
J1900–7951	$4 \pm 2$	–	< 0.1	–	0.4 – 0.8	–	–	–	–
J1901+0331	$39 \pm 6$	–	$0.9 \pm 0.2$	pl	0.1 – 4.9	$-2.7 \pm 0.1$	–	–	–
J1901–0906	$6.0 \pm 1.0$	–	$0.19 \pm 0.07$	pl	0.4 – 3.4	$-2.4 \pm 0.3$	–	–	–
J1902+0556	–	–	$0.5 \pm 0.1$	pl	0.1 – 4.9	$-1.8 \pm 0.1$	–	–	–
J1903+0135	$29 \pm 4$	–	$1.3 \pm 0.2$	pl	0.4 – 4.9	$-2.0 \pm 0.1$	–	–	–
J1903–0632	$7 \pm 2$	–	$0.13 \pm 0.03$	hard cut-off	0.1 – 3.1	–	–	–	–
J1903–0848	$0.7 \pm 0.2$	–	< 0.02	–	0.7 – 0.8	–	–	–	–
J1904+0004	$8 \pm 2$	–	$0.6 \pm 0.1$	pl	0.4 – 3.5	$-1.8 \pm 0.2$	–	–	–
J1905–0056	$1.7 \pm 0.3$	–	$0.12 \pm 0.03$	pl	0.1 – 3.1	$-2.19 \pm 0.08$	–	–	–
J1907+0534	$0.9 \pm 0.1$	–	–	–	0.7 – 1.4	–	–	–	–
J1908+0500	$3.4 \pm 0.7$	–	$0.4 \pm 0.1$	pl	0.4 – 3.4	$-1.6 \pm 0.2$	–	–	–
J1909+1102	$12 \pm 3$	–	$0.34 \pm 0.09$	pl	0.1 – 3.4	$-2.5 \pm 0.1$	–	–	–
J1909–3744	$1.5 \pm 0.8$	$1.0 \pm 1.0$	$0.5 \pm 0.4$	pl	0.7 – 3.1	$-1.2 \pm 0.1$	–	–	–
J1913–0440	$28 \pm 5$	–	$1.8 \pm 0.5$	low turn-over	0.1 – 3.5	–	–	–	–
J1915+1009	–	–	$0.39 \pm 0.09$	pl	0.1 – 3.3	$-2.0 \pm 0.1$	–	–	–
J1916+1312	–	–	$0.5 \pm 0.1$	pl	0.1 – 4.9	$-1.8 \pm 0.2$	–	–	–
J1920+1040	–	–	< 0.01	–	1.3 – 1.5	–	–	–	–
J1932–3655	$2.3 \pm 0.8$	–	$0.09 \pm 0.04$	–	0.4 – 3.1	–	–	–	–
J1933–6211	$2 \pm 2$	–	$0.2 \pm 0.2$	–	0.7 – 3.1	–	–	–	–
J1941–2602	$4 \pm 2$	–	$0.5 \pm 0.2$	pl	0.4 – 3.3	$-1.6 \pm 0.3$	–	–	–
J1946–2913	$3.0 \pm 1.0$	–	< 0.1	pl	0.4 – 1.4	$-2.0 \pm 0.5$	–	–	–
J1947–4215	< 0.07	–	–	–	0.4 – 0.4	–	–	–	–
J2006–0807	$11 \pm 5$	–	< 0.02	pl	0.1 – 1.4	$-1.5 \pm 0.3$	–	–	–
J2010–1323	$1.1 \pm 0.7$	–	–	–	0.7 – 1.4	–	–	–	–
J2038–3816	$1.4 \pm 0.7$	–	< 0.2	–	0.4 – 0.7	–	–	–	–
J2046–0421	–	–	$0.2 \pm 0.1$	pl	0.1 – 3.1	$-1.7 \pm 0.2$	–	–	–
J2048–1616	$40 \pm 30$	–	$4 \pm 4$	broken pl	0.08 – 8.5	–	–	–	–
J2051–0827	$3 \pm 2$	–	–	pl	0.1 – 3.0	$-1.5 \pm 0.2$	–	–	–

**Table 1** – *continued*

PSRJ	$S_{728}$ (mJy)	$S_{1382}$ (mJy)	$S_{3100}$ (mJy)	Class	$\Delta\nu$ (GHz)	$\alpha$	$m_{\mathrm{r}, 728}$	$m_{\mathrm{r}, 1382}$	$m_{\mathrm{r}, 3100}$
J2053–7200	$11 \pm 7$	–	$0.3 \pm 0.2$	broken pl	0.1 – 3.3	–	–	–	–
J2108–3429	$2.0 \pm 1.0$	–	–	–	0.4 – 0.7	–	–	–	–
J2145–0750	$10 \pm 10$	$0.8 \pm 0.4$	$2 \pm 2$	pl	0.1 – 5.0	$-1.8 \pm 0.1$	–	–	–
J2222–0137	$1.0 \pm 1.0$	–	$0.5 \pm 0.7$	–	0.7 – 3.1	–	–	–	–
J2317+1439	–	–	$< 0.02$	pl	0.1 – 1.4	$-1.3 \pm 0.4$	–	–	–