



Aalto University

Linearisation of nonlinear models: Example

CHEM-E7190 (was E7140), 2021

Francesco Corona

Chemical and Metallurgical Engineering
School of Chemical Engineering

Example I

Linearisation of nonlinear models

Example I

Consider two chemical species A and B in a solvent feed entering a chemical reactor

- The two species react to form a third one, the product component P
- $A + 2B \longrightarrow P$

Liquid-phase chemical reactor

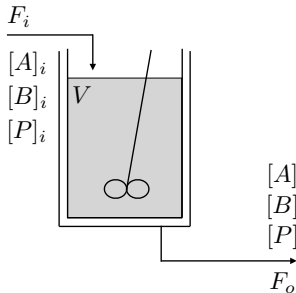
↪ Volume $V(t)$

Temperature is constant

↪ $T(t) = \text{constant}$

Volumetric flow-rates

↪ $F_i(t)$ and $F_o(t)$



Assuming perfect mixing, our main interest is in the concentrations inside the reactor

- ↪ The concentration of species as a function of time $[A](t)$, $[B](t)$, and $[P](t)$
- (Interest also in $V(t)$, because we do not want to flood/dry the tank)

Example I (cont.)

Total mass balance

$$\begin{aligned}
 \underbrace{\frac{dM(t)}{dt}}_{(\text{mass}/\text{time})} &= \underbrace{\frac{dV(t)\rho_o(t)}{dt}}_{(\text{volume} \times (\text{mass} / \text{volume}) / \text{time})} \\
 &= \underbrace{\rho_i(t)}_{(\text{mass} / \text{volume})} \underbrace{F_i(t)}_{(\text{volume} / \text{time})} - \underbrace{\rho_o(t)}_{(\text{mass} / \text{volume})} \underbrace{F_o(t)}_{(\text{volume} / \text{time})}
 \end{aligned}$$

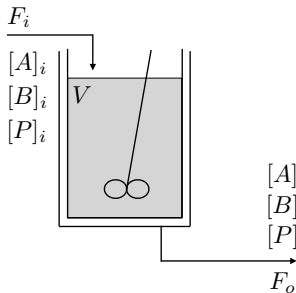
Assuming (!) that the density does not depend on the concentration of A , B and P , we get

$$\rho_o(t) = \rho_i(t) = \rho \quad \rightsquigarrow \quad \rho \neq \rho(t)$$

↗ Density does not depend on time

The resulting total mass balance,

$$\rightsquigarrow \frac{dV(t)}{dt} = F_i(t) - F_o(t)$$

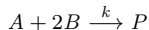


Example I (cont.)

Component mass balance

Let $[A]$, $[B]$ and $[P]$ be molar concentrations (moles/volume) of species A , B and P

- Based on some kinetic modelling, we are given the stoichiometric equation



Assuming that there is no product P in the feed ($[P]_i(t) = 0$ for all $t \geq t(0)$), we have

$$\frac{dV(t)[A](t)}{dt} = F_i(t)[A]_i(t) - F_o(t)[A]_o(t) + V(t)r_A(t)$$

$$\frac{dV(t)[B](t)}{dt} = F_i(t)[B]_i(t) - F_o(t)[B]_o(t) + V(t)r_B(t)$$

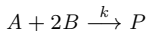
$$\frac{dV(t)[P](t)}{dt} = F_i(t)\cancel{[P]_i(t)} - F_o(t)[P]_o(t) + V(t)r_P(t)$$

$r_A(t)$, $r_B(t)$ and $r_P(t)$ denote generation/consumption rates of species A , B and P

- Given per unit volume, and assume we know the reaction rate constant k

$$\rightsquigarrow \left(\frac{\text{moles}}{\text{time}} \right) / \text{volume}$$

Example I (cont.)



We can assume that the reaction rate per unit volume for component A is second order

- We can also assume that it depends on the composition of both $A(t)$ and $B(t)$

$$r_A(t) = -k[A](t)[B](t), \quad (\text{rate of generation of } A, \text{ per unit volume})$$

The stoichiometric equation tells us that one mole of A reacts with two moles of B

- ... to produce one mole of P

We can also write the generation rates (per unit volume) for the remaining species

$$r_B(t) = -2k[A](t)[B](t)$$

$$r_P(t) = k[A](t)[B](t)$$

At this point, we need to substitute their expressions in the mass balances

Example I (cont.)

Consider the mass balance for component A and differentiate with respect to time

$$\begin{aligned}\frac{dV(t)[A](t)}{dt} &= V(t)\frac{d[A](t)}{dt} + [A](t)\frac{dV(t)}{dt} \\ &= F_i(t)[A]_i(t) - F_o(t)[A](t) - \underbrace{V(t)k[A](t)[B](t)}_{-r_A}\end{aligned}$$

Dividing by $V(t)$ and rearranging terms, we get

$$\frac{d[A](t)}{dt} = \frac{F_i(t)}{V(t)}[A]_i(t) - \frac{F_o(t)}{V(t)}[A](t) - \frac{V(t)}{V(t)}k[A](t)[B](t) - \frac{1}{V(t)}\frac{dV(t)}{dt}[A](t)$$

From the total mass balance, we know that $\frac{dV(t)}{dt} = F_i(t) - F_o(t)$

$$\begin{aligned}\frac{d[A](t)}{dt} &= \frac{F_i(t)}{V(t)}[A]_i(t) - \cancel{\frac{F_o(t)}{V(t)}[A](t)} - k[A](t)[B](t) - \frac{F_i(t)}{V(t)}[A](t) + \cancel{\frac{F_o(t)}{V(t)}[A](t)} \\ &= \frac{F_i(t)}{V(t)}([A]_i(t) - [A](t)) - k[A](t)[B](t)\end{aligned}$$

Example I (cont.)

We can proceed similarly for component B and component P to get their dynamics

$$\begin{aligned}\rightsquigarrow \quad \frac{d[B](t)}{dt} &= \frac{F_i(t)}{V(t)} \left([B]_i(t) - [B](t) \right) - 2k[A](t)[B](t) \\ \rightsquigarrow \quad \frac{d[P](t)}{dt} &= \frac{F_i(t)}{V(t)} \left(\underbrace{[P]_i(t)}_{=0} - [P](t) \right) + k[A](t)[B](t)\end{aligned}$$

Example I (cont.)

Altogether, we have model equations involving 4 state variables and 4 input variables

$$\begin{aligned}\frac{d[A](t)}{dt} &= \frac{F_i(t)}{V(t)}([A]_i(t) - [A](t)) - k[A](t)[B](t) \\ \frac{d[B](t)}{dt} &= \frac{F_i(t)}{V(t)}([B]_i(t) - [B](t)) - 2k[A](t)[B](t) \\ \frac{d[P](t)}{dt} &= -\frac{F_i(t)}{V(t)}[P](t) + k[A](t)[B](t) \\ \frac{dV(t)}{dt} &= F_i(t) - F_o(t)\end{aligned}$$

The state equations of the model consists of four first-order differential equations

- ~> Thus four state variables, they are associated with the derivatives
- ~> Variables $V(t)$, $[A](t)$, $[B](t)$ and $[P](t)$ have dynamics

As for the four (five) input variables, some are controls others are disturbances

- ~> $F_i(t)$, $F_o(t)$, $[A]_i(t)$, $[B]_i(t)$ (and $[P]_i(t)$)

Example I (cont.)

Four initial conditions (at $t = 0$) are needed for determining the temporal evolution

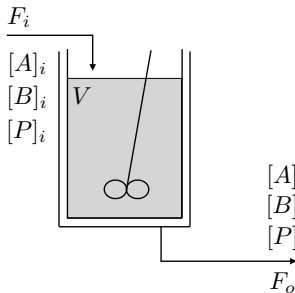
↪ $V(0)$, $[A](0)$, $[B](0)$ and $[P](0)$

To determine the temporal evolution, we also need to set the inputs to be applied

↪ $F_i(t)$, $F_o(t)$, $[A]_i(t)$, $[B]_i(t)$ (and $[P]_i(t)$)

- From the initial time $t = 0$ onwards

$$\begin{bmatrix} \dot{V} \\ \dot{[A]} \\ \dot{[B]} \\ \dot{[P]} \end{bmatrix} = \begin{bmatrix} F_i - F_o \\ \frac{F_i}{V} ([A]_i - [A]) - k[A][B] \\ \frac{F_i}{V} ([B]_i - [B]) - 2k[A][B] \\ -\frac{F_i}{V} [P] + k[A][B] \end{bmatrix}$$



Note how the state equations of the state-space model contains also a parameter, k

↪ We assumed it to be time-invariant (that is, $k \neq k(t)$)

Example I (cont.)

$$\begin{aligned}
 \begin{bmatrix} \dot{V} \\ \dot{[A]} \\ \dot{[B]} \\ \dot{[P]} \end{bmatrix} &= \begin{bmatrix} F_i - F_o \\ \frac{F_i}{V} ([A]_i - [A]) - k[A][B] \\ \frac{F_i}{V} ([B]_i - [B]) - 2k[A][B] \\ -\frac{F_i}{V} [P] + k[A][B] \end{bmatrix} \\
 &= \begin{bmatrix} f_1(V, [A], [B], [P], F_i, F_o, [A]_i, [B]_i, [P]_i | k, B) \\ f_2(V, [A], [B], [P], F_i, F_o, [A]_i, [B]_i, [P]_i | k, B) \\ f_3(V, [A], [B], [P], F_i, F_o, [A]_i, [B]_i, [P]_i | k, B) \\ f_4(V, [A], [B], [P], F_i, F_o, [A]_i, [B]_i, [P]_i | k, B) \end{bmatrix}
 \end{aligned}$$

↪ For the state variables, $x(t)$

$$x(t) = \begin{bmatrix} x_1(t) \\ x_2(t) \\ x_3(t) \\ x_4(t) \end{bmatrix} = \begin{bmatrix} V(t) \\ [A](t) \\ [B](t) \\ [P](t) \end{bmatrix}$$

Example I (cont.)

$$\begin{aligned}
 \begin{bmatrix} \dot{V} \\ \dot{[A]} \\ \dot{[B]} \\ \dot{[P]} \end{bmatrix} &= \begin{bmatrix} F_i - F_o \\ \frac{F_i}{V} ([A]_i - [A]) - k[A][B] \\ \frac{F_i}{V} ([B]_i - [B]) - 2k[A][B] \\ -\frac{F_i}{V} [P] + k[A][B] \end{bmatrix} \\
 &= \begin{bmatrix} f_1(V, [A], [B], [P], F_i, F_o, [A]_i, [B]_i, [P]_i | k, B) \\ f_2(V, [A], [B], [P], F_i, F_o, [A]_i, [B]_i, [P]_i | k, B) \\ f_3(V, [A], [B], [P], F_i, F_o, [A]_i, [B]_i, [P]_i | k, B) \\ f_4(V, [A], [B], [P], F_i, F_o, [A]_i, [B]_i, [P]_i | k, B) \end{bmatrix}
 \end{aligned}$$

↪ For the input variables, $u(t)$

$$u(t) = \begin{bmatrix} u_1(t) \\ u_2(t) \\ u_3(t) \\ u_4(t) \end{bmatrix} = \begin{bmatrix} F_i(t) \\ F_o(t) \\ [A]_i(t) \\ [B]_i(t) \end{bmatrix},$$

Example I (cont.)

$$\begin{aligned}
 \begin{bmatrix} \dot{V} \\ \dot{[A]} \\ \dot{[B]} \\ \dot{[P]} \end{bmatrix} &= \begin{bmatrix} F_i - F_o \\ \frac{F_i}{V} ([A]_i - [A]) - k[A][B] \\ \frac{F_i}{V} ([B]_i - [B]) - 2k[A][B] \\ -\frac{F_i}{V} [P] + k[A][B] \end{bmatrix} \\
 &= \begin{bmatrix} f_1(V, [A], [B], [P], F_i, F_o, [A]_i, [B]_i, [P]_i | k, B) \\ f_2(V, [A], [B], [P], F_i, F_o, [A]_i, [B]_i, [P]_i | k, B) \\ f_3(V, [A], [B], [P], F_i, F_o, [A]_i, [B]_i, [P]_i | k, B) \\ f_4(V, [A], [B], [P], F_i, F_o, [A]_i, [B]_i, [P]_i | k, B) \end{bmatrix}
 \end{aligned}$$

↪ For the parameter(s), θ_x

$$\theta_x = \begin{bmatrix} \theta_1^x \\ \theta_2^x \end{bmatrix} = \begin{bmatrix} k \\ B \end{bmatrix}$$

Strictly speaking, B is embedded in the state variable V and hence not a parameter

- We still need to know its value to be able to do computations

Example I (cont.)

$$\begin{bmatrix} \dot{V} \\ \dot{[A]} \\ \dot{[B]} \\ \dot{[P]} \end{bmatrix} = \begin{bmatrix} F_i - F_o \\ \frac{F_i}{V}([A]_i - [A]) - k[A][B] \\ \frac{F_i}{V}([B]_i - [B]) - 2k[A][B] \\ -\frac{F_i}{V}[P] + k[A][B] \end{bmatrix}$$

For compactness, we can now write the state-space equations using the control notation

$$\underbrace{\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \dot{x}_3 \\ \dot{x}_4 \end{bmatrix}}_{\dot{x}} = \underbrace{\begin{bmatrix} f_1(x, u | \theta_x) \\ f_2(x, u | \theta_x) \\ f_3(x, u | \theta_x) \\ f_4(x, u | \theta_x) \end{bmatrix}}_{f(x, u | \theta_x)} = \begin{bmatrix} u_1 - u_2 \\ \frac{u_1}{x_1}(u_3 - x_2) - kx_2x_3 \\ \frac{u_1}{x_1}(u_4 - x_3) - 2kx_2x_3 \\ -\frac{u_1x_4}{x_1} + kx_2x_3 \end{bmatrix}$$

Example I (cont.)

Let $x'(t) = [x(t) - x_{SS}(t)]$, $u'(t) = [u(t) - u_{SS}(t)]$, for some steady-state (x_{SS}, u_{SS})

We write a linearised model, $\dot{x}'(t) = Ax'(t) + Bu'(t)$ by computing matrix A and B

$$A = \begin{bmatrix} \left. \frac{\partial f_1(x, u)}{\partial x_1} \right|_{x_{SS}, u_{SS}} & \left. \frac{\partial f_1(x, u)}{\partial x_2} \right|_{x_{SS}, u_{SS}} & \left. \frac{\partial f_1(x, u)}{\partial x_3} \right|_{x_{SS}, u_{SS}} & \left. \frac{\partial f_1(x, u)}{\partial x_4} \right|_{x_{SS}, u_{SS}} \\ \left. \frac{\partial f_2(x, u)}{\partial x_1} \right|_{x_{SS}, u_{SS}} & \left. \frac{\partial f_2(x, u)}{\partial x_2} \right|_{x_{SS}, u_{SS}} & \left. \frac{\partial f_2(x, u)}{\partial x_3} \right|_{x_{SS}, u_{SS}} & \left. \frac{\partial f_2(x, u)}{\partial x_4} \right|_{x_{SS}, u_{SS}} \\ \left. \frac{\partial f_3(x, u)}{\partial x_1} \right|_{x_{SS}, u_{SS}} & \left. \frac{\partial f_3(x, u)}{\partial x_2} \right|_{x_{SS}, u_{SS}} & \left. \frac{\partial f_3(x, u)}{\partial x_3} \right|_{x_{SS}, u_{SS}} & \left. \frac{\partial f_3(x, u)}{\partial x_4} \right|_{x_{SS}, u_{SS}} \\ \left. \frac{\partial f_4(x, u)}{\partial x_1} \right|_{x_{SS}, u_{SS}} & \left. \frac{\partial f_4(x, u)}{\partial x_2} \right|_{x_{SS}, u_{SS}} & \left. \frac{\partial f_4(x, u)}{\partial x_3} \right|_{x_{SS}, u_{SS}} & \left. \frac{\partial f_4(x, u)}{\partial x_4} \right|_{x_{SS}, u_{SS}} \end{bmatrix}$$

$$B = \begin{bmatrix} \left. \frac{\partial f_1(x, u)}{\partial u_1} \right|_{x_{SS}, u_{SS}} & \left. \frac{\partial f_1(x, u)}{\partial u_2} \right|_{x_{SS}, u_{SS}} & \left. \frac{\partial f_1(x, u)}{\partial u_3} \right|_{x_{SS}, u_{SS}} & \left. \frac{\partial f_1(x, u)}{\partial u_4} \right|_{x_{SS}, u_{SS}} \\ \left. \frac{\partial f_2(x, u)}{\partial u_1} \right|_{x_{SS}, u_{SS}} & \left. \frac{\partial f_2(x, u)}{\partial u_2} \right|_{x_{SS}, u_{SS}} & \left. \frac{\partial f_2(x, u)}{\partial u_3} \right|_{x_{SS}, u_{SS}} & \left. \frac{\partial f_2(x, u)}{\partial u_4} \right|_{x_{SS}, u_{SS}} \\ \left. \frac{\partial f_3(x, u)}{\partial u_1} \right|_{x_{SS}, u_{SS}} & \left. \frac{\partial f_3(x, u)}{\partial u_2} \right|_{x_{SS}, u_{SS}} & \left. \frac{\partial f_3(x, u)}{\partial u_3} \right|_{x_{SS}, u_{SS}} & \left. \frac{\partial f_3(x, u)}{\partial u_4} \right|_{x_{SS}, u_{SS}} \\ \left. \frac{\partial f_4(x, u)}{\partial u_1} \right|_{x_{SS}, u_{SS}} & \left. \frac{\partial f_4(x, u)}{\partial u_2} \right|_{x_{SS}, u_{SS}} & \left. \frac{\partial f_4(x, u)}{\partial u_3} \right|_{x_{SS}, u_{SS}} & \left. \frac{\partial f_4(x, u)}{\partial u_4} \right|_{x_{SS}, u_{SS}} \end{bmatrix}$$

Example I (cont.)

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \dot{x}_3 \\ \dot{x}_4 \end{bmatrix} = \begin{bmatrix} u_1 - u_2 \\ \frac{u_1}{x_1}(u_3 - x_2) - kx_2x_3 \\ \frac{u_1}{x_1}(u_4 - x_3) - 2kx_2x_3 \\ -\frac{u_1x_4}{x_1} + kx_2x_3 \end{bmatrix}$$

By taking the partial derivatives of f with respect to the state variables x , we obtain

$$A = \begin{bmatrix} 0 & 0 & 0 & 0 \\ -\frac{u_1(u_3 - x_2)}{x_1^2} \Big|_{x_{SS}, u_{SS}} & \left(-\frac{u_1}{x_1} - kx_3\right) \Big|_{x_{SS}, u_{SS}} & -kx_2 \Big|_{x_{SS}, u_{SS}} & 0 \\ -\frac{u_1(u_4 - x_3)}{x_1^2} \Big|_{x_{SS}, u_{SS}} & -2kx_3 \Big|_{x_{SS}, u_{SS}} & \left(-\frac{u_1}{x_1} - 2kx_2\right) \Big|_{x_{SS}, u_{SS}} & 0 \\ \frac{u_1x_4}{x_1^2} \Big|_{x_{SS}, u_{SS}} & k & kx_2 \Big|_{x_{SS}, u_{SS}} & -\frac{u_1}{x_1} \Big|_{x_{SS}, u_{SS}} \end{bmatrix}$$

For some fixed point (x_{SS}, u_{SS})

Example I (cont.)

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \dot{x}_3 \\ \dot{x}_4 \end{bmatrix} = \begin{bmatrix} u_1 - u_2 \\ \frac{u_1}{x_1}(u_3 - x_2) - kx_2x_3 \\ \frac{u_1}{x_1}(u_4 - x_3) - 2kx_2x_3 \\ -\frac{u_1x_4}{x_1} + kx_2x_3 \end{bmatrix}$$

By taking the partial derivatives of f with respect to the input variables u , we obtain

$$B = \begin{bmatrix} 1 & -1 & 0 & 0 \\ \left. \frac{u_3 - x_2}{x_1} \right|_{x_{SS}, u_{SS}} & 0 & \left. \frac{u_1}{x_1} \right|_{x_{SS}, u_{SS}} & 0 \\ \left. \frac{u_4 - x_3}{x_1} \right|_{x_{SS}, u_{SS}} & 0 & 0 & \left. \frac{u_1}{x_1} \right|_{x_{SS}, u_{SS}} \\ -\left. \frac{x_4}{x_1} \right|_{x_{SS}, u_{SS}} & 0 & 0 & 0 \end{bmatrix}$$

Again, for some fixed point (x_{SS}, u_{SS})

The nonlinear model linearised around (x_{SS}, u_{SS})

$$\dot{x}'(t) = \begin{bmatrix} 0 & 0 & 0 & 0 \\ -\frac{u_1(u_3 - x_2)}{x_1^2} & -\frac{u_1}{x_1} - kx_3 & -kx_2 & 0 \\ -\frac{u_1(u_4 - x_3)}{x_1^2} & -2kx_3 & -\frac{u_1}{x_1} - 2kx_2 & 0 \\ \frac{u_1 x_4}{x_1^2} & k & kx_2 & -\frac{u_1}{x_1} \end{bmatrix}_{SS} x'(t) + \begin{bmatrix} 1 & -1 & 0 & 0 \\ \frac{u_3 - x_2}{x_1} & 0 & \frac{u_1}{x_1} & 0 \\ \frac{u_4 - x_3}{x_1} & 0 & 0 & \frac{u_1}{x_1} \\ -\frac{x_4}{x_1} & 0 & 0 & 0 \end{bmatrix}_{SS} u'(t)$$

Assuming that we can measure all the state variables, for $y'(t) = y(t) - y_{SS}$ we have

$$y'(t) = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} x'(t) + \begin{bmatrix} 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix} u'(t)$$

What is y_{SS} ?