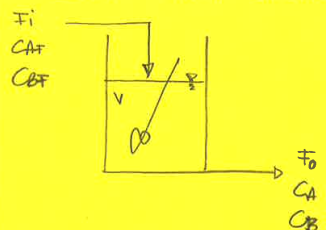


# CSTR FIRST-ORDER IRREVERSIBLE REACTION



Consider a single irreversible reaction  $A \rightarrow B$

→ Assume a rate of generation per unit volume that is first order with respect to  $C_A$

→ MOLAR RATE OF REACTION OF A PER UNIT VOLUME =  $r_A$

$$r_A = -K C_A$$

→ EACH MOLE OF A CREATES A MOLE OF B

→ MOLAR RATE OF FORMATION OF B PER UNIT VOLUME =  $r_B$

$$r_B = K C_A$$

WE START BY WRITING THE DYNAMIC MODELING EQUATIONS

**COMPONENT A**

$$\frac{dV C_A}{dt} = F C_{Ai} - F C_A - V K C_A \quad (\text{WITH } K \text{ THE REACTION } \overset{\text{RATE}}{\text{CONSTANT}})$$

ASSUMING THAT  $V$  IS CONSTANT, WE HAVE

$$(T_i = T_0)$$

$$\begin{aligned} \frac{dC_A}{dt} &= \frac{F}{V} C_{Ai} - \frac{F}{V} C_A - K C_A \\ &= \frac{F}{V} C_{Ai} - \left( \frac{F}{V} + K \right) C_A \end{aligned}$$

**COMPONENT B**

$$\frac{dV C_B}{dt} = F C_{Bi} - F C_B + V K C_A$$

ASSUMING CONSTANT VOLUME AND NO B IN THE FEED

$$\frac{dC_B}{dt} = -\frac{F}{V} C_B + K C_A$$

(1)

$$\begin{cases} \frac{dC_A}{dt} = \frac{F}{V} C_{Ai} - \left( \frac{F}{V} + K \right) C_A \\ \frac{dC_B}{dt} = -\frac{F}{V} C_B + K C_A \end{cases}$$

The concentration of B does not play any role in the dynamics of component A

$$\begin{bmatrix} \dot{C}_A \\ \dot{C}_B \end{bmatrix} = \begin{bmatrix} \frac{F}{V} C_{Ai} - \left( \frac{F}{V} + K \right) C_A \\ -\frac{F}{V} C_B + K C_A \end{bmatrix} \quad \text{OR} \quad \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} C_A \\ C_B \end{bmatrix}, \quad \begin{bmatrix} u_1 \\ u_2 \end{bmatrix} = \begin{bmatrix} F \\ C_{Ai} \end{bmatrix}$$

$$\theta = [K, V]$$

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} u_1/V - (u_1/V + K) x_1 \\ -u_2/V x_2 + K x_1 \end{bmatrix} = \begin{bmatrix} f_1(x_1, x_2, u_1, u_2 | \theta_1, \theta_2) \\ f_2(x_1, x_2, u_1, u_2 | \theta_1, \theta_2) \end{bmatrix}$$

## BASIC LINEARIZATION AROUND A FIXED POINT

$$A = \begin{bmatrix} \frac{\partial f_1}{\partial x_1} \Big|_{ss} & \frac{\partial f_1}{\partial x_2} \Big|_{ss} \\ \frac{\partial f_2}{\partial x_1} \Big|_{ss} & \frac{\partial f_2}{\partial x_2} \Big|_{ss} \end{bmatrix} \quad B = \begin{bmatrix} \frac{\partial f_1}{\partial u_1} \Big|_{ss} & \frac{\partial f_1}{\partial u_2} \Big|_{ss} \\ \frac{\partial f_2}{\partial u_1} \Big|_{ss} & \frac{\partial f_2}{\partial u_2} \Big|_{ss} \end{bmatrix}$$

$$\frac{\partial f_1}{\partial x_1} = -u_1/V - K$$

$$\frac{\partial f_1}{\partial x_2} = 0$$

$$\frac{\partial f_2}{\partial x_1} = K$$

$$\frac{\partial f_2}{\partial x_2} = -u_2/V$$

$$\frac{\partial f_1}{\partial u_1} = u_1/V - x_1/V$$

$$\frac{\partial f_1}{\partial u_2} = 0$$

$$\frac{\partial f_2}{\partial u_1} = 0$$

$$\frac{\partial f_2}{\partial u_2} = 0$$

$$u_1/V \Big|_{ss} = 0.2 \text{ min}^{-1}$$

$$u_2 \Big|_{ss} = 1.0 \frac{\text{gmol}}{\text{lt}}$$

$$K = 0.2 \text{ min}^{-1}$$

$$A = \begin{bmatrix} -0.4 & 0 \\ 0.2 & -0.2 \end{bmatrix}$$

$$B = \begin{bmatrix} ** & 0.2 \\ ** & 0 \end{bmatrix}$$

↑  
TO BE COMPUTED → SEE (2)

WE ASSUME THAT  $F/V$  IS THE CONTROL VARIABLE OF INTEREST

- $F/V$  IS CALLED SPACE VELOCITY
- $V/F$  IS CALLED RESIDENCE TIME

→ CONSIDER  $\frac{dC_A}{dt} = \frac{F}{V} C_{A\text{F}} - \left(\frac{F}{V} + k\right) C_A$  AND ASSUME STEADY-STATE CONDITIONS

- THAT IS  $dC_A/dt = 0$ , WE HAVE  $C_A^{ss} = \frac{F/V C_{A\text{F}}^{ss}}{F/V + k}$

- AS  $F/V$  GETS LARGER (MORE FEED),  $C_A^{ss}$  TENDS TO  $C_{A\text{F}}^{ss}$  (the flow is so fast, that there is no conversion)

- AS  $F/V$  GETS SLOWER (LESS FEED),  $C_A^{ss}$  TENDS TO ZERO (the flow is so slow, that everything gets converted)

N.B.  $F^{ss}/V = 0$  MEANS  $F^{ss} = 0$  → BATCH REACTOR

INPUT-OUTPUT

The steady-state gain is the derivative of  $C_A^{ss}$  w.r.t  $F^{ss}/V$

$$* \frac{\partial C_A^{ss}}{\partial F^{ss}/V} = \frac{k C_{A\text{F}}^{ss}}{(kV/F^{ss} + k)^2}$$

DISTURBANCE-OUTPUT

The steady-state gain is the derivative of  $C_A^{ss}$  w.r.t  $C_{A\text{F}}^{ss}$

$$* \frac{\partial C_A^{ss}}{\partial C_{A\text{F}}^{ss}} = \frac{kV/F^{ss}}{kV/F^{ss} + k}$$

$$* b_{11} = \left. \frac{\partial f_1}{\partial u_1} \right|_{ss} = u_2/V - x_1/V \Big|_{ss} = \frac{1}{V} (u_2^{ss} - x_1^{ss})$$

$$K = 0.2 \text{ min}^{-1}$$

$$F^{ss}/V = 0.2 \text{ min}^{-1}$$

$$u_2^{ss} = C_{A\text{F}}^{ss} = 1.0$$

$$x_1^{ss} = C_A^{ss} = \frac{F^{ss}/V \cdot (C_{A\text{F}}^{ss})}{F^{ss}/V + k} = \frac{(0.2) \cdot (1.0)}{0.2 + 0.2} = \frac{0.2}{0.4} = 0.50$$

$$\rightarrow b_{11} = \frac{1}{V} \cdot \frac{1}{6}$$

$$* b_{21} = -u_2/V = -\frac{1}{V} u_2^{ss} = -\frac{1}{V}$$

→ CONSIDER  $\frac{dC_B}{dt} = -\frac{F}{V} C_B + K C_A$  AND ASSUME STEADY STATE COND.

- THAT IS  $dC_B/dt = 0$ , WE HAVE  $C_B^{ss} = \frac{K C_A^{ss}}{F^{ss}/V}$  WITH  $C_A^{ss}$

$$C_A^{ss} = \frac{F^{ss}/V C_{A\#}^{ss}}{F^{ss}/V + K}, \text{ BY SUBSTITUTION WE HAVE } X_1^{ss} = \frac{0.2 \cdot 1}{0.2 + 0.2} = 0.5$$

$$C_B^{ss} = \frac{K}{F^{ss}/V} \frac{F^{ss}/V (C_{A\#}^{ss})}{F^{ss}/V + K} = \frac{K C_{A\#}^{ss}}{F^{ss}/V + K} = \frac{0.2 \cdot 1}{0.2 + 0.2} = 0.5$$

- AS  $F^{ss}/V$  GETS LARGER,  $C_B^{ss}$  TENDS TO ZERO

- AS  $F^{ss}/V$  GETS SMALLER,  $C_B^{ss}$  APPROACHES  $C_{A\#}^{ss}$

$$X_2^{ss} = \frac{0.2 + 1}{0.2 + 0.2} = 0.5$$

LINEARISATION AROUND A STEADY-STATE (FIXED POINT)

Define  $\begin{cases} X_1 = C_A - C_A^{ss} \\ X_2 = C_B - C_B^{ss} \end{cases}$ , we have  $\begin{cases} \dot{X}_1 = dC_A/dt - 0 \\ \dot{X}_2 = dC_B/dt - 0 \end{cases}$

Also define  $\begin{cases} u_1 = F - F^{ss} \\ u_2 = C_{A\#} - C_{A\#}^{ss} \end{cases}$

WE HAVE, BY SUBSTITUTING AND LINEARISING:

$$\frac{dX_1}{dt} = -\left(\frac{F^{ss}}{V} + K\right) X_1 + (C_{A\#} - C_A^{ss}) u_1 + \frac{F^{ss}}{V} u_2$$

$$\frac{dX_2}{dt} = K X_1 + \left(-\frac{F^{ss}}{V}\right) X_2 - C_B^{ss} u_1$$

$$\begin{bmatrix} \dot{X}_1 \\ \dot{X}_2 \end{bmatrix} = \begin{bmatrix} -(F^{ss}/V + K) & 0 \\ K & -F^{ss}/V \end{bmatrix} \begin{bmatrix} X_1 \\ X_2 \end{bmatrix} + \begin{bmatrix} C_{A\#}^{ss} - C_A^{ss} \\ -C_B^{ss} \end{bmatrix} \frac{F^{ss}/V}{1} \begin{bmatrix} u_1 \\ u_2 \end{bmatrix}$$

$$= \begin{bmatrix} -0.4 & 0 \\ 0.2 & -0.2 \end{bmatrix} \begin{bmatrix} X_1 \\ X_2 \end{bmatrix} + \begin{bmatrix} 0.5 & 0.2 \\ -0.5 & 0 \end{bmatrix} \begin{bmatrix} u_1 \\ u_2 \end{bmatrix}$$

(3)

$$\frac{dC_A}{dt} = \frac{F}{V} C_{A\#} - \left(\frac{F}{V} + K\right) C_A$$

$$\frac{dC_B}{dt} = -\frac{F}{V} C_B + K C_A$$

$$\text{let } \begin{cases} x_1 = C_A \\ x_2 = C_B \end{cases}$$

$$\text{let } \begin{cases} u_1 = F/V \\ u_2 = C_{A\#} \end{cases}$$

$$u_1^{ss} = 0.2 \text{ min}^{-1}$$

$$u_2^{ss} = 1 \text{ g mol/l}$$

$$K = 0.2 \text{ min}^{-1}$$

$$\frac{dx_1}{dt} = u_1 u_2 - \underbrace{(u_1 + K) x_1}_{f_1(x_1, x_2, u_1, u_2)}$$

$$\frac{dx_2}{dt} = -u_1 x_2 + K x_1 \underbrace{f_2(x_1, x_2, u_1, u_2)}$$

$$\frac{dx_1}{dt} \approx f_1(x^{ss}, u^{ss}) + \left. \frac{\partial f_1}{\partial x_1} \right|_{ss} (x_1 - x_1^{ss}) + \left. \frac{\partial f_1}{\partial x_2} \right|_{ss} (x_2 - x_2^{ss}) + \left. \frac{\partial f_1}{\partial u_1} \right|_{ss} (u_1 - u_1^{ss}) + \left. \frac{\partial f_1}{\partial u_2} \right|_{ss} (u_2 - u_2^{ss}) + \dots$$

$$\frac{dx_2}{dt} \approx f_2(x^{ss}, u^{ss}) + \left. \frac{\partial f_2}{\partial x_1} \right|_{ss} (x_1 - x_1^{ss}) + \left. \frac{\partial f_2}{\partial x_2} \right|_{ss} (x_2 - x_2^{ss}) + \left. \frac{\partial f_2}{\partial u_1} \right|_{ss} (u_1 - u_1^{ss}) + \left. \frac{\partial f_2}{\partial u_2} \right|_{ss} (u_2 - u_2^{ss}) + \dots$$

$$\frac{\partial f}{\partial x} = \begin{bmatrix} -(u_1 + K) & 0 \\ K & -u_1 \end{bmatrix} \xrightarrow{ss} \begin{bmatrix} -(0.2 + 0.2) & 0 \\ 0.2 & -0.2 \end{bmatrix}$$

$$\frac{\partial f}{\partial u} = \begin{bmatrix} u_2 - x_1 & u_1 \\ -x_2 & 0 \end{bmatrix} \xrightarrow{ss} \begin{bmatrix} 1 - 0.5 & 0.2 \\ 0.5 & 0 \end{bmatrix}$$

(4)

$$\text{let } \begin{cases} x_1' = x_1 - x_{1ss} \\ x_2' = x_2 - x_{2ss} \end{cases}$$

$$\text{let } \begin{cases} u_1' = u_1 - u_{1ss} \\ u_2' = u_2 - u_{2ss} \end{cases}$$

$$\frac{dx_1}{dt} = \frac{dx_1}{dt}$$

$$\frac{dx_2}{dt} = \frac{dx_2}{dt}$$

$$\frac{dx_1'}{dt} \approx \left. \frac{\partial f_1}{\partial x_1} \right|_{ss} x_1' + \left. \frac{\partial f_1}{\partial x_2} \right|_{ss} x_2' + \left. \frac{\partial f_1}{\partial u_1} \right|_{ss} u_1' + \left. \frac{\partial f_1}{\partial u_2} \right|_{ss} u_2'$$

$$\frac{dx_2'}{dt} = \left. \frac{\partial f_2}{\partial x_1} \right|_{ss} x_1' + \left. \frac{\partial f_2}{\partial x_2} \right|_{ss} x_2' + \left. \frac{\partial f_2}{\partial u_1} \right|_{ss} u_1' + \left. \frac{\partial f_2}{\partial u_2} \right|_{ss} u_2'$$

$$\begin{bmatrix} x_1' \\ x_2' \end{bmatrix} = \underbrace{\begin{bmatrix} -0.4 & 0 \\ 0.2 & -0.2 \end{bmatrix}}_A \begin{bmatrix} x_1' \\ x_2' \end{bmatrix} + \underbrace{\begin{bmatrix} 0.5 & 0.2 \\ 0.5 & 0 \end{bmatrix}}_B \begin{bmatrix} u_1' \\ u_2' \end{bmatrix}$$

$$x'(t) = \underbrace{e^{At}}_{FF} x'(0) + \int_0^t e^{A(t-\tau)} B u(\tau) d\tau$$

» symc t

$$\Rightarrow A = \begin{bmatrix} -0.4 & 0 \\ 0.2 & -0.2 \end{bmatrix};$$

$$\Rightarrow \text{expmAt} = \text{expm}(A * t)$$

$$\Rightarrow x_0 = [1; 1]$$

$$\Rightarrow x_u = \text{expmAt} * x_0$$

$$\Rightarrow \text{fplot}(x_u, [0, 20])$$

FORCE - FREE  
RESPONSE

DISCOVER IN CLASS how to do  
THE FORCED RESPONSE