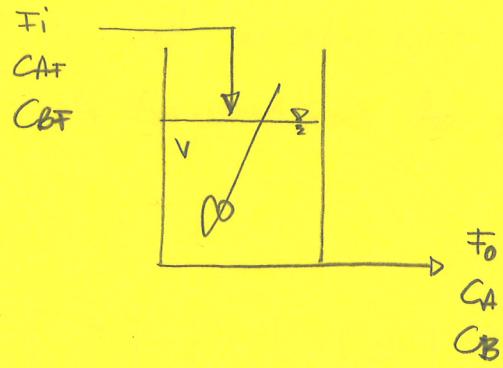


# CSTR FIRST-ORDER IRREVERSIBLE REACTION



Consider a single irreversible reaction  $A \rightarrow B$

→ Assume a rate of generation per unit volume that is first order with respect to  $C_A$

and MOLAR RATE OF REACTION OF A PER UNIT VOLUME =  $r_A$

$$r_A = k C_A$$

→ EACH MOLE OF A CREATES A MOLE OF B

and MOLAR RATE OF FORMATION OF B PER UNIT VOLUME =  $r_B$

$$r_B = k C_A$$

WE START BY WRITING THE DYNAMIC MODELING EQUATIONS

COMPONENT A

$$\frac{dV C_A}{dt} = F C_{AF} - F C_A - V k C_A \quad (\text{WITH } k \text{ THE REACTION RATE CONSTANT})$$

ASSUMING THAT  $V$  IS CONSTANT, WE HAVE

$$(F_i = F_o)$$

$$\frac{dC_A}{dt} = \frac{F}{V} C_{AF} - \frac{F}{V} C_A - k C_A$$

$$= \frac{F}{V} C_{AF} - \left( \frac{F}{V} + k \right) C_A$$

COMPONENT B

$$\frac{dV C_B}{dt} = F C_{BF} - F C_B + V k C_A$$

$$\frac{dC_B}{dt} = - \frac{F}{V} C_B + k C_A$$

ASSUMING CONSTANT VOLUME AND NO B IN THE FEED

$$\begin{cases} \frac{dC_A}{dt} = \frac{F}{V} C_{AF} - \left( \frac{F}{V} + K \right) C_A \\ \frac{dC_B}{dt} = -\frac{F}{V} C_B + K C_A \end{cases}$$

The concentration of B does not play any role in the dynamics of component A

$$\begin{bmatrix} \dot{C}_A \\ \dot{C}_B \end{bmatrix} = \begin{bmatrix} F/V C_{AF} - (F/V + K) C_A \\ -F/V C_B + K C_A \end{bmatrix}$$

OR  $\begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} C_A \\ C_B \end{bmatrix}, \begin{bmatrix} u_1 \\ u_2 \end{bmatrix} = \begin{bmatrix} F \\ C_{AF} \end{bmatrix}$   
 $\theta = [K, V]$

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} u_1/V M_2 - (u_1/V + K) x_1 \\ -u_2/V x_2 + K x_1 \end{bmatrix} = \begin{bmatrix} f_1(x_1, x_2, u_1, u_2 | \theta_1, \theta_2) \\ f_2(x_1, x_2, u_1, u_2 | \theta_1, \theta_2) \end{bmatrix}$$

### BASIC LINEARIZATION AROUND A FIXED POINT

$$A = \begin{bmatrix} \frac{\partial f_1}{\partial x_1} \Big|_{ss} & \frac{\partial f_1}{\partial x_2} \Big|_{ss} \\ \frac{\partial f_2}{\partial x_1} \Big|_{ss} & \frac{\partial f_2}{\partial x_2} \Big|_{ss} \end{bmatrix} \quad B = \begin{bmatrix} \frac{\partial f_1}{\partial u_1} \Big|_{ss} & \frac{\partial f_1}{\partial u_2} \Big|_{ss} \\ \frac{\partial f_2}{\partial u_1} \Big|_{ss} & \frac{\partial f_2}{\partial u_2} \Big|_{ss} \end{bmatrix}$$

$$\begin{aligned} \frac{\partial f_1}{\partial x_1} &= -M_1/V - K \\ \frac{\partial f_1}{\partial x_2} &= 0 \\ \frac{\partial f_2}{\partial x_1} &= K \\ \frac{\partial f_2}{\partial x_2} &= -M_2/V \end{aligned}$$

$$\begin{aligned} \frac{\partial f_1}{\partial u_1} &= M_2/V - x_1/V \\ \frac{\partial f_1}{\partial u_2} &= M_1/V \\ \frac{\partial f_2}{\partial u_1} &= -M_2/V \\ \frac{\partial f_2}{\partial u_2} &= 0 \end{aligned}$$

$$M_1/V \Big|_{ss} = 0.2 \text{ min}^{-1}$$

$$M_2 \Big|_{ss} = 1.0 \frac{\text{g mol}}{\text{lt}}$$

$$K = 0.2 \text{ min}^{-1}$$

$$A = \begin{bmatrix} -0.4 & 0 \\ 0.2 & -0.2 \end{bmatrix}$$

$$B = \begin{bmatrix} ** & 0.2 \\ ** & 0 \end{bmatrix}$$

↑  
TO BE COMPUTED → SEE (2)

WE ASSUME THAT  $F/V$  IS THE CONTROL VARIABLE OF INTEREST

- $F/V$  IS CALLED SPACE VELOCITY
- $V/F$  IS CALLED RESIDENCE TIME

→ CONSIDER CONDITIONS  $\frac{dC_A}{dt} = \frac{F}{V} C_{A\text{f}} - \left( \frac{F}{V} + k \right) C_A$  AND ASSUME STEADY-STATE

$$\text{THAT IS } \frac{dC_A}{dt} = 0, \text{ WE HAVE } C_A^{\text{ss}} = \frac{\frac{ss}{F/V} C_{A\text{f}}^{\text{ss}}}{\frac{ss}{F/V} + k}$$

- AS  $F/V$  GETS LARGER (MORE FEED),  $C_A^{\text{ss}}$  TENDS TO  $C_{A\text{f}}^{\text{ss}}$   
(the flow is so fast, that there is no conversion)

- AS  $F/V$  GETS SMALLER (LESS FEED),  $C_A^{\text{ss}}$  TENDS TO ZERO  
(the flow is so slow, that everything gets converted)

N.B.  $F/V = 0$  MEANS  $F = 0$  AND BATCH REACTOR

INPUT-OUTPUT

The steady-state gain is the derivative of  $C_A^{\text{ss}}$  wrt  $F/V$

$$* \frac{\partial C_A^{\text{ss}}}{\partial F/V} = \frac{k C_{A\text{f}}^{\text{ss}}}{(kV/F^{\text{ss}} + k)^2}$$

DISTURBANCE-OUTPUT

The steady-state gain is the derivative of  $C_A^{\text{ss}}$  wrt  $C_{A\text{f}}^{\text{ss}}$

$$* \frac{\partial C_A^{\text{ss}}}{\partial C_{A\text{f}}^{\text{ss}}} = \frac{kV/F^{\text{ss}}}{kV/F^{\text{ss}} + k}$$

$$* b_{11} = \frac{\partial f_1}{\partial U_1} \Big|_{ss} = U_2/V - X_1/V \Big|_{ss} = \frac{1}{V} (U_2^{ss} - X_1^{ss})$$

$K = 0.2 \text{ min}^{-1}$   
 $F^{ss}/V = 0.2 \text{ min}^{-1}$

$$U_2^{ss} = C_{AF}^{ss} = 1.0$$

$$X_1^{ss} = C_A^{ss} = \frac{F^{ss}/V \cdot (C_{AF}^{ss})}{F^{ss}/V + K} = \frac{(0.2) \cdot (1.0)}{0.2 + 0.2} = \frac{0.2}{0.4} = 0.50$$

$$\Rightarrow b_{11} = \frac{1}{V} \cdot \frac{1}{6}$$

$$* b_{21} = -U_2/V = -\frac{1}{V} U_2^{ss} = -\frac{1}{V}$$

→ CONSIDER  $\frac{dC_B}{dt} = -\frac{F}{V} C_B + K C_A$  AND ASSUME STEADY STATE COND.

- THAT IS  $\frac{dC_B}{dt} = 0$ , WE HAVE  $C_B^{ss} = \frac{K C_A^{ss}}{F^{ss}/V}$  WITH  $C_A^{ss}$

$$C_A^{ss} = \frac{F^{ss}/V C_A^{ss}}{F^{ss}/V + K}, \text{ BY SUBSTITUTION WE HAVE } X_1^{ss}$$

$$C_B^{ss} = \frac{K}{F^{ss}/V} \frac{\frac{F^{ss}/V (C_A^{ss})}{F^{ss}/V + K}}{= \frac{0.2 \cdot 1}{0.2 + 0.2} = \frac{0.2}{0.4} = 0.5}$$

- AS  $F^{ss}/V$  GETS LARGER,  $C_B^{ss}$  TENDS TO ZERO

- AS  $F^{ss}/V$  GETS SMALLER,  $C_B^{ss}$  APPROACHES  $C_A^{ss}$

$$\frac{0.2 \cdot 1}{0.2 + 0.2} = \underline{0.5}$$

### LINEARISATION AROUND A STEADY-STATE (FIXED POINT)

Define  $\begin{cases} x_1 = C_A - C_A^{ss} \\ x_2 = C_B - C_B^{ss} \end{cases}$ , we have  $\begin{cases} \dot{x}_1 = dC_A/dt - 0 \\ \dot{x}_2 = dC_B/dt - 0 \end{cases}$

Also define  $\begin{cases} M_1 = F - F^{ss} \\ M_2 = C_{A^f} - C_{A^f}^{ss} \end{cases}$

WE HAVE, BY SUBSTITUTING AND LINEARISING:

$$\frac{dx_1}{dt} = -\left(\frac{F^{ss}}{V} + K\right)x_1 + (C_{A^f} - C_A^{ss}) u_1 + \frac{F^{ss}}{V} M_2$$

$$\frac{dx_2}{dt} = Kx_1 + \left(-\frac{F^{ss}}{V}\right)x_2 - C_B^{ss} M_1$$

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} -(F^{ss}/V + K) & 0 \\ K & -F^{ss}/V \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} C_{A^f} - C_A^{ss} & \frac{F^{ss}/V}{M_2} \\ -C_B^{ss} & 0 \end{bmatrix} \begin{bmatrix} u_1 \\ u_2 \end{bmatrix}$$

$$= \begin{bmatrix} -0.4 & 0 \\ 0.2 & -0.2 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 0.5 & 0.2 \\ -0.5 & 0 \end{bmatrix} \begin{bmatrix} u_1 \\ u_2 \end{bmatrix}$$



$$\frac{dC_A}{dt} = \frac{\pm}{V} C_{A\pm} - \left( \frac{\pm}{V} + k \right) C_A$$

$$\frac{dC_B}{dt} = - \frac{\pm}{V} C_B + k C_A$$

let  $x_1 = C_A$   
 $x_2 = C_B$

let  $u_1 = \pm/V$   
 $u_2 = C_A\pm$

$$u_1^{ss} = 0.2 \text{ min}^{-1}$$

$$u_2^{ss} = 1 \text{ g/mol/lit}$$

$$k = 0.2 \text{ min}^{-1}$$

$$\frac{dx_1}{dt} = u_1 u_2 - \underbrace{(u_1 + k)}_{f_1(x_1, x_2, u_1, u_2)} x_1$$

$$\frac{dx_2}{dt} = - u_1 x_2 + \underbrace{k x_1}_{f_2(x_1, x_2, u_1, u_2)}$$

$$\frac{dx_1}{dt} \approx f_1(x_1^{ss}, u_1^{ss}) + \frac{\partial f_1}{\partial x_1} \Big|_{ss} (x_1 - x_1^{ss}) + \frac{\partial f_1}{\partial u_1} \Big|_{ss} (u_1 - u_1^{ss}) + \dots$$

$$+ \frac{\partial f_1}{\partial u_2} \Big|_{ss} (u_2 - u_2^{ss}) + \frac{\partial f_1}{\partial x_2} \Big|_{ss} (x_2 - x_2^{ss}) + \dots$$

$$\frac{dx_2}{dt} \approx f_2(x_2^{ss}, u_2^{ss}) + \frac{\partial f_2}{\partial x_1} \Big|_{ss} (x_1 - x_1^{ss}) + \frac{\partial f_2}{\partial x_2} \Big|_{ss} (x_2 - x_2^{ss}) + \dots$$

$$+ \frac{\partial f_2}{\partial u_1} \Big|_{ss} (u_1 - u_1^{ss}) + \frac{\partial f_2}{\partial u_2} \Big|_{ss} (u_2 - u_2^{ss}) + \dots$$

$$\frac{\partial f}{\partial x} = \begin{bmatrix} -(u_1 + k) & 0 \\ k & -u_1 \end{bmatrix} \xrightarrow{ss} \begin{bmatrix} -(0.2 + 0.2) & 0 \\ [-0.4] & 0.2 \end{bmatrix} \xrightarrow{ss} \begin{bmatrix} 0 & 0 \\ 0.2 & -0.2 \end{bmatrix}$$

$$\frac{\partial f}{\partial u} = \begin{bmatrix} u_2 - x_1 & u_1 \\ -x_2 & 0 \end{bmatrix} \xrightarrow{ss} \begin{bmatrix} 1 - 0.5 \\ [0.5] \end{bmatrix} \begin{bmatrix} 0.2 & 0 \\ 0.5 & 0 \end{bmatrix}$$



$$\text{let } \begin{cases} x'_1 = x_1 - x_{1ss} \\ x'_2 = x_2 - x_{2ss} \end{cases}$$

$$\text{let } \begin{cases} u'_1 = u_1 - u_{1ss} \\ u'_2 = u_2 - u_{2ss} \end{cases}$$

$$\frac{dx'_1}{dt} = \frac{dx_1}{dt}$$

$$\frac{dx'_2}{dt} = \frac{dx_2}{dt}$$

$$\left| \begin{array}{l} \frac{dx'_1}{dt} \approx \frac{\partial f_1}{\partial x_1} \Big|_{ss} x'_1 + \frac{\partial f_1}{\partial x_2} \Big|_{ss} x'_2 + \frac{\partial f_1}{\partial u_1} \Big|_{ss} u'_1 \\ \quad \quad \quad + \frac{\partial f_1}{\partial u_2} \Big|_{ss} u'_2 \\ \frac{dx'_2}{dt} = \frac{\partial f_2}{\partial x_1} \Big|_{ss} x'_1 + \frac{\partial f_2}{\partial x_2} \Big|_{ss} x'_2 + \frac{\partial f_2}{\partial u_1} \Big|_{ss} u'_1 \\ \quad \quad \quad + \frac{\partial f_2}{\partial u_2} \Big|_{ss} u'_2 \end{array} \right.$$

$$\begin{bmatrix} x'_1 \\ x'_2 \end{bmatrix} = \underbrace{\begin{bmatrix} -0.4 & 0 \\ 0.2 & -0.2 \end{bmatrix}}_A \begin{bmatrix} x'_1 \\ x'_2 \end{bmatrix} + \underbrace{\begin{bmatrix} 0.5 & 0.2 \\ 0.5 & 0 \end{bmatrix}}_B \begin{bmatrix} u'_1 \\ u'_2 \end{bmatrix}$$

$$x'(t) = \underbrace{e^{At} x'(0)}_{FF} + \int_0^t e^{A(t-\tau)} B u(\tau) d\tau$$

» sym t

» A = [-0.4 0; 0.2 -0.2];

» expmAt = expm(A\*t)

» x0 = [1; 1]

» x\_u = expmAt \* x0

» fplot(x\_u, [0, 20])

FORCE-FREE  
RESPONSE

DISCOVER IN CLASS how to do  
THE FORCED RESPONSE



$$\left\{ \begin{array}{l} \frac{dC_A}{dt} = \underbrace{\frac{F}{V} C_{Af}}_{f_1} - \left( \frac{F}{V} + k \right) C_A \\ \frac{dC_B}{dt} = - \underbrace{\frac{F}{V} C_B}_{f_2} + k C_A \end{array} \right. \quad \left\{ \begin{array}{l} \frac{\partial f_1}{\partial C_A} = - \left( \frac{F}{V} + k \right) \\ \frac{\partial f_2}{\partial C_A} = k \end{array} \right. \quad \begin{array}{l} \frac{\partial f_1}{\partial C_B} = 0 \\ \frac{\partial f_2}{\partial C_B} = - \frac{F}{V} \end{array}$$

$$x_1 = C_A - C_A^{ss}$$

$$x_2 = C_B - C_B^{ss}$$

$$u_1 = F - F^{ss}$$

$$u_2 = C_{Af} - C_{Af}^{ss}$$

$$\left\{ \begin{array}{l} \frac{\partial f_1}{\partial F} = \frac{C_{Af}}{V} - \frac{C_A}{V} \\ \frac{\partial f_2}{\partial F} = - \frac{C_B}{V} \end{array} \right.$$

$$\begin{array}{l} \frac{\partial f_1}{\partial C_{Af}} = \frac{F}{V} \\ \frac{\partial f_2}{\partial C_{Af}} = 0 \end{array}$$

$$A = \begin{bmatrix} \frac{\partial f_1}{\partial C_A} \Big|_{ss} & \frac{\partial f_2}{\partial C_B} \Big|_{ss} \\ \frac{\partial f_2}{\partial C_A} \Big|_{ss} & \frac{\partial f_1}{\partial C_B} \Big|_{ss} \end{bmatrix} = \begin{bmatrix} - \left( \frac{F^{ss}}{V} + k \right) & 0 \\ k & - \frac{F^{ss}}{V} \end{bmatrix}$$

$$B = \begin{bmatrix} \frac{\partial f_1}{\partial F} \Big|_{ss} & \frac{\partial f_1}{\partial C_{Af}} \Big|_{ss} \\ \frac{\partial f_2}{\partial F} \Big|_{ss} & \frac{\partial f_2}{\partial C_{Af}} \Big|_{ss} \end{bmatrix} = \begin{bmatrix} \frac{C_{Af}^{ss} - C_A^{ss}}{V} & \frac{F^{ss}}{V} \\ - \frac{C_B^{ss}}{V} & 0 \end{bmatrix}$$

$$\begin{bmatrix} \frac{dx_1}{dt} \\ \frac{dx_2}{dt} \end{bmatrix} = \begin{bmatrix} - \left( \frac{F^{ss}}{V} + k \right) & 0 \\ k & - \frac{F^{ss}}{V} \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} \frac{C_{Af}^{ss} - C_A^{ss}}{V} & \frac{F^{ss}}{V} \\ - \frac{C_B^{ss}}{V} & 0 \end{bmatrix} \begin{bmatrix} u_1 \\ u_2 \end{bmatrix}$$

$$\dot{x}_1 = - \left( \frac{F^{ss}}{V} + k \right) x_1 + \underbrace{\frac{C_{Af}^{ss} - C_A^{ss}}{V} u_1}_{\text{Feedback}} + \frac{F^{ss}}{V} u_2$$

$$\dot{x}_2 = k x_1 - \frac{F^{ss}}{V} x_2 - \frac{C_B^{ss}}{V} u_1$$

