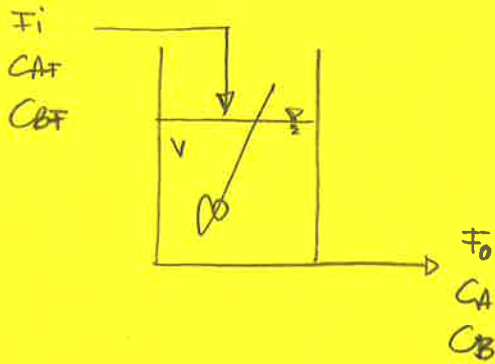


CSTR FIRST-ORDER IRREVERSIBLE REACTION



Consider a single irreversible reaction $A \rightarrow B$

→ Assume a rate of generation per unit volume that is first order with respect to C_A

→ MOLAR RATE OF REACTION OF A PER UNIT VOLUME = r_A

$$r_A = -k C_A$$

→ EACH MOLE OF A CREATES A MOLE OF B

→ MOLAR RATE OF FORMATION OF B PER UNIT VOLUME = r_B

$$r_B = k C_A$$

WE START BY WRITING THE DYNAMIC MODELLING EQUATIONS

COMPONENT A

$$\frac{dV C_A}{dt} = F C_{Af} - F C_A - V k C_A \quad (\text{WITH } k \text{ THE REACTION } \overset{\text{RATE}}{\text{CONSTANT}})$$

ASSUMING THAT V IS CONSTANT, WE HAVE

$$(F_i = F_o)$$

$$\begin{aligned} \frac{dC_A}{dt} &= \frac{F}{V} C_{Af} - \frac{F}{V} C_A - k C_A \\ &= \frac{F}{V} C_{Af} - \left(\frac{F}{V} + k \right) C_A \end{aligned}$$

COMPONENT B

$$\frac{dC_B}{dt} = -\frac{F}{V} C_B + k C_A$$

$$\frac{dV C_B}{dt} = F C_{Bf} - F C_B + V k C_A$$

ASSUMING CONSTANT VOLUME AND NO B IN THE FEED

$$\begin{cases} \frac{dC_A}{dt} = \frac{F}{V} C_{AF} - \left(\frac{F}{V} + K \right) C_A \\ \frac{dC_B}{dt} = -\frac{F}{V} C_B + K C_A \end{cases}$$

The concentration of B does not play any role in the dynamics of component A

$$\begin{bmatrix} \dot{C}_A \\ \dot{C}_B \end{bmatrix} = \begin{bmatrix} \frac{F}{V} C_{AF} - \left(\frac{F}{V} + K \right) C_A \\ -\frac{F}{V} C_B + K C_A \end{bmatrix}$$

$$\text{OR } \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} C_A \\ C_B \end{bmatrix}, \begin{bmatrix} u_1 \\ u_2 \end{bmatrix} = \begin{bmatrix} F \\ C_{AF} \end{bmatrix}$$

$$\theta = [K, V]$$

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} u_1/V - (u_1/V + K) x_1 \\ -u_1/V x_2 + K x_1 \end{bmatrix} = \begin{bmatrix} f_1(x_1, x_2, u_1, u_2 | \theta_1, \theta_2) \\ f_2(x_1, x_2, u_1, u_2 | \theta_1, \theta_2) \end{bmatrix}$$

BASIC LINEARIZATION AROUND A FIXED POINT

$$A = \begin{bmatrix} \left. \frac{\partial f_1}{\partial x_1} \right|_{ss} & \left. \frac{\partial f_1}{\partial x_2} \right|_{ss} \\ \left. \frac{\partial f_2}{\partial x_1} \right|_{ss} & \left. \frac{\partial f_2}{\partial x_2} \right|_{ss} \end{bmatrix}$$

$$B = \begin{bmatrix} \left. \partial f_1 / \partial u_1 \right|_{ss} & \left. \partial f_1 / \partial u_2 \right|_{ss} \\ \left. \partial f_2 / \partial u_1 \right|_{ss} & \left. \partial f_2 / \partial u_2 \right|_{ss} \end{bmatrix}$$

$$\partial f_1 / \partial x_1 = -u_1/V - K$$

$$\partial f_1 / \partial x_2 = 0$$

$$\partial f_2 / \partial x_1 = K$$

$$\partial f_2 / \partial x_2 = -u_1/V$$

$$\partial f_1 / \partial u_1 = u_1/V - x_1/V$$

$$\partial f_1 / \partial u_2 = u_1/V$$

$$\partial f_2 / \partial u_1 = -u_2/V$$

$$\partial f_2 / \partial u_2 = 0$$

$$u_1/V \big|_{ss} = 0.2 \text{ min}^{-1}$$

$$u_2 \big|_{ss} = 1.0 \frac{\text{gmol}}{\text{lt}}$$

$$K = 0.2 \text{ min}^{-1}$$

$$A = \begin{bmatrix} -0.4 & 0 \\ 0.2 & -0.2 \end{bmatrix}$$

$$B = \begin{bmatrix} ** & 0.2 \\ ** & 0 \end{bmatrix}$$



TO BE COMPUTED → SEE (2)

WE ASSUME THAT F/V IS THE CONTROL VARIABLE OF INTEREST

- F/V IS CALLED SPACE VELOCITY
- V/F IS CALLED RESIDENCE TIME

→ CONSIDER $\frac{dC_A}{dt} = \frac{F}{V} C_{A^F} - \left(\frac{F}{V} + k \right) C_A$ AND ASSUME STEADY-STATE CONDITIONS

- THAT IS $dC_A/dt = 0$, WE HAVE $C_A^{ss} = \frac{\frac{F}{V} C_{A^F}^{ss}}{\frac{F}{V} + k}$

- AS F^{ss}/V GETS LARGER (MORE FEED), C_A^{ss} TENDS TO $C_{A^F}^{ss}$
(the flow is so fast, that there is no conversion)

- AS F^{ss}/V GETS SMALLER (LESS FEED), C_A^{ss} TENDS TO ZERO
(the flow is so slow, that everything gets converted)

N.B $F^{ss}/V = 0$ MEANS $F^{ss} = 0$ → BATCH REACTOR

INPUT - OUTPUT
The steady-state gain is the derivative of C_A^{ss} wrt F^{ss}/V

$$* \frac{\partial C_A^{ss}}{\partial F^{ss}/V} = \frac{k C_{A^F}^{ss}}{(kV/F^{ss} + k)^2}$$

DISTURBANCE - OUTPUT
The steady-state gain is the derivative of C_A^{ss} wrt $C_{A^F}^{ss}$

$$* \frac{\partial C_A^{ss}}{\partial C_{A^F}^{ss}} = \frac{kV/F^{ss}}{kV/F^{ss} + k}$$

$$* b_{11} = \frac{\partial f_1}{\partial u_1} \Big|_{ss} = u_2/V - x_1/V \Big|_{ss} = \frac{1}{V} (u_2^{ss} - x_1^{ss})$$

$$K = 0.2 \text{ min}^{-1}$$

$$F^{ss}/V = 0.2 \text{ min}^{-1}$$

$$u_2^{ss} = C_{A^+}^{ss} = 1.0$$

$$x_1^{ss} = C_A^{ss} = \frac{F^{ss}/V \cdot (C_{A^+}^{ss})}{F^{ss}/V + K} = \frac{(0.2) \cdot (1.0)}{0.2 + 0.2} = \frac{0.2}{0.4} = 0.50$$

$$\Rightarrow b_{11} = \frac{1}{V} \cdot \frac{1}{6}$$

$$* b_{21} = -u_2/V = -\frac{1}{V} u_2^{ss} = -\frac{1}{V}$$

→ CONSIDER $\frac{dC_B}{dt} = -\frac{F}{V}C_B + KC_A$ AND ASSUME STEADY STATE COND.

- THAT IS $dC_B/dt = 0$, WE HAVE $C_B^{ss} = \frac{KC_A^{ss}}{F^{ss}/V}$ WITH C_A^{ss}

$$C_A^{ss} = \frac{F^{ss}/V C_{A+}^{ss}}{F^{ss}/V + K}, \text{ BY SUBSTITUTION WE HAVE } X_1^{ss} = \frac{0.2 \cdot 1}{0.2 + 0.2} = \frac{0.2}{0.4} = 0.5$$

$$C_B^{ss} = \frac{K}{F^{ss}/V} \frac{F^{ss}/V (C_{A+}^{ss})}{F^{ss}/V + K} = \frac{KC_{A+}^{ss}}{F^{ss}/V + K}$$

- AS F^{ss}/V GETS LARGER, C_B^{ss} TENDS TO ZERO

- AS F^{ss}/V GETS SMALLER, C_B^{ss} APPROACHES C_{A+}^{ss}

$$X_2^{ss} = \frac{0.2 \cdot 1}{0.2 + 0.2} = 0.5$$

LINEARISATION AROUND A STEADY-STATE (FIXED POINT)

Define $\begin{cases} X_1 = C_A - C_A^{ss} \\ X_2 = C_B - C_B^{ss} \end{cases}$, we have $\begin{cases} \dot{X}_1 = dC_A/dt - 0 \\ \dot{X}_2 = dC_B/dt - 0 \end{cases}$

Also define $\begin{cases} u_1 = F - F^{ss} \\ u_2 = C_{A+} - C_{A+}^{ss} \end{cases}$

WE HAVE, BY SUBSTITUTING AND LINEARISING:

$$\frac{dx_1}{dt} = -\left(\frac{F^{ss}}{V} + K\right)x_1 + (C_{A+} - C_A^{ss})u_1 + \frac{F^{ss}}{V}u_2$$

$$\frac{dx_2}{dt} = Kx_1 + \left(-\frac{F^{ss}}{V}\right)x_2 - C_B^{ss}u_1$$

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} -\left(\frac{F^{ss}}{V} + K\right) & 0 \\ K & -\frac{F^{ss}}{V} \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} C_{A+}^{ss} - C_A^{ss} \\ -C_B^{ss} \end{bmatrix} \begin{bmatrix} F^{ss}/V \\ 0 \end{bmatrix} \begin{bmatrix} u_1 \\ u_2 \end{bmatrix}$$

$$= \begin{bmatrix} -0.4 & 0 \\ 0.2 & -0.2 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 0.5 & 0.2 \\ -0.5 & 0 \end{bmatrix} \begin{bmatrix} u_1 \\ u_2 \end{bmatrix}$$

$$\frac{dC_A}{dt} = \frac{F}{V} C_{A\#} - \left(\frac{F}{V} + k \right) C_A$$

$$\frac{dC_B}{dt} = -\frac{F}{V} C_B + k C_A$$

$$\begin{aligned} \text{let } x_1 &= C_A \\ x_2 &= C_B \end{aligned}$$

$$\begin{aligned} \text{let } u_1 &= F/V \\ u_2 &= C_{A\#} \end{aligned}$$

$$u_1^{ss} = 0.2 \text{ min}^{-1}$$

$$u_2^{ss} = 1 \text{ g mol/l}$$

$$k = 0.2 \text{ min}^{-1}$$

$$\frac{dx_1}{dt} = u_1 u_2 - \underbrace{(u_1 + k)}_{f_1(x_1, x_2, u_1, u_2)} x_1$$

$$\frac{dx_2}{dt} = -u_1 x_2 + \underbrace{k x_1}_{f_2(x_1, x_2, u_1, u_2)}$$

$$\begin{aligned} \frac{dx_1}{dt} \approx f_1(x^{ss}, u^{ss}) &+ \left. \frac{\partial f_1}{\partial x_1} \right|_{ss} (x_1 - x_1^{ss}) + \left. \frac{\partial f_1}{\partial x_2} \right|_{ss} (x_2 - x_2^{ss}) + \\ &\left. \frac{\partial f_1}{\partial u_1} \right|_{ss} (u_1 - u_1^{ss}) + \left. \frac{\partial f_1}{\partial u_2} \right|_{ss} (u_2 - u_2^{ss}) + \dots \end{aligned}$$

$$\begin{aligned} \frac{dx_2}{dt} \approx f_2(x^{ss}, u^{ss}) &+ \left. \frac{\partial f_2}{\partial x_1} \right|_{ss} (x_1 - x_1^{ss}) + \left. \frac{\partial f_2}{\partial x_2} \right|_{ss} (x_2 - x_2^{ss}) + \\ &+ \left. \frac{\partial f_2}{\partial u_1} \right|_{ss} (u_1 - u_1^{ss}) + \left. \frac{\partial f_2}{\partial u_2} \right|_{ss} (u_2 - u_2^{ss}) + \dots \end{aligned}$$

$$\frac{\partial f}{\partial x} = \begin{bmatrix} -(u_1 + k) & 0 \\ k & -u_1 \end{bmatrix} \xrightarrow{ss} \begin{bmatrix} -(0.2 + 0.2) & 0 \\ 0.2 & -0.2 \end{bmatrix}$$

$$\frac{\partial f}{\partial u} = \begin{bmatrix} u_2 - x_1 & u_1 \\ -x_2 & 0 \end{bmatrix} \xrightarrow{ss} \begin{bmatrix} 1 - 0.5 & 0.2 \\ 0.5 & 0 \end{bmatrix}$$

$$\text{let } \begin{cases} x_1' = x_1 - x_{1ss} \\ x_2' = x_2 - x_{2ss} \end{cases}$$

$$\text{let } \begin{cases} u_1' = u_1 - u_{1ss} \\ u_2' = u_2 - u_{2ss} \end{cases}$$

$$\frac{dx_1'}{dt} = \frac{dx_1}{dt}$$

$$\frac{dx_2'}{dt} = \frac{dx_2}{dt}$$

$$\frac{dx_1'}{dt} \approx \left. \frac{\partial f_1}{\partial x_1} \right|_{ss} x_1' + \left. \frac{\partial f_1}{\partial x_2} \right|_{ss} x_2' + \left. \frac{\partial f_1}{\partial u_1} \right|_{ss} u_1'$$

$$+ \left. \frac{\partial f_1}{\partial u_2} \right|_{ss} u_2'$$

$$\frac{dx_2'}{dt} = \left. \frac{\partial f_2}{\partial x_1} \right|_{ss} x_1' + \left. \frac{\partial f_2}{\partial x_2} \right|_{ss} x_2' + \left. \frac{\partial f_2}{\partial u_1} \right|_{ss} u_1'$$

$$+ \left. \frac{\partial f_2}{\partial u_2} \right|_{ss} u_2'$$

$$\begin{bmatrix} x_1' \\ x_2' \end{bmatrix} = \underbrace{\begin{bmatrix} -0.4 & 0 \\ 0.2 & -0.2 \end{bmatrix}}_A \begin{bmatrix} x_1' \\ x_2' \end{bmatrix} + \underbrace{\begin{bmatrix} 0.5 & 0.2 \\ 0.5 & 0 \end{bmatrix}}_B \begin{bmatrix} u_1' \\ u_2' \end{bmatrix}$$

$$x'(t) = \underbrace{e^{At}}_{FF} x'(0) + \int_0^t e^{A(t-\tau)} B u(\tau) d\tau$$

» symc t

» $A = [-0.4 \ 0; 0.2 \ -0.2];$

» $\text{expm}At = \text{expm}(A*t)$

» $x_0 = [1; 1]$

» $x_u = \text{expm}At * x_0$

» $\text{fplot}(x_u, [0, 20])$

FORCE - FREE
RESPONSE

DISCOVER IN CLASS how to do
THE FORCED RESPONSE