

Analysis and Discretization of Time-Domain Impedance Boundary Conditions in Aeroacoustics

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Motivation: noise reduction



Fig. Trent 900 (A380). Inlet lined with a sound absorbing material.

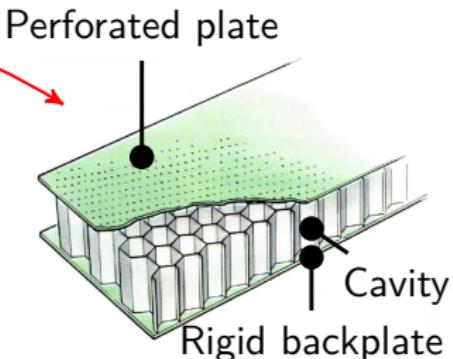


Fig. Example of liner.

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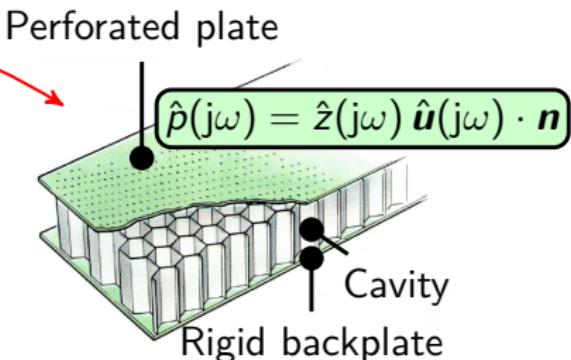


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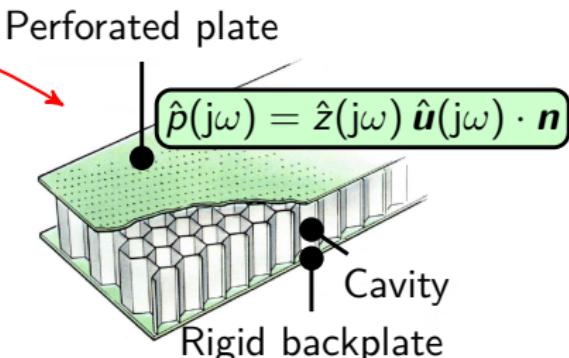


Fig. Example of liner.

Time-harmonic (ω) or time-domain (t) formulation?

Pros of a time-domain formulation (Tam 2012)

- Broadband sources
- Nonlinear PDE (CFD)
- Nonlinear absorption
- + Theoretical interest

⇒ **Objective** Time-domain **impedance** boundary condition (IBC).

Outline

1

Introduction

- Applicability and admissibility of IBCs
- Existing impedance models
- Objectives

Outline

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Introduction

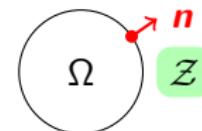
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IBC: Definition and applicability

PDE of interest

$$\partial_t \begin{pmatrix} \mathbf{u} \\ p \end{pmatrix} + \sum_{i=1}^d A_i \partial_{x_i} \begin{pmatrix} \mathbf{u} \\ p \end{pmatrix} = 0 \quad \text{on } \Omega$$

with IBC on $\partial\Omega$.



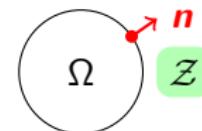
Definition of an impedance boundary condition (IBC)

$$p = \mathcal{Z}(\mathbf{u} \cdot \mathbf{n})$$

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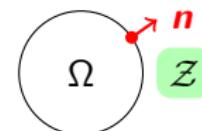
$$p = \mathcal{Z}(\mathbf{u} \cdot \mathbf{n}) \quad \xrightarrow{\text{LTI}} \quad p(t) = \left[z \star_t \mathbf{u} \cdot \mathbf{n} \right] (t)$$

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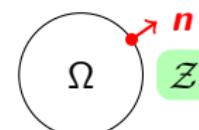
$$\mathbf{u} \cdot \mathbf{n} = \mathcal{Y}(p) \quad \xrightarrow{\text{LTI}} \quad \mathbf{u} \cdot \mathbf{n} = \mathcal{Y}_t \star p$$

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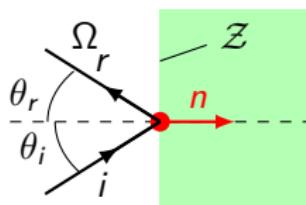
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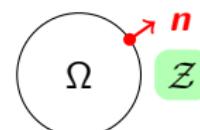
Applicability Only to locally reacting surfaces (Kinsler et al. 1962, § 6.7).



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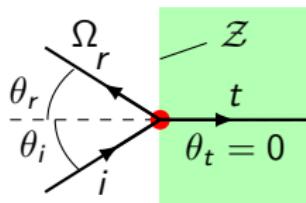
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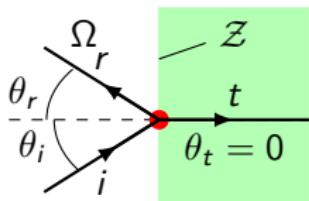
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⇒ Properties of \mathcal{Z}, \mathcal{B} and \mathcal{Y}, β ?

IBC: Admissibility conditions

Intuition: an **admissible** IBC dissipates energy at $\partial\Omega$.

Admissibility conditions from System Theory: $u \mapsto \mathcal{Z}(u)$ is admissible if
(Beltrami et al. 1966; Zemanian 1965)

- real-valued
- passive
- causal

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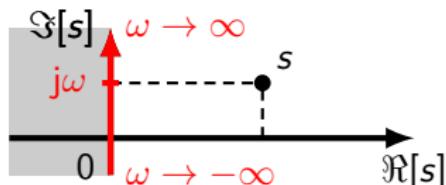
Characterization in the linear time-invariant (LTI) case

$u \mapsto \int_t^\infty z(t) u(t) dt$ is admissible $\Leftrightarrow \hat{z}(s)$ is a positive-real function.

$$\Leftrightarrow \hat{\beta}(s) = \frac{\hat{z}(s) - 1}{\hat{z}(s) + 1} \text{ is a bounded-real function}$$

Laplace transform:

$$\hat{z}(s) := \int_0^\infty z(t) e^{-st} dt \quad (\Re[s] > 0)$$



\Rightarrow What do impedance models look like ?

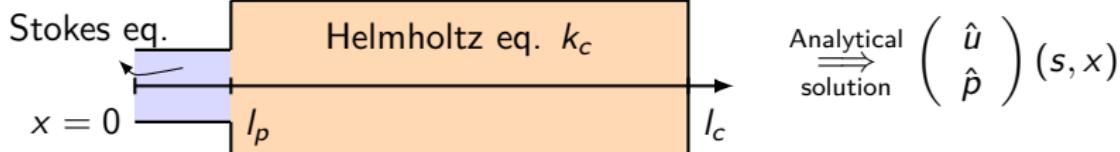
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Physical models: linear acoustics

1D modeling of SDOF liner

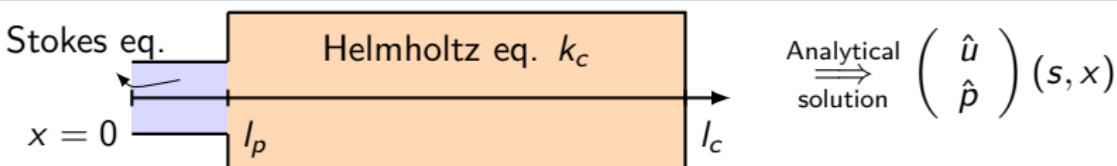


$$\hat{z}_{\text{phys}}(s) = \frac{1}{\sigma_p} \frac{\hat{p}(0)}{\hat{u}(0)}$$

,

Physical models: linear acoustics

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$$\begin{aligned}\hat{z}_{\text{phys}}(s) &= \frac{1}{\sigma_p} \frac{\hat{p}(0)}{\hat{u}(0)} \simeq \frac{1}{\sigma_p} \hat{z}_{\text{perf}}(s) + \frac{1}{\sigma_c} \coth(jk_c(s) l_c) \\ &= a_0 + a_{1/2} \sqrt{s} + a_1 s + \frac{1}{\sigma_c} \coth(b_0 + b_{1/2} \sqrt{s} + b_1 s),\end{aligned}$$

where fractional terms are linked to viscothermal diffusion

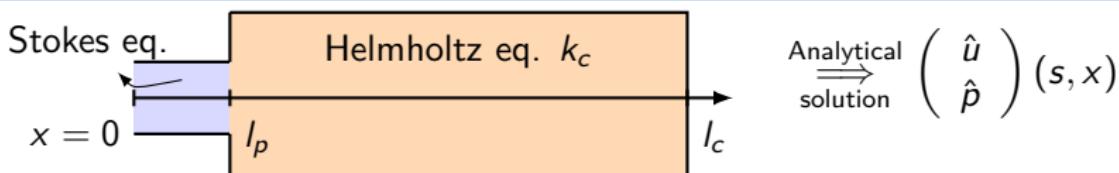
$$a_{1/2}, b_{1/2} \propto \sqrt{\nu}.$$

⇒ Corrections

⇒ Expression of $\hat{z}_{\text{phys}}(s)$ readily follows

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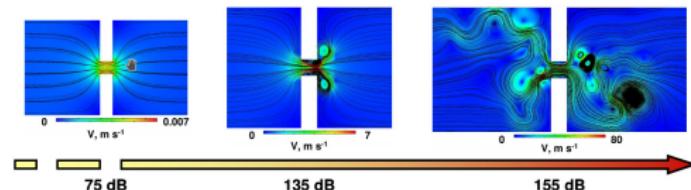
Departure from linear acoustics:

- ① nonlinear absorption mechanisms

- ② base flow effects
(aeroacoustics)

Physical models: nonlinear acoustics & grazing flow

Phenomenon 1 High incident amplitude \Rightarrow Vortex shedding

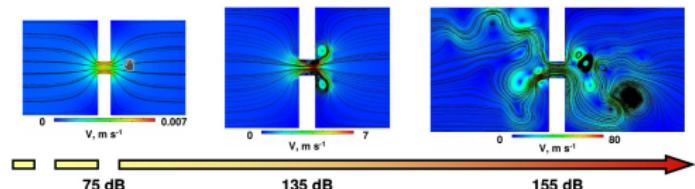


Acoustic field with increasing incident sound pressure (DNS). (Roche 2011)

Modeling

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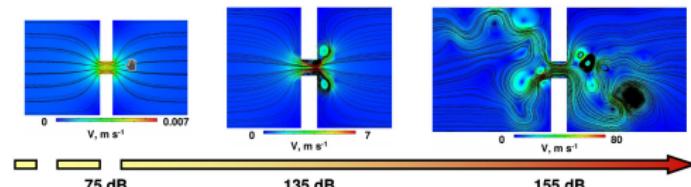
Modeling Nonlinear operator \mathcal{Z} (Cummings 1986; Meissner 1999):

$$\mathcal{Z}(\mathbf{u} \cdot \mathbf{n}) = \rho_0 C_{\text{nl}} |\mathbf{u} \cdot \mathbf{n}| \mathbf{u} \cdot \mathbf{n}, \quad C_{\text{nl}} \geq 0.$$

- Evidence: theoretical (Rienstra et al. 2018) & numerical (Zhang et al. 2016)
- Expression of $\mathcal{B} = (\mathcal{Z} - \mathcal{I}) \circ (\mathcal{Z} + \mathcal{I})^{-1}$

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Phenomenon 2 Grazing flow $u_0 \neq 0 \Rightarrow$ Impedance \hat{z}_{exp} varies

Modeling Empirical & linear impedance correction $\hat{z}_{\text{corr}}(s, u_{0*})$
(Cummings 1986)

Working assumption IBC remains locally reacting and

$$\hat{z}_{\text{phys}}(s) = \hat{z}_{\text{phys}}(s, \mathbf{u}_0)$$

Numerical models

Components of a numerical “time-domain IBC” (TDIBC):

- ① Discrete model \mathcal{Z}_{num}
- ② Algorithm to evaluate $\mathcal{Z}_{\text{num}}(u)$
- ③ (Semi)-discrete formulation
(i.e. coupling with PDE)

Challenges of numerical simulations with IBC given by \mathcal{Z}_{num} :

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- Memory / CPU cost
- Agreement btw \mathcal{Z}_{num} & $\mathcal{Z}_{\text{phys}}$

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Early works: (Davis 1991), (Tam et al. 1996), (Özyörük et al. 1998).

Common models EHR (Rienstra 2006)

$$\hat{\mathcal{Z}}_{\text{num}}(s) = a_0 + a_1 s + a_2 \coth(b_0 + b_1 s)$$

Multipole (Fung et al. 2001)

$$\hat{\mathcal{Z}}_{\text{num}}(s) = \sum_{k=1}^N \frac{r_k}{s - s_k}$$

⇒ Discretization (Chevaugeon et al. 2006)

⇒ “Recursive” convolution
⇒ ODE (Bin et al. 2009)

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Objectives

State of the art

- Physical \neq numerical models
- Numerical models mostly linear
- Admissibility & stability explored by different communities

Objectives

Consider physical, computational, and mathematical aspects of IBCs.

- (a) Time-domain structure of physical impedance models?
- (b) Well-posedness and stability?
- (c) Discretization?
- (d) Nonlinear absorption mechanisms?

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|----------|---|
| Intro | Admissibility and examples of IBCs |
| Part I | Time-domain analysis of physical models |
| Part II | Discontinuous Galerkin discretization |
| Part III | Stability of wave equation |

Part I: objectives and contributions

Objective Time-domain expression of linear physical models \hat{z}_{phys}

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Objective Time-domain expression of linear physical models \hat{z}_{phys}

Principle \hat{z}_{phys} can be expressed using two simpler kernels:

Time delay

$$e^{-s\tau}$$

Oscillatory-diffusive (OD)

$$\hat{h}(s)$$

⇒ Enables to deduce discrete model \hat{z}_{num} **from** \hat{z}_{phys}

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Contributions of Chapter 2:

- ① Characterization of OD kernels h
- ② Discretization of OD kernels h (quadrature method)
- ③ Application to physical models \hat{z}_{phys} , \hat{y}_{phys} , $\hat{\beta}_{\text{phys}}$

Outline

- ② Physical impedance models in the time domain
 - Application to CT impedance model

Application to CT model: representation

Application to a CT liner impedance model ($z_c, \sigma_c = 1$):

$$\hat{z}_{\text{phys}}(s) = \coth(\overbrace{b_0 + b_{1/2}\sqrt{s} + b_1 s}^{:=jk_c(s)}) \quad (\Re(s) > 0),$$

with $b_1 > 0$, $b_0, b_{1/2} \geq 0$.

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with $\hat{h} \in \mathcal{C}((0, \infty))$ and $e^{-\kappa t} \hat{h} \in L^1(0, \infty)$ for any $\kappa > 0$.

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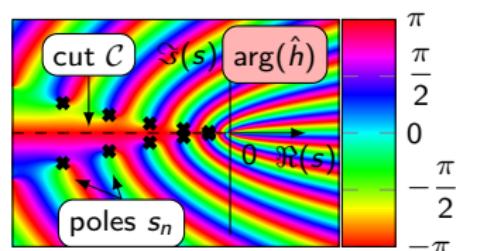
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Oscillatory-diffusive representation

$$\hat{h}(s) = \underbrace{\sum_{k \in \mathbb{Z}} \frac{r_k}{s - s_k}}_{\text{oscillatory part (poles } s_k \text{)}} + \underbrace{\int_0^\infty \frac{\mu(\xi)}{s + \xi} d\xi}_{\text{diffusive part (cut)}}$$



- 3 components: Delay / Oscillatory / Diffusive

Application to CT model: realization

Two steps to express $z_{\text{phys}} \star u(t) = u(t) + h \star u(t - \tau)$.

(1) Oscillatory-Diffusive

(2) Delay

Application to CT model: realization

Two steps to express $z_{\text{phys}} * u(t) = u(t) + h * u(t - \tau)$.

(1) Oscillatory-Diffusive Convolution expressed with diffusive variable φ

$$h * u(t) = \sum_{k \in \mathbb{Z}} r_k \varphi(t, -s_k) + \int_0^\infty \varphi(t, \xi) \mu(\xi) d\xi,$$

which can be computed through first-order ODEs

$$\partial_t \varphi(t, x) = -x \varphi(t, x) + u(t), \quad \varphi(t=0, x) = 0 \iff \varphi(t, x) := e^{-xt} * u.$$

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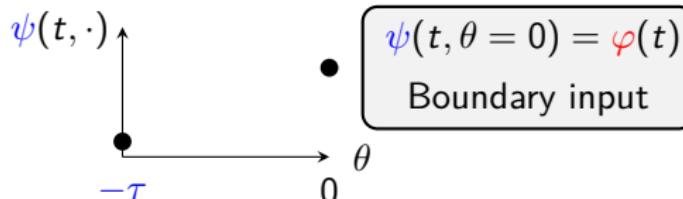
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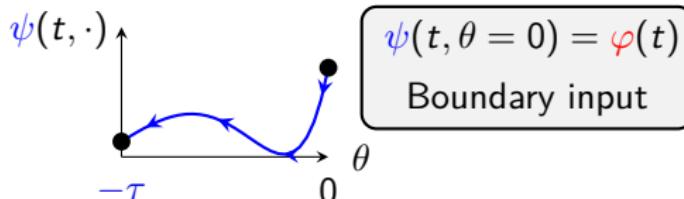
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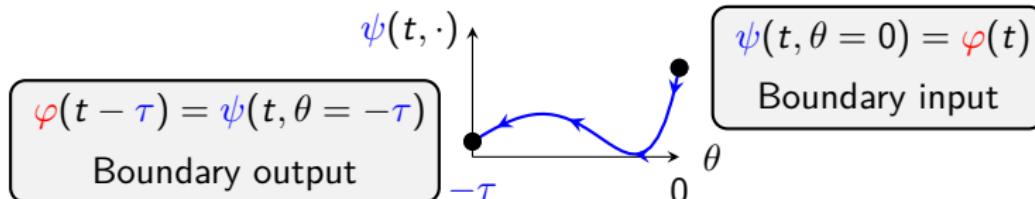
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Application to CT model: discretization

The representation of \hat{z}_{phys} suggests

$$\hat{z}_{\text{num}}(s) := 1 + e^{-\tau s} \hat{h}_{\text{num}}(s), \quad \hat{h}_{\text{num}}(s) = \sum_{k=1}^{N_s} \frac{r_k}{s - s_k} + \sum_{k=1}^{N_\xi} \frac{\mu_k}{s + \xi_k}$$

Time-local computation of $z_{\text{num}} \star u$ through

PDE \circ ODE, $(N_\psi + 1) \times (N_s + N_\xi)$ variables

Application to CT model: discretization

The representation of \hat{z}_{phys} suggests

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Oscillatory-Diffusive Cost function

$$J(r_k, \mu_k, \xi_k, s_k) = \sum_{k=1}^K |\hat{h}(j\omega_k) - \hat{h}_{\text{num}}(j\omega_k)|^2$$

- ① Choose ξ_k , compute s_k and $r_k = \text{Res}(\hat{h}, s_k)$
- ② Compute $\mu_k = \operatorname{argmin} J(r_k, \cdot, \xi_k, s_k)$
- ③ (If still needed) adjust $\|\hat{z}_{\text{num}} - \hat{z}\|_2$ against experimental data

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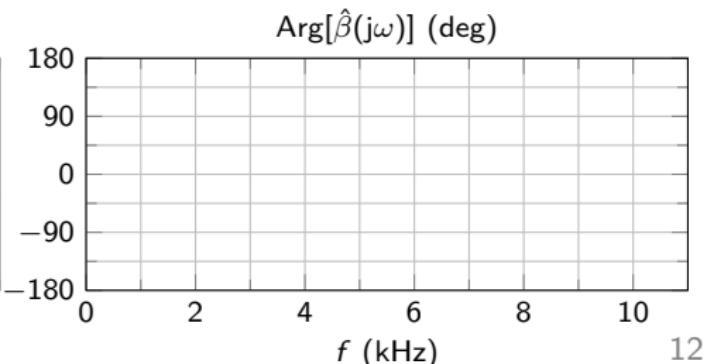
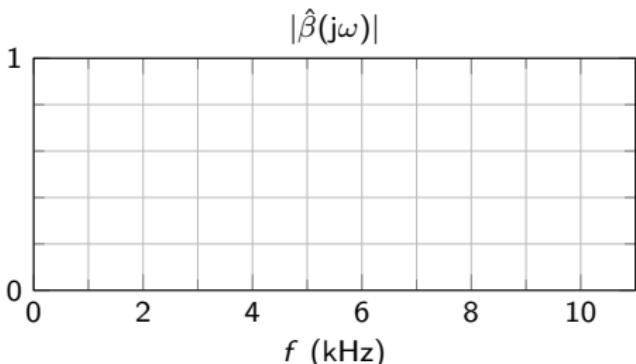
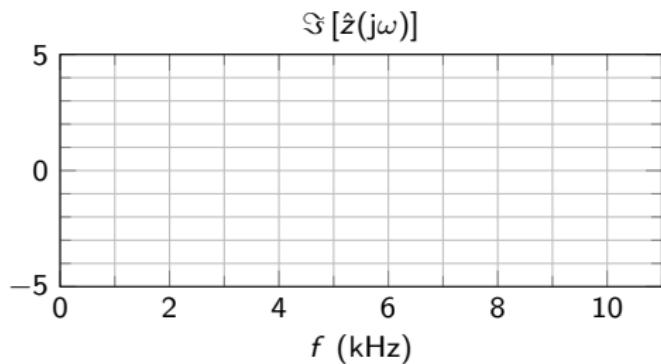
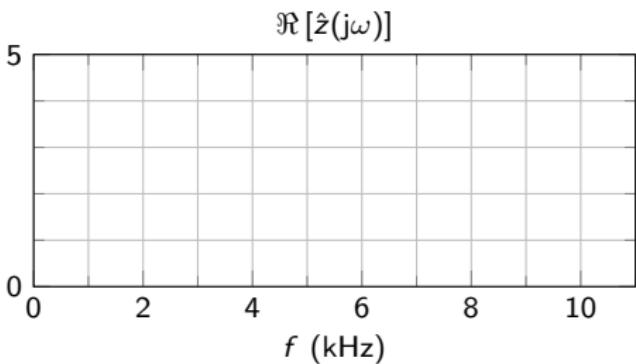
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Delay Discontinuous Galerkin (DG) of order N_ψ on $(-\tau, 0)$

$$\text{PPW}(f) := \frac{N_\psi}{\tau f}$$

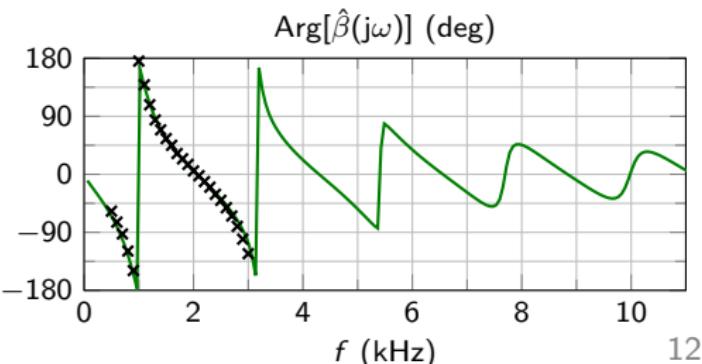
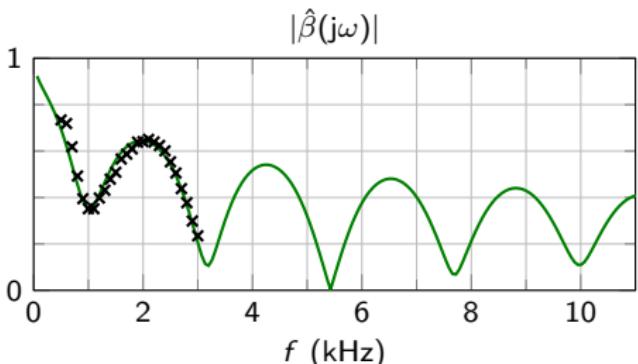
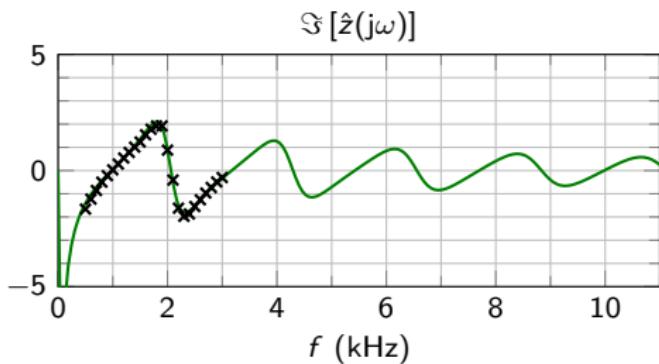
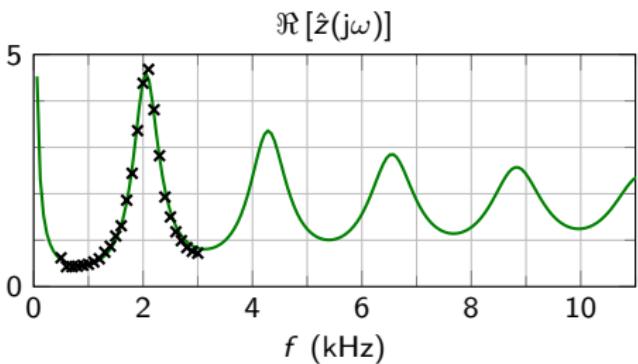
Application to CT model: illustration

$$\hat{z}_{\text{phys}}(j\omega) \simeq 1 + e^{-\tau j\omega} \left[\sum_{k=1}^{N_s} \frac{r_k}{j\omega - s_k} + \sum_{k=1}^{N_\xi} \frac{\mu_k}{j\omega + \xi_k} \right] =: \hat{z}_{\text{num}}(j\omega)$$



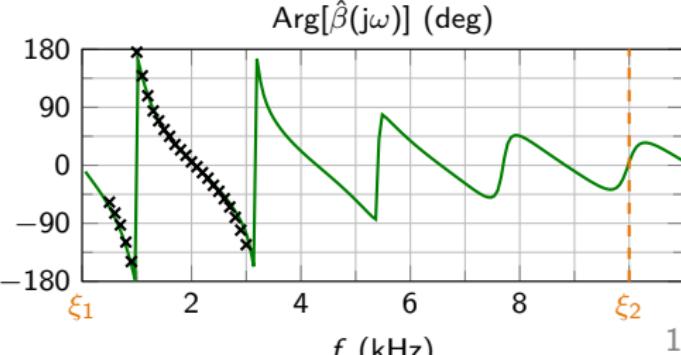
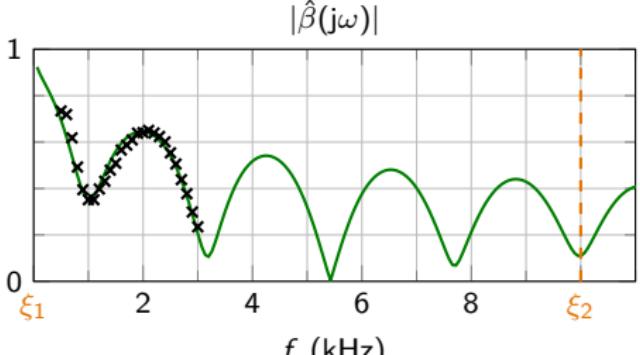
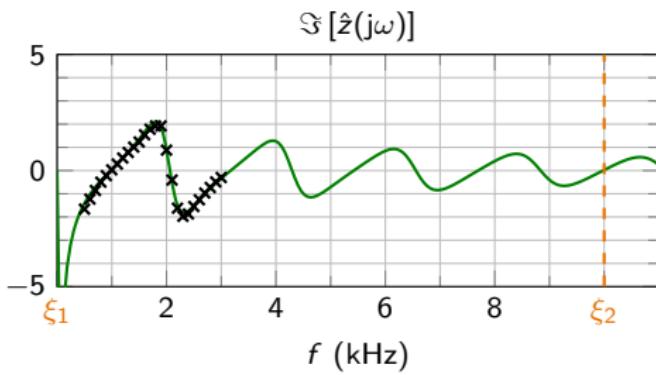
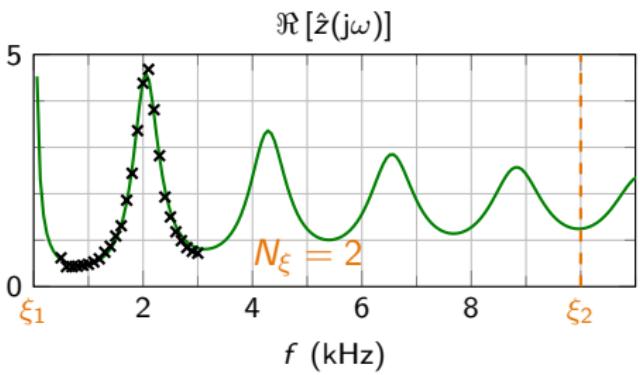
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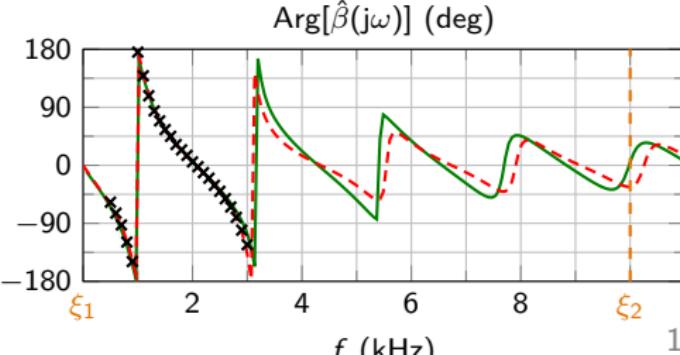
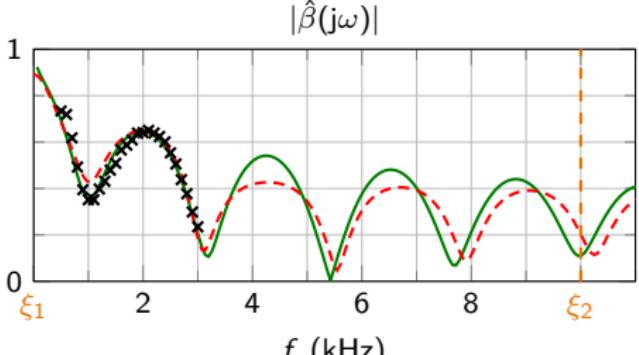
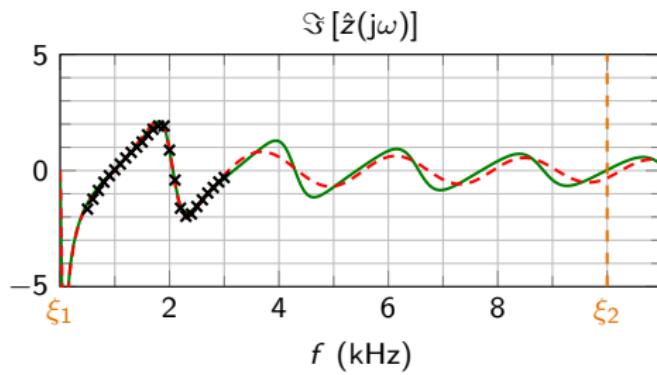
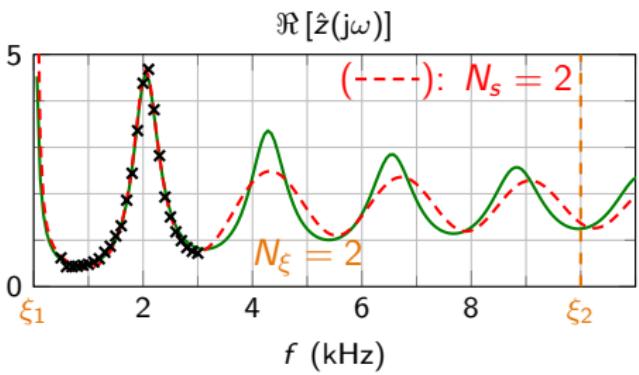
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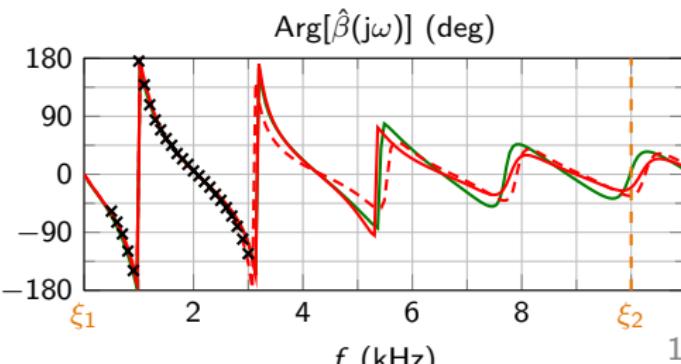
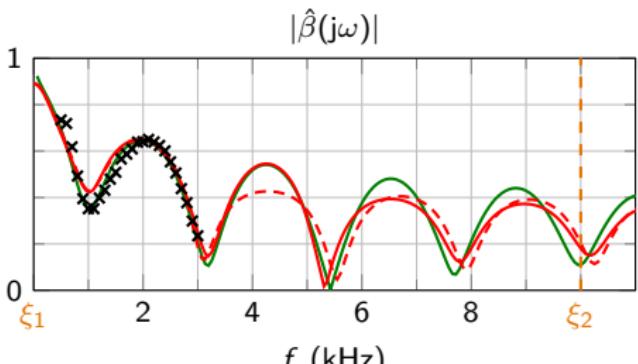
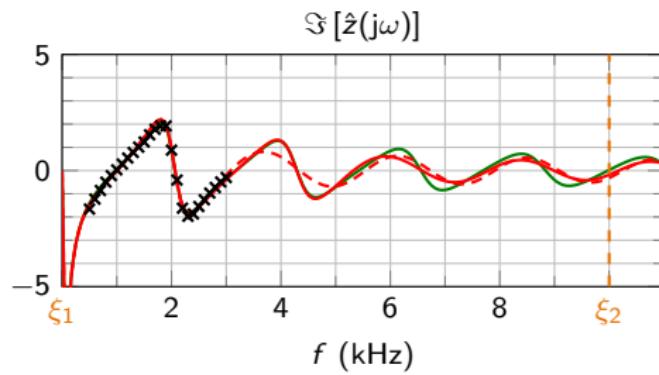
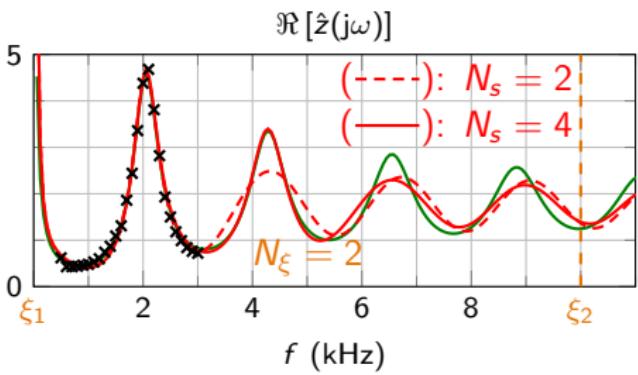
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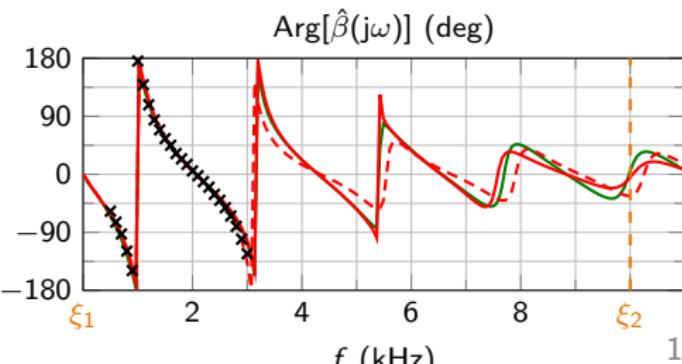
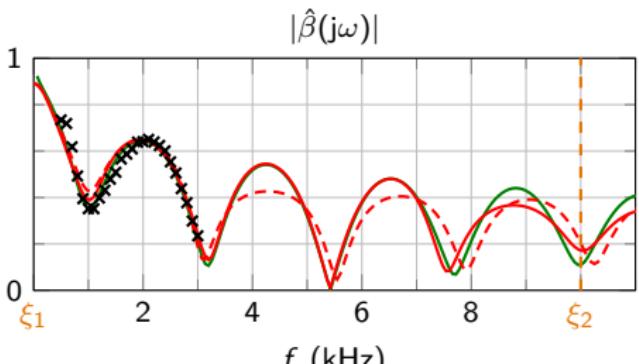
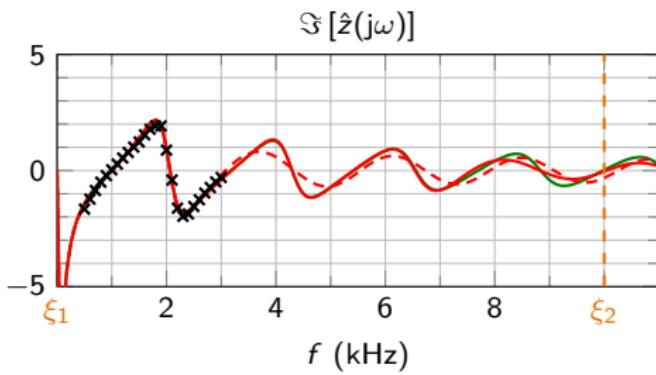
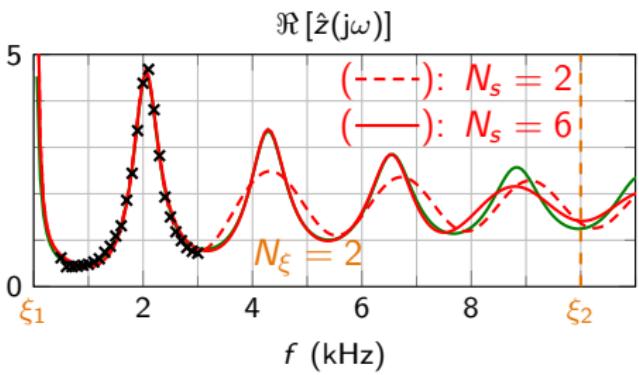
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Summary of Part I: Model analysis

Questions addressed in Part I

- (a) Structure of physical impedance models?
- (b) Well-posedness and stability?
- (c) Discretization?
- (d) Nonlinear absorption mechanisms?

Contributions (Chapter 2)

- ① Characterization of OD kernels h
- ② Discretization of OD representation (quadrature method)
- ③ Application to physical models \hat{z}_{phys} , \hat{y}_{phys} , $\hat{\beta}_{\text{phys}}$

⇒ Part II: Discretization with Discontinuous Galerkin

Part II: Objectives and contributions

Linearized Euler equations on $(0, T) \times \Omega$, $\Omega \subset \mathbb{R}^d$

$$\begin{cases} \partial_t p + (\mathbf{u}_0 \cdot \nabla) p + c_0 \nabla \cdot \mathbf{u} + \gamma p \nabla \cdot \mathbf{u}_0 = 0 \\ \partial_t \mathbf{u} + (\mathbf{u}_0 \cdot \nabla) \mathbf{u} + c_0 \nabla p + (\mathbf{u} \cdot \nabla) \mathbf{u}_0 + p(\mathbf{M}_0 \cdot \nabla) \mathbf{u}_0 = 0 \end{cases}$$

with IBC on $\Gamma_z \subset \partial\Omega$, $\mathbf{M}_0 = \mathbf{u}_0/c_0$.

Objective Discretization with Discontinuous Galerkin (DG) method

Contributions of Chapters 5 and 6:

① Continuous, (Semi)-discrete energy analysis

⇒ Computational advantage of β, \mathcal{B} over z, \mathcal{Z}

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- ② Numerical validation
on impedance tube

→ β

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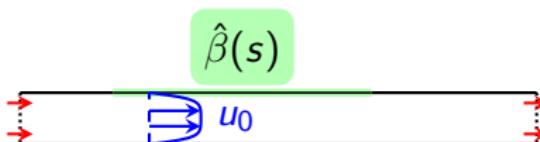
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- ③ Numerical application
in duct aeroacoustics



Outline

3

DG discretization of IBCs

- Energy analysis
- Validation on nonlinear impedance tube
- Application to duct aeroacoustics

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③ DG discretization of IBCs

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Continuous formulation

LEEs written as **Friedrichs system**: Let $\mathbf{v} := \begin{bmatrix} \mathbf{u} \\ p \end{bmatrix}$

$$\partial_t \mathbf{v} + A(\nabla) \mathbf{v} + B \mathbf{v} = 0, \quad A(\mathbf{n}) = \begin{pmatrix} (\mathbf{u}_0 \cdot \mathbf{n}) \mathbb{I}_d & c_0 \mathbf{n} \\ c_0 \mathbf{n}^\top & \mathbf{u}_0 \cdot \mathbf{n} \end{pmatrix}$$

Continuous **energy balance**:

$$\frac{1}{2} \frac{d}{dt} \|\mathbf{v}(t)\|_{L^2(\Omega)}^2 = -\frac{1}{2} (C(\mathbf{u}_0) \mathbf{v}, \mathbf{v})_{L^2(\Omega)} - \frac{1}{2} (A(\mathbf{n}) \mathbf{v}, \mathbf{v})_{L^2(\partial\Omega)}$$

with boundary term

$$(A(\mathbf{n}) \mathbf{v}, \mathbf{v})_{L^2(\partial\Omega)} = \int_{\partial\Omega} (\mathbf{u}_0 \cdot \mathbf{n}) [p^2 + |\mathbf{u}|^2] + 2c_0 \int_{\partial\Omega} p(\mathbf{u} \cdot \mathbf{n})$$

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Assumption $\mathbf{u}_0 \cdot \mathbf{n} = 0$ at the impedance boundary Γ_z .

⇒ Due to this assumption, an admissible **IBC** yields

$$\int_0^t (A(\mathbf{n}) \mathbf{v}, \mathbf{v})_{L^2(\Gamma_z)} d\tau \geq 0 \quad (t > 0).$$

Uniqueness in $e^{-\kappa t} C((0, \infty); H^1(\Omega)^{d+1})$: well-posedness? (Chapter 3)

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Continuous problem $\partial_t \boldsymbol{v} + \mathcal{A}\boldsymbol{v} = 0$ with $\boldsymbol{v} := \begin{bmatrix} \boldsymbol{u} \\ p \end{bmatrix}$.

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 $V_h := \mathbb{P}_n^k(\mathcal{T}_h)^{n+1}$ (Di Pietro et al. 2012; Ern et al. 2006)

$$\mathbb{P}_n^k(\mathcal{T}_h) := \left\{ v \in L^2(\Omega) \mid \forall T \in \mathcal{T}_h, v|_T \in \mathbb{P}_n^k(T) \right\}.$$

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Semi-discrete problem Find $\mathbf{v}_h \in \mathcal{C}^1([0, \infty), V_h)$ such that

$$\partial_t \mathbf{v}_h + \mathcal{A}_h \mathbf{v}_h = 0,$$

where $\mathcal{A}_h : V_h \rightarrow V_h$ is defined by $\forall \mathbf{w}_h \in V_h$,

$$(\mathcal{A}_h \mathbf{v}_h, \mathbf{w}_h)_{L^2(\Omega)} := \underbrace{\sum_{T \in \mathcal{T}_h} (\mathcal{A} \mathbf{v}_h, \mathbf{w}_h)_{L^2(T)}}_{\text{weak formulation on } T} + \underbrace{\left((A(\mathbf{n}) \mathbf{v}_h)^* - A(\mathbf{n}) \mathbf{v}_h, \mathbf{w}_h \right)_{L^2(\partial T)}}_{\text{weak coupling}}$$

Objective Definition of numerical flux $(A(\mathbf{n}) \mathbf{v}_h)^*$ to weakly enforce impedance boundary condition at Γ_z ?

Weak enforcement of IBCs

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Objective Definition of numerical flux $(A(\mathbf{n})\mathbf{v}_h)^*$ to weakly enforce impedance boundary condition at Γ_z ?

⇒ Centered flux with ghost state \mathbf{v}^g

$$(A(\mathbf{n})\mathbf{v})^* := \frac{1}{2} A(\mathbf{n})\mathbf{v} + \frac{1}{2} A(\mathbf{n})\mathbf{v}^g, \quad \text{with } \mathbf{v}^g = \mathbf{v}^g(\mathbf{n}, \mathcal{Z}(\mathbf{v}), \mathbf{v}).$$

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Definition of admissibility conditions

The flux $(A(\mathbf{n})\mathbf{v})^*$ is said to be *admissible* if it is both consistent and passive.

- (Consistency) Let $\mathbf{v}(t) \in V$ be the exact solution.
- (Passivity) $\forall \mathbf{v}_h(t) \in V_h, t > 0,$

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- + desirable continuity conditions as " $\mathcal{Z}(\mathbf{v}) \rightarrow 0$ " or " $\mathcal{Z}(\mathbf{v}) \rightarrow \infty$ ".

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Results

- Consistent and unstable fluxes are possible
- 3 fluxes based on \mathcal{Z} , \mathcal{Y} , \mathcal{B}
- \mathcal{Y} may be preferable to \mathcal{Z}
- "Ideal": scattering operator $\mathcal{B} := (\mathcal{Z} - \mathcal{I}) \circ (\mathcal{Z} + \mathcal{I})^{-1}$

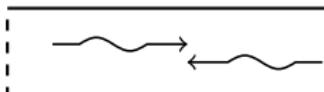
Outline

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DG discretization of IBCs

- Energy analysis
- Validation on nonlinear impedance tube
- Application to duct aeroacoustics

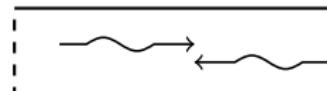
Validation: nonlinear impedance tube

 \mathcal{B}

| Space: ArtimonDG(4)
| Time: LSERK (8,4)
|(Toulorge et al. 2012)

- Analytical solution even with nonlinear $\mathcal{B} \Rightarrow$ enables validation

Validation: nonlinear impedance tube

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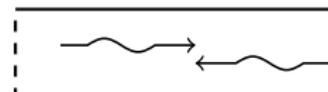
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$$\mathcal{Z}_C(u) = a_0 u + \frac{C_{\text{nl}}}{c_0} |u| u$$

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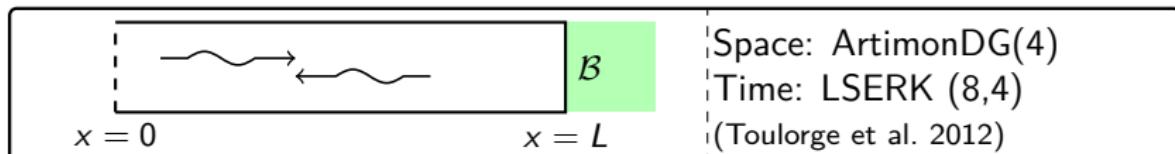
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$$\mathcal{B}_C(v) = \beta_0 \frac{2v}{\Phi(v)} + \frac{C_{\text{nl}}}{c_0 (a_0 + 1)^2} \frac{4|v|v}{\Phi(v)^2}, \quad \Phi(v) = 1 + \sqrt{1 + 4 \frac{C_{\text{nl}}}{c_0 (a_0 + 1)^2} |v|}.$$

$$\Rightarrow \mathcal{B}_C(v) \leq v.$$

Validation: nonlinear impedance tube

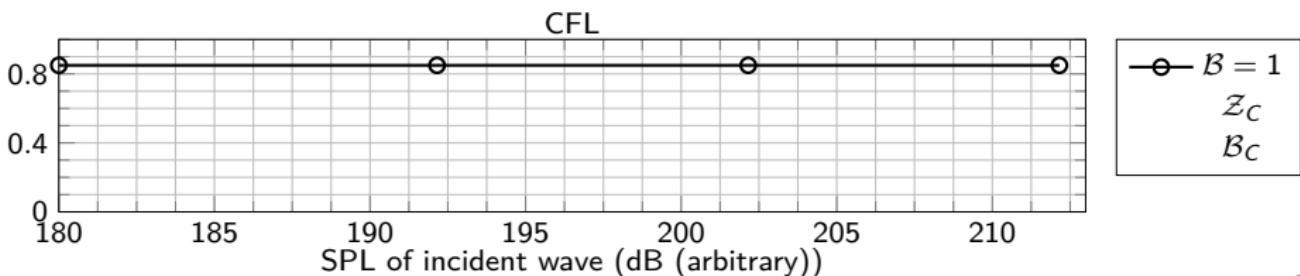


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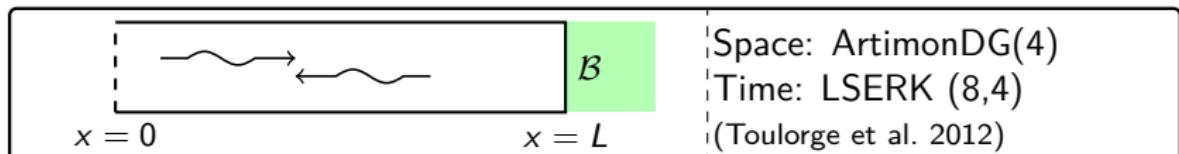
Focus on algebraic model given by $\mathcal{Z}_C(u) = a_0 u + \frac{C_{\text{nl}}}{c_0} |u|u$ and

$$\mathcal{B}_C(v) = \beta_0 \frac{2v}{\Phi(v)} + \frac{C_{\text{nl}}}{c_0 (a_0 + 1)^2} \frac{4|v|v}{\Phi(v)^2}, \quad \Phi(v) = 1 + \sqrt{1 + 4 \frac{C_{\text{nl}}}{c_0 (a_0 + 1)^2} |v|}.$$

$\Rightarrow \mathcal{B}_C(v) \leq v$. Differences between \mathcal{Z} and \mathcal{B} fluxes?



Validation: nonlinear impedance tube

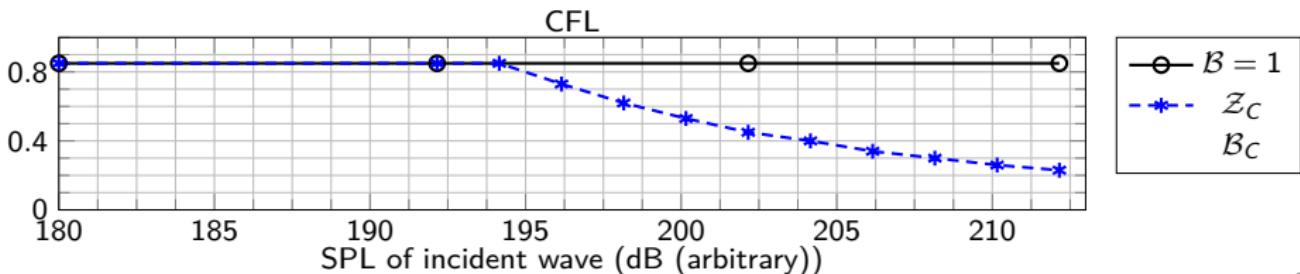


- Analytical solution even with nonlinear \mathcal{B} \Rightarrow enables validation

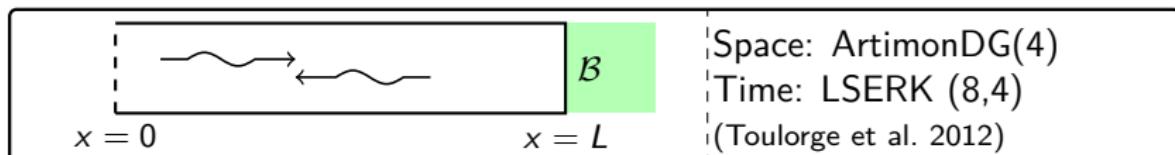
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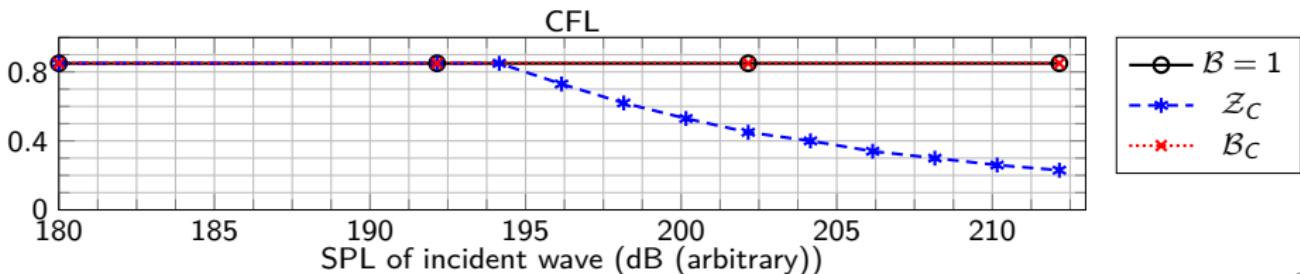


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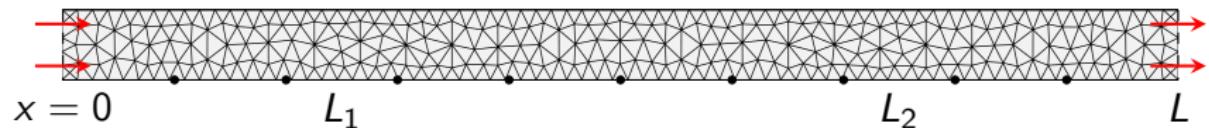
Outline

3

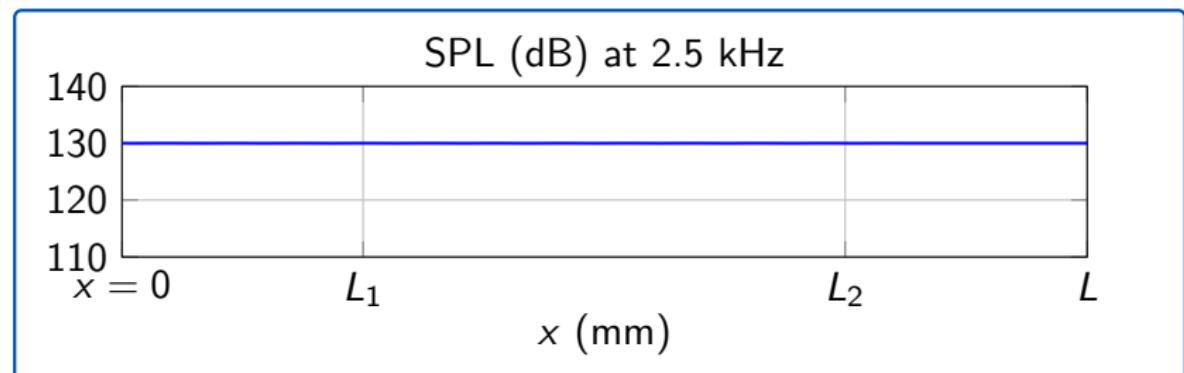
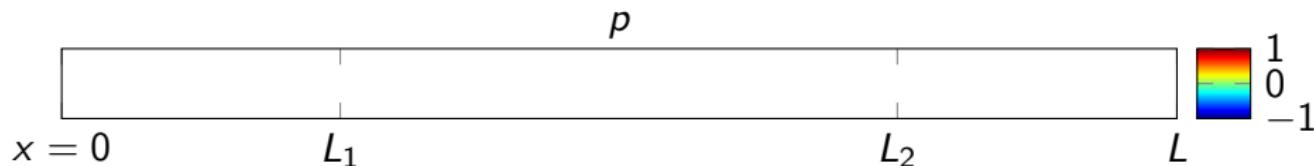
DG discretization of IBCs

- Energy analysis
- Validation on nonlinear impedance tube
- Application to duct aeroacoustics

Aeroacoustical duct: overview

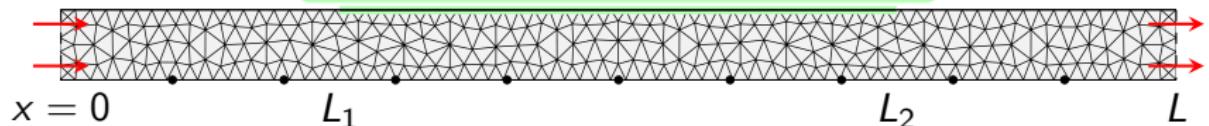


ArtimonDG(4). 552 triangles. CFL = 0.5. LSERK (8,4) (Toulorge et al. 2012)

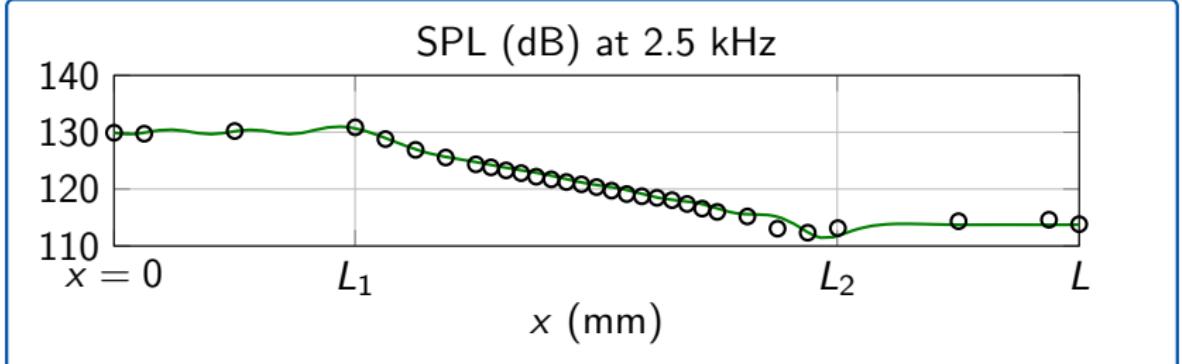
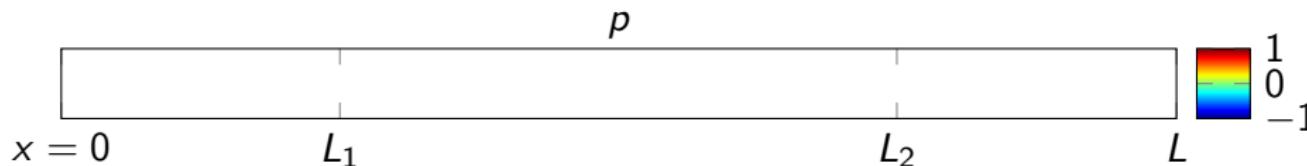


Aeroacoustical duct: overview

$\hat{\beta}_a(s)$ (liner CT57 – NASA Langley)

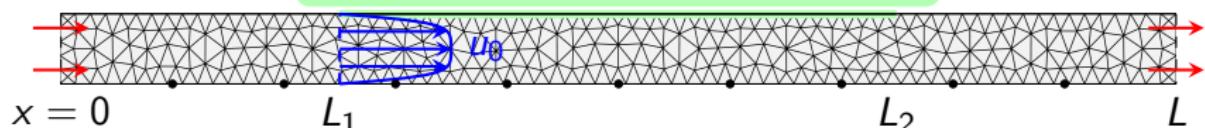


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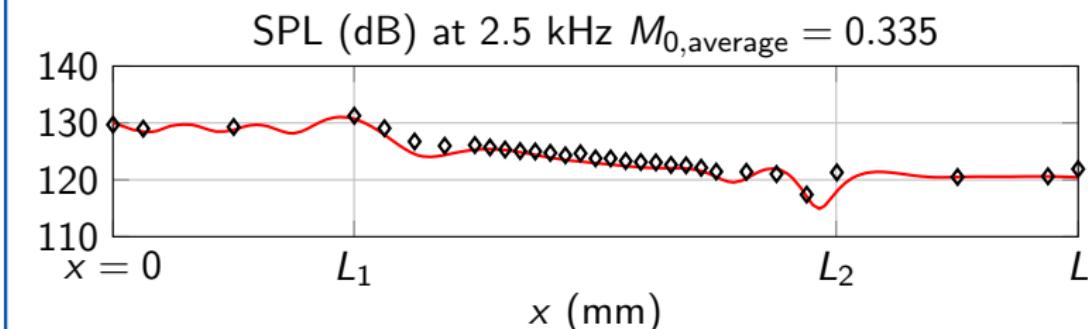
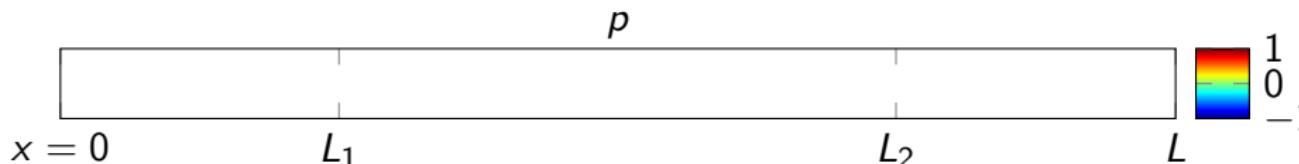


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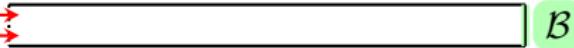
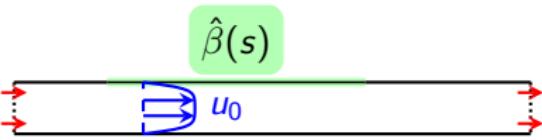


Summary of Part II: Discontinuous Galerkin discretization

Questions addressed in Part II

- (a) Structure of physical impedance models?
- (b) Well-posedness and stability?
- (c) **Discretization?**
- (d) **Nonlinear absorption mechanisms?**

Contributions (Chapters 5&6)

- ① Continuous, (Semi)-discrete energy analysis
⇒ Computational advantage of β, \mathcal{B} over z, \mathcal{Z}
- ② Numerical validation on  \mathcal{B}
- ③ Numerical application in  $\hat{\beta}(s)$
duct aeroacoustics

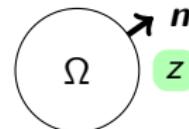
⇒ Part III: Stability of wave equation with IBC

Part III: objectives and contributions

Cauchy problem Let $\Omega \subset \mathbb{R}^d$ be a C^∞ bounded open set.

$$\partial_t \begin{pmatrix} \mathbf{u} \\ p \end{pmatrix} + \begin{pmatrix} \nabla p \\ \operatorname{div} \mathbf{u} \end{pmatrix} = \mathbf{0}$$

with $p = z \star \int_t^{\infty} \mathbf{u} \cdot \mathbf{n}$ on $\partial\Omega$.



Contribution Asymptotic stability: $\forall X_0, \|X(t)\|_H \xrightarrow{t \rightarrow \infty} 0$

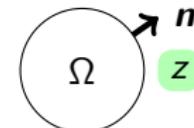
Strategy (Intuition)

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where \hat{Z} is strictly proper rational and $\hat{z}_{\text{diff},i} \in L^1_{\text{loc}}$ completely monotone.

Limitation Each term is positive-real: $\tau > 0, z_\tau \in \mathbb{R}, z_0 \geq |z_\tau|, z_1 > 0$.

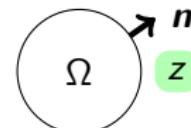
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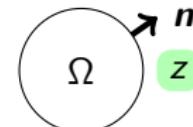
- ① Find dynamical system in state-space Φ to compute $z \star \mathbf{u} \cdot \mathbf{n}$
- ② Formulate an extended Cauchy problem
 $\dot{X} = \mathcal{A}X$, with extended state $X = (\mathbf{u}, p, \varphi) \in L^2(\Omega)^{n+1} \times L^2(\partial\Omega; \Phi)$.
- ③ Study energy balance: $\dot{\mathcal{E}} = \dot{\mathcal{E}}_{\text{ac}} + \dot{\mathcal{E}}_\Phi \leq 0$, use Lümer-Phillips.
- ④ Inspect $\sigma(\mathcal{A})$, if needed for stability.

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Outline

4 Stability of wave equation with IBCs

- Diffusive impedance
- Delay impedance

Outline

④ Stability of wave equation with IBCs

- Diffusive impedance
- Delay impedance

Standard diffusive impedance: setup

Kernel Let $\mu \geq 0$ Radon measure s.t. $\int(1 + \xi)^{-1} d\mu(\xi) < \infty$.

$$\hat{z}(s) := \hat{z}_{\text{diff}}(s) = \int_0^\infty \frac{1}{s + \xi} d\mu(\xi).$$

Setup

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\Rightarrow Realization of $\mathbf{z} \star u$ has an energy balance in \mathcal{V}_0 where

$$\mathcal{V}_s := \left\{ \varphi : (0, \infty) \rightarrow \mathbb{C} \text{ measurable} \mid \int_0^\infty |\varphi(\xi)|^2 (1 + \xi)^s d\mu(\xi) < \infty \right\}.$$

Setup

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Setup Energy space: $H := \nabla H^1(\Omega) \times L^2(\Omega) \times L^2(\partial\Omega; V_0)$

$$X := \begin{pmatrix} \mathbf{u} \\ p \\ \varphi \end{pmatrix}, \quad \mathcal{A}X := \begin{pmatrix} -\nabla p \\ -\operatorname{div} \mathbf{u} \\ -\xi \varphi + \mathbf{u} \cdot \mathbf{n} \end{pmatrix}$$

$$\mathcal{D}(\mathcal{A}) := \left\{ (\mathbf{u}, p, \varphi) \in H \mid \begin{array}{l} (\mathbf{u}, p, \varphi) \in H_{\operatorname{div}}(\Omega) \times H^1(\Omega) \times L^2(\partial\Omega; V_1) \\ (-\xi \varphi + \mathbf{u} \cdot \mathbf{n}) \in L^2(\partial\Omega; V_0) \\ p = \int \varphi d\mu \text{ in } H^{\frac{1}{2}}(\partial\Omega) \end{array} \right\}$$

Standard diffusive impedance: stability

3 steps to prove **Asymptotic stability** (Arendt et al. 1988; Lyubich et al. 1988)

- ① " \mathcal{A} is dissipative".
- ② " \mathcal{A} is injective".
- ③ " $s\mathcal{I} - \mathcal{A}$ is bijective for $s \in (0, \infty) \cup j\mathbb{R}^*$ ".

Standard diffusive impedance: stability

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- ② " \mathcal{A} is injective". Crucially relies on Hodge decomposition:

$$H_{\text{div}, 0, 0}(\Omega) \cap \nabla H^1(\Omega) = \{0\}, \quad \text{since} \quad (L^2(\Omega))^d = \nabla H^1(\Omega) \oplus H_{\text{div}, 0, 0}(\Omega).$$

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- ③ " $s\mathcal{I} - \mathcal{A}$ is bijective for $s \in (0, \infty) \cup j\mathbb{R}^*$ ". Key step is result below.

Proposition

Let \hat{z} be a positive-real function. Then, $\forall I \in H^{-1}(\Omega)$ and $s \in \mathbb{C}^*$ such that $\Re(s) \geq 0$, there is a unique $p \in H^1(\Omega)$ solving

$$\forall \psi \in H^1(\Omega), \quad (\nabla p, \nabla \psi) + s^2(p, \psi) + \frac{s}{\hat{z}(s)}(p, \psi)_{L^2(\partial\Omega)} = \overline{I(\psi)}, \quad (1)$$

with $\|p\|_{H^1(\Omega)} \leq C(s) \|I\|_{H^{-1}(\Omega)}$.

Ingredients of proof. Fredholm alternative and Rellich identity.

Outline

④ Stability of wave equation with IBCs

- Diffusive impedance
- Delay impedance

Delay impedance: overview

Kernel $\hat{z}(s) = z_0 + z_\tau e^{-\tau s}$ (positive-real iff $z_0 \geq |z_\tau|$)

⇒ Expression of $z \star u$ in $L^2(-\tau, 0)$ through transport equation.

Setup

Asymptotic stability

Delay impedance: overview

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Setup Energy space $H := \nabla H^1(\Omega) \times L^2(\Omega) \times L^2(\partial\Omega; L^2(-\tau, 0))$

$$X := \begin{pmatrix} \mathbf{u} \\ p \\ \psi \end{pmatrix}, \quad \mathcal{A}X := \begin{pmatrix} -\nabla p \\ -\operatorname{div} \mathbf{u} \\ \partial_\theta \psi \end{pmatrix}$$

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Asymptotic stability

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Asymptotic stability

- ① “ \mathcal{A} is dissipative”. This holds iff $z_0 \geq |z_\tau|$.

Summary of Part III: Stability of wave equation with IBC

Questions addressed in Part II

- (a) Structure of physical impedance models?
- (b) Well-posedness and stability?**
- (c) Discretization?
- (d) Nonlinear absorption mechanisms?

Contribution Asymptotic stability: $\forall X_0, \|X(t)\|_H \xrightarrow{t \rightarrow \infty} 0$ with

$$\hat{z}(s) = (z_0 + z_\tau e^{-\tau s}) + z_1 s + \hat{Z}(s) + \hat{z}_{\text{diff},1}(s) + s \hat{z}_{\text{diff},2}(s) \quad (\Re(s) > 0)$$

where \hat{Z} is strictly proper rational and $\hat{z}_{\text{diff},i} \in L^1_{\text{loc}}$ completely monotone.

⇒ Overall conclusion

Main contributions & outlook

Contributions

(a) Structure of physical models?

- Admissibility using System theory
- Characterization of OD kernels h
- Application to physical models \hat{z}_{phys} ,
 \hat{y}_{phys} , $\hat{\beta}_{\text{phys}}$

(b) Well-posedness and stability?

- Asymptotic stability of wave equation with positive-real IBC

(c) Discretization?

- Discretization of OD representation
- Computational advantage of β , \mathcal{B} over z , \mathcal{Z}
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- Computation of algebraic \mathcal{B} and validation in nonlinear impedance tube

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Outlook

- TDIBC for DDOF liners & “exact” acoustical models

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Outlook

- TDIBC for DDOF liners & “exact” acoustical models
- Computation of differential \mathcal{B}
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- Quadrature-based discretization of diffusive representations
- Stability of wave eq. with IBC
- IBCs with Euler or Navier-Stokes

Communications & Publications (1)

Publications

F. Monteghetti et al. (2016a). "Design of broadband time-domain impedance boundary conditions using the oscillatory-diffusive representation of acoustical models". In: *The Journal of the Acoustical Society of America* 140.3, pp. 1663–1674. DOI: [10.1121/1.4962277](https://doi.org/10.1121/1.4962277)

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Publications (submitted)

F. Monteghetti et al. (2018a). "Asymptotic stability of the multidimensional wave equation coupled with classes of positive real impedance boundary conditions". (Submitted.)

F. Monteghetti et al. (2018d). "Time-local discretization of fractional and related diffusive operators using Gaussian quadrature with applications". (Submitted.)

Communications & Publications (2)



Communications

F. Monteghetti et al. (2016c). "Simulation temporelle d'un modèle d'impédance de liner en utilisant la représentation diffusive d'opérateurs". In: *13e Congrès Français d'Acoustique*. (Le Mans, France). 000130, pp. 2549–2555

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F. Monteghetti et al. (2017a). "Stability of linear fractional differential equations with delays: a coupled parabolic-hyperbolic PDEs formulation". In: *20th World Congress of the International Federation of Automatic Control (IFAC)*. (Toulouse, France). DOI: 10.1016/j.ifacol.2017.08.1966

F. Monteghetti et al. (2018c). "Quadrature-based diffusive representation of the fractional derivative with applications in aeroacoustics and eigenvalue methods for stability". In: *10th Workshop Structural Dynamical Systems: Computational Aspects (SDS2018)*. (Capitolo (Monopoli), Italy)

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Analysis and Discretization of Time-Domain Impedance Boundary Conditions in Aeroacoustics

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- 3 DG discretization of IBCs
- 4 Stability of wave equation with IBCs
- 5 Conclusion

Thanks for your attention. Any questions?

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