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## Chapter 5 - MOSFETs

→ In this chapter:

- 1- The physical structure of MOS transistors and how it works
- 2- How voltage between two terminals of transistor controls the current.
- 3- How to analyze and design circuits with MOS transistors, resistors and DC sources

Info:

→ voltage between 2 terminals control current in third.  
3-terminal devices (MOSFETs, BJT's)

MOSFETs (actually a 4-T device)

BJT's

• Analog circuits  
• Digital circuits → logic.

• Analog.

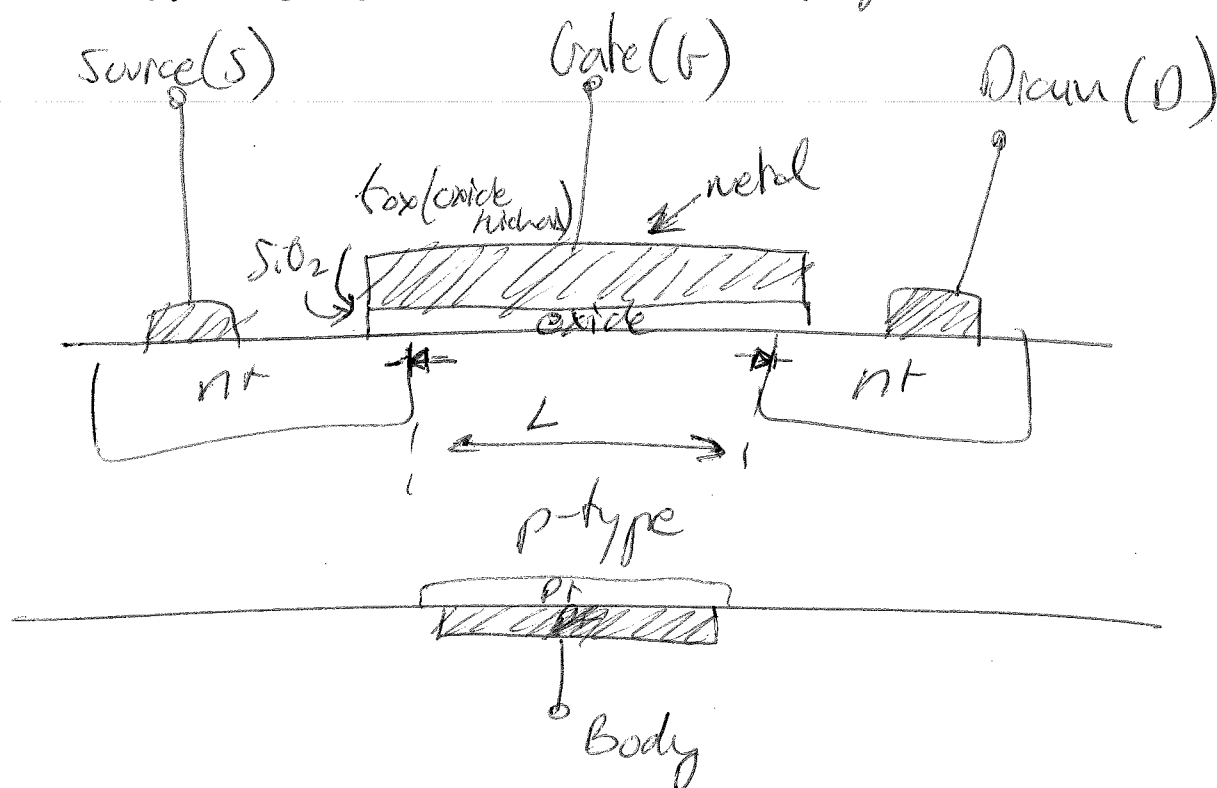
→ Amplifiers, filters, rectifiers, regulators...

## 5.1 - Device structure and physical operation.

Metal Oxide Semiconductor Field Effect Transistor

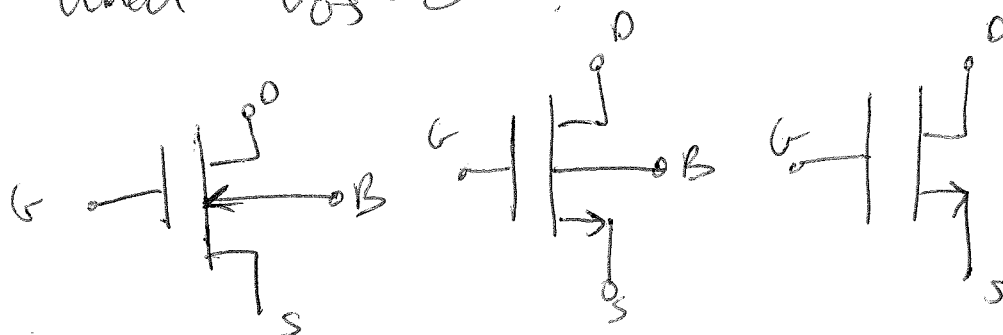
MOSFET

→ Enhancement mode → most popular.



→ Generally source and Body are connected together to ensure  $V_D > V_B$  (PN diodes are shut off)

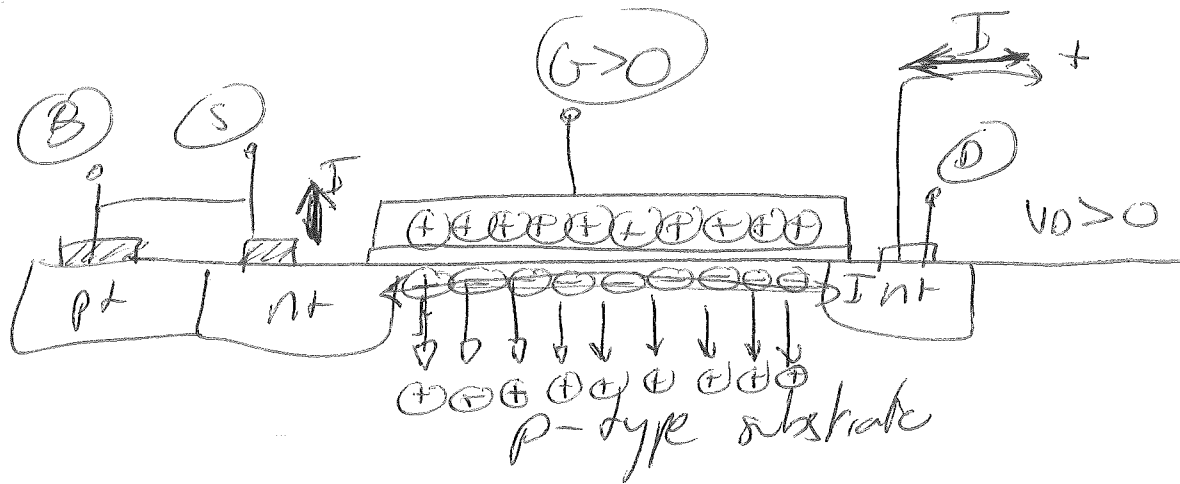
→ Back to back diodes prevent current when  $V_{GS} \leq 0$



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### S.1.3 Creating a channel for current flow.



→ n-channel MOSFET or NMOS transistor.

→ NMOS is formed in p-type substrates.

The channel is created by inverting the substrate surface from p to n-type.

The induced channel → inversion layer.  
→ enhances the channel.

→ Value for which  $V_{GS}$  is sufficient to invert the surface is called the threshold voltage →  $V_t$  (0.3 → 10V)  $\neq V_r$  (Forward voltage of diode)

→ Field effect by charge on gate.  
enhances

At  $V_{GS} = V_t$  → voltage on channel is just inverted and equal to 0. Higher voltages will affect the width/depth of inversion layer.

$$V_{ov} = V_{os} - V_t$$

→ over-drive voltage (voltage of ~~os~~  $V_{os}$  higher than  $V_t$ )

→ Charge in channel:

$$|Q| = C_{ox} (W \cdot L) V_{ov}$$

$$C_{ox} = \frac{\epsilon_{ox}}{t_{ox}}$$

$$\epsilon_{ox} = 3.9 \cdot \epsilon_0$$

$$= 3.9 \cdot 8.854 \times 10^{-12} \text{ F/m}$$

$$= 3.45 \times 10^{-11} \text{ F/m}$$

for typical  $t_{ox} \approx 4 \text{ nm}$

$$C_{ox} = \frac{3.45 \times 10^{-11} \text{ F/m}}{4 \times 10^{-9} \text{ m}} = 8.6 \times 10^{-3} \text{ F/m}^2$$

↓

$$8.6 \times 10^{-15} \text{ F/\mu m}^2$$

$$8.6 \times 10 \text{ fF/\mu m}^2$$

typical  $W = 0.78 \mu\text{m}$   $L = 0.18 \mu\text{m}$

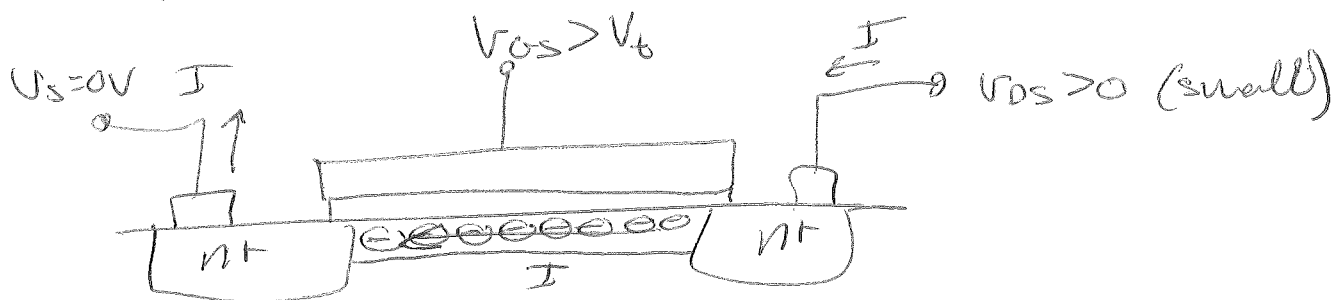
$$C = C_{ox} \frac{W}{L} = 8.6 \text{ fF/\mu m}^2 \cdot 0.78 \mu\text{m} \cdot 0.18 \mu\text{m}$$

$$\boxed{C = 1.1 \text{ fF}}$$

### 5.1.4. Applying a small $V_{DS}$ .

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- current is opposite of direction of electrons. (negative charges)
- electrons move from  $\ominus$  to  $\oplus$
- current flows from  $\oplus$  to  $\ominus$ .
- current goes from drain to source (source is source of electrons).
- since  $V_{DS}$  is small voltage on channel is  $V_{OV} = V_{GS} - V_t$

$$\frac{Q_c}{\text{unit length}} = C_{ox} W \cdot V_{OV}$$

$$V_{DS} \text{ lead to } E_{\text{field}} = \frac{V_{DS}}{L}$$

$$\text{Electron drift velocity} = \mu_n |E| = \mu_n \frac{V_{DS}}{L}$$

↓  
electron mobility.

$$i_D = \text{charge} \times \text{drift velocity} = \left[ (\mu_n C_{ox}) \left( \frac{W}{L} \right) V_{OV} \right] \cdot V_{DS}$$

$$V_{OV} = V_{GS} - V_t$$

$$I_D = \left[ (\mu_n C_{ox}) \left( \frac{W}{L} \right) (V_{GS} - V_t) \right] V_{DS}$$

linear equation depends on value of  $V_{GS}$  and  $V_{DS}$ .

conductance of channel (Resistance)  $g_{DS} = \frac{1}{r_{DS}}$

$$g_{DS} = (\mu_n C_{ox}) \left( \frac{W}{L} \right) (V_{GS} - V_t)$$

$\mu_n C_{ox} \rightarrow$  process technology ( $K'_n = \mu_n C_{ox}$ )

process transconductance parameter.  $\left[ \frac{A}{V^2} \right]$

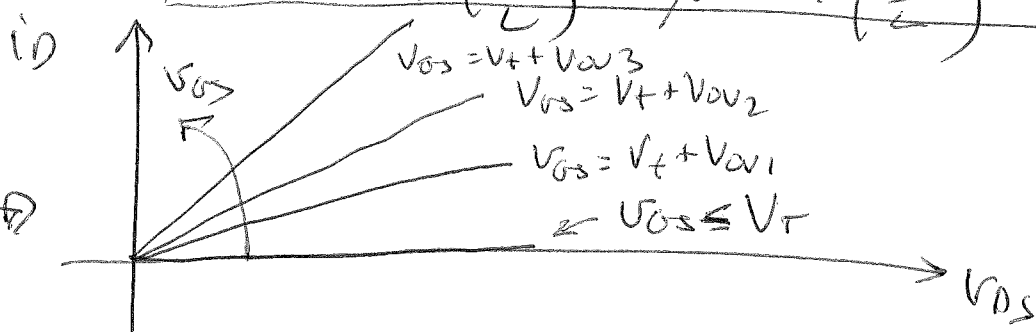
$$K'_n \rightarrow \left[ \frac{A}{V^2} \right]$$

$$\left[ \frac{F}{m^2} \right]$$

$\frac{W}{L} \rightarrow$  designer chosen for  $I_{inh}$ .

MOSFET transconductance parameter  $K_n$

$$K_n \equiv K'_n \left( \frac{W}{L} \right) = \mu_n C_{ox} \left( \frac{W}{L} \right) \left[ \frac{A}{V^2} \right]$$

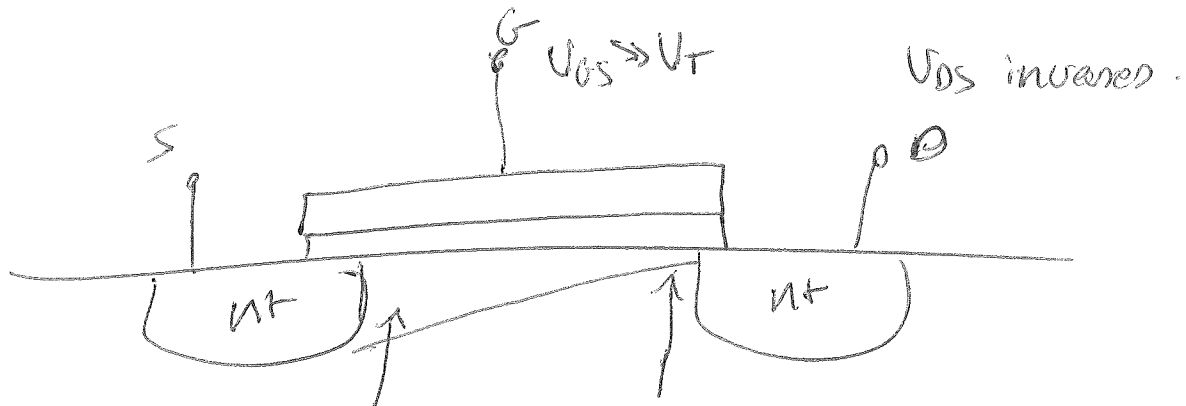


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Electronics 1.

5.1.5 operation as  $V_{DS}$  is increased:

$$V_{ov} = V_{GS} - V_T$$

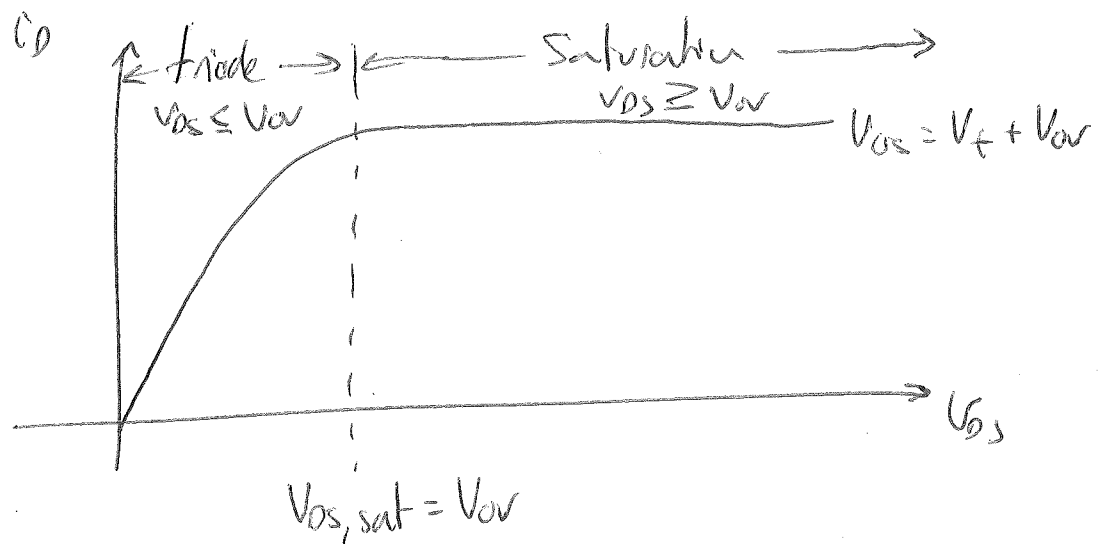


Channel voltage =  $V_T + V_{ov}$

Source side

$$V_T + V_{ov} - V_{DS}$$

drain side.



$$i_D = k_n \left( \frac{W}{L} \right) \left[ (V_{GS} - V_T) V_{DS} - \frac{1}{2} V_{DS}^2 \right] \quad \text{for } V_{DS} < V_{GS} - V_T$$

$V_{DS} < V_{ov}$

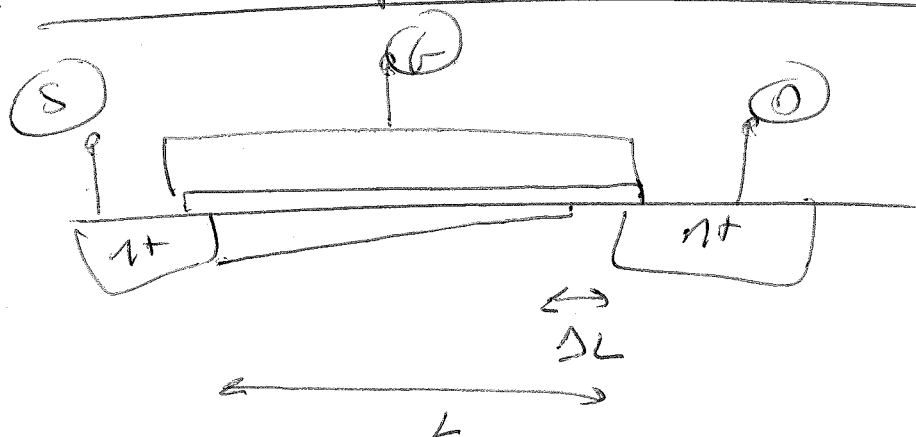
S.1.6 Operation for  $V_{DS} \geq V_{OV}$ ; channel pinch-off and current saturation.

→ When  $V_{DS} \geq V_{OV}$   $V_{DS} \geq V_{GS} - V_t$ ,  $V_{GD} = V_t$   
and channel depth is zero at drain end.  
Channel is pinched off → current saturates.

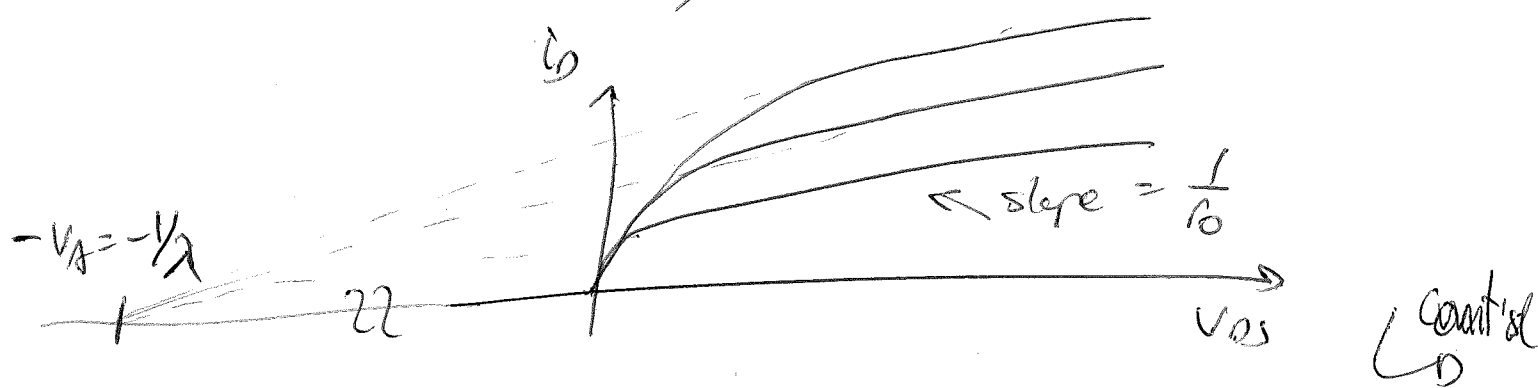
$$V_{DS, sat} = V_{OV} = V_{GS} - V_t$$

$$I_{D, sat} = \frac{1}{2} k'_n \left( \frac{W}{L} \right) (V_{GS} - V_t)^2$$

S.2.4 Finite output resistance in saturation.



$$I_{D, sat} = \frac{1}{2} k'_n \left( \frac{W}{L} \right) (V_{GS} - V_t)^2 (1 + \lambda V_{DS})$$





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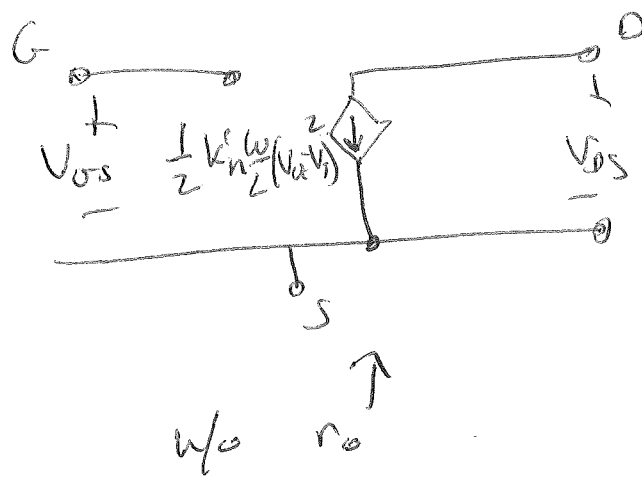
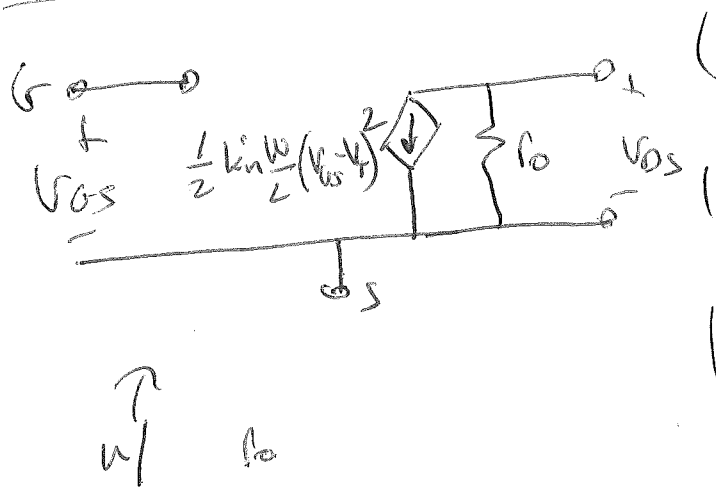
$$r_o \equiv \left[ \frac{\partial i_o}{\partial v_{os}} \right]_{v_{os} \text{ constant}}$$

$$r_o = \left[ \lambda \frac{k'_n}{2} \frac{W}{L} (V_{os} - V_{tn})^2 \right]^{-1}$$

$$r_o = \frac{1}{\lambda I'_D} \quad \text{OR} \quad r_o = \frac{V_A}{I'_D}$$

$$\text{where } I'_D = \frac{1}{2} k'_n \frac{W}{L} (V_{os} - V_{tn})^2$$

Large signal equivalent-circuit model.



ex NMOS fabricated, of 0.18- $\mu\text{m}$  process w/  $L=0.18\mu\text{m}$   
 $W=2\mu\text{m}$ .  $C_{ox}=8.6\text{ fF}/\mu\text{m}^2$   $\mu_n=450\text{ cm}^2/\text{V}\cdot\text{s}$   
 $V_{tn}=0.5\text{V}$ .

→ Find  $V_{GS}$  and  $V_{DS}$  to operate MOSFET at edge of saturation with  $I_D=100\mu\text{A}$ .

\* First find process transconductance  $K'_n$

$$K'_n = \mu_n C_{ox} = (450\text{ cm}^2/\text{V}\cdot\text{s}) (8.6 \times 10^{-15} \frac{\text{F}}{\mu\text{m}^2})$$

$$= 387\mu\text{A}/\text{V}^2$$

## 5.4. Body effect - Role of substrate.

Effect of  $V_{SB}$  on the channel can be represented as a change in threshold voltage  $V_t$ .

$$V_t = V_{t0} + \gamma \left[ \sqrt{2\phi_F + V_{SB}} - \sqrt{2\phi_F} \right]$$

$V_{t0}$  = threshold voltage for  $V_{SB}=0$

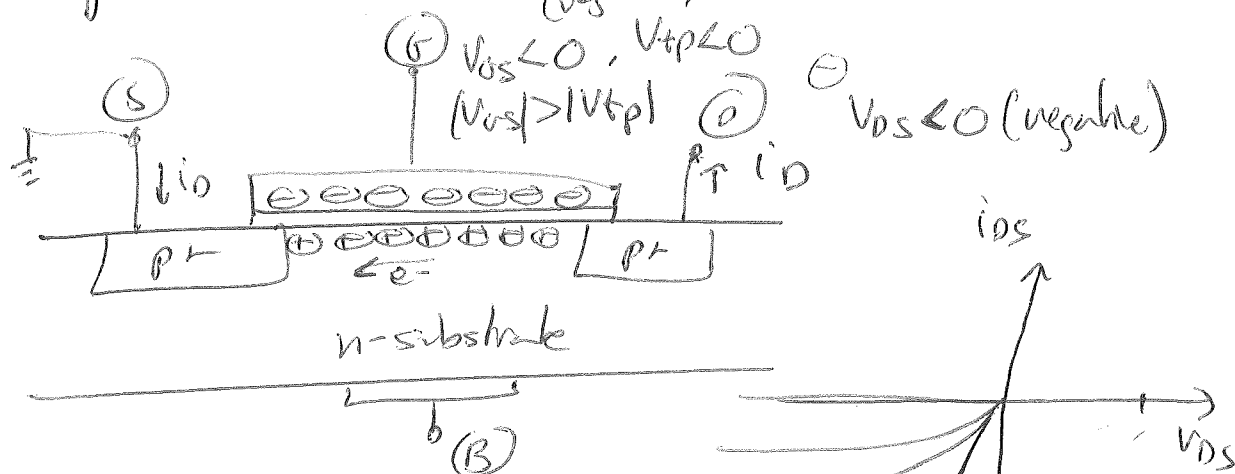
$\phi_F$  = physical parameter  $\Rightarrow 2\phi_F=0.6\text{V}$

$$\gamma = \frac{\sqrt{2qNA\epsilon_s}}{C_{ox}}$$

$q = 1.6 \times 10^{-19}\text{ C}$   
 $N_A$  - dopin concentration  
 $\epsilon_{Si} = 1.04 \times 10^{-12}\text{ F/cm}$

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S.1.7. The p-channel MOSFET. (negative)



Avoid dealing w/ negative signs.

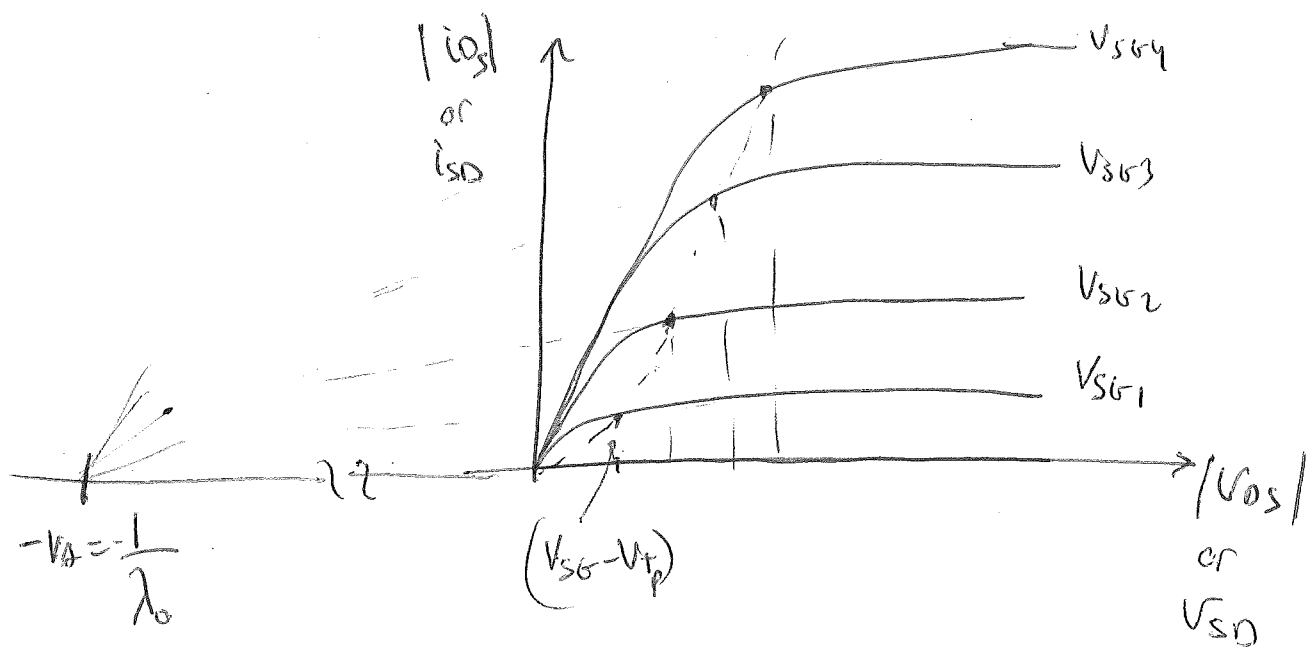
To meet channel  $|V_{GS}| \geq |V_{tp}|$

PMOS  $k'_p = \mu_p C_{ox}$  ( $\mu_p < \mu_n$ )

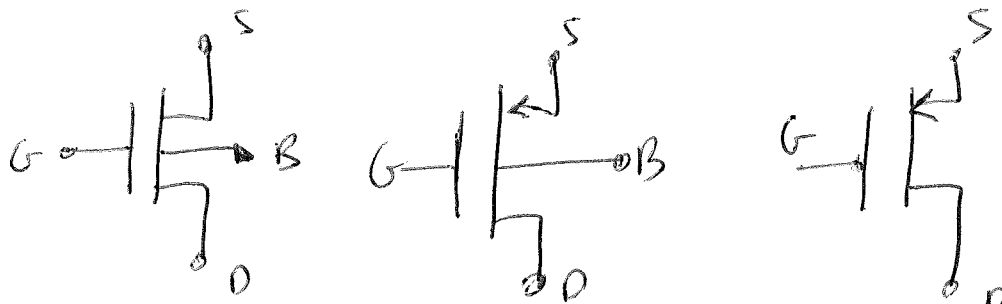
$\mu_p = \frac{1}{4} \text{ to } \frac{1}{2} \mu_n$

Transistor transconductance

parameter:  $k_p = k'_p \left( \frac{W}{L} \right) = \mu_p C_{ox} \frac{W}{L}$



→ PMOS symbols and conventions:

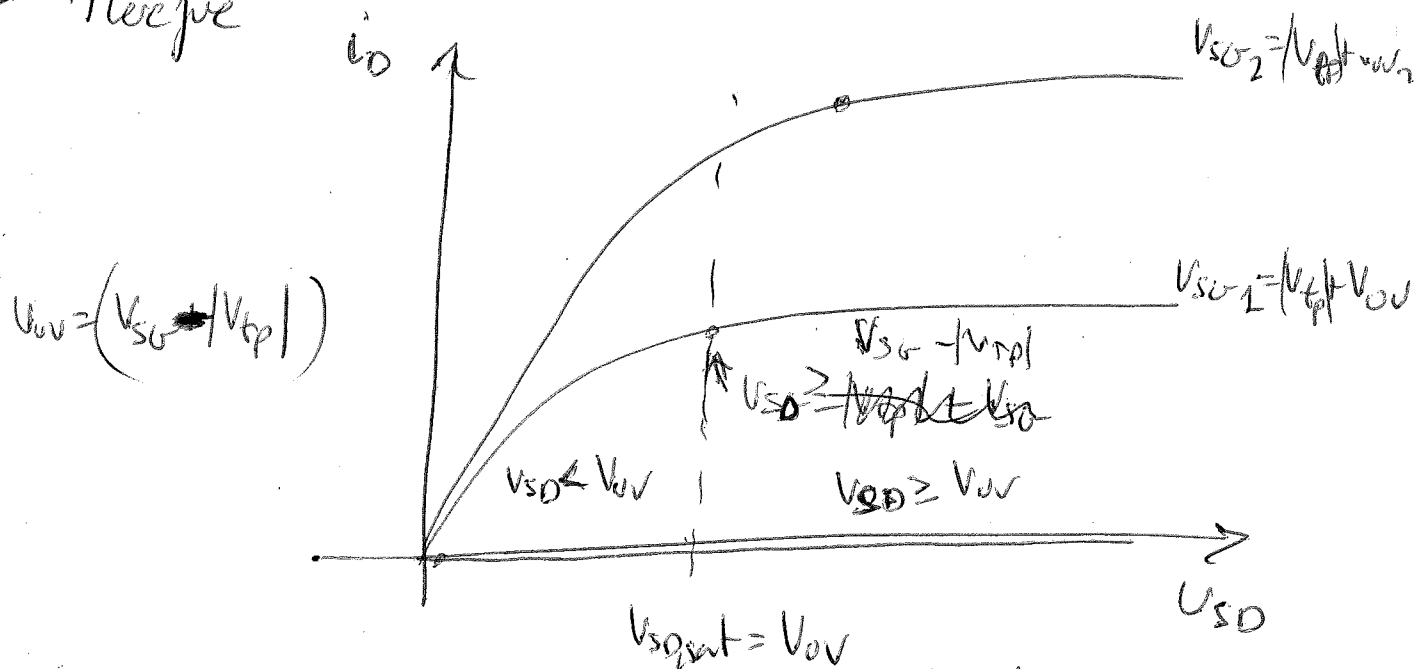


→ Although  $V_{tp}$  is negative, write as  $|V_{tp}|$

→ Generally draw p-channel devices with their sources on top so current flows from top to bottom.

→ Write voltage w/ respect to drain to make them positive and simplify analysis.

→ Therefore



Triode region

$$V_{DS} < V_{SG} - |V_{tp}|$$

Saturation region

$$V_{DS} \geq V_{SG} - |V_{tp}|$$

$$i_D = k_p' \left( \frac{W}{L} \right) \left[ (V_{SG} - |V_{tp}|) V_{DS} - \frac{1}{2} V_{DS}^2 \right]$$

$$i_D = \frac{1}{2} k_p' \left( \frac{W}{L} \right) (V_{SG} - |V_{tp}|)^2$$

### Example 8.2

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NMOS  $L=0.18\mu\text{m}$ ,  $W=2\mu\text{m}$

$$C_{ox}=8.6\text{ fF}/\mu\text{m}^2, \mu_n=450\text{ cm}^2/\text{V}\cdot\text{s}, V_{tn}=0.5\text{ V}$$

a) Find  $V_{ov}$  and  $V_{DS}$  at edge of saturation when  $I_D=100\mu\text{A}$ .

→ First find  $k'_n$  (process transconductance parameter).

$$k'_n = \mu_n C_{ox} = 450 \frac{\text{cm}^2}{\text{V}\cdot\text{s}} \cdot 8.6\text{ fF}/\mu\text{m}^2$$

$\text{cm}^2 \rightarrow 1 \times 10^{-4} \text{ m}^2$   
 $\cancel{450 \text{ cm}^2} \rightarrow \cancel{450 \times 10^{-4}} \text{ m}^2$   
 $\mu\text{m}^2 \rightarrow 1 \times 10^{-12} \text{ m}^2$

$$k'_n = \frac{450 \times 10^{-4} \frac{\text{m}^2}{\text{V}\cdot\text{s}} \cdot 8.6 \times 10^{-15}}{1 \times 10^{-12} \text{ m}^2} = 387 \times 10^{-6} \text{ A/V}^2$$

→ Find transistor transconductance:

$$k_n = k'_n \left( \frac{W}{L} \right) = 387 \times 10^{-6} \text{ A/V}^2 \left( \frac{2\mu\text{m}}{0.18\mu\text{m}} \right) = 4.3 \frac{\text{mA}}{\text{V}^2}$$

$4.3 \times 10^{-3} \text{ A/V}^2$

→ Use saturation equation

$$I_{D_{\text{sat}}} = \frac{1}{2} k_n (V_{GS} - V_T)^2$$

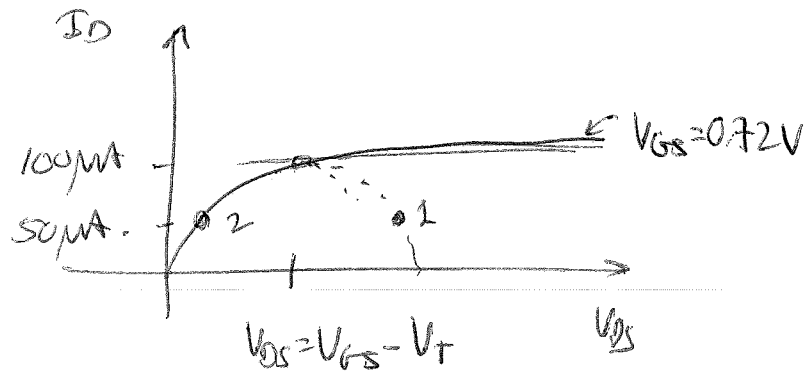
$$V_{GS} - V_T = V_{ov}$$

$$100\mu\text{A} = \frac{1}{2} (4.3 \times 10^{-3}) \frac{\text{A}}{\text{V}^2} (V_{ov})^2$$

$$V_{ov}^2 = (V_{GS} - V_T)^2 = 46\text{ mV} \rightarrow V_{ov} = V_{GS} - V_T = 0.22\text{ V} = \sqrt{0.046}$$

$$\therefore V_{GS} = 0.22 + 0.5 = 0.72\text{ V}.$$

(b) ~~Find~~ <sup>IF</sup>  $V_{DS}$  is kept constant find  $V_{DS}$  for  $I_D = 50 \mu A$ .



$$V_{DS_{sat}} = 0.72 - 0.5 = 0.22 V$$

$I_D$  in triode region (parabolic region)

$$I_D = k_n \left[ (V_{GS} - V_T) V_{DS} - \frac{1}{2} V_{DS}^2 \right]$$

$$50 \times 10^{-6} A = 4.3 \times 10^{-3} A/V^2 \left[ (0.72 - 0.5) V_{DS} - \frac{1}{2} V_{DS}^2 \right]$$

$$\frac{50 \times 10^{-6} A}{4.3 \times 10^{-3} A/V^2} = 0.22 V_{DS} - 0.5 V_{DS}^2$$

$$0.5 V_{DS}^2 - 0.22 V_{DS} + 0.011 = 0$$

$$V_{DS} = \frac{-b \pm \sqrt{b^2 - 4ac}}{2a}$$

$$V_{DS1} = \frac{0.22 + \sqrt{(0.22)^2 - 4(0.5)(0.011)}}{2(0.5)} = 0.39 V$$

$$V_{DS2} = \frac{0.22 - \sqrt{(0.22)^2 - 4(0.5)(0.011)}}{2(0.5)} = 0.06 V$$

$V_{DS1} > V_{DS,sat}$  (not possible for this case)

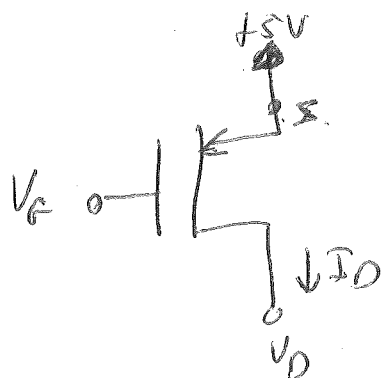
$V_{DS2} = 0.06 V \leftarrow$  correct answer.

S.7

PMOS transistor  $V_{tp} = -1V$ ,  $k'_p = 60 \mu A/V^2$

$$\frac{W}{L} = 10$$

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a) Find  $V_G$  range for which transistor conducts.

when  $V_{SG} \geq |V_{tp}| = 1V$

$$\Rightarrow V_G \leq 5 - 1 = 4V$$

$$V_G \leq 4V \quad V_{SG} \geq 1V$$

b) In terms of  $V_G$ , find the range of  $V_D$  for triode (linear) operation.

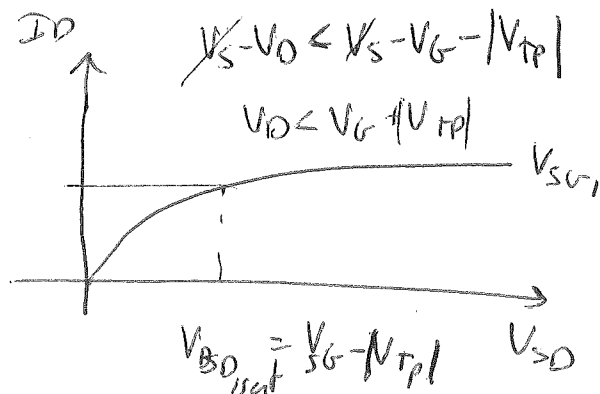
Triode when  $V_{SD} \geq |V_{tp}| = 1V$

$$\Rightarrow V_D \geq V_G + 1$$

c) For saturation.

$$V_{SD} \leq |V_{tp}| = 1V$$

$$\Rightarrow V_D \leq V_G + 1$$



$$V_{SD} \leq V_{SD} - |V_{tp}| \quad V_{SD} > V_{SD} - |V_{tp}|$$

$$V_D \leq V_G + |V_{tp}| \quad V_D > V_G + |V_{tp}|$$

$$V_{DG} > |V_{tp}| \quad V_{DG} < |V_{tp}|$$

$$V_G < V_D + 1$$

d) Assuming  $\lambda = 0$ , find values

of  $|V_{ov}|$  and  $V_G$  and range

of  $V_D$  to operate in sat  $I_{D,sat} = 75 \mu A$

$$I_D = \frac{1}{2} k'_p \frac{W}{L} (V_{SG} - |V_{tp}|)^2$$

$$75 \times 10^{-6} A = \frac{1}{2} 60 \times 10^{-6} \frac{A}{V^2} (10) (V_{SG} - 1)^2$$

$$(V_{SG} - V_T)^2 = 0.25V$$

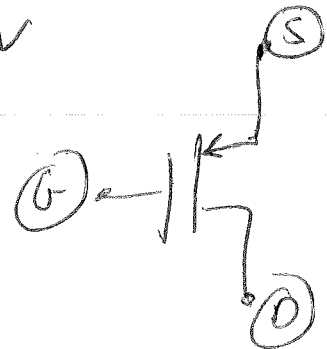
$$(V_{SG} - V_T) = 0.5V$$

$$\therefore V_{SG} - |V_{TP}| = 0.5V = |V_{OV}|$$

$$V_{SG} = 0.5V + |V_{TP}| = 1.5V$$

$$\Rightarrow V_{SG} = V_S - V_G \rightarrow V_G = V_S - V_{SG} = 5V - 1.5V = 3.5V$$

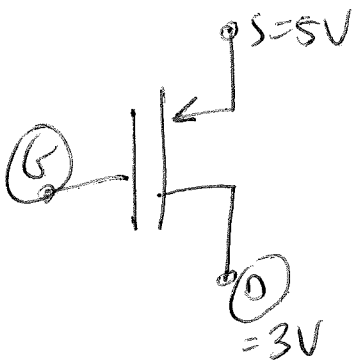
$$V_D \leq V_G + 1 = 4.5V \quad V_D \leq 4.5V$$



(c) If  $\lambda = -0.02V^{-1}$ , find  $r_o$  at  $|V_{OV}| = 0.5V = |V_{SG} - |V_{TP}||$

$$r_o = \frac{1}{|\lambda| I_D} = \frac{1}{(0.02)(75 \times 10^{-6}A)} = 667k\Omega$$

(f) Find  $I_D$  at  $V_{OV} = 0.5V$  with  $\lambda = -0.02V^{-1}$ , at  $V_D = 3V$



$$V_{SD} = 2V$$

$$V_{SD} = V_S - V_D = 5V$$

$$I_D = \frac{1}{2} k'_n \left( \frac{W}{L} \right) |V_{OV}|^2 (1 + |\lambda| V_{SD}) \rightarrow \begin{aligned} V_{SD} &= V_S - V_D \\ V_{SD} &= 5V - 3V \\ V_{SD} &= 2V \end{aligned}$$

$$I_D = (75\mu A) (1 + (0.02V^{-1})(2V))$$

$$I_D = 75 \times 10^{-6} \times 1.04 = 78 \times 10^{-6} \text{ Amp}$$



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### 5.3. MOSFET CIRCUITS AT DC.

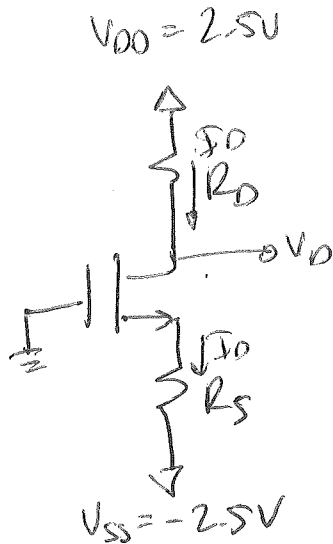
→ Quick DC analysis:

→ Generally neglect channel-length modulation.

→  $V_{OV} = V_{GS} - V_{TN}$  → NMOS

$V_{OV} = V_{SG} - |V_{TP}|$  → PMOS

ex. 5.3



Find  $R_D$  and  $R_S$  for  
transistor  $I_D = 0.4 \text{ mA}$  and  
 $V_O = 0.5 \text{ V}$ . NMOS  $V_{TN} = 0.7 \text{ V}$   
 $\mu_n C_{ox} = 100 \mu\text{A/V}^2$ ,  $L = 1 \mu\text{m}$ ,  
 $W = 32 \mu\text{m}$ .  $\lambda = 0$

$$R_D = \frac{V_{DD} - V_O}{I_D} = \frac{(2.5 - 0.5) \text{ V}}{0.4 \times 10^{-3} \text{ A}}$$

$$R_D = 5 \times 10^3 \Omega.$$

→ Need  $V_S$  to find  $R_S$ .

Since  $V_O = 0.5 > V_G$  ( $V_G = 0 \text{ V}$ ). ~~Assume saturation~~

$$V_{DS} \geq (V_{GS} - V_T) \quad \text{sat}$$

And  $I_D = \frac{1}{2} \mu_n C_{ox} \frac{W}{L} \underbrace{(V_{GS} - V_T)^2}_{(V_{OV})^2}$

$$0.4 \times 10^{-3} = \frac{1}{2} 100 \times 10^{-6} \frac{\text{A}}{\text{V}^2} \left( \frac{32}{1} \right) V_{OV}^2$$

$$V_{OV} = 0.5 \text{ V}$$

$$(V_{GS} - V_T) = 0.5 \text{ V}$$

$$V_{GS} = 1.2 \text{ V}$$

$$V_G - V_S = 1.2 \text{ V}$$

$$V_G - V_S - V_T = 0.5$$

$$0 \text{ V} - V_S - 0.7 = 0.5$$

$$V_S = -1.2 \text{ V}$$

1)  $V_S = -1.2V$  then

$$R_S = \frac{V_S - V_{SS}}{I_D} = \frac{-1.2 - (-2.5)V}{0.4mA}$$

$$\boxed{R_S = 325k\Omega}$$

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Qw #3

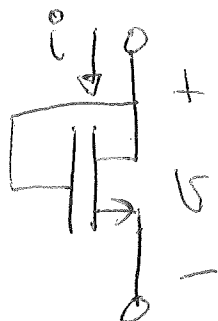
5.18, 5.19, 5.27, 5.38, 5.39, 5.44, 5.45

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→ Diode-connected transistor

$$V_{DS} = V_{GS} - V_t$$

ex. 5.4 (pg 278)



→ Gate and drain terminals connected together.  $V_{GD} = 0, < V_{tn}$

→ Find  $i$ - $v$  relationship in terms of  $k_n$  and  $V_{tn}$ . Neglect  $\lambda$ .

→  $V_D = V_G$ , implies operation in saturation mode.

$$i_D = \frac{1}{2} k_n \left( \frac{W}{L} \right) (V_{GS} - V_{tn})^2$$

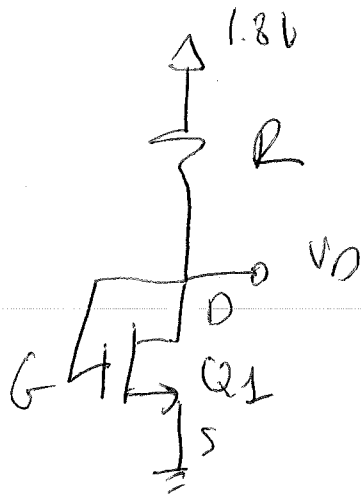
$$i = i_D \quad \downarrow \quad v = v_{GS}$$

$$\boxed{i = \frac{1}{2} k_n (v - V_{tn})^2}$$

lec 14 1  
lec 15 6

Q.59.

Find  $R$  for  $V_D = 0.7V$ .



$$\boxed{\begin{aligned} V_{th} &= 0.8V \\ \mu_n C_{ox} &= 0.4 \text{ mA/V}^2 & \lambda &= 0 \\ \frac{W}{L} &= \frac{0.72 \mu\text{m}}{0.18 \mu\text{m}} = 4.0 \end{aligned}}$$

Sat. mode ( $V_{DS} = 0 < V_{th}$ )

$$V_D = 0.7V = 1.8 - I_D R$$

$$I_D = \frac{1}{2} \mu_n C_{ox} \left( \frac{W}{L} \right) (V_D - V_{th})^2 = 0.032 \text{ mA}$$

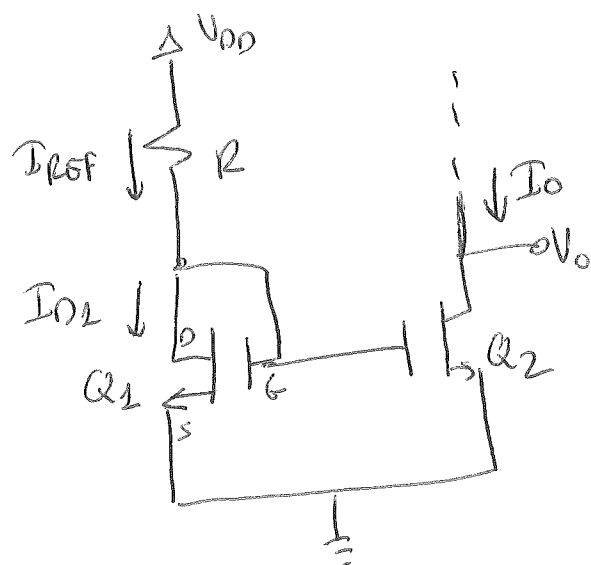
$$\therefore R = \frac{1.8 - 0.7}{0.032 \text{ mA}} = 34.4 \text{ k}\Omega$$

~~$V_{DS} = V_{GS} - V_T$~~   
 ~~$V_D - V_S \geq V_G - V_S - V_T$~~   
 ~~$V_D - V_G > V_T$~~

## 8.2.1 - Current Sources, current Mirrors,

9/29/2016

### Basic MOSFET current source.



$Q_2 \rightarrow$  "Heart" of circuit.

Diode connected  $\rightarrow$  always sat.

$$I_{D1} = \frac{1}{2} k_n \left( \frac{W}{L} \right)_1 (V_{GS} - V_{th})^2 \quad (1)$$

(assume  $\lambda_0 \rightarrow 0$ )

Drain current supplied thru  $V_{DD}$  and resistor  $R$  (external to circuit)

Cake current  $\rightarrow 0$

$$\therefore I_{D1} = I_{REF} = \frac{V_{DD} - V_{DS}}{R} \quad (2)$$

$\rightarrow$  Equations (1) + (2) used to determine  ~~$I_{REF}$~~   $R$  for a set  $I_{REF}$ .

$\rightarrow Q_2 \rightarrow$  has same  $V_{GS}$  as  $Q_1$  (also in saturation)

$$\therefore I_O = I_{D2} = \frac{1}{2} k_n \left( \frac{W}{L} \right)_2 (V_{GS} - V_{th})^2 \quad (3)$$

From (1) and (3)

$$\frac{I_O}{I_{REF}} = \frac{\frac{1}{2} k_n \left( \frac{W}{L} \right)_2 (V_{GS} - V_{th})^2}{\frac{1}{2} k_n \left( \frac{W}{L} \right)_1 (V_{GS} - V_{th})^2} = \frac{\left( \frac{W}{L} \right)_2}{\left( \frac{W}{L} \right)_1}$$

$\rightarrow$  If  $\left( \frac{W}{L} \right)_1 = \left( \frac{W}{L} \right)_2$  then  $I_{REF} = I_O \rightarrow$  "current mirror"

$\rightarrow$  Scaling  $\left( \frac{W}{L} \right)_1$  to  $\left( \frac{W}{L} \right)_2$  scales  $I_O$  to  $I_{REF} \rightarrow$  current gain or current transfer ratio.

## Effect of $V_o$ and $I_o$

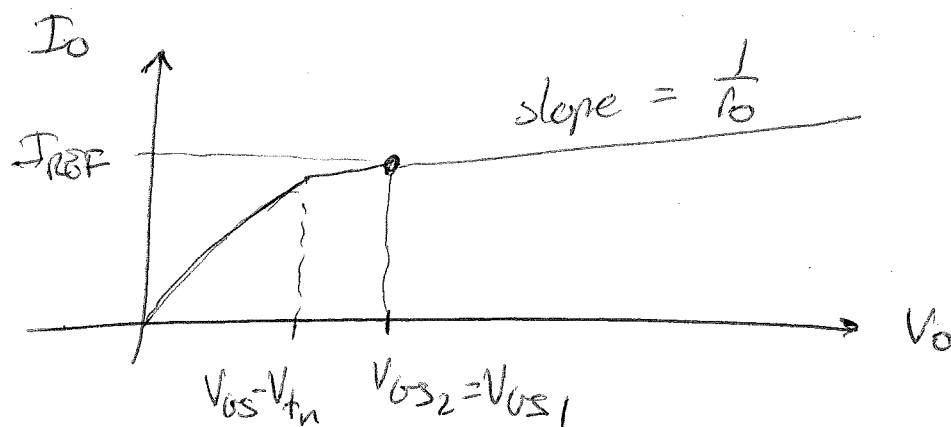
→  $Q_2$  must remain in saturation.

$$\therefore V_o = V_{DS2} \geq V_{GS2} - V_{tn} \quad \text{or} \quad V_o \geq V_{ov}$$

$V_{ov}$  generally a few  
tenths of VLS.

→ Also channel-length modulation  $\lambda$  can have significant effect on the operation of the current source.

As  $V_o$  increases beyond initial value of  $V_{DS1}$ ,  $I_o$  increases according to  $r_{o2}$  of  $Q_2$ .



$\therefore$  Output resistance of current source

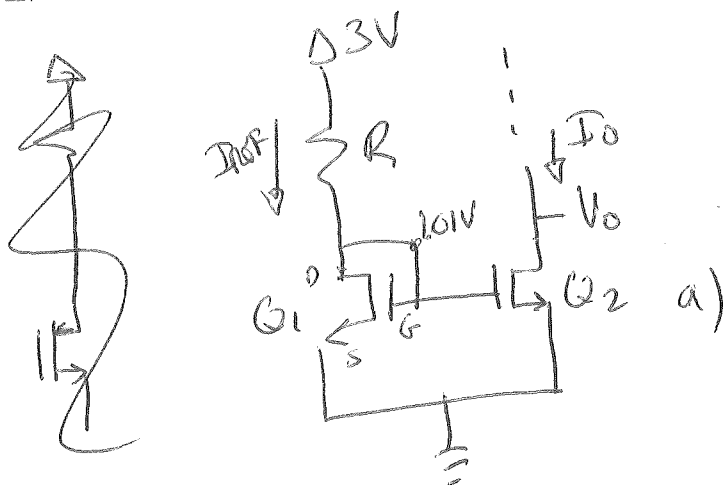
$$R_o = \frac{\Delta V_o}{\Delta I_o} = r_{o2} = \frac{V_{A2}}{I_o} = \frac{1}{\lambda_2 I_o}$$

→ use long  
channel trans.  
to get high  $R_o$ .

Also 
$$I_o = \frac{(W/L)_2}{(W/L)_1} I_{REF} \left( 1 + \frac{V_o - V_{DS}}{V_{A2}} \right)$$
 take into account  
channel length mod.

# Ex. 8.1 - Current mirror example:

9/29/2016 (2)



$$V_{DD} = 3V$$

$$I_{REF} = 100 \mu A$$

Design circuit for  $I_O = 100 \mu A$

Find R for  $Q_1 = Q_2$  and  $L = 1 \mu m$ ,  $W = 10 \mu m$ ,  $V_T = 0.7V$

$$K_n = 200 \mu A/V^2$$

a)  $Q_1 = Q_2$  in saturation  $V_O = V_{GS}$

$$I_{D1} = I_{REF} = \frac{1}{2} K_n \left( \frac{W}{L} \right)_1 \underbrace{(V_{GS} - V_T)^2}_{(V_{OV})^2}$$

$$100 \times 10^{-6} A = \frac{1}{2} 200 \times 10^{-6} A/V^2 \left( \frac{10}{1} \right) V_{OV}^2$$

$$V_{OV}^2 = 0.316 V \rightarrow V_{OV} = \sqrt{0.316} = 0.562 V$$

$$\sqrt{V_{OV}^2} = \sqrt{0.316}$$

$$V_{OV} = V_{GS} - V_T = 0.316 V$$

$$V_{GS} = 0.316 V + 0.7 V = 1.016 V$$

$$R = \frac{3V - 1.016V}{100 \times 10^{-6} A} = 19.83 k\Omega$$

b) Find lowest possible value of  $V_O$ ?

$$V_{Omin} = V_{GS} - V_T = V_{OV} = 0.316 V$$

c) Assuming  $V_A' = 20\text{V}/\mu\text{m}$  (length dependent early voltage)  
 find output resistance of the current source.

$$R_o = r_{o2} = \frac{V_{A2}}{I_{D2}}$$

$$V_{A2} = V_A' \times (\text{length})$$

$$V_{A2} = 20\text{V}/\mu\text{m} \times 1\mu\text{m} = 20\text{V}$$

$$\boxed{R_o = \frac{20\text{V}}{100\mu\text{A}} = 200\text{k}\Omega}$$

d) Find change in output current resulting from a  
 +1-V change in  $V_o$ .

$$\Delta V_o = \Delta I_{D2} \cdot R_o \rightarrow \Delta V_o = 1\text{V}, R_o = 200\text{k}\Omega.$$

$$\boxed{\Delta I_{D2} = \frac{1\text{V}}{200\text{k}\Omega} = 5\mu\text{A}}$$

HW #4:

5.46, 5.50, 5.61

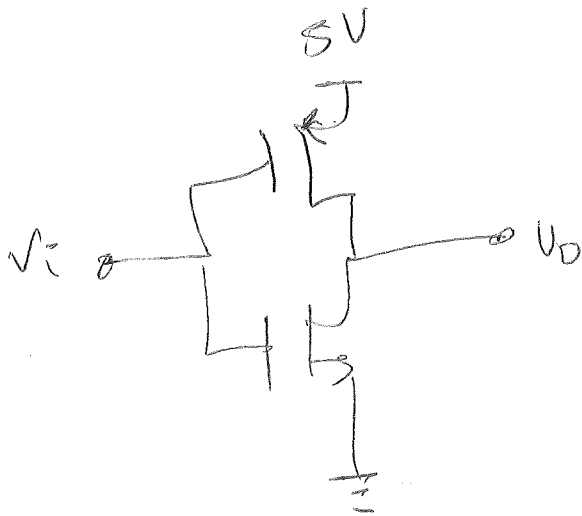
↳ sol: (a)  $R = 21\text{k}\Omega$  (b)  $W_2 = 14.4\mu\text{m}$   $R_2 = 3.1\text{k}\Omega$

$$V_{DS} = V_{DS2} - V_T = 0.25\text{V}$$



# CMOS-LOGIC QUIZZ

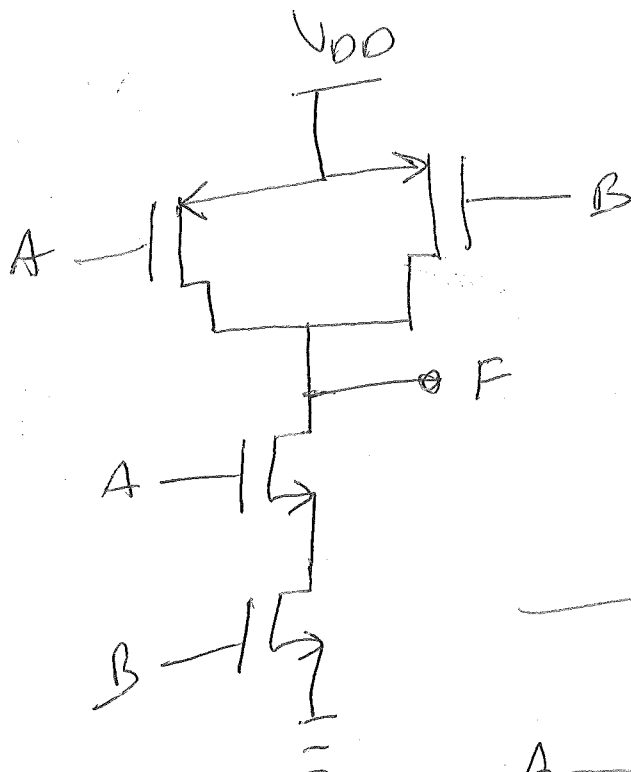
9/30/2016



Q1: Is the top transistor?

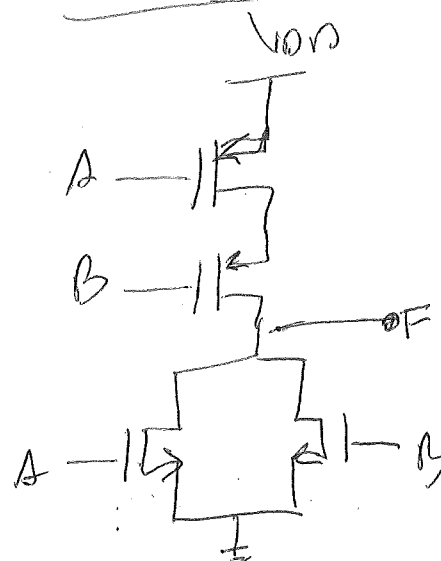
A: PMOS

B: NMOS



A	B	F
0	0	1
0	1	1
1	0	1
1	1	0

NAND



A	B	F
0	0	1
0	1	0
1	0	0
1	1	0

NOR

