板级射频电路开发



国部等特别

第三讲 半集总LC低通滤波器设计

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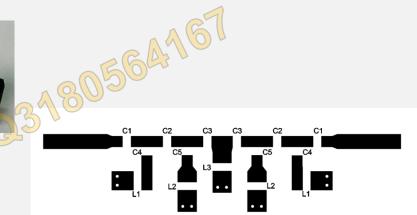
01 归一化LC低通滤波器设计02 半集总低通滤波器03 半集总微带低通滤波器

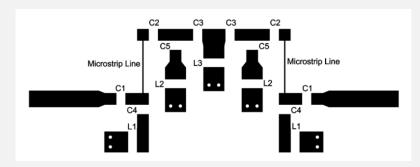
LC滤波器版图











归一化LC低通滤波器

Part

低通滤波 器原型

低通原型 滤波器拓 扑

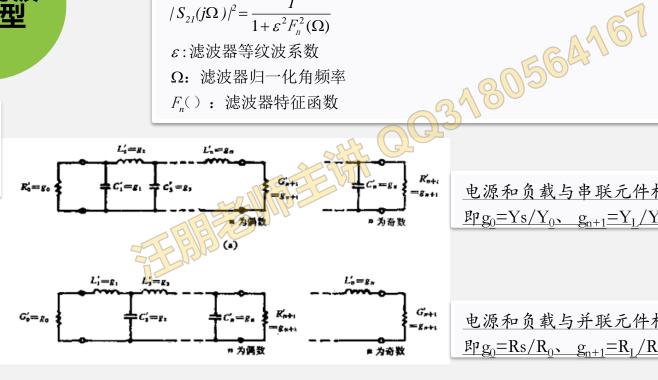
无耗、无源二端口滤波器网络传输函数S21数学表达式:

$$|S_{2I}(j\Omega)|^2 = \frac{1}{1 + \varepsilon^2 F_n^2(\Omega)}$$

 ε :滤波器等纹波系数

Ω: 滤波器归一化角频率

 $F(\cdot)$: 滤波器特征函数



电源和负载与串联元件相连时,表示电导, $p_0 = Y_s/Y_0, g_{n+1} = Y_1/Y_0;$

电源和负载与并联元件相连时,表示电阻, $\mathbb{E}_{p} g_0 = Rs/R_0, g_{n+1} = R_1/R_0;$

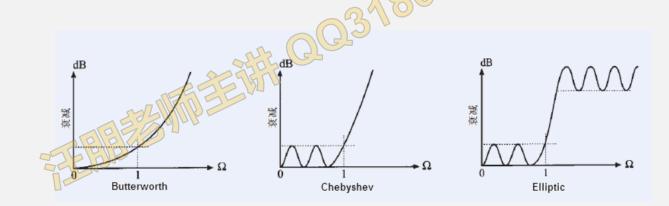
低通滤波 器原型

三种滤波器逼近函数

<1>最平坦型原型滤波器 (Butterworth)

<2>切比雪夫原型滤波器 (Chebyshev)

<3>椭圆函数滤波器





巴特沃思响应适用于幅度向应尽可能平坦的设计,为中等Q值滤波器

$$A_{dB} = 10lg[1 + \varepsilon(\frac{w}{w_c})^{2n}]$$

 ε 是纹波系数: $\varepsilon = 10^{L_{Ar}/10} - 1$

带内最大插损: $L_{Ar} = 10 \lg(1 + \varepsilon)$

带外最小衰减: $L_{AS} = 10 \lg(1 + \epsilon \Omega_s^{2n})$

滤波器阶数:

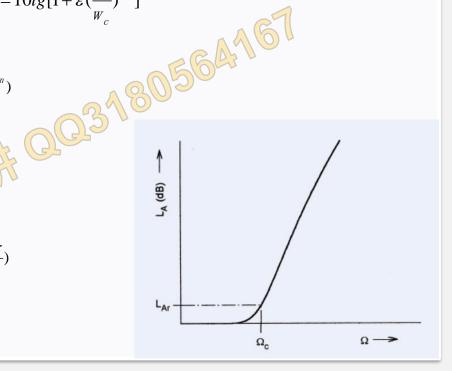
$$n \ge \frac{\lg(10^{0.1L_{AS}} - 1)}{2\lg \Omega_s}$$

低通原型滤波器元件值:

$$g_0 = 1.0$$

$$g_i = 2\sin(\frac{(2i-1)\pi}{2n})$$

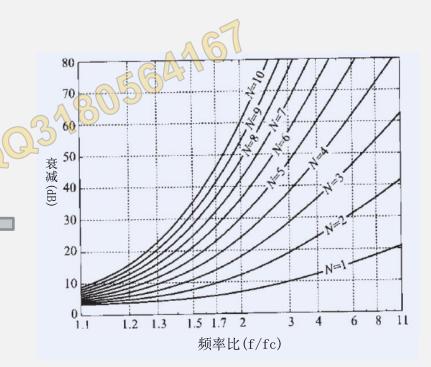
$$g_{n+1} = 1.0$$





巴特沃斯滤波器衰减特性:

例:设计一个截止频率为50MHz,且在 150MHz至少有50dB衰减的巴特沃斯滤波器, 判断元件数量?

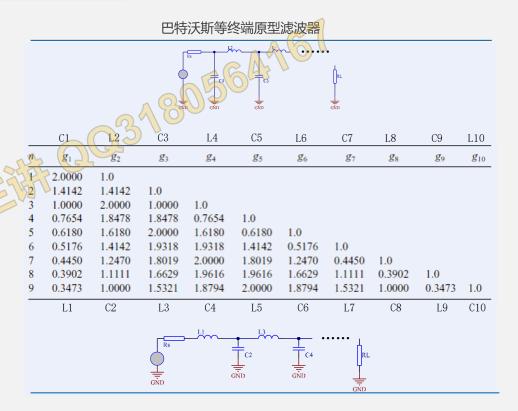


g0 = 1.0

 $g_i = 2\sin(\frac{(2i-1)\pi}{2n})$ $g_{n+1} = 1.0$



采用网络综合法进行巴特沃斯滤波器设计



巴特沃思 滤波器

巴特沃斯滤波器设计实例:

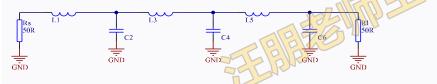
设计一个源端和终端阻抗都为50Ω,截止频率为50MHz,且在150MHz至少有50dB衰减的巴特沃斯滤波器

<1>根据频率比和带外衰减值分析滤波器阶数

f/fc=150/50=3

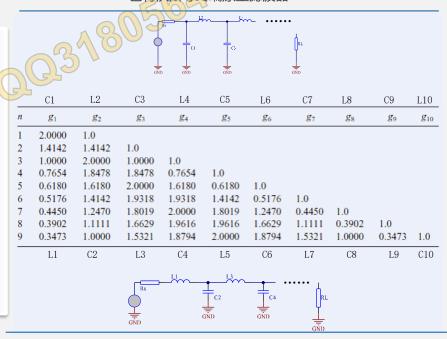
由滤波器衰减响应曲线n=6

<2>确定拓扑结构图



<3>采用查表形式确定归一化值 g1=0.5176, g2=1.4142, g3=1.9318 g4=1.9318, g5=1.4142, g6=0.5176

巴特沃斯等终端原型滤波器





一切比雪夫滤波器为高Q值滤波器,应用场景包括: [1]阻带下降较陡; [2]允许带内有纹波,与巴特沃斯相比有更好的频率选择性。

衰减函数:
$$A_{dB} = 10 \lg[1 + \varepsilon^2 T_n^2(\Omega)], \quad \varepsilon = \sqrt{10^{RdB/10} - 1}$$

$$T_n(x) = \begin{cases} (-1)^n ch(n \times arcch/x/) & x < -1 \\ cos(n \times arccosx) & -1 < x < 1 \\ ch(n \times arcchx) & x > 1 \end{cases}$$

滤波器阶数:

$$arccos \sqrt{\frac{10^{0.1L_{As}} - 1}{10^{0.1L_{Ar}} - 1}}$$

低通原型滤波器元件值:

$$g_{I} = \frac{2A_{I}\alpha}{\gamma}$$

$$g_{K} = \frac{4A_{K-I}A_{K}\alpha^{2}}{g_{K-I} \cdot B_{K-I}}, \quad K = 2,3,...,n$$

其中:

$$\ddot{\chi}_{x} = \cos\theta, \quad \boxed{\mathbb{U}}$$

$$T_{n}(x) = \cos(n\theta \circ s) \leq \theta \leq \pi.$$

$$T_{0}(x) = \cos(0) = 1$$

$$T_{1}(x) = \cos(arc\cos x) = x$$

$$T_{2}(x) = \cos(2arc\cos x) = 2x^{2} - 1$$

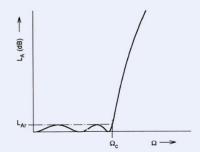
$$T_{3}(x) = \cos(3arc\cos x) = 4x^{3} - 3x$$

$$\alpha = \cosh\left\{\frac{1}{N}\cosh^{-1}\left[\frac{1}{\varepsilon}\right]\right\}$$

$$\beta = \ln\left[\coth\frac{rp}{17.37}\right] , \quad \gamma = \sinh\frac{\beta}{2N}$$

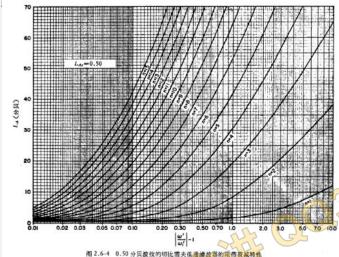
$$A_K = \sin\frac{(2K-1)\pi}{2N} , \quad K = 1, 2, ..., N$$

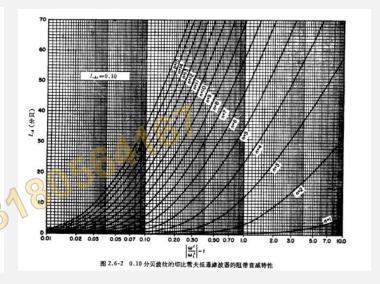
$$B_K = \gamma^2 + \sin^2\left(\frac{K\pi}{N}\right)$$



LC滤波器流流

切比雪夫 滤波器衰 减特性





# 值	g,	g ₁	83	g,	g,	g.	5 80	Ra	8.	810	g11
				0	.5 5	四 波	*RIV				
1	0.6986	1.0000			00	CJR.					
2	1.4029	0.7071	1.9841								
3	1.5963	1.0967	1.5963	1.0000							
4	1.6703	1.1926	2.3661	0.8419	1.9841						
5	1.7058	1.2296	2.5408	1.2296	1.7058	1.0000			ł		
6	1.7254	1.2479	2,6064	1.3137	2.4758	0.8696	1.9841				
7	1.7372	1.2583	2,6381	1.3444	2.6381	1.2583	1.7372	1.0000			
8	1.7451	1.2647	2.6564	1.3590	2.6964	1,3389	2.5093	0.8796	1,9841		
9	1.7504	1.2690	2.6678	1.3673	2.7239	1.3673	2,6678	1,2690	1,7504	1,0000	
10	1.7543	1.2721	2.6754	1.3725	2.7392	1.3806	2.7231	1.3485	2,5239	0.8842	1.984

1	0.3052	1.0000									
2	0.8430	0.6220	1.3554								
3	1.0315	1.1474	1.0315	1.0000							1
4	1.1088	1.3061	1.7703	0.8180	1.3554				1		
5	1.1468	1.3712	1.9750	1.3712	1.1468	1.0000					
6	1,1681	1.4039	2.0562	1.5170	1.9029	0.8618	1.3554	3			
7	1,1811	1.4228	2.0966	1.5733	2.0966	1.4228	1.1811	1.0000			
8	1.1897	1.4346	2.1199	1,6010	2.1699	1.5640	1.9444	0.8778	1.3554		
9	1.1956	1.4425	2.1345	1.6167	2,2053	1.6167	2.1345	1.4425	1.1956	1,0000	
10	1.1999	1.4481	2.1444	1.6265	2.2253	1.6418	2.2046	1.5821	1.9628	0.8853	1.355

切比雪夫低 通滤波器设 计实例

例:设计一个带内纹波为0.1dB,源端和终端阻抗为50Ω,截止频率为1GHz,且在2GHz至少有30dB衰减的切比雪夫原型滤波器?

<1>分析滤波器阶数

采用阻带衰减频率值和截止频率关系进行:

根据切比雪夫衰减响应曲线fs/fc-1=1时, n=5时, A>30dB, 因此滤波器 阶数n=5

<2>设计滤波器拓扑结构



<3>通过查表获得归一化元件值 g1=1.1468, g2=1.3712, g3=1.9750, g4=1.3712, g5=1.1468

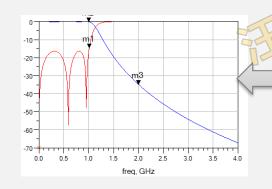


滤波器的反归一化是指低通原型滤波器到真实滤波器参数值的过程,本质为将归一化值转为实际的电感和电容值。

$$L = \frac{Z_0 g_L}{2\pi f_c}$$

$$C = \frac{g_C}{2\pi f_c Z_0}$$

例1:设计一个带内纹波为0.1dB,源端和终端阻抗为50Ω,截止频率为1GHz, 且在2GHz至少有30dB衰减的切比雪夫滤波器?



例1: g1=1.1468, g2=1.3712, g3=1.9750, g4=1.3712, g5=1.1468,

反归一化: L1=L5=(50*1.1468)/(2*3.14*1*10^9)=9.1nH;

 $C2=C4=1.3712/(2*3.14*10^9*50)=4.36pF;$

 $L3=(50*1.9750)/(2*3.14*1*10^9)=15.7nH$

半集总低通滤波器

半集总的 本质

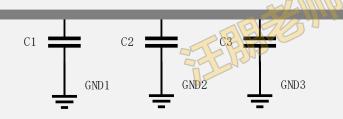
- [1] 滤波器中同时具有LC元件和微带线
- [2] 采用微带线对位模拟相应的LC元件

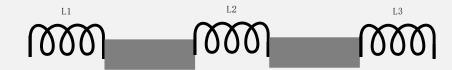
结构类型:

低通滤波器主要有半集总L型滤波器和半集总C型滤波器

优点:

解决特殊值或不常见值





串联半集 总的设计

设计原理:

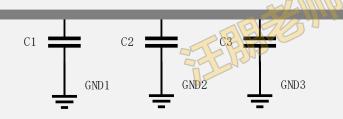
采用高阻线代替电感,采用低阻线代替电容

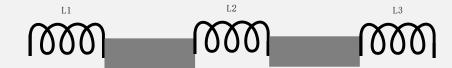
经验公式:

Zol> $(gl\ Z0)/(\pi/4)$;

 $Zoc < \pi/4 \times Z0/(gc)$;

7564167 微带线长度约为45°电角度,长度越大,截止频率越低。



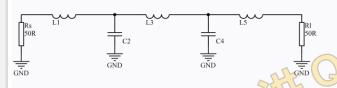


半集总的 本质

实例:

_ 设计一个带内纹波为0.1dB, 源端和终端阻抗为50Ω, 截止频率为1GHz, 且在2GHz 至少有30dB衰减的切比雪夫滤波器?

g1=1.1468, g2=1.3712, g3=1.9750, g4=1.3712, g5=1.1468,



将电感转化为微带线, 电容保持

Zol>(*gl Z*0)/(π /4)

$$Z_L = \frac{g_L Z_O}{\frac{\pi}{4}} = \frac{1.9750 * 50}{3.14/4} = \frac{98.75}{0.785} = 125.8$$

并联半集 总的设计

设计原理:

采用高阻线代替电感,采用低阻线代替电容,电容并联开路连接

经验公式:

Zol>($gl\ Z0$)/(π /4);

 $Zoc < \pi/4 \times Z0/(gc)$;

低阻微带线长度:

高阻微带线长度:

$$l_L = \frac{\lambda_g L}{2\pi} \arcsin(\frac{w_c L}{Z_o L})$$

$$l_C = \frac{\lambda_g C}{2\pi} \arctan(w_C C Z_{OC})$$



子 半集总微带低通滤波器 Part

阶跃高低阻 抗滤波器

微带滤波器设计意义;

- [1] LC元件在高频设计中的局限性;
- [2] 微带线模拟LC元件灵活可控,可以自由模拟任意值的LC元件;

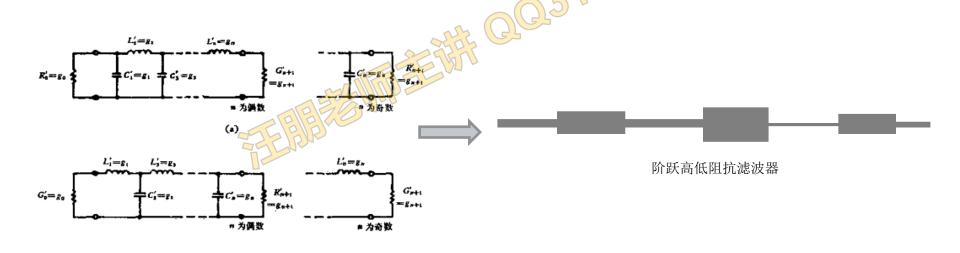
阶跃高低阻抗滤波器

椭圆函数微带低通滤波器

阶跃高低阻 抗滤波器

微带滤波器设计方法:

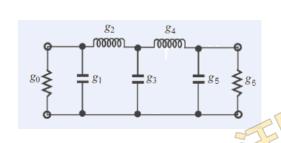
- •设计原理: 高阻抗线等效为电感元件、低阻抗线等效为电容元件
- 建立分布式参数的高、低阻抗线和低通原型滤波器元件值之间的等效计算关系
- 关键结构参数的计算: 高低阻抗线的特征阻抗、高低阻抗线的长度



阶跃高低阻 抗滤波器

阶跃高低阻抗滤波器设计要求:

- [1] 将电容等效为低阻微带线Zoc, 电感等效为高阻微带线Zol;
- [2] Zoc<Zo<Zol, Zo为源阻抗;
- [3] Zoc越低,集总电容近似度越好; Zol越大,集总电感近似度越好。



阻抗确定: $Z_{ol} > \frac{g_{i}Z_{o}}{\pi/4}$

$$Z_{oc} < \frac{\pi}{4} \frac{Z_{c}}{g_{c}}$$

根据阻抗确定微带线宽度

电感(高阻):
$$L_L = \frac{g_L Z_0}{Z_L} * \frac{\lambda_g}{2\pi};$$

电容(低阻):
$$L_c = \frac{g_c Z_c}{Z_0} * \frac{\lambda_g}{2\pi}$$

阶跃高低阻 抗滤波器

例:设计一个带内纹波为0.1dB,源端和终端阻抗为50Ω,截止频率为1GHz,且在2GHz至少有30dB衰减的切比雪夫原型微带线高低阻抗滤波器?

[1]基于指标确定滤波器节数

$$f_s = 2/1 = 2, f_{ls} = 2-1 = 1$$

根据查表:滤波器节数为5阶

[2]确定滤波器拓扑结构, 先电感后电容

[3]根据查表求解归一化值

$$g_1 = 1.1468, g_2 = 1.3712, g_3 = 1.9750, g_4 = 1.3712, g_5 = 1.1468$$

[4]微带高阻线计算

特征阻抗
$$Z_l > \frac{g_l Z_o}{\pi/4}$$
,取 g_l 最大的值带入,即 $Z_l > \frac{1.9750 \times 50}{3.1415/4} = 125.7$,定 $Z_l = 130$

[5]微带低阻抗线的计算

$$Z_c < \frac{\pi}{4} \times \frac{Z_o}{g_c} = \frac{3.1415}{4} \times \frac{50}{1.3712} = 28.6, \text{ m } \equiv Z_c = 15$$

[6]计算高阻线线长

$$L_{t_1} = \frac{g_1 \times Z_a}{Z_t} \times \frac{\lambda_s}{2\pi} = \frac{1.1468 \times 50}{130} \times \frac{177.9}{6.28} = 12.5 = L_{t_5}$$

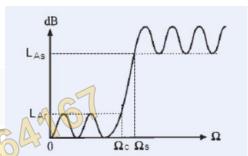
$$L_{13=} \frac{1.9750 \times 50}{130} * \frac{177.9}{6.28} = 21.5$$

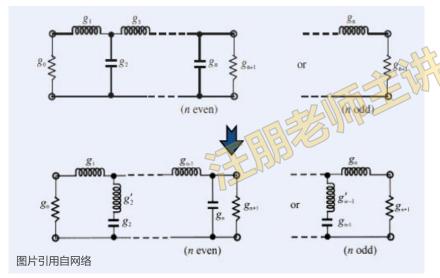
[7]计算低阻线长度

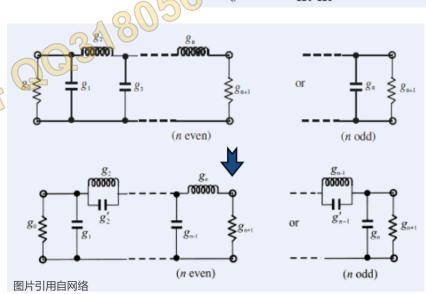
$$L_{c2} = \frac{g_c \times Z_c}{Z_o} \times \frac{\lambda_g}{2\pi} = \frac{1.3712 \times 15}{50} \times \frac{152.3}{6.28} = 9.97 = L_{c4}$$

椭圆函数微 带滤波器

- [1] 椭圆函数逼近理想低通滤波器的衰减特性
- [2] 椭圆函数原型滤波器具有更陡的带外衰减



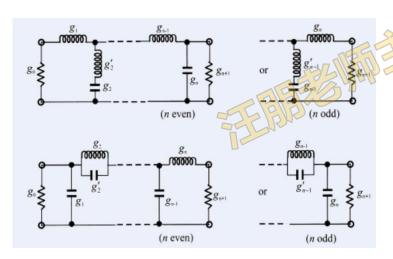


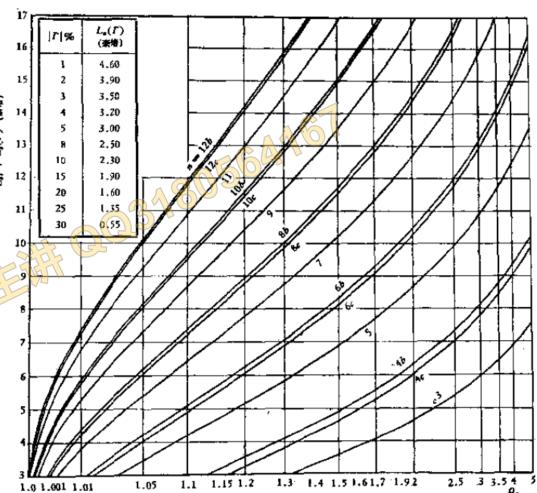


椭圆函数微 带滤波器

Las (dB) =
$$(LY-4.6)*8.68$$

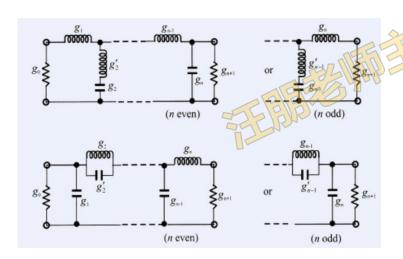
椭圆函数滤波器阶数确定





椭圆函数微 带滤波器

椭圆函数滤波器归一化数值表



1,186 35 1.439 0.3580.9671,762 1.116 0.6001.026 1.270 40 1.495 0.2791.016 1.880 1.114 0.840 0.6961.369 1,530 0.218 45 1.063 1,997 0.627 1.241 0.7931.481 0.1722.113 50 1.563 1.099 0.482 1.320 0.8751.618 55 1.559 0.134 1.140 2.188 0.369 1.342 0.9491.782 1.603 0.1081.143 2.248 0.2910.9951.449 1.963 1,626 65 0.0860 1.158 2,306 0.230 1.037 1.501 2.164 70 1.624 0.0679 1.178 2,319 0.182 1.521 1.078

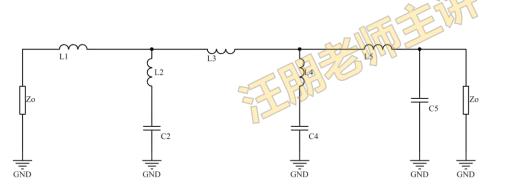
	L_{Ar}	=	0.1	分	见
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	12 (L_A	, = 0.1 分	贝			
35	1.309	35	0.977	0.230	1,139	1.488	0,742	0.740	0.701
	1,414	40	1.010	0.177	1.193	1.586	0.530	0.875	0.766
	1.540	45	1.032	0.140	1.228	1.657	0.401	0.964	0.836
	1,690	50	1.044	0,1178	1.180	1.726	0.283	1.134	0.885
	1.860	55	1.072	0.0880	1.275	1.761	0.241	1.100	0.943
	2.048	60	1.095	0.0699	1.292	1.801	0.192	1.148	0.988
	2,262	65	1.108	0.0555	1.308	1.834	0.151	1.191	1.022
	2,512	70	1.112	0.0440	1.319	1.858	0.119	1.225	1.044
	Ω,	L_{As}	L_1	L ₂	C 2	L_3	L.	с.	L,

椭圆函数微 带滤波器

设计步骤:

- [1] 通过查表求解滤波器阶数和归一化元件值;
- [2] 求解实际集总元件值;
- [3] 计算椭圆函数滤波器传输极点;
- [4] 设定电容电感等效高低阻抗值;
- [5] 求解微带线宽度和长度;



$$L_i = \frac{1}{2\pi f_c} Z_o g_{Li}$$

实际元件值
$$C_i = \frac{1}{2\pi f_o} \frac{1}{Z_o} g_{Ci}$$

传输极点

$$f_p = \frac{1}{2\pi\sqrt{L_f C_f}} \quad [谐振枝节]$$

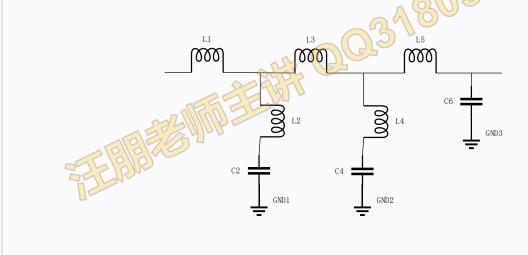
$$l_{Ci} = \frac{\lambda_{gC}(f_c)}{2\pi} \arcsin(2\pi f_c Z_c C_i)$$

椭圆函数微 带滤波器

设计实例:

设计指标: 截止频率fc=1GHz, 通带纹波Lar=0.18dB, 归一化阻带角频率 $\Omega s=1.194$, 对应的最小阻带衰减Las=38dB, 源阻抗和负载阻抗Zo=50欧姆

1.194 38.1 0.8214 0.3892 1.084 1.188 0.7413 0.9077 1.117 1.136



椭圆函数微 带滤波器 设计实例:

设计指标: 截止频率fc=1GHz, 通带纹波Lar=0.18dB, 归一化阻带角频率 $\Omega s=1.194$, 对

$$L1 = 6.56nH$$
, $L2 = 3.1nH$, $L3 = 9.5nH$, $L4 = 5.9nH$, $L5 = 8.9nH$

$$C2 = 3.5 pF, C4 = 2.9 pF, C6 = 3.6 pF$$

$$L_{1} = \frac{1}{2\pi f_{o}} \times Z_{o} \times g_{11} = \frac{1}{6.28 \times 1 \times 10^{9}} \times 50 \times 0.8214 = 6.56 \times 10^{-9} H = 6.56 nH$$

$$L_2 = \frac{1}{2\pi f_c} \times Z_o \times g_{12} = \frac{1}{6.28 \times 1 \times 10^9} \times 50 \times 0.3892 = 3.1 \times 10^{-9} H = 3.1 nH$$

$$C2 = \frac{1}{2\pi f_c Z_o} \times g_{c2} = \frac{1}{6.28 \times 1 \times 10^9 \times 50} \times 1.084 = 0.0035 \times 10^{-9} F = 3.5 pF$$

[3] 传输极点的计算
$$f_{p1} = \frac{1}{2\pi\sqrt{lc}} = \frac{1}{2\times3.14\sqrt{l_2c_2}} = \frac{1}{2\times3.14\times\sqrt{3.1\times3.5\times10^{-21}}} = 1.24GHz$$

$$f_{p2} = \frac{1}{\sqrt{l_2c_2}} = \frac{1}{2\times3.14\times\sqrt{3.1\times3.5\times10^{-21}}} = 1.53GHz$$

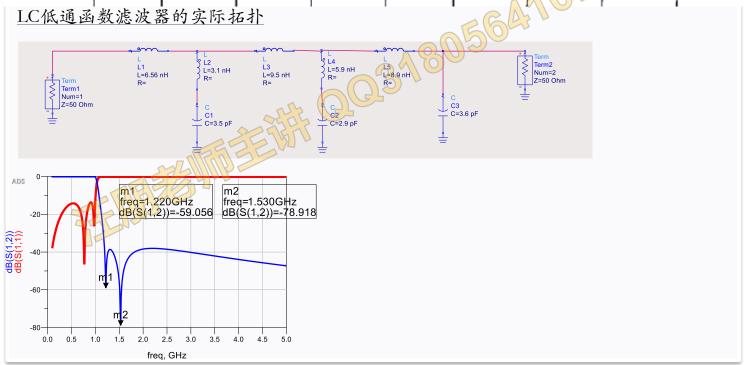
椭圆函数微 带滤波器

设计实例:

设计指标: 截止频率fc=1GHz, 通带纹波Lar=0.18dB, 归一化阻带角频率 $\Omega s=1.194$, 对

应的最小阻带衰减Las=38dB,源阻抗和负载阻抗Zo=50欧姆

1.194 38.1 0.8214 0.3892 1.084 1.188 0.7413 0.9077 1.117 1.136



[4] 设定微带线的高低阻抗值

Zoc<Zo<Zol 设定: Zol=95, Zoc=15

$$f_c = 1GHz, Z_{oL} = 95, \lambda_g = 173.4mm$$

 $f_c = 1GHz, Z_{oC} = 15, \lambda_g = 152.3mm$

$$t_c = 1GHz, Z_{oC} = 15, \lambda_g = 152.3mm$$

$$\lambda_c \qquad L \qquad \lambda_c$$

$$l_{Li} = \frac{\lambda_{gL}(f_c)}{2\pi} \arcsin(2\pi f_c \frac{L_i}{Z_L})$$

$$l_{Ci} = \frac{\lambda_{gC}(f_c)}{2\pi} \arcsin(2\pi f_c Z_C C_i)$$

$$f_{c} = 1GHz, Z_{oC} = 15, \lambda_{g} = 152.3mm$$

$$l_{L1} = \frac{\lambda_{g}}{2\pi} \arcsin(2\pi f_{c} \frac{L_{1}}{Z_{c}}) = \frac{\lambda_{g}}{2\pi} \arcsin(2\times3.14\times10^{9} \times \frac{6.56\times10^{-9}}{95}) = \frac{\lambda_{g}}{2\pi} \arcsin(0.43) = \frac{\lambda_{g}}{2\pi} \times 0.44 = \frac{173.4}{6.28} \times 0.44 = 12.15mm$$

$$l_{L2} = \frac{\lambda_g}{2\pi} \arcsin(2\pi f_c \frac{L_1}{Z_L}) = \frac{\lambda_g}{2\pi} \arcsin(2\times3.14\times10^9 \times \frac{3.1\times10^{-9}}{95}) = \frac{\lambda_g}{2\pi} \arcsin(0.20) = \frac{\lambda_g}{2\pi} \times 0.44 = \frac{173.4}{6.28} \times 0.21 = 5.8mm$$

$$l_{C2} = \frac{\lambda_g}{2\pi} \arcsin(2\pi f_c C_2 Z_C) = 24.25 \times \arcsin(6.28\times10^9 \times 3.5\times10^{-12} \times 15) = 24.25 \times 0.30 = 8.16mm$$

$$l_{L3} = \frac{\lambda_g}{2\pi} \arcsin(2\pi f_c \frac{L_3}{2\pi}) = 27.6 \times \arcsin(2 \times 3.14 \times 10^9 \times \frac{9.5 \times 10^{-9}}{95}) = 19mm$$

$$(\frac{10}{5}) = 19mm$$

$$l_{L4} = \frac{\lambda_g}{2\pi} \arcsin(2\pi f_c \frac{L_4}{Z_L}) = 27.6 \times \arcsin(2 \times 3.14 \times 10^9 \times \frac{5.9 \times 10^{-9}}{95}) = 11.3 mm$$

$$l_{L5} = \frac{\lambda_g}{2\pi} \arcsin(2\pi f_c \frac{L_5}{Z}) = 27.6 \times \arcsin(2 \times 3.14 \times 10^9 \times \frac{8.9 \times 10^{-9}}{95}) = 17.5 mm$$

$$l_{C4} = \frac{\lambda_g}{2\pi} \arcsin(2\pi f_c C_4 Z_C) = 24.25 \times \arcsin(6.28 \times 10^9 \times 2.9 \times 10^{-12} \times 15) = 6.1 mm$$

$$l_{C4} = \frac{\lambda_g}{2\pi} \arcsin(2\pi f_c C_4 Z_C) = 24.25 \times \arcsin(6.28 \times 10^9 \times 2.9 \times 10^{-12} \times 15) = 6.1 mm$$

$$l_{C6} = \frac{\lambda_g}{2\pi} \arcsin(2\pi f_c C_6 Z_C) = 24.25 \times \arcsin(6.28 \times 10^9 \times 3.6 \times 10^{-12} \times 15) = 7.7 mm$$

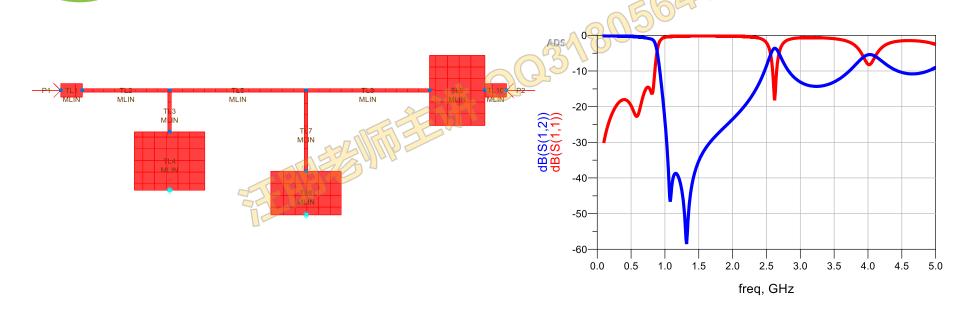
椭圆函数微 带滤波器

[4] 设定微带线的高低阻抗值

Zoc<Zo<Zol 设定: Zol=95, Zoc=15

 $l_{Li} = \frac{\lambda_{gL}(f_c)}{2\pi} \arcsin(2\pi f_c \frac{L_i}{Z_L})$

 $l_{Ci} = \frac{\lambda_{gC}(f_c)}{2\pi} \arcsin(2\pi f_c Z_c C_i)$



THANK YOU!!