

# Energy and exergy analysis of a cruise ship

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## Abstract

*Keywords:*

low carbon shipping, energy analysis, exergy analysis, energy efficiency

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## 1. Introduction

### 1.1. Background

According to the third IMO GHG Study, in 2012 CO<sub>2</sub> emissions from shipping amounted to a total of 949 million tonnes, contributing to 2.7% of global anthropogenic CO<sub>2</sub> emissions [1]. Although this contribution appears relatively low, the trend is that shipping will play an even greater role in the future due to the increased transport demand according to all IMO future scenarios [1]. As an example, global transport demand has increased by 3.4% in 2014, compared to a global GDP growth of 2.5% the same year, which shows how shipping tends to rise even faster than global economy [2].

International Energy Agency data show that the OECD countries have reduced the CO<sub>2</sub> impact from shipping, but a larger amount has been moved to the non-OECD countries [3]. The fact that shipping needs to even further reduce its CO<sub>2</sub> emissions in the near future is essential for being able to achieve the goals of maintaining the climate below a 2-degree level in 2050 [4]. Finally, in the Baltic Sea an emission control area is enforced by the International Maritime Organisation since January 2015 which stipulates that the fuel used must not contain more than 0.1% sulphur, therefore requiring

the use of more expensive distillate fuels. More generally making shipping sustainable is a challenge that will demand growing attention by the shipping industry [3]

Altogether, these conditions present a challenge to the shipping companies who attempt to reduce their fuel consumption, environmental impact, and operative costs. A wide range of fuel saving solutions for shipping are available and partially implemented in the existing fleet, both from the design and operational perspective; several specific studies have been conducted on these technologies, and a more detailed treatise would be out of the scope of this work. In this context, it has been acknowledged that the world fleet is heterogeneous, and measures need to be evaluated on a ship-to-ship basis [4]. In this process, a deeper understanding of energy use on board of the specific ship is vital.

### *1.2. Previous work*

The idea of improving the understanding of the behavior of the energy system of a ship is not new. Most of the work published around this subject relates to the use of mathematical models of the ship systems.

Most authors focused on the propulsion part of the problem, as this is often the most relevant energy demand on board. Shi et al. proposed a modeling approach for predicting ship fuel consumption of a cargo/passenger ferry [5]; Theotokoats and Tzelepis applied a similar procedure to the case of a Handymax product carrier [6], similarly to Tillig et al., who also added the dynamic element to their predictive model [7].

The work referenced above allowed improving the understanding of how many operational (such as the ship's speed) and environmental (such as wave height and wind speed) parameters influence the ship's energy performance. These studies, however, are not based on actual measurements of the ship's operations. Also, they focus entirely on the ship's power demand for propulsion. This is a very reasonable practice for most ship types, given that propulsion represent the largest part of the total energy demand, but does not allow improving the knowledge of the remaining part of the system.

Other authors filled the gap by both including electric energy demand, and by basing their work on measurements from actual ship operations. The work presented by Thomas et al. [8] and Basurko et al. [9] shows the application of energy auditing methods to fishing vessels. This approach represents a step forward towards improving the understanding of how energy is used on board during actual ship operations.

More generally, several authors have highlighted the importance of a detailed knowledge of the ship's operational profile in order to appropriately assess and optimize possible alternatives for improving ship energy efficiency [10]. Coraddu et al., started from a statistical analysis of measured ship operations and used the aggregated data, together with a computational model of the vessel, to provide a better prediction of the actual ship's operational efficiency [11]. The importance of considering the operational profile was also showed in the case of the optimization of engine-propeller interaction [12], in the process of retrofitting existing systems [13, 14], and in ship design [15, 16].

Heat demand is rarely a subject of concern on board ships, with some notable exceptions. This is due to a combination of generally low demand and high availability from the waste heat of the engines. In a previous publications by the authors, for instance, it is shown that in the case of a product tanker, although the heat demand was estimated to account for roughly 20% of the total energy demand of the ship on a yearly basis, it only contributes to 4.1% of the total fuel consumption (contribution of the auxiliary boilers), while the rest of the demand is fulfilled using waste heat [17].

It should be noted that, however, much research effort has been devoted, especially in recent times, to the improvement of the efficiency of ship energy systems by recovering the waste heat available from the engines. With reference to different types of technologies, case studies, and designs, the several authors showed the existence of a quite significant potential for energy saving when WHR systems are employed, ranging from around 1% for single-pressure steam cycles applied to two-stroke engines [18] to more complex systems based on ORCs (up to 10%, [19]) or including the cooling systems as a source of waste heat (over 10%, [20]). The case of the installation of an ORC on board of the vessel investigated in this study (see Section 2.3) was presented in [21], showing a similar potential.

The potential uses for waste heat on board are not limited to improving the efficiency of the power plant. Waste heat is commonly used for fulfilling on board heat demand for spatial heating and freshwater generation [22, 17, 23]; Balaji et al. proposed the use of waste heat for ballast-water systems [24]; Salmi et al. suggested its use for adsorption refrigeration systems [25]. A detailed review of potential uses for waste heat from marine engines is presented by Shu et al [26].

Some ship types constitute notable examples. On cruise ships the heat demand is significantly higher compared to standard cargo ships. Referring

to winter conditions, Marty et al. estimated the instantaneous heat demand of a selected cruise ship to reach roughly 23 MW, compared to an estimated peak of 49 MW for propulsion and electric auxiliaries combined [27].

This shows how the heat from the engines should be considered as a potential resource, rather than a waste, and that there is potential for improvement based on the optimal use of these heat sources. The work presented by the authors in [28] represent a step in this direction; however, there is the need for an increased detail in the estimation of the heat demand.

Exergy analysis provides a more accurate estimation of the potential for energy recovery on board. The application of exergy analysis to the case of ship energy systems is, however, still limited. Dimopoulos et al. showed how the process optimizing the WHR system of a container ship can be more efficient if exergy efficiency, rather than energy efficiency, is used as the target of the optimization [20]; Baldi et al. also analyzed the exergy flows on board of a product tanker, showing that this allows having a more accurate understanding of what parts of the system show potential for improvement [17]; similar results were obtained by Marty et al., who focused on the power plant of a cruise ship [29]. Koroglu et al. made a step further also including advanced exergy analysis in their study [30].

### *1.3. Aim*

Given the existing limitations of the current available information in scientific literature highlighted in the previous section, the objective of this work is the following:

- Analyse the demand of a cruise ship in terms of propulsion power, electric power and heat, based on operational measurements.
- Analyse the current efficiency of the system, and potential ways to improve it, by means of applying exergy analysis
- Provide a more detailed analysis of the heat demand of a cruise ship, as a basis for further studies on how to optimize the whole efficiency of the propulsion plant.

## **2. Method**

Here an overview of the method is provided:

- Data gathering

- Data filtering
- Data pre-processing
- Heat demand estimation
- Statistical analysis
- Energy and exergy analysis

### 2.1. *Energy analysis*

### 2.2. *Exergy analysis*

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### 2.3. *Case study vessel*

The ship under study is a cruise ship operating on a daily basis in the Baltic Sea between Stockholm and the island of land. The ship is 176.9 m long and has a beam of 28.6 m, and has a design speed of 21 knots. The ship was built in Aker Finnyards, Raumo Finland in 2004. The ship has a capacity of 1800 passengers and has several restaurants, night clubs and bars, as well as saunas and pools. This means that the energy system regarding the heat and electricity demand is more complex than a regular cargo vessel in the same size. Typical ship operations, although they can vary slightly between different days, are represented in Figure 1. It should be noted that the ship stops and drifts in open sea during night hours before mooring at its destination in the morning, if allowed by weather conditions.

The ship systems are summarized in Figure 2. The propulsion system is composed of two equal propulsion lines, each made of two engines, a gearbox, and a propeller. The main engines are four Wartsil 4-stroke Diesel engines (ME) rated 5850 kW each. All engines are equipped with selective catalytic reactors (SCR) for NOX emissions abatement. Propulsion power is needed whenever the ship is sailing; however, it should be noted that the ship rarely sails at full speed, and most of the time it only needs one or two engines operated simultaneously.

Auxiliary power is provided by four auxiliary engines (AE) rated 2760 kW each. Auxiliary power is needed on board for a number of alternative functions, from pumps in the engine room to lights, restaurants, ventilation and entertainment for the passengers.

Auxiliary heat needs are fulfilled by the exhaust gas steam generators (HRSG) located on all four AEs and on two of the four MEs or by oil-fired auxiliary boilers (mainly when in port, or during winter), by the heat recovery on the HT cooling water systems (HRHT), and by the auxiliary, oil fired boilers (AB). The heat is needed for passenger and crew accommodation, as well as for the heating of the highly viscous heavy fuel oil used for engines and boilers. This last part, however, is drastically reduced since the 1st of January 2015, as new regulations entering into force require the use of low-sulphur fuels, which require a much more limited heating.

#### *2.4. Data gathering*

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#### *2.5. Data pre-processing: Ship energy system modeling*

Not all of the variables required to perform a full energy and exergy analysis of the system are available from measurements. In some cases, they are measurable, but not measured (e.g. some temperatures, mass flows, etc.). In other cases, they are simply impossible, or impractical, to measure (e.g. specific enthalpy, specific entropy). For this reason, part of the ship systems needed to be modeled in order to derive the unknown variables.

*Main engines*

*Auxiliary engines*

*Auxiliary boilers*

*Cooling systems*

#### *2.6. Estimation of the heat demand*

*Production-side*

In a top-down model, the demand of an energy system is modeled based on the production side of the energy balance. According to the top-down approach, the total heat consumption is calculated based on the sum of the heat provided by the three main heat sources available on board:

- Exhaust gas boilers
- Auxiliary oil-fired boilers
- Heat recovery on the HT cooling systems

For the case of the EGBs, the heat transferred from the exhaust gas to the steam ( $\dot{Q}_{EGB}$ ) is calculated according to equation 2.6:

$$\dot{Q}_{EGB} = \dot{m}_{eg} c_{p,eg} (T_{eg,EGB,in} - T_{eg,EGB,out}) \quad (1)$$

Where measurements of the exhaust gas temperature before and after the EGBs (respectively  $T_{eg,EGB,in}$  and  $T_{eg,EGB,out}$ ) are available from the DLS; the mass flow of exhaust gas ( $\dot{m}_{eg}$ ) is calculated as described in appendices ?? and ??; and the specific heat at constant pressure of the exhaust gas ( $c_{p,eg}$ ) is assumed to be constant and equal to  $1.08 \frac{kJ}{kgK}$ .

For the case of the ABs, the heat transferred to the steam ( $\dot{Q}_{AB}$ ) is calculated according to equation 2.6:

$$\dot{Q}_{AB} = \dot{m}_{fuel,AB} \eta_{AB} \quad (2)$$

Where the fuel consumption of the ABs ( $\dot{m}_{fuel,AB}$ ) is available on a monthly basis. No information was available concerning the first-law efficiency of the boilers ( $\eta_{AB}$ ). [31] estimated it to vary between 0.83 and 0.89 depending on the load of the boiler, while according to a more recent experimental campaign presented in [32] the efficiency varies between 0.7 and 0.79. In the absence of more specific available data, a value of 0.8 was selected for  $\eta_{AB}$ .

The contribution from the heat recovery on the high temperature cooling systems of the engines ( $\dot{Q}_{HRHT}$ ) represents the main uncertainty related to the top-down estimations. This contribution cannot be measured, neither directly or indirectly, and hence needs to be estimated.

For this reason, two calculated values for the top-down heat demand are provided:

- A **high boundary** case, where it is assumed that almost all of the heat available from the HT cooling systems (an utilization factor of 0.9 is assumed to account for losses) is used. This corresponds to the assumption that the use of the waste heat from the HT cooling systems is prioritized over the use of waste heat from the exhaust gas of the engines.

$$\dot{Q}_{HRHT} = f_{HRHT} \dot{Q}_{HT,tot} \quad (3)$$

- a **low boundary** case, where it is assumed that the waste heat from the cooling systems is only used when the ship is in port (again assuming a utilization factor of 0.9).

In both cases, the available heat from the HT cooling systems is estimated as explained in Section ??.

#### *Consumers-side*

Following, the assumptions that we have made related to the bottom-up estimations of ship heat demand:

- The maximum demand for **spacial heating** is connected to a design minimum outer air temperature of  $-5^{\circ}\text{C}$ .
- The minimum demand for **spacial heating** is 0 for an external temperature of  $20^{\circ}\text{C}$  (NOTE: Maybe 15 is more reasonable?)
- **Spacial heating** demand is linearly dependent on the external air temperature
- In the HVAC unit, the "**Preheater**" is only used when heating (i.e., in winter) while the "**Reheater**" is only used when cooling (i.e., in summer)
- Every passenger contributes with a total of 150 W of free heat during the day (8-23, ref. to "walking, seated" activity from [33]) and 100 W during night (23-8, ref. to "seated at rest" activity from [33]). For the crew, as it is assumed that they perform a more intense activity than the passengers, the daily contribution is considered equal to 160 (ref. to "moderate work" activity from [33])
- The heat required for **tank heating** is linearly dependent on the external sea water temperature. The maximum heat is required for an external seawater temperature of  $0^{\circ}\text{C}$
- The heat required from the **galley** depends on two parameters:
  - The **number of passengers** (linear dependence)
  - the **hour of the day**. The hour-dependent factor is 0 at night (21-7), 0.1 during non-eating times (10-11 and 14-18) and 1 during eating times



Name	$\dot{Q}_{des}$ [kW]	Depends on...					
		$T_{air}$	$t$	$N_{pax}$	$f_{TL}$	$\lambda$	
Hot water heater	1200		x	x			
HVAC Preheater	3500	x	x	x			
HVAC Reheater	1780	x	x	x			
Tank heating	208				x		
Other tanks	138				x		
HFO Tank heating	271				x		
Machinery space heaters	281	x					
Bilge water separator	26						
Hot water calorifier	366		x				
Fuel oil heater	103					x	
HFO Separator	37						
Galley	602		x	x			

- The heat required from the **hot water** depends on two parameters:
  - The **number of passengers** (linear dependence)
  - the **hour of the day**. The hour-dependent factor is assumed based on the estimations for a land-based hotel reported in [34].

In Table 2.6 we summarize all heat consumers on board the case study vessel. For each entry, we provide the design heat demand and the variables we assumed the actual heat demand to depend on:

### 3. Results (and discussion)

#### 3.1. Exploratory analysis

Here we show and discuss about some interesting values.

- External temperature
- Sea water temperature
- Propulsion power distribution
- Electric power distribution
- Other

3.2. *Energy analysis*

3.3. *Exergy Analysis*

3.4. *Heat demand*

#### 4. Discussion

#### 5. Conclusion

#### Appendix A. Estimation of air and exhaust gas flows in the main engines

#### Appendix B. Estimation of air and exhaust gas flows in the auxiliary engines

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