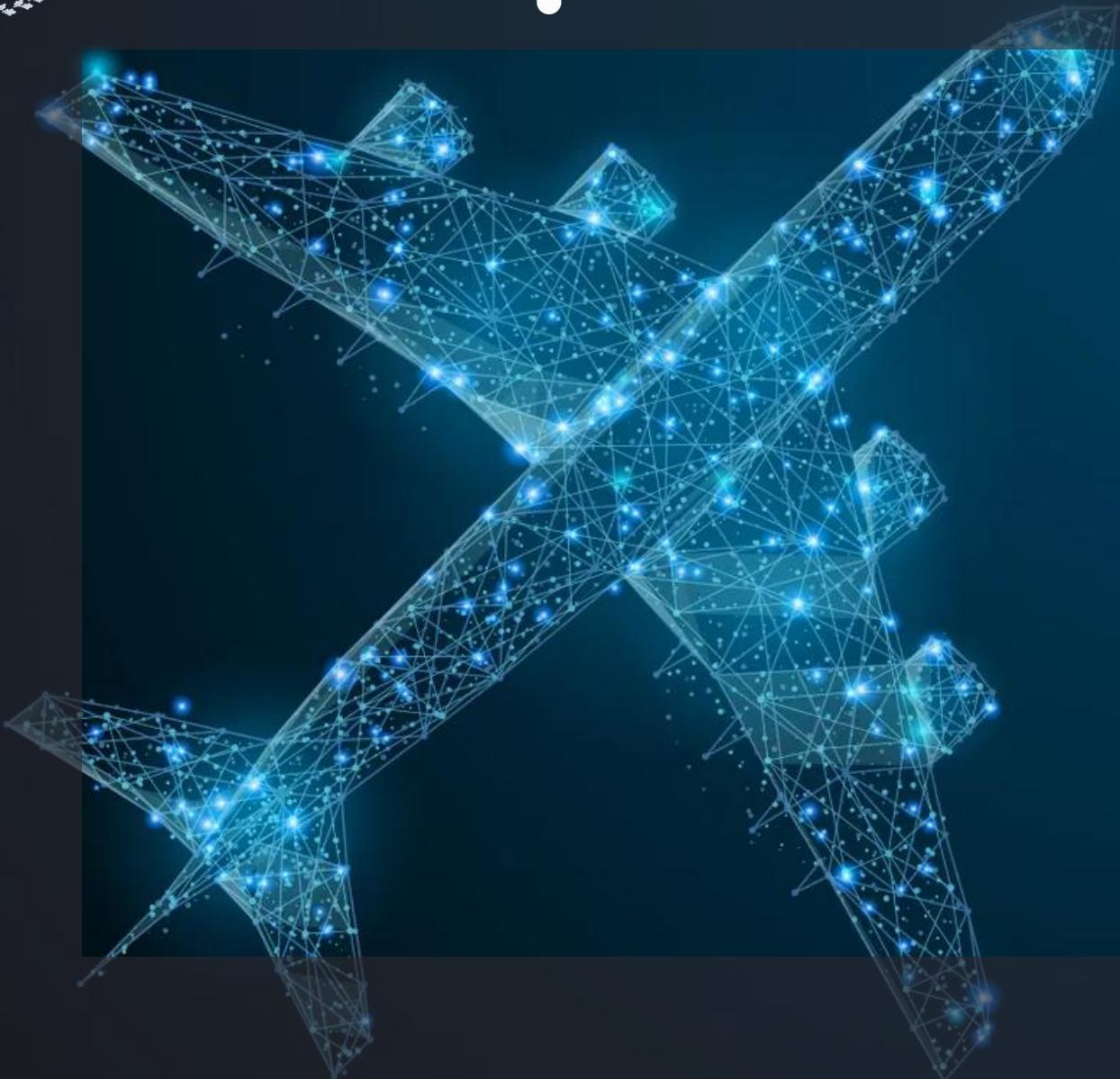




Politecnico
di Torino



Progettazione di veicoli
aerospaziali (AA-LZ)

E1. Conceptual Design of
subsonic commercial
aircraft

2. **TAKE-OFF WEIGHT**

Karim Abu Salem
karim.abusalem@polito.it

Giuseppe Palaia
giuseppe.palaia@polito.it

Introduction



A brief recap...

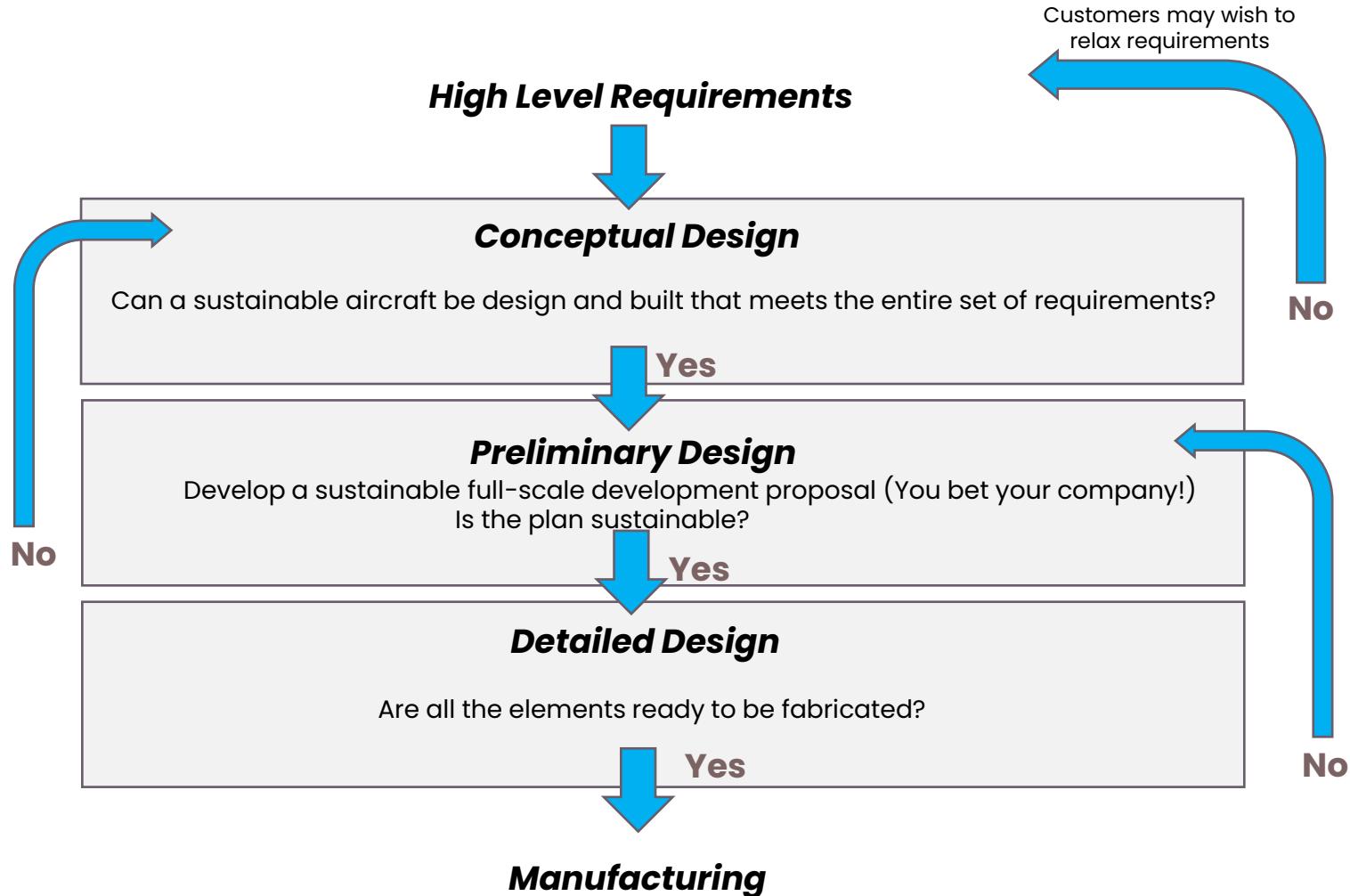
Main Goals



- 1** To understand the importance of Conceptual Design among the design and development phases of an aircraft.
- 2** To acquire knowledge about the most up-to-date methodologies for Conceptual Design of aircraft
- 3** To understand the most influential factors on the Conceptual Design of a modern commercial aircraft
- 4** To be able to perform a Conceptual Design of a modern commercial aircraft



Aircraft Design Phases



Aircraft design results to be iterative and highly multidisciplinary process!



High Level Requirements

$$HR = (x_{j_1}) \cup (p_{j_2}) \cup (q_{j_3}) \cup (r_{j_4})$$

Set of Performance $\left\{ \begin{array}{l} \text{Cruise Mach Number: } x_1 \geq 0.85 \\ \text{Range: } x_2 \geq 5000 \text{ km} \\ \dots \end{array} \right.$

Set of Design Parameters $\left\{ \begin{array}{l} \text{Payload Mass: } p_1 \geq 10 \text{ t} \\ \text{Fuselage Length: } p_2 \leq 40 \text{ m} \\ \text{Wing span: } p_3 \leq 35 \text{ m} \\ \dots \end{array} \right.$

Set of Operational Requirements $\left\{ \begin{array}{l} \text{Cruise Altitude: } 11 \text{ km} \leq q_1 \leq 12 \text{ km} \\ \text{Turn Around Time: } q_2 \leq 2 \text{ h} \\ \dots \end{array} \right.$

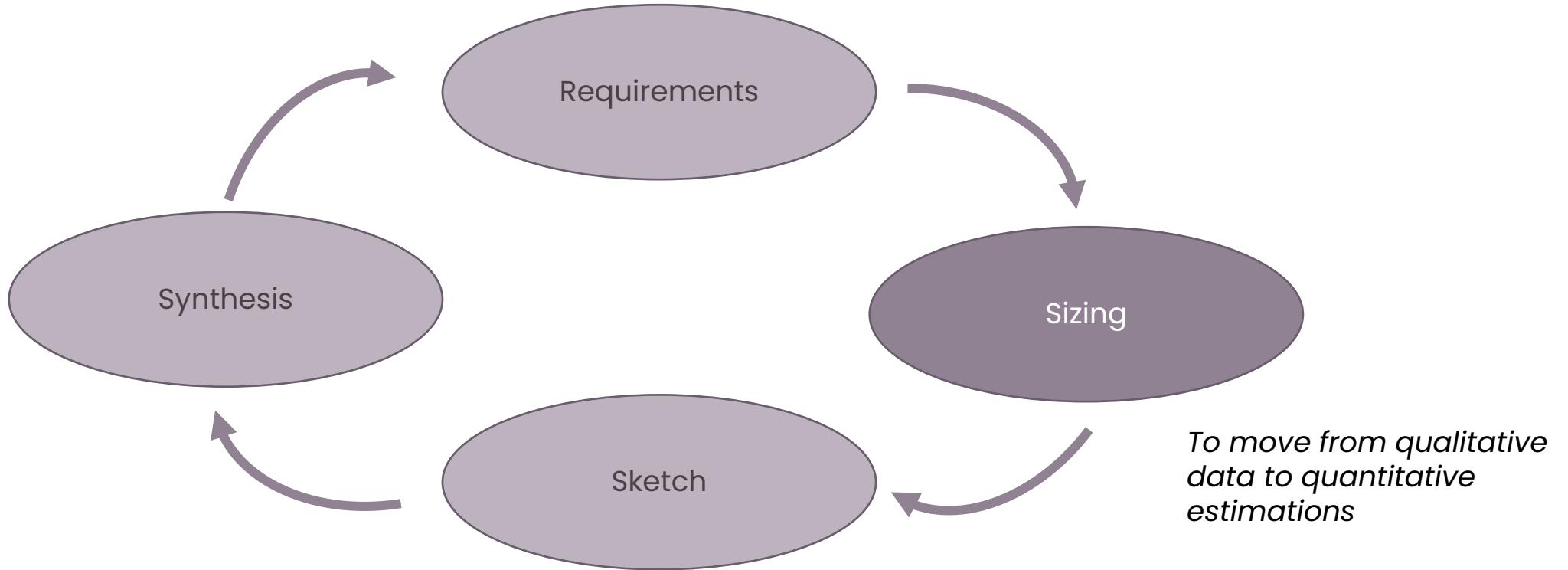
Set of Constraints from Regulatory Framework $\left\{ \begin{array}{l} n_{exits} = f(n_{pax}, g[m_{pay}]) \\ \text{Balance Field Length} \\ \dots \end{array} \right.$

Where

- ✓ HR is the entire set of Design Specifications;
- ✓ x_{j_1} ($j_1 = 1:n_1$) is the set of target performance to be reached
- ✓ p_{j_2} ($j_2 = 1:n_2$) is the set of design parameters initially set by customers
- ✓ q_{j_3} ($j_3 = 1:n_3$) is the set of operational requirements
- ✓ r_{j_4} ($j_4 = 1:n_4$) is the set of constraints superimposed by the applicable regulatory framework

New Requirements for new
aircraft configurations

Design Problem



Conceptual Design Process

Highly Iterative
Highly Multidisciplinary

The Aircraft Design process



Multi-Stage

Initial Sizing

Conceptual Design

Preliminary Design

Detailed Design

Production

Testing

..Fly!



The Aircraft Design process

Multi-Stage

Requirements

Initial Sizing

Conceptual Design

Thousands of configurations

Preliminary Design

Layout fixed

Detailed Design

Production

Testing

..Fly!



The Aircraft Design process

Multi-Stage

Requirements

Initial Sizing

Conceptual Design

Preliminary Design

Detailed Design

Production

Testing

..Fly!

Multi-Disciplinary

Aerodynamics

Structures

Flight mechanics

Propulsion

On-board systems

Weights optimization

Payload

Performance

Control systems

The Aircraft Design process



Multi-Stage

Requirements

Initial Sizing

Conceptual Design

Preliminary Design

Detailed Design

Production

Testing

..Fly!

Multi-Disciplinary

Aerodynamics

Structures

Flight mechanics

Propulsion

On-board sys.

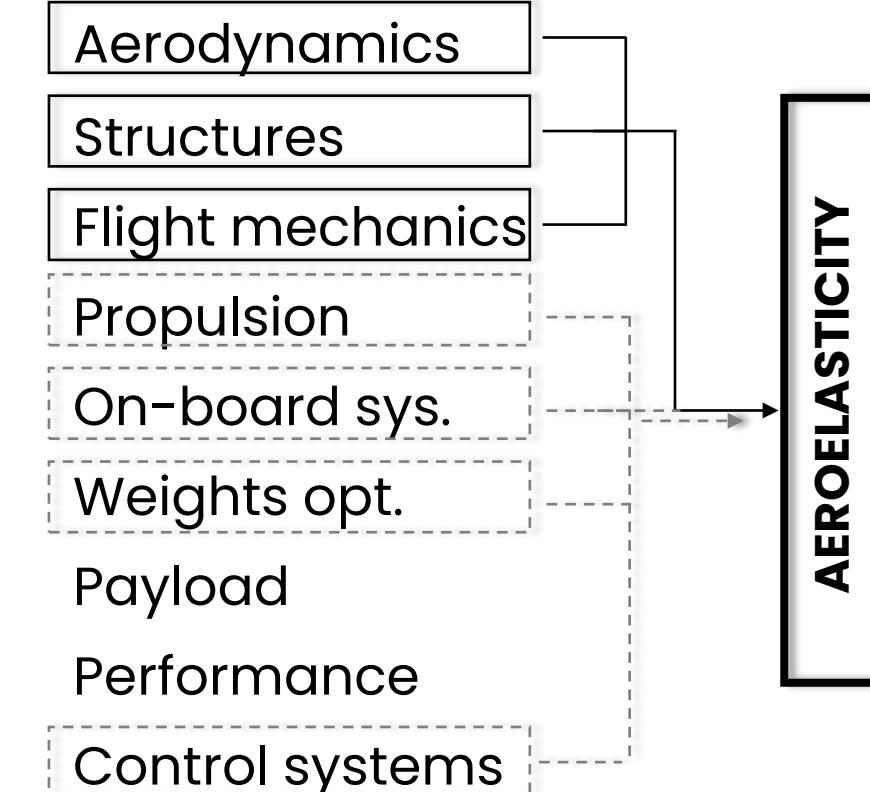
Weights opt.

Payload

Performance

Control systems

AEROELASTICITY





The Aircraft Design process

Multi-Stage

Requirements
Initial Sizing
Conceptual Design

Preliminary Design

Detailed Design
Production
Testing
..Fly!

Multi-Disciplinary

Aerodynamics
Structures
Flight mechanics
Propulsion
On-board systems
Weights optimization
Payload
Performance
Control systems

Multi-Fidelity

Textbook methods
Statistics/empirical data
Analytical methods
Numerical simulations
Level 1
Level 2
Level 3
Experimental
Flight test



The Aircraft Design process

Multi-Stage

Requirements
Initial Sizing

Conceptual Design

Preliminary Design

Detailed Design

Production
Testing
..Fly!

Multi-Disciplinary

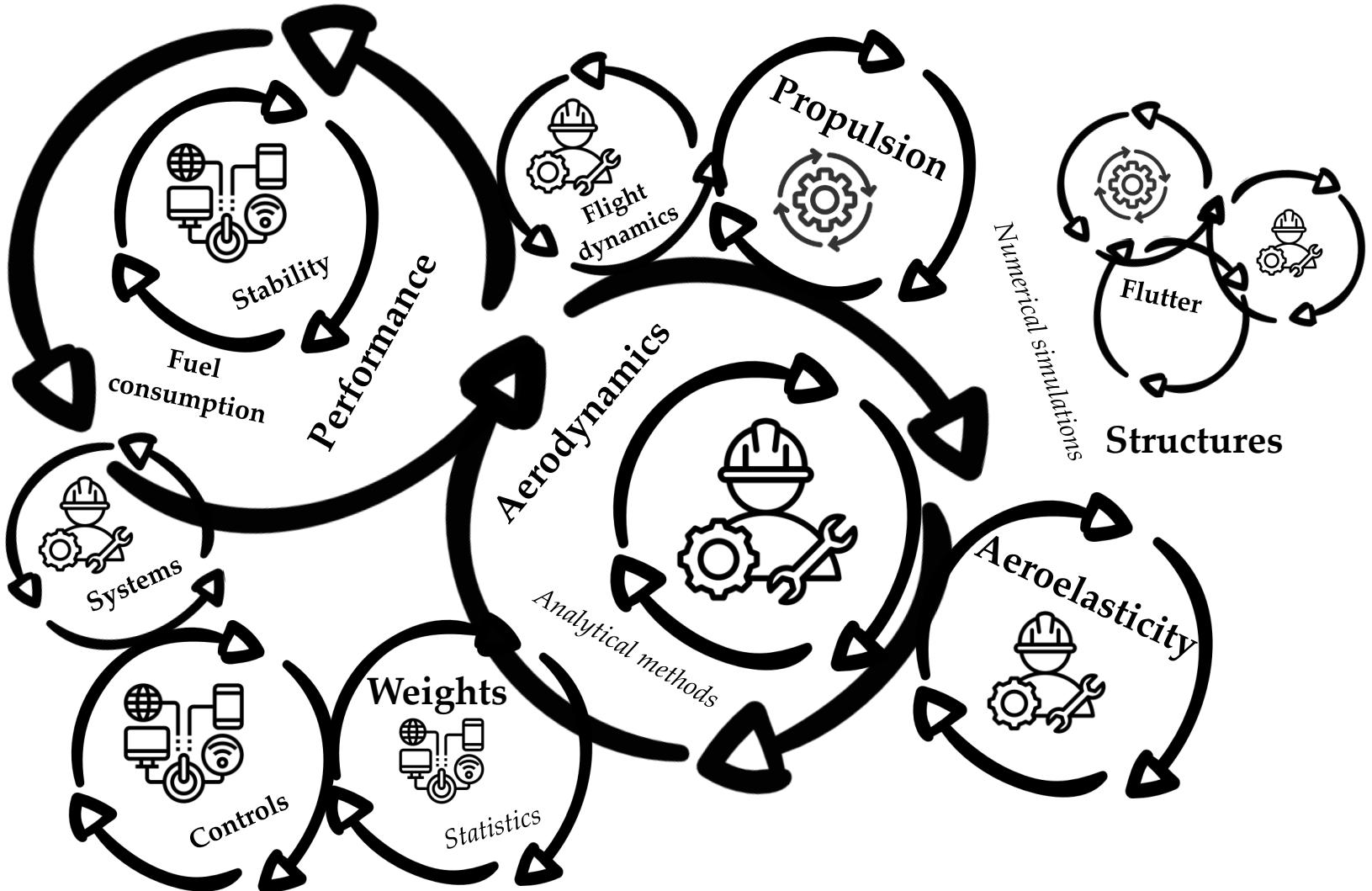
Aerodynamics
Structures
Flight mechanics
Propulsion
On-board systems
Weights optimization
Payload
Performance
Control systems

Multi-Fidelity

Textbook methods
Statistics/empirical data
Analytical methods
Numerical simulations
Level 1
Level 2
Level 3
Experimental
Flight test



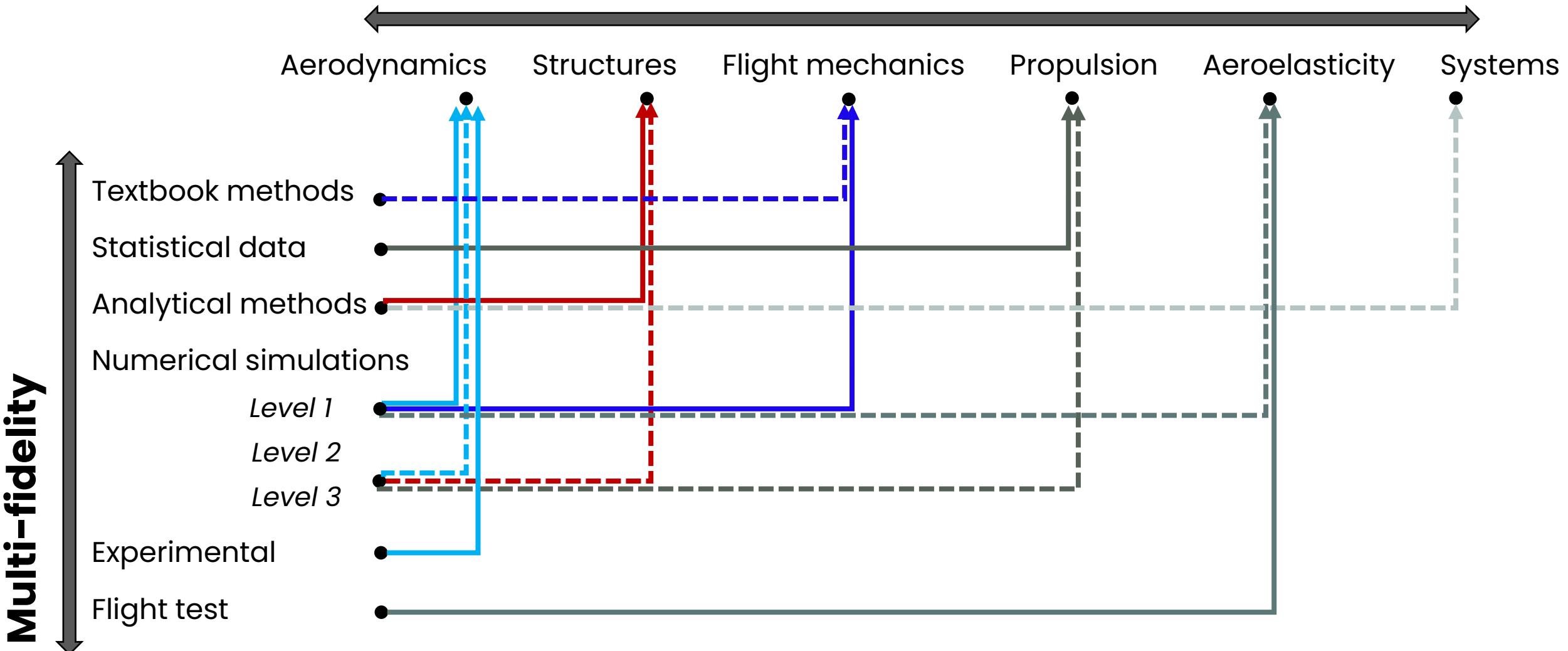
The Aircraft Design process





The Aircraft Design process

Multi-disciplinary



Lesson Topic



Assessment of the aircraft initial
MTOW

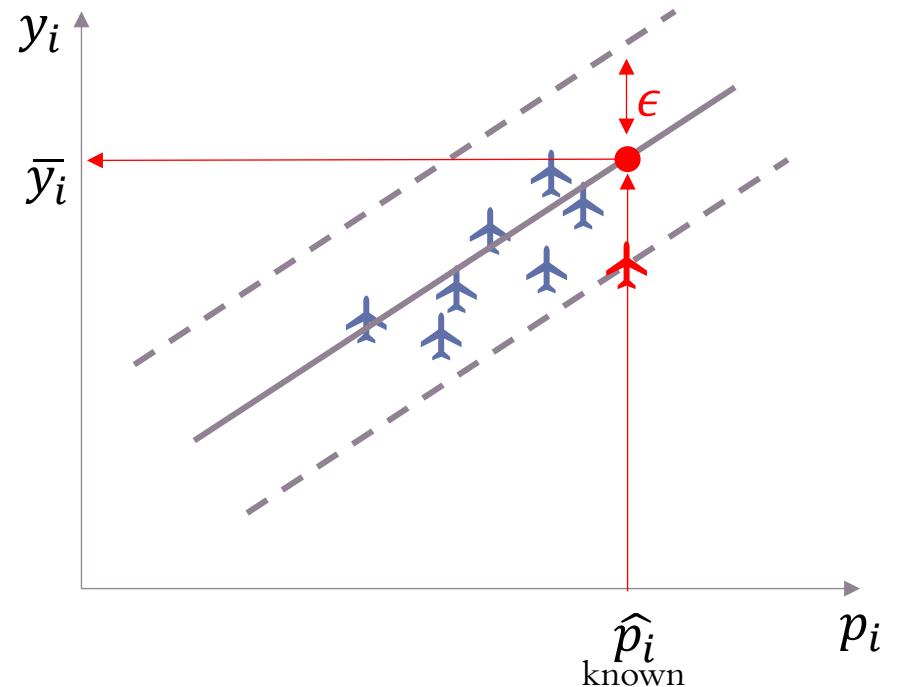
Guess Data Estimation



At the very beginning of the design process, it is important to understand the limits of the design space (sizing procedure), thus it is fundamental to start estimating the main design variables, such as:

- Maximum Take-Off Mass (MTOM)
- Aircraft Level Mass Breakdown ($m_{OE}, m_{fuel}, etc \dots$)
- Thrust (T_{req})
- Wing Loading
- Lift-over-Drag

For conventional configurations, methods for Guess Data Estimation are usually based on statistical analysis. Error margins shall be duly considered.



Take-off weight



Design **Take-off mass** can be broken into different contributions including, crew, payload, structures, subsystems, etc...

$$m_{TO} = m_{crew} + m_{payload} + m_{fuel} + m_{empty}$$

(known from Requirements, including regulations) (known from Requirements, including applicable regulations)

Pilots and all crew members Passengers and related equipment

This can be rewritten as follows:

$$m_{TO} = \frac{m_{crew} + m_{payload}}{1 - \left(\frac{m_{fuel}}{m_{TO}} \right) - \left(\frac{m_{empty}}{m_{TO}} \right)}$$

?

?

This equation can only be solved **iteratively!**

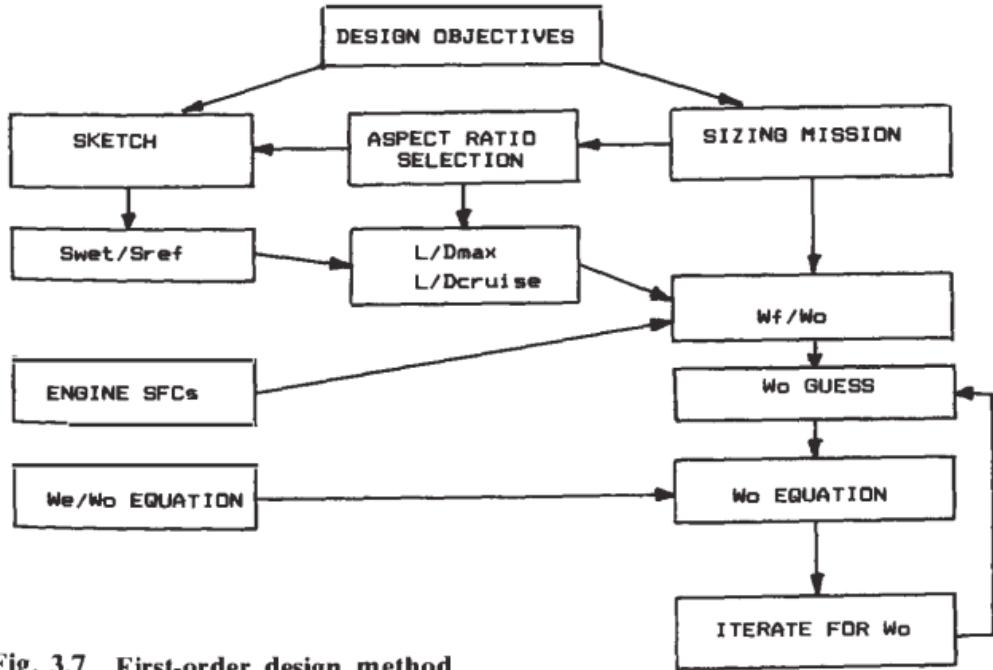


Fig. 3.7 First-order design method.

Payload mass



Payload $m_{payload}$ is calculated from:

1. number of seats n_{seat}
2. mass of cargo m_{cargo}

$$m_{payload} = m_{pax} N_{seats} + m_{baggage} N_{seats} + m_{cargo}$$

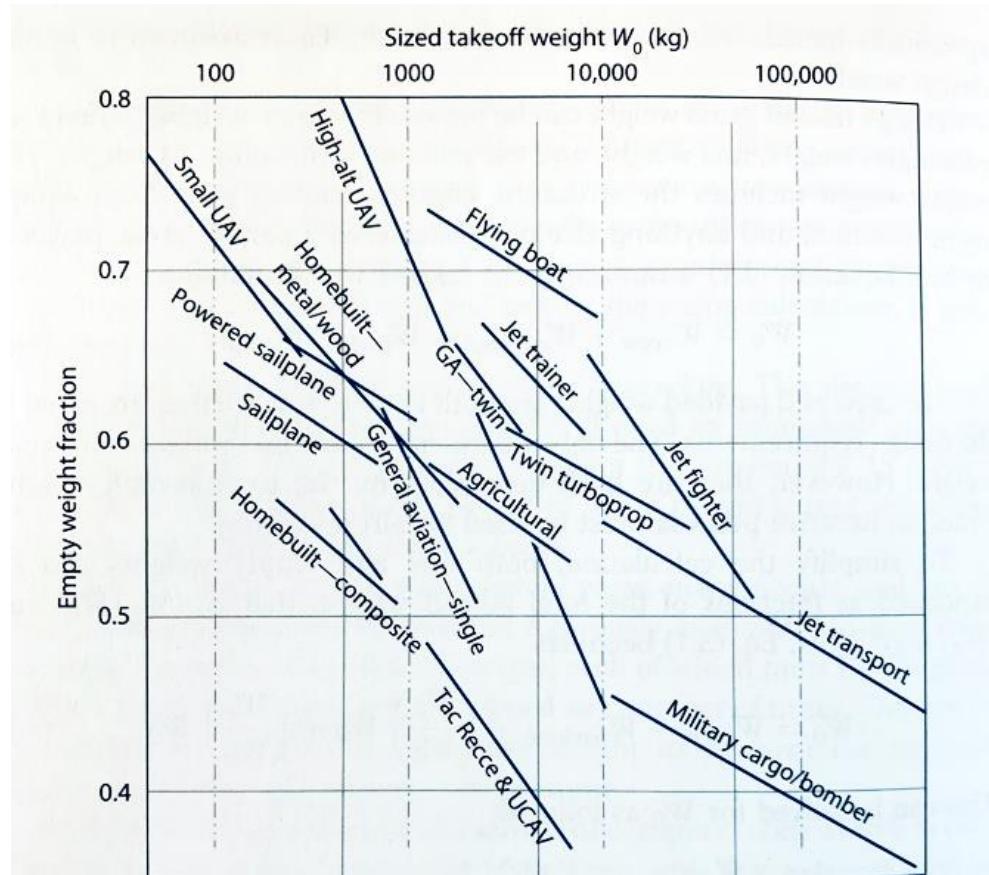
Table 3.1: Assumptions on mass of passengers und their baggage (**Roskam I**)

average mass of	short and medium range	long range
passenger, m_{PAX}	79.4 kg	79.4 kg
baggage, $m_{baggage}$	13.6 kg	18.1 kg
Sum	93.0 kg	97.5 kg

Empty mass fraction trend



$$m_{TO} = \frac{m_{crew} + m_{payload}}{1 - \left(\frac{m_{fuel}}{m_{TO}} \right) - \left(\frac{m_{empty}}{m_{TO}} \right)}$$



The trends can be represented by the following equation:

$$\frac{m_{empty}}{m_{TO}} = A m_{TO}^C$$

Table 3.1 Empty Weight Fraction vs W_0

$W_e/W_0 = A W_0^C K_{vs}$	A	{A-metric}	C
Sailplane—unpowered	0.86	{0.83}	-0.05
Sailplane—powered	0.91	{0.88}	-0.05
Homebuilt—metal/wood	1.19	{1.11}	-0.09
Homebuilt—composite	1.15	{1.07}	-0.09
General aviation—single engine	2.36	{2.05}	-0.18
General aviation—twin engine	1.51	{1.4}	-0.10
Agricultural aircraft	0.74	{0.72}	-0.03
Twin turboprop	0.96	{0.92}	-0.05
Flying boat	1.09	{1.05}	-0.05
Jet trainer	1.59	{1.47}	-0.10
Jet fighter	2.34	{2.11}	-0.13
Military cargo/bomber	0.93	{0.88}	-0.07
Jet transport	1.02	{0.97}	-0.06
UAV—Tac Recce & UCAV	1.67	{1.53}	-0.16
UAV—high altitude	2.75	{2.48}	-0.18
UAV—small	0.97	{0.86}	-0.06

K_{vs} = variable sweep constant = 1.04 if variable sweep = 1.00 if fixed sweep

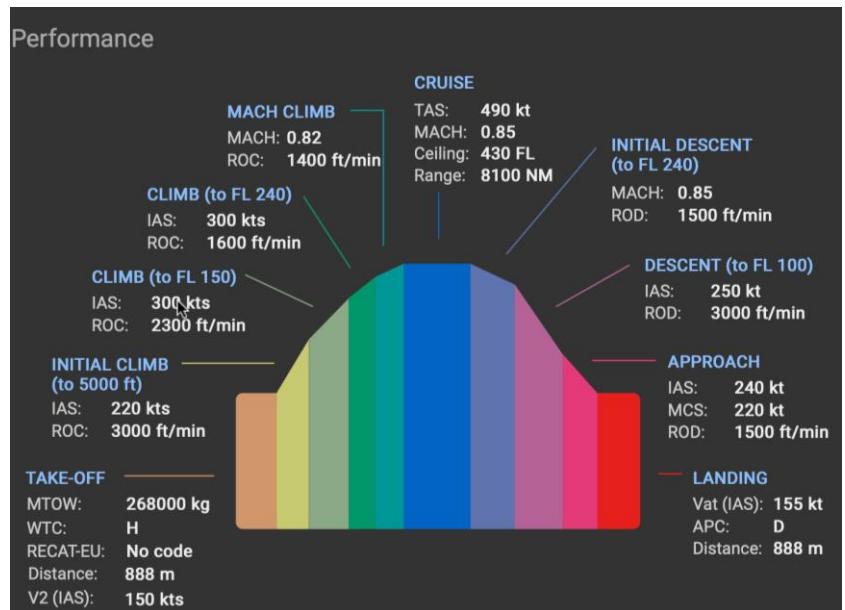
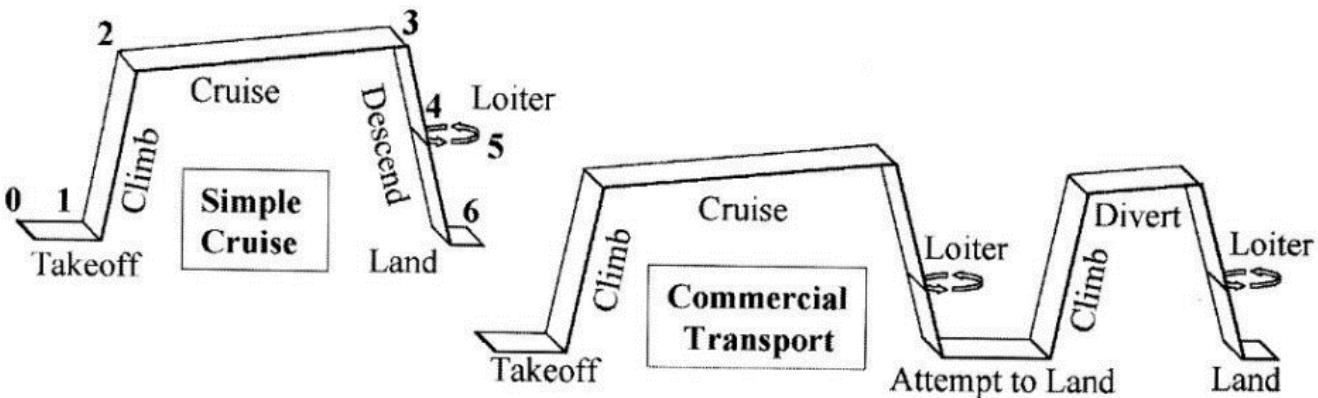


Fuel mass ratios

$$m_{TO} = \frac{m_{crew} + m_{payload}}{1 - \left(\frac{m_{fuel}}{m_{TO}}\right) - \left(\frac{m_{empty}}{m_{TO}}\right)}$$

Fuel Fraction can be estimated based on the **mission to be flown**, once an estimate of **fuel consumption** and **aerodynamic efficiency** is available

For the definition of a **Mission Profile** for commercial aircraft, various simplified models can be found out in literature. However, for a more precise estimate, real mission profiles can be used and discretized.

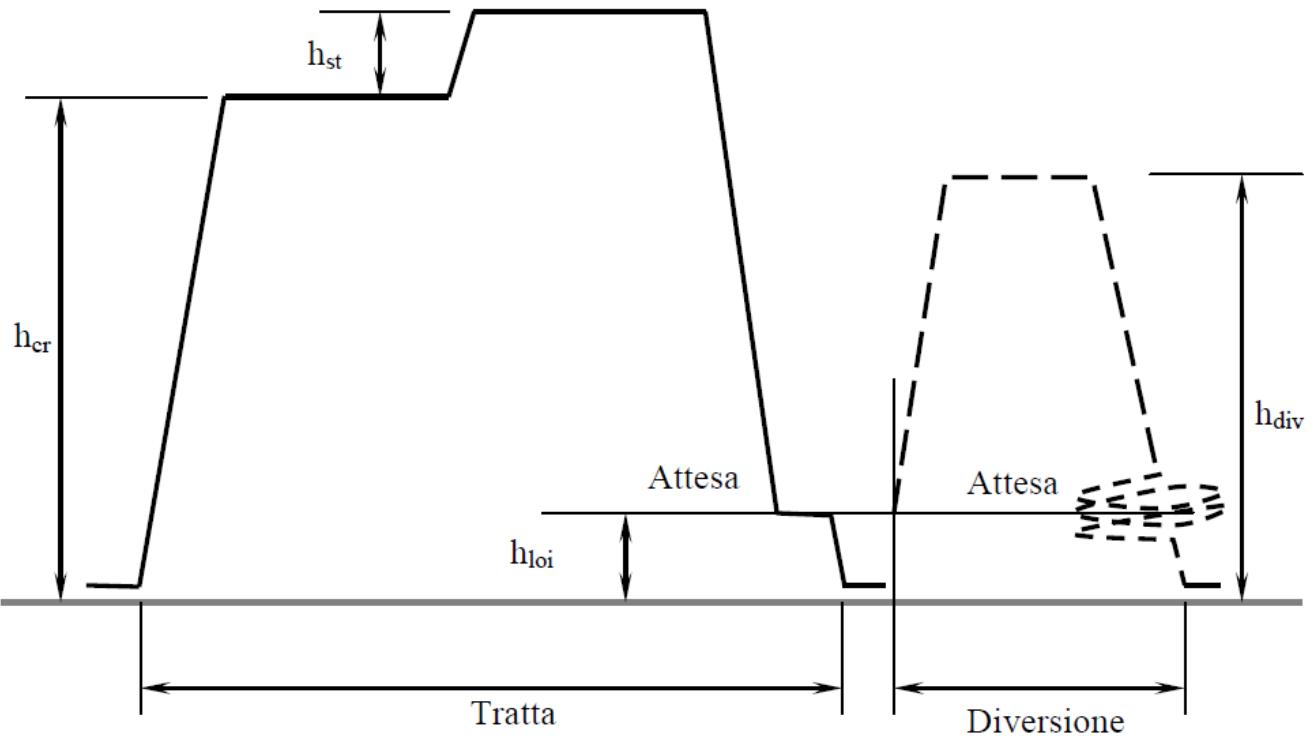


Data taken from Eurocontrol
Aircraft Performance Database
<https://contentzone.eurocontrol.int/aircraftperformance>



Fuel mass ratios

Definizione della missione di progetto - Esempio



<i>Definizioni</i>	<i>Lunghezza di tratta</i>	
Grandezza	<i>SHORT-MEDIUM RANGE</i>	<i>LONG RANGE</i>
SHORT-MEDIUM RANGE	< 3000 n.m.	< 5556 km.
LONG RANGE	> 3000 n.m.	> 5556 km.
<i>Missione Ordinaria</i>		
Tratta	Da requisito	
h_{cr}	Selezionare 25000 ft < h_{cr} < 35000 ft	
n_{st}^1	0-1	1-3
h_{st} (se $n_{st} > 0$)	4000 ft (possibile ridurre a 2000 ft per tratte brevi)	
$h_{lo}i$	1500 ft.	1500 ft
Attesa ²	8 min.	8 min.
<i>Riserve</i>		
Riserve (trip fuel) ³	5 %	5 %
Diversione ⁴	200 n.m.	250 n.m.
h_{div}	30000 ft	
Attesa ⁵	30 min.	30 min.
$h_{lo}i$	1500 ft	1500 ft.



Fuel mass ratios

$$m_{TO} = \frac{m_{crew} + m_{payload}}{1 - \left(\frac{m_{fuel}}{m_{TO}} \right) - \left(\frac{m_{empty}}{m_{TO}} \right)}$$

Fuel Fraction can be estimated based on the **mission to be flown**, once an estimate of **fuel consumption** and **aerodynamic efficiency** is available

By multiplying the weight fractions, the total mission weight fraction, $\frac{m_{final}}{m_{TO}}$, can be calculated .

$$\frac{m_{final}}{m_{TO}} = \prod_{i=1}^n \left(\frac{m_i}{m_{i-1}} \right)$$

where n is the number of mission phases (or legs)

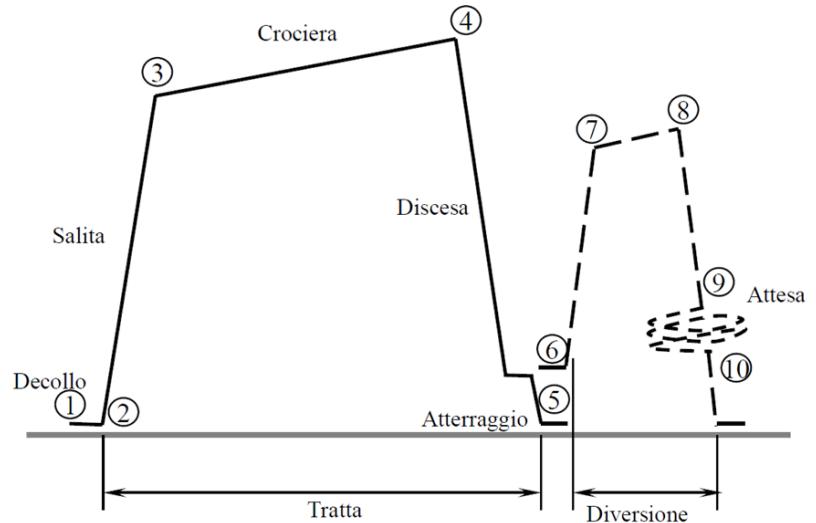
Since the simplified sizing method does not allow segments involving payload drops, all weight lost during the mission must be due to fuel usage. If we assume a typical 5% allowance for reserved and trapped fuel, the total fuel fraction can be estimated as:

$$\frac{m_{fuel}}{m_{TO}} = 1.05 \left(1 - \frac{m_{final}}{m_{TO}} \right)$$



Fuel mass ratios

$$m_{TO} = \frac{m_{crew} + m_{payload}}{1 - \left(\frac{m_{fuel}}{m_{TO}} \right) - \left(\frac{m_{empty}}{m_{TO}} \right)}$$



Fuel Fraction can be estimated based on the **mission to be flown**, once an estimate of **fuel consumption** and **aerodynamic efficiency** is available

$$\left(\frac{W_2^{(i)}}{W_{TO}^{(i)}} \right) = 0.970 \quad \left(\frac{W_7^{(i)}}{W_6^{(i)}} \right) \cong 1$$

$$\left(\frac{W_3^{(i)}}{W_2^{(i)}} \right) = 0.985 \quad \left(\frac{W_8^{(i)}}{W_7^{(i)}} \right) = ?$$

$$\left(\frac{W_4^{(i)}}{W_3^{(i)}} \right) = ? \quad \left(\frac{W_9^{(i)}}{W_8^{(i)}} \right) \cong 1$$

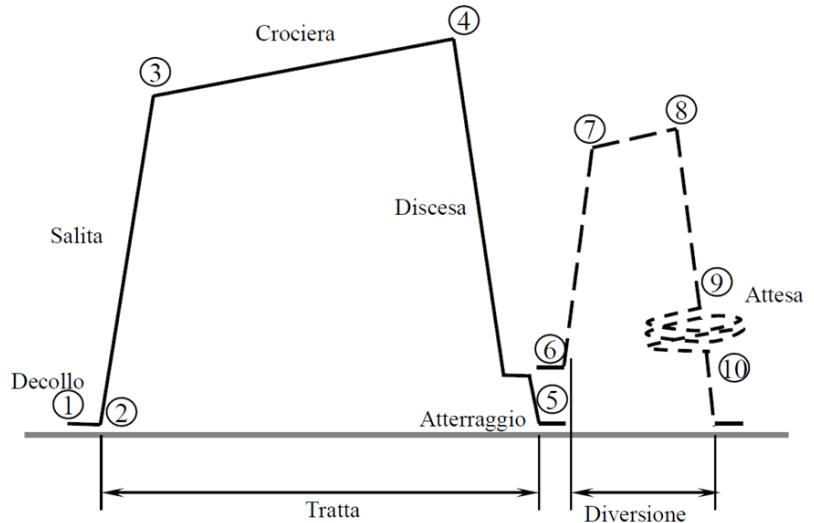
$$\left(\frac{W_5^{(i)}}{W_4^{(i)}} \right) = 0.995 \quad \left(\frac{W_{10}^{(i)}}{W_9^{(i)}} \right) = ?$$

$$\begin{aligned}
 \frac{W_{TO}^{(i)}}{} & \rightarrow \left(\frac{W_F^{(i)}}{W_{TO}^{(i)}} \right) = \left(\frac{W_{F-MIS}^{(i)}}{W_{TO}^{(i)}} \right) + \left(\frac{W_{F-RIS}^{(i)}}{W_{TO}^{(i)}} \right) \\
 & \left(\frac{W_{F-MIS}^{(i)}}{W_{TO}^{(i)}} \right) = 1 - \left(\frac{W_2^{(i)}}{W_{TO}^{(i)}} \right) \left(\frac{W_3^{(i)}}{W_2^{(i)}} \right) \left(\frac{W_4^{(i)}}{W_3^{(i)}} \right) \left(\frac{W_5^{(i)}}{W_4^{(i)}} \right) \\
 & \left(\frac{W_{F-RIS}^{(i)}}{W_{TO}^{(i)}} \right) = 0.05 \frac{W_{F-MIS}^{(i)}}{W_{TO}^{(i)}} + \left(1 - \frac{W_{F-MIS}^{(i)}}{W_{TO}^{(i)}} \right) \left[1 - \left(\frac{W_7^{(i)}}{W_6^{(i)}} \right) \left(\frac{W_8^{(i)}}{W_7^{(i)}} \right) \left(\frac{W_9^{(i)}}{W_8^{(i)}} \right) \left(\frac{W_{10}^{(i)}}{W_9^{(i)}} \right) \right]
 \end{aligned}$$



Fuel mass ratios

$$m_{TO} = \frac{m_{crew} + m_{payload}}{1 - \left(\frac{m_{fuel}}{m_{TO}} \right) - \left(\frac{m_{empty}}{m_{TO}} \right)}$$



$$\frac{W_{TO}^{(i)}}{W_{TO}} = \left(\frac{W_F^{(i)}}{W_{TO}} \right) = \left(\frac{W_{F-MIS}^{(i)}}{W_{TO}} \right) + \left(\frac{W_{F-RIS}^{(i)}}{W_{TO}} \right)$$

$$\left(\frac{W_{F-MIS}^{(i)}}{W_{TO}} \right) = 1 - \left(\frac{W_2^{(i)}}{W_{TO}^{(i)}} \right) \left(\frac{W_3^{(i)}}{W_2^{(i)}} \right) \left(\frac{W_4^{(i)}}{W_3^{(i)}} \right) \left(\frac{W_5^{(i)}}{W_4^{(i)}} \right)$$

$$\left(\frac{W_{F-RIS}^{(i)}}{W_{TO}} \right) = 0.05 \frac{W_{F-MIS}^{(i)}}{W_{TO}} + \left(1 - \frac{W_{F-MIS}^{(i)}}{W_{TO}} \right) \left[1 - \left(\frac{W_7^{(i)}}{W_6^{(i)}} \right) \left(\frac{W_8^{(i)}}{W_7^{(i)}} \right) \left(\frac{W_9^{(i)}}{W_8^{(i)}} \right) \left(\frac{W_{10}^{(i)}}{W_9^{(i)}} \right) \right]$$

$$\left(\frac{W_F^{(i)}}{W_{TO}} \right)$$

Fuel Fraction can be estimated based on the **mission to be flown**, once an estimate of **fuel consumption** and **aerodynamic efficiency** is available

$$\left(\frac{W_2^{(i)}}{W_{TO}^{(i)}} \right) = 0.970$$

$$\left(\frac{W_7^{(i)}}{W_6^{(i)}} \right) \cong 1$$

$$\left(\frac{W_3^{(i)}}{W_2^{(i)}} \right) = 0.985$$

$$\left(\frac{W_8^{(i)}}{W_7^{(i)}} \right) = ?$$

$$\left(\frac{W_4^{(i)}}{W_3^{(i)}} \right) = ?$$

$$\left(\frac{W_9^{(i)}}{W_8^{(i)}} \right) \cong 1$$

$$\left(\frac{W_5^{(i)}}{W_4^{(i)}} \right) = 0.995$$

$$\left(\frac{W_{10}^{(i)}}{W_9^{(i)}} \right) = ?$$

$$\frac{dx}{dW} = -\frac{V}{c \cdot T} \quad T = D \quad L = W \quad \frac{dx}{dW} = -\frac{V \cdot L}{c \cdot D \cdot L} = -\frac{V \cdot E}{c \cdot W}$$

$$\frac{dW}{W} = -\frac{c \cdot dx}{V \cdot E}$$

Ipotesi:

$V =$ Costante Assetto Costante $\rightarrow E =$ Costante

$$\frac{W_{i+1}}{W_i} = e^{-\frac{c \cdot \Delta x_i}{V \cdot E}}$$

Autonomia chilometrica

$$\frac{W_{i+1}}{W_i} = e^{-\frac{C \Delta t}{E}}$$

Autonomia oraria



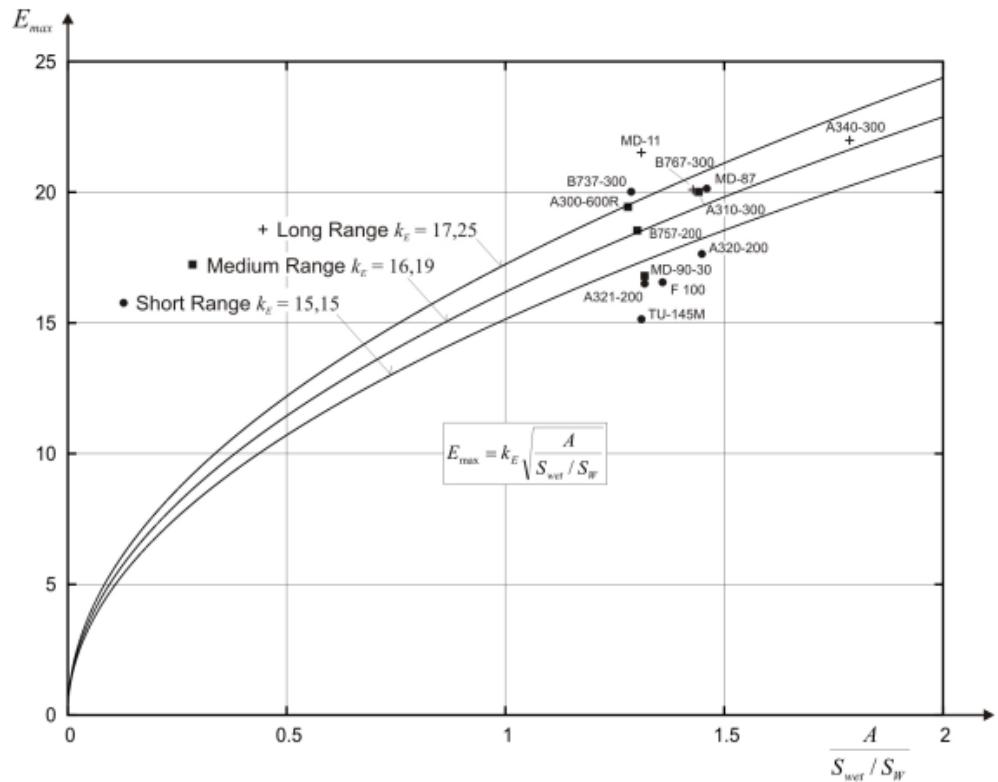
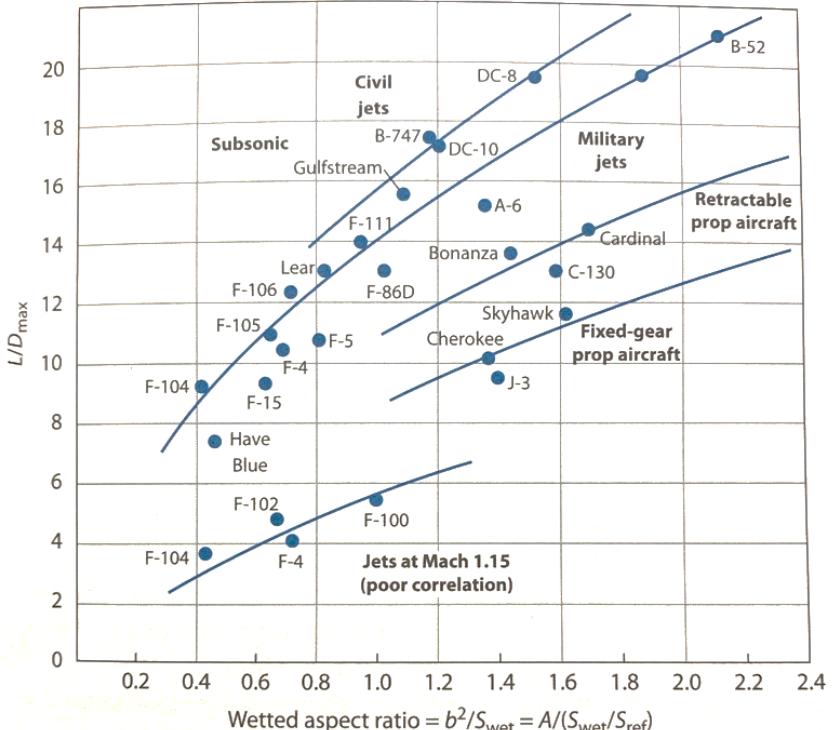
Maximum L/D

$$\left(\frac{L}{D}\right)_{max} = k_E \sqrt{AR_w}$$

Where

- k_E has different values depending upon the type of aircraft (e.g. 15.5 for civil jets,...)

$$AR_w = \frac{AR}{\frac{S_{wet}}{S_{ref}}}$$



	Cruise	Loiter
Jet Prop	$0.866 L/D_{max}$ L/D_{max}	L/D_{max} $0.866 L/D_{max}$



S_{wet} / S_W

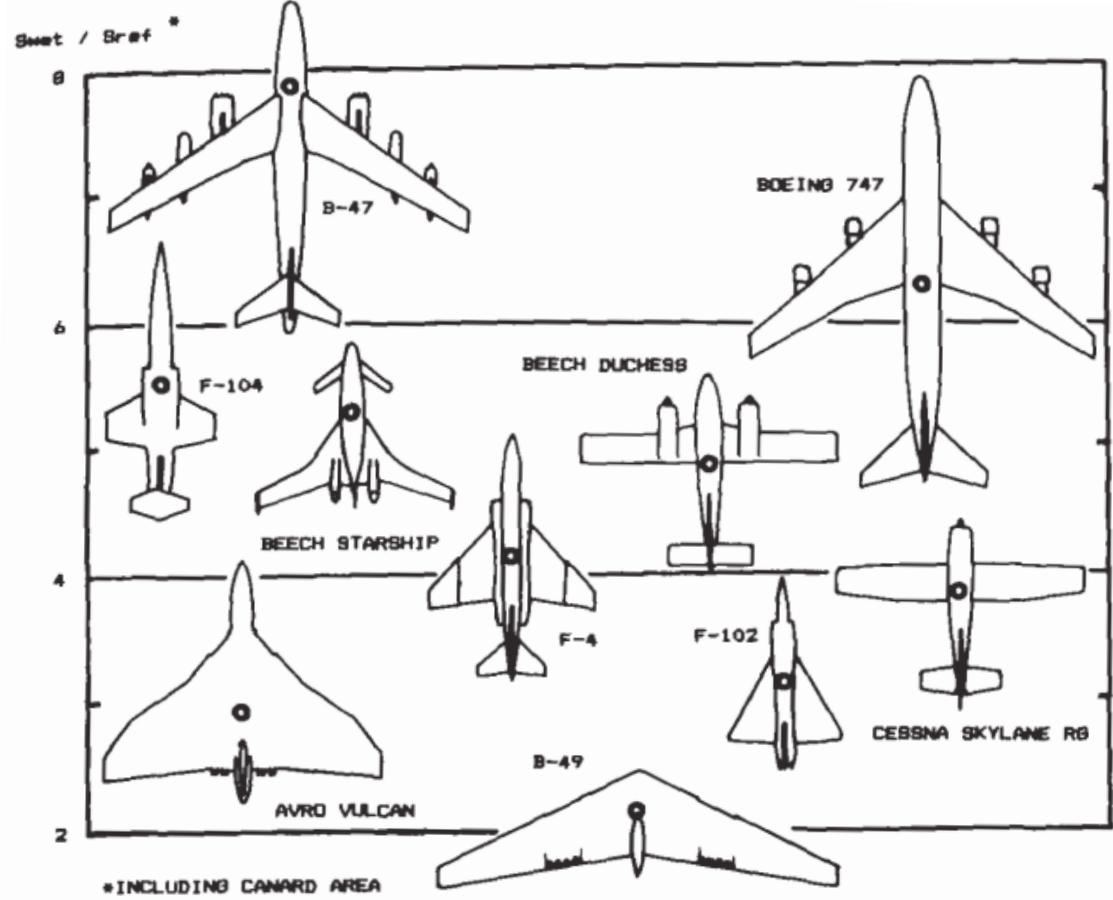
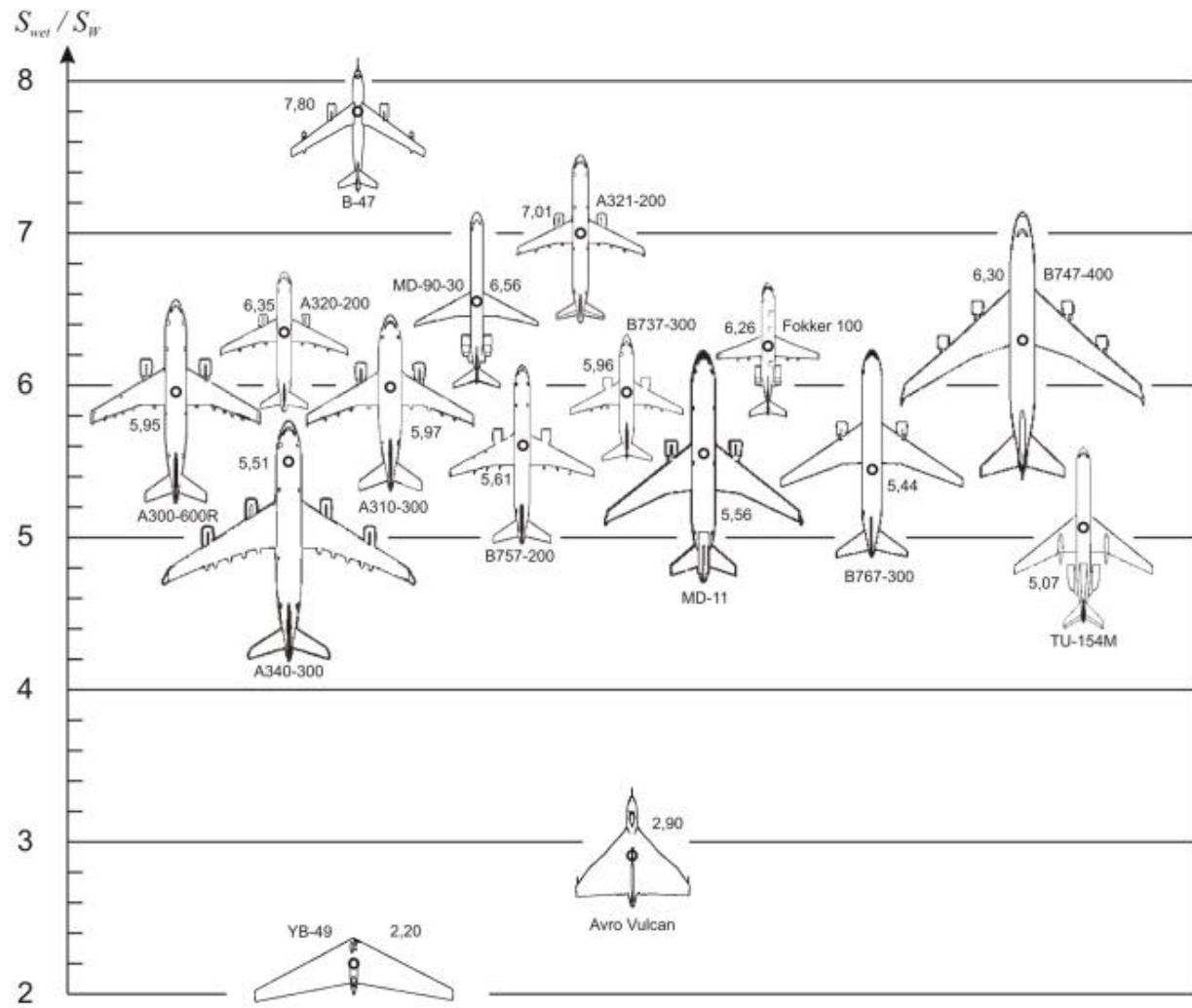


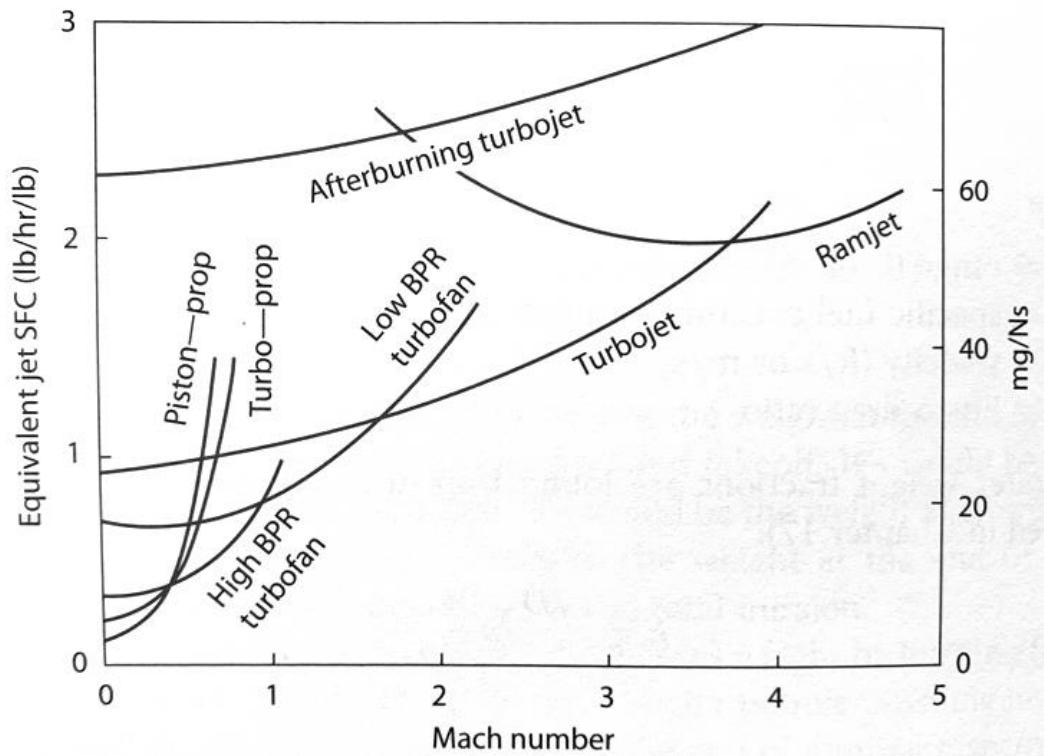
Fig. 3.5 Wetted area ratios.



Specific fuel consumption

$$m_{TO} = \frac{m_{crew} + m_{payload}}{1 - \left(\frac{m_{fuel}}{m_{TO}}\right) - \left(\frac{m_{empty}}{m_{TO}}\right)}$$

Fuel Fraction can be estimated based on the **mission to be flown**, once an estimate of **fuel consumption** and **aerodynamic efficiency** is available



Typical Values for subsonic jet aircraft are reported hereafter

Table 3.3 Specific fuel consumption (C)

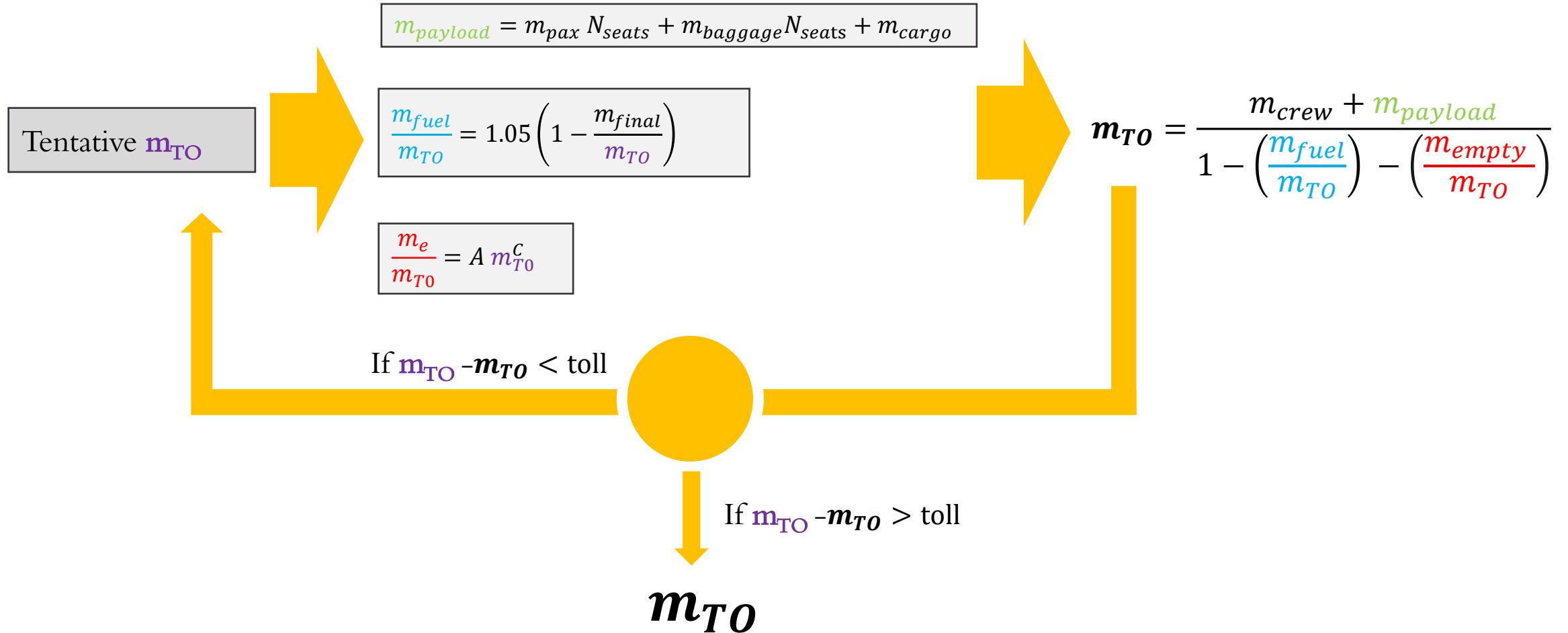
Typical jet SFC's	Cruise	Loiter
Pure turbojet	0.9	0.8
Low bypass turbofan	0.8	0.7
High-bypass turbofan	0.5	0.4

Unit [1/h]

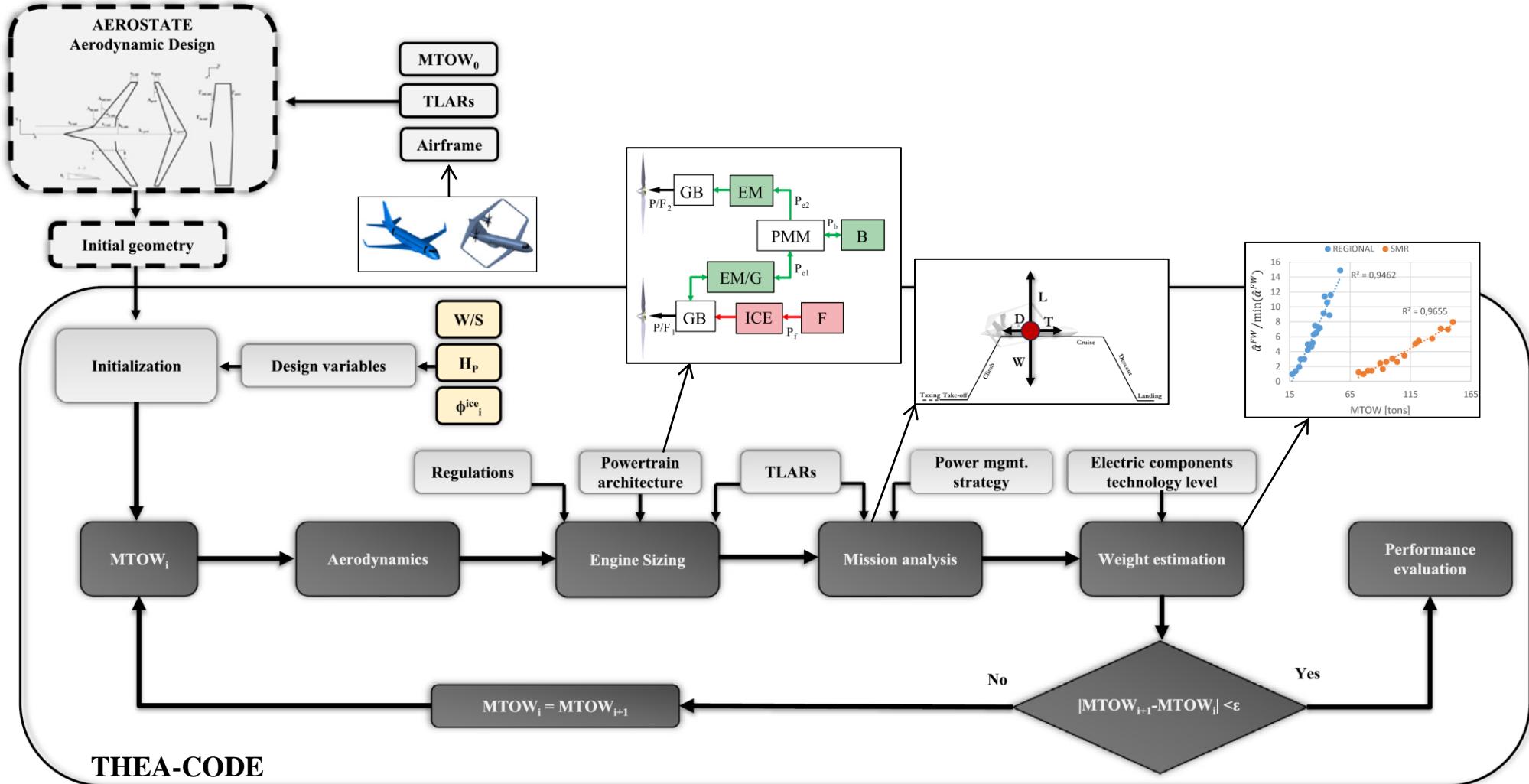
TSFC or SFC for thrust engines is the mass of fuel needed to provide the net thrust for a given period.



Iterative solution



Iterative solution



Task 2.1



On the basis of the formulation presented, estimate the take-off mass of the aircraft. Perform a trade-off analysis considering different ranges, payload and performances (sfc, L/D).