

## Laboratory Report 2:RC Circuit Analysis

Circuit Theory and Electronics Fundamentals

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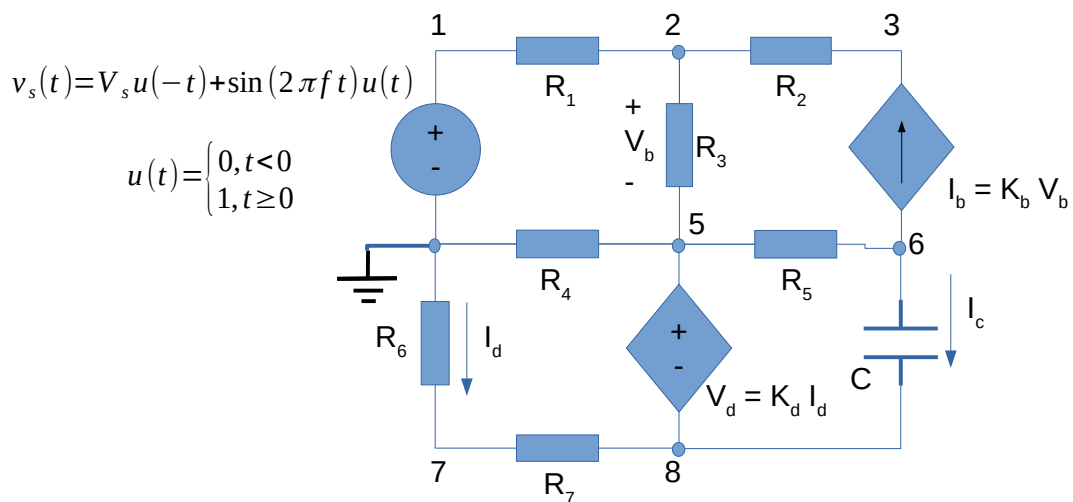
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# 1 Introduction

The objective of this laboratory assignment is to analyze a RC circuit to find the natural and forced response as well as doing a frequency analysis. Furthermore, it is asked to run a simulation using NgSpice to detect small differences between the different approaches and understand why said differences happen. The circuit can be seen in Figure 1.

In Section 2, a theoretical analysis of the circuit is presented. In Section 3, the circuit is analysed by simulation and the results are compared to the theoretical results obtained in Section 2. The conclusions of this study are outlined in Section 4.

Figure 1: RC Circuit with alternate voltage source ( $V_s$ ), linear dependent sources ( $V_d$ -linear current controlled voltage source and  $I_b$ -linear voltage controlled current source) and capacitor  $C$



The values given for this report can be found in table 1 (Obtained with the number 95789).

Name	Values
R1	1.01949191994 KΩ
R2	2.05054429461 KΩ
R3	3.09286027724 KΩ
R4	4.12838973576 KΩ
R5	3.06635427647 KΩ
R6	2.01254230153 KΩ
R7	1.00502981701 KΩ
Va	5.24204797361 V
C	1.01905568201 μF
Kb	7.23185131759 mS
Kd	8.12820254987 KΩ

Table 1: Values obtained by using the Python program that can be found in folder *python*.

## 2 Theoretical Analysis

In this section we will present the answers to questions 2.1 to 2.6. For solving purposes, all the unknown currents used in the node analysis were considered to be diverging from the node. The node  $V_4$  is connected to the ground (GND) in every exercise, the voltage in it being 0V.

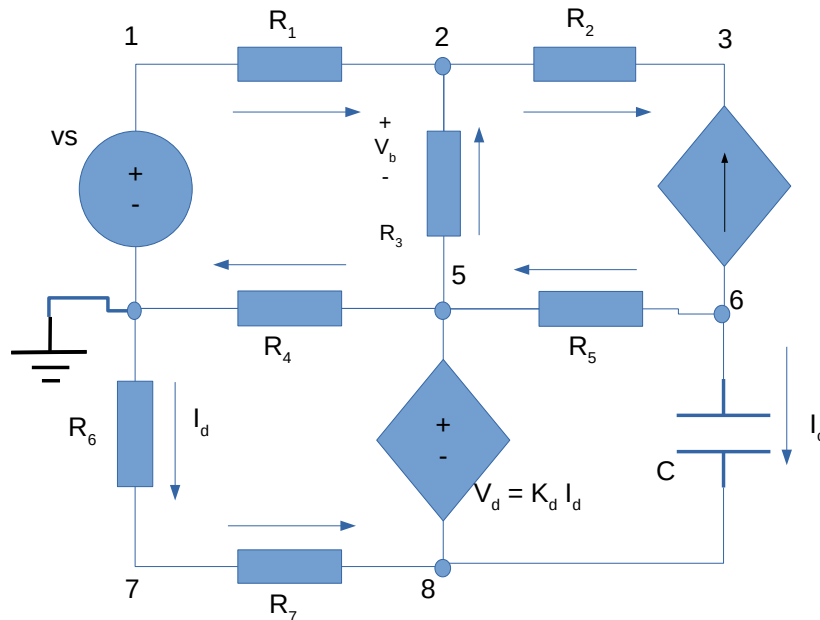


Figure 2: Representation of the current directions considered.

### 2.1 Exercise 1

The first thing which must be noticed is that there is an independent voltage source ( $V_s$ ) and a linear current controlled voltage source ( $V_d$ ) in this circuit. Knowing that a nodal analysis can't include the analysis of nodes that are connected to voltage sources, it becomes clear that is useless to analyze nodes 1 and 4 (connected to  $V_s$ ) and also nodes 5 and 8 (connected to  $V_d$ ) using this method.

From figure 2, we can easily conclude that there are 11 unknown variables:  $V_b$ ,  $I_b$ ,  $V_d$ ,  $I_d$ ,  $V_1$ ,  $V_2$ ,  $V_3$ ,  $V_5$ ,  $V_6$ ,  $V_7$  and  $V_8$ . In this exercise,  $V_s$  is constant and the capacitor is assumed to be also constant and fully charged, meaning that the current  $I_c$  is 0 (open circuit behavior).

For the node analysis, it is necessary to consider 7 linearly independent equations to reach all the values corresponding to the voltages in each node and consequently solve the circuit. As referred above, it is possible to use the nodal method to analyze nodes 2, 3, 6 and 7.

We begin by establishing the following equations, being that equations 1 and 2 were given by the professor. Equation 3 was obtained by relating the voltage difference between nodes 2 and 5 to the voltage  $V_b$ . Finally, by using Ohm's Law for resistor  $R_6$  and remembering that  $V_4$  is null, we get the last equation (4) for  $I_d$ .

$$I_b = K_b V_b, \quad (1)$$

$$V_d = K_d I_d, \quad (2)$$

$$V_b = V_2 - V_5, \quad (3)$$

$$I_d = -V_7 G_6, \quad (4)$$

The equation written below (5) is a direct consequence of our choice of connecting node 4 to the ground (GND), because this choice makes evident that the value of  $V_4$  is 0 and then:

$$V_1 - V_s = 0, \quad (5)$$

By analysing node 2 using Kirchoff's Current Law and Ohm's Law for the resistors  $R_1$ ,  $R_2$  and  $R_3$ , we get the following equation:

$$(V_3 - V_1)G_1 + (V_2 - V_3)G_2 + (V_2 - V_5)G_3 = 0, \quad (6)$$

The following equation (7), in which was also used Kirchoff's Current Law and Ohm's Law for resistor  $R_2$ , refers to node 3. Here we consider the given equation 1 and the equation 3 to substitute the current  $I_b$ .

$$(V_3 - V_2)G_2 - (V_2 - V_5)K_b = 0, \quad (7)$$

For node 6, the ensuing equation (8) was figured out by resorting to Ohm's Law for the resistor  $R_5$  and Kirchoff's Current Law. Equations 1 and 3 were once again used to avoid using  $I_b$ . Remember that, for this exercise,  $I_c$  is null.

$$(V_6 - V_5)G_5 + (V_2 - V_5)K_b = 0, \quad (8)$$

Finally, for node 7, Kirchoff's Circuit Law and Ohm's Law (for resistors  $R_6$  and  $R_7$ ) were used to establish the following mathematical relation:

$$V_7 G_6 + (V_7 - V_8)G_7 = 0, \quad (9)$$

Since there are 7 unknown variables, we need two more equations. The first one (10) is obtained by relating  $V_d$  to the voltage difference in nodes 5 and 8 and replacing  $V_d$  for the equations 2 and 4.

$$-V_7 G_6 K_d - (V_5 - V_8) = 0, \quad (10)$$

Ultimately, to discover the last equation, there are some theoretical concepts that must be considered. Kirchoff's Current Law implies that there is no current stuck at any node. It is also known that neither voltage sources nor resistors retain current. Then, any branch that only contains one of the said elements does not retain current as well. Merging the two branches placed on the left side of circuit (branch containing  $V_s$  with branch containing  $R_6$ ) and calling Supernode to the result of this merger, it is still true that no current is retained in the Supernode. Then, considering that all unknown currents are diverging from the nodes, the resultant equation (11) is the one written right below.

$$(V_1 - V_2)G_1 - V_5 G_7 - V_7 G_6 = 0, \quad (11)$$

A system with the 7 linearly independent equations and 7 variables (regarding the voltage in each node) is, of course, possible to solve but not easy (and certainly not practical) to deal with.

The following matrix equation (12) summarizes the 7 referred equations so it is easier to read and to instantaneously solve (by using Octave).

$$\begin{bmatrix} 1 & 0 & 0 & 0 & 0 & 0 & 0 \\ -G_1 & G_1 + G_2 + G_3 & -G_2 & -G_3 & 0 & 0 & 0 \\ 0 & -G_2 - K_b & G_2 & K_b & 0 & 0 & 0 \\ 0 & K_b & 0 & -K_b - G_5 & G_5 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & G_6 + G_7 & -G_7 \\ G_1 & -G_1 & 0 & -G_4 & 0 & -G_6 & 0 \\ 0 & 0 & 0 & -1 & 0 & -K_d G_6 & 1 \end{bmatrix} \times \begin{bmatrix} V_1 \\ V_2 \\ V_3 \\ V_5 \\ V_6 \\ V_7 \\ V_8 \end{bmatrix} = \begin{bmatrix} V_s \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{bmatrix} \quad (12)$$

To find all the required branches' currents we can use Ohm's Law for each resistor, which can be seen in equations 13 to 19: Now we no longer consider the currents to be diverging from the nodes, but assume the directions shown in figure ??.

$$R_1[i] = \frac{V_1 - V_2}{R_1}, \quad (13)$$

$$R_2[i] = \frac{V_2 - V_3}{R_2}, \quad (14)$$

$$R_3[i] = \frac{V_5 - V_2}{R_3}, \quad (15)$$

$$R_4[i] = \frac{V_5}{R_4}, \quad (16)$$

$$R_5[i] = \frac{V_6 - V_5}{R_5}, \quad (17)$$

$$R_6[i] = -\frac{V_7}{R_6}, \quad (18)$$

$$R_7[i] = \frac{V_7 - V_8}{R_7}, \quad (19)$$

Here we have table 2 in which the final values of the unknown variables are printed.

Node	Voltage[V]	Branch	Current[A]
$V_b$	-3.39683549e-02	$I_b$	-2.43438254e-04
$V_d$	8.09007714e+00	$I_c$	0.00000000e+00
$V_1$	5.21186473e+00	$R_6 = I_d$	9.96071751e-04
$V_2$	4.97878426e+00	$R_1$	2.32169954e-04
$V_3$	4.46943736e+00	$R_2$	2.43438254e-04
$V_5$	5.01275261e+00	$R_3$	1.12682999e-05
$V_6$	5.77611328e+00	$R_4$	1.22824170e-03
$V_6$	-2.03266942e+00	$R_5$	2.43438254e-04
$V_8$	-3.07732453e+00	$R_7$	9.96071751e-04

Table 2: Voltage and Current values(Exercise 1)

## 2.2 Exercise 2

To solve this exercise, we first needed to get the value of  $V_x$ , which we did by applying the equation given by the professor (??), using the values of  $V_6$  and  $V_8$  we got from the matrix 12. This value corresponds to the voltage in the capacitor that now functions as a voltage source, as seen in figure ?? . This happens because, as mentioned before, we can assume that an infinite time has passed until  $t=0$  and it is fully charged, meaning it starts with the voltage given before we start the time.

To get the value intended of  $R_{eq}$ , it is necessary to achieve the value of the current supplied by the new voltage source ( $V_x$ ),  $I_x$ . This is done by the following node analysis.

Since  $V_s$  is now null, it can be ignored, making it so that node 1 is the same as node 4, with a voltage of 0V. This means that the node 4 that could not be used for node analysis before provides another equation. However, the voltage source  $V_x$  is connected to node 6, this one being no longer useful. For this exercise, we have 6 unknown variables for the node voltages ( $V_2$ ,  $V_3$ ,  $V_5$ ,  $V_6$ ,  $V_7$  and  $V_8$ ) and we can analyse the nodes 2, 3, 4 and 7.

These 3 equations are all obtained from the exercise above (reference to equations 6, 7 and 9) to, but assuming that  $V_1$  is null, since in the nodes 2, 3 and 7, nothing has changed from the previous circuit, when it comes to connected components.

$$(V_3 - V_1)G_1 + (V_2 - V_3)G_2 + (V_2 - V_5)G_3 = 0, \quad (20)$$

$$(V_3 - V_2)G_2 - (V_2 - V_5)K_b = 0, \quad (21)$$

$$V_7G_6 + (V_7 - V_8)G_7 = 0, \quad (22)$$

From node 1, we can achieve the equation below by using Kirchhoff's Circuit Law and Ohm's Law for resistors  $R_1$ ,  $R_6$  and  $R_7$ .

$$-V_7G_6 - V_5G_4 - V_2G_1 = 0, \quad (23)$$

The following equations are also trivial. The first one, equation 24 is explained in the first exercise (reference to equation 10) and equation 25 is given by the professor and can be used as the value of  $V_x$  is constant.

$$-V_7G_6K_d - (V_5 - V_8) = 0, \quad (24)$$

$$V_6 - V_8 = V_x, \quad (25)$$

These equations are now enough to solve for the value of  $V_2$ ,  $V_3$ ,  $V_5$ ,  $V_6$ ,  $V_7$  and  $V_8$ , using the matrix below. This was solved in Octave as it was not practical to solve it normally and the results are presented in table ??.

$$\begin{bmatrix} G_1 + G_2 + G_3 & -G_2 & -G_3 & 0 & 0 & 0 \\ -G_2 - K_b & G_2 & K_b & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & G_6 + G_7 & -G_7 \\ -G_1 & 0 & -G_4 & 0 & -G_6 & 0 \\ 0 & 0 & -1 & 0 & -K_dG_6 & 1 \\ 0 & 0 & 0 & 1 & 0 & -1 \end{bmatrix} \times \begin{bmatrix} V_2 \\ V_3 \\ V_5 \\ V_6 \\ V_7 \\ V_8 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ V_x \end{bmatrix} \quad (26)$$

The value of  $I_x$  is achieved by using Kirchhoff Current Law (KCL) in node 6. We considered the currents to be diverging from the node. From this, the equation below was obtained.

$$I_x + (V_2 - V_5)K_b + (V_5 - V_6)G_6 = 0, \quad (27)$$

Finally, we get the value of  $R_{eq}$ :

$$R_{eq} = \frac{V_x}{I_x}, \Rightarrow R_{eq} = \frac{8.85343781e+00}{2.82339074e-03} \Leftrightarrow R_{eq} = 3.13574656e+03 \Omega \quad (28)$$

The value of  $\tau$  is  $R_{eq} * C$  which is equal to  $3.26093677e-03 \Omega * \mu F$ .

Node	Voltage[V]	Branch	Current[A]
$V_b$	-0.00000000e+00	$I_b$	0.00000000e+00
$V_d$	-0.00000000e+00	$R_6 = I_d$	-0.00000000e+00
$V_1$	0.00000000e+00	$R_1$	0.00000000e+00
$V_2$	-0.00000000e+00	$R_2$	-0.00000000e+00
$V_3$	0.00000000e+00	$R_3$	0.00000000e+00
$V_5$	-0.00000000e+00	$R_4$	-0.00000000e+00
$V_6$	8.85343781e+00	$R_5$	2.82339074e-03
$V_6$	0.00000000e+00	$R_7$	0.00000000e+00
$V_8$	-0.00000000e+00	$I_x$	2.82339074e-03
$V_x$	8.85343781e+00		

Component	Value
$R_{eq}$	3.13574656e+03 $\Omega$
$\tau$	3.26093677e-03 $\Omega * \mu F$

Table 3: Voltage and Current values(Exercise 2)

## 2.3 Exercise 3

For this exercise, we used the capacitor voltage  $V_x$  for  $t < 0$  as the initial condition, as suggested. Using the equivalent resistance  $R_{eq}$  calculated in the previous exercise, we can assume that the natural solution for  $V_6$  is like the one on equation 29, as this is a RC series.

$$V_{6n}(t) = Ae^{-\frac{t}{RC}}, \quad (29)$$

Since the amplitude for which  $V_6$  varies is given by the initial condition  $V_6 = V_x + V_8$ , the A in the equation above can be replaced by those two voltages. The value for  $V_8$  was the one calculated on exercise 2 (2.2). The equation for the natural solution  $V_6$  is then represented below as the graph of  $V_{6n}$  in function of t, in the interval [0, 20] ms (3).

$$V_{6n}(t) = (V_x + V_8)e^{-\frac{t}{RC}}, \quad (30)$$

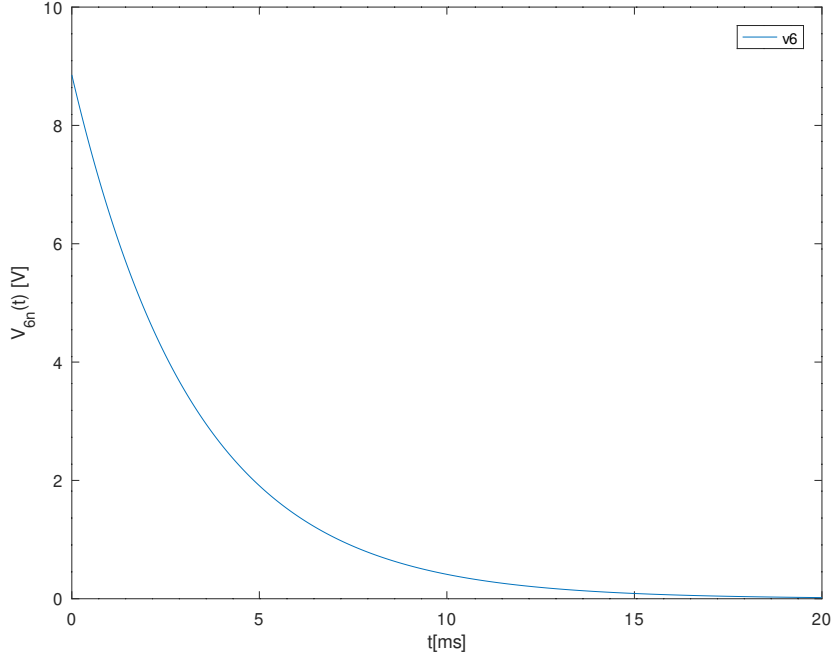
## 2.4 Exercise 4

For this exercise, to find the forced solution  $V_6 f(t)$ , we will work with the frequency  $f = 1000$  Hz and the phasor voltage source  $V_s$ . Since the voltage source for  $t > 0$  is  $v_s(t) = \sin(2\pi ft)$ , to simplify the calculations and as suggested, we will work with the absolute of  $V_s$ , which was given and it is 1V.

The node analysis for this exercise is pretty similar to the one in 2.1 as the voltage source is once again  $V_s$  and the capacitor no longer works as a voltage source. This means that we now have 7 variables  $V_1, V_2, V_3, V_5, V_6, V_7$  and  $V_8$  and we can use the node method in nodes 2, 3, 6 and 7, since all the other ones are connected to voltage sources.

Equations ?? to ?? were all obtained from the node analysis in exercise 1. The first three are achieved, correspondingly, by nodes 2,3 and 7. The second to last equation refers to the

Figure 3: Natural Response of  $v_{6n}(t)$  in the interval  $[0, 20]ms$  using  $V_x(t < 0)$  as the initial condition



current controlled voltage source  $V_d$ . Finally, the last one is the supernode that we got from merging the two branches placed on the left side of circuit.

$$(V_3 - V_1)G_1 + (V_2 - V_3)G_2 + (V_2 - V_5)G_3 = 0, \quad (31)$$

$$(V_3 - V_2)G_2 - (V_2 - V_5)K_b = 0, \quad (32)$$

$$V_7G_6 + (V_7 - V_8)G_7 = 0, \quad (33)$$

$$-V_7G_6K_d - (V_5 - V_8) = 0, \quad (34)$$

$$(V_1 - V_2)G_1 - V_5G_7 - V_7G_6 = 0, \quad (35)$$

The seventh and final equation (39) necessary to complete the matrix is obtained by analysing node 6, using Kirchoff's Circuit Law and Ohm's Law for the resistor  $R_5$ . The equation for  $V_b$  was secured previously (3). Because we are working with phasors, equations 36 and 38 are used to figure out the current flowing through the capacitor, by using its impedance  $Z_c$ .

$$I_cZ_c = V_c, \quad (36)$$

$$Z_c = \frac{1}{j\omega C}, \quad (37)$$

$$Y_c = \frac{1}{Z_c}, \quad (38)$$

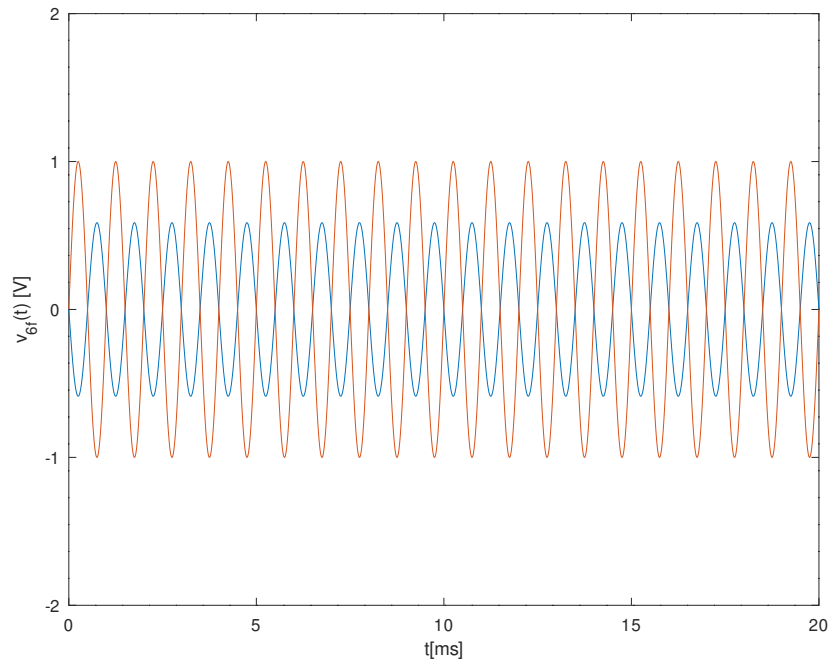
$$(V_6 - V_5)G_5 + (V_2 - V_5)K_b + (V_6 - V_8)Y_c = 0, \quad (39)$$



From this we get the following matrix. Knowing that  $w = 2\pi * f$  with  $f = 1kHz$ , the matricial equation was solved in Octave. The results are printed on the table ??.

$$\begin{bmatrix} 1 & 0 & 0 & 0 & 0 & 0 & 0 \\ -G_1 & G_1 + G_2 + G_3 & -G_2 & -G_3 & 0 & 0 & 0 \\ 0 & -G_2 - K_b & G_2 & K_b & 0 & 0 & 0 \\ 0 & K_b & 0 & -K_b - G_5 & G_5 + Y_c & 0 & -Y_c \\ 0 & 0 & 0 & 0 & 0 & G_6 + G_7 & -G_7 \\ G_1 & -G_1 & 0 & -G_4 & 0 & -G_6 & 0 \\ 0 & 0 & 0 & -1 & 0 & -K_d G_6 & 1 \end{bmatrix} \times \begin{bmatrix} V_1 \\ V_2 \\ V_3 \\ V_5 \\ V_6 \\ V_7 \\ V_8 \end{bmatrix} = \begin{bmatrix} V_s \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{bmatrix} \quad (40)$$

Figure 4: Forced solution  $v_{6f}(t)$  for  $f = 1kHz$  in the interval  $[-5, 20]ms$



## 2.5 Exercise 5

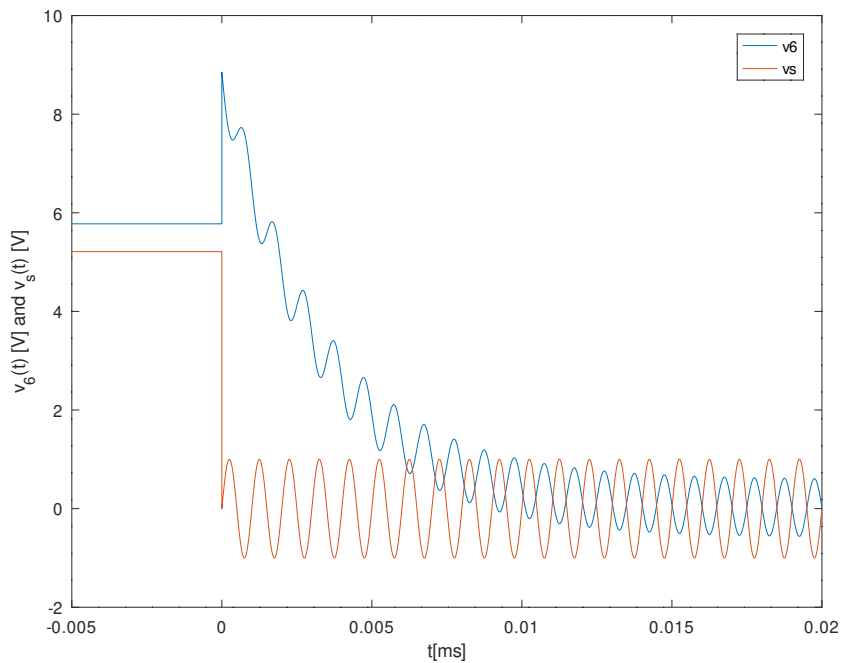
To figure out  $V_6$ , we simply had to convert the phasor to real time functions, being so that the value of  $V_6$  is just the sum of the natural solution with the forced solution, calculated in exercises 3 and 4. The equation for  $V_s(t)$  is given and it is written below, as the one for  $V_6(t)$ . The frequency used was 1000 Hz.

$$V_s(t) = \sin 2\pi ft, \quad (41)$$

$$V_6(t) = (V_x + V_8)e^{-\frac{t}{RC}} + V_{6f}(t), \quad (42)$$

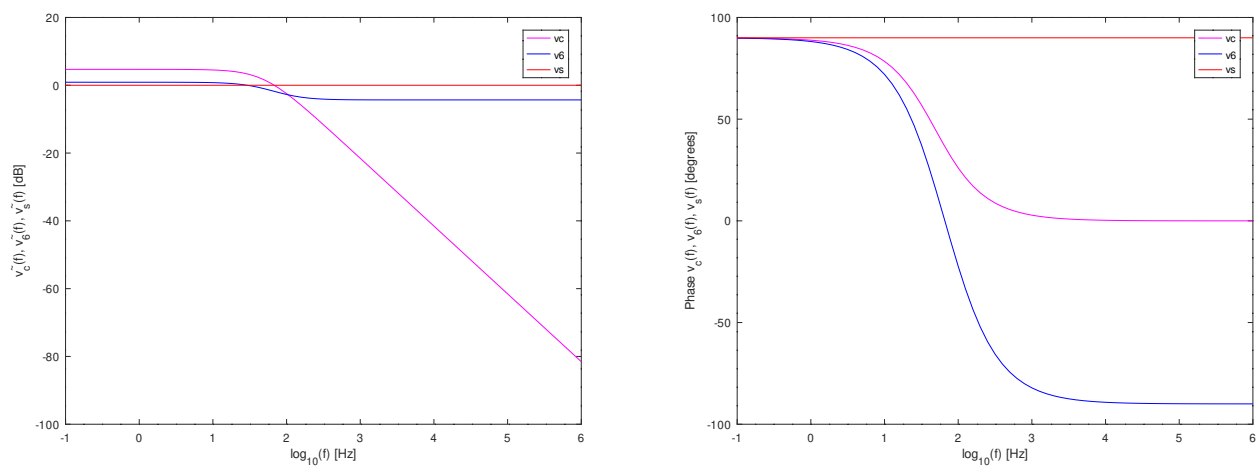
Finally, in figure 5, we have the graph for both  $V_s$  and  $V_6$  in function of  $t$ , in the interval  $[-5, 20]$  ms. As stated in the simulation analysis, it was expected for  $V_s$  to not show a frequency response, since it is the source of frequency change. The same is not the case for  $V_6$  as it depends on  $V_s$ .

Figure 5: Final solution of  $v_6(t)$  and  $v_s(t)$  in the interval  $[-5, 20]$  ms



## 2.6 Exercise 6

Figure 6: Frequency response,  $v_c(f)$ ,  $v_6(f)$ , and  $v_s(f)$  in  $V$ . Magnitude in  $dB$  and Phase is in degrees



### 3 Simulation Analysis

#### 3.1 Exercise 1

In this section we proceed to do the anlysis of the circuit through the use of the Ngspice simulation program. In figure 7 we have the circuit that was inputted into Ngspice (and also the considered current flows and nodes). The file can be found at the *sim* folder inside the *T2* folder.

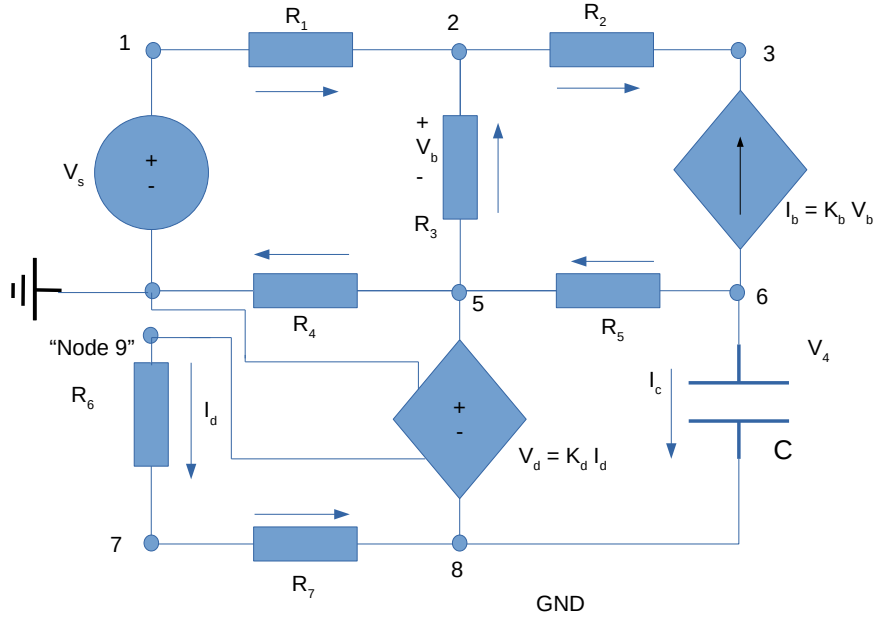


Figure 7: Considered circuit for Ngspice simulation

$V_9$  refers to an extra fictitious node created specifically for the Ngspice simulation, and it is below  $0(GND)$  and above resistor  $R_6$  as it can be seen above in figure 7. The reason this node is necessary is because when creating a current controlled voltage source, Ngspice gets the current value by refering to a voltage source from where the current goes through. Since  $I_d$  does not go through any voltage source in the circuit (does not go through  $V_s$ ) we used this extra node to create a voltage source of  $0V$  (Which can be confirmed since  $V_9 = GND = 0$ ) from which we are certain  $I_d$  is passing by.

Table 4 shows the simulated operating point results for the circuit under analysis given the values found on Table 1, considering  $t < 0$ , which means  $v_s(t) = V_s$  as seen in Figure 1. The variables representation and format are automatically determined by Ngspice.

We can get all the missing values given the voltage different of the nodes where they are defined.

$$V_b = v(v2, v5) = -3.39684e - 02V \quad (43)$$

$$V_d = v(v5, v8) = 8.090077e + 00V \quad (44)$$

#### 3.2 Exercise 2

In this section, we simulate the operating point for  $v_s(0) = 0$ , replacing the capacitor with a voltage source  $V_x = V_6 - V_8$  using the values of the respective nodes as obtained in section 3.1.

Table 4: Operating point for  $t < 0$ . A variable preceded by @ is of type *current* and expressed in Ampere; other variables are of type *voltage* and expressed in Volt. (the g in "gib" refers to the Ngspice notation of a voltage controlled current source)

Name	Value [A or V]
@c1[i]	0.000000e+00
@gib[i]	-2.43438e-04
@r1[i]	2.321700e-04
@r2[i]	2.434383e-04
@r3[i]	1.126830e-05
@r4[i]	1.228242e-03
@r5[i]	2.434383e-04
@r6[i]	9.960718e-04
@r7[i]	9.960718e-04
v1	5.211865e+00
v2	4.978784e+00
v3	4.469437e+00
v5	5.012753e+00
v6	5.776113e+00
v7	-2.03267e+00
v8	-3.07732e+00
v9	0.000000e+00

It is required to replace the capacitor since we can assume that an infinite time as passed until  $t=0$  and it is fully charged, meaning it starts with the voltage given before we start the time.

Table 5 shows the simulated operating point results for the circuit under analysis given the values found on Table 1, considering  $t=0$ , and the above mentioned considerations.

Table 5: Operating point for  $t = 0$ ,  $v_s(0) = 0$  and capacitor replaced with  $V_x = V_6 - V_8$ . A variable preceded by @ is of type *current* and expressed in Ampere; other variables are of type *voltage* and expressed in Volt. (the g in "gib" refers to the Ngspice notation of a voltage controlled current source)

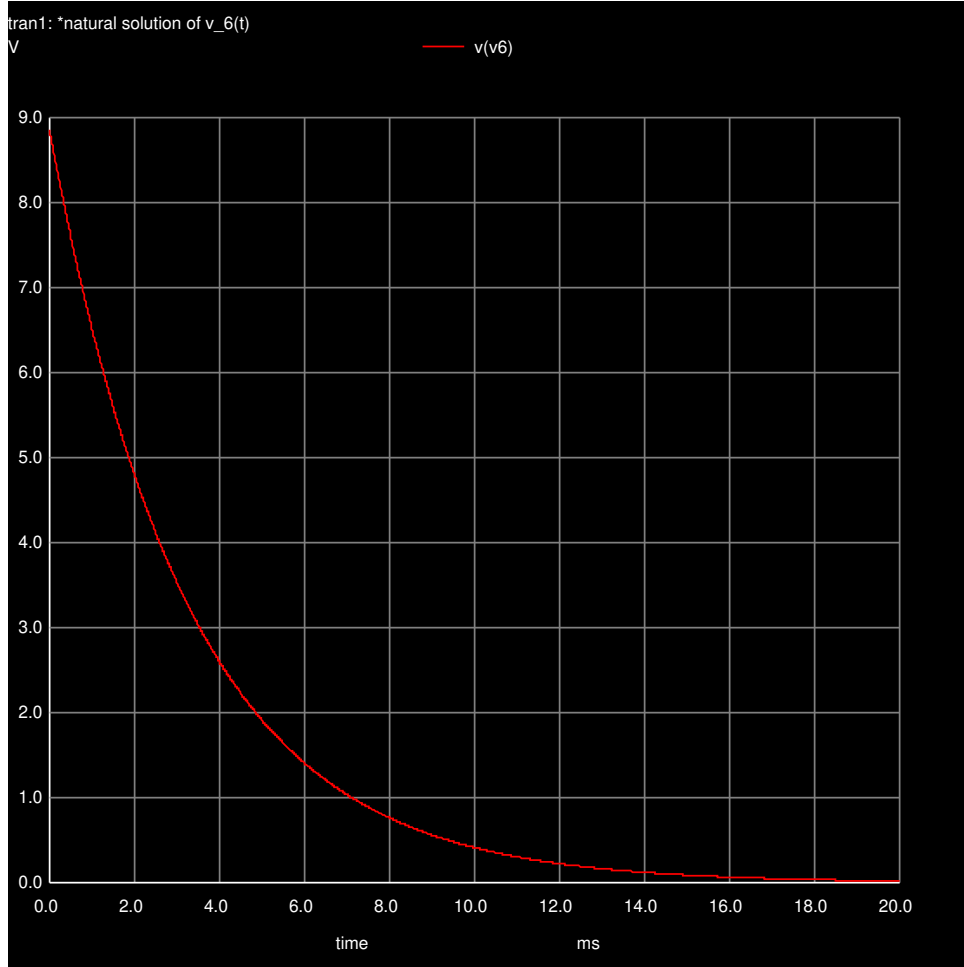
Name	Value [A or V]
@gib[i]	3.537727e-18
@r1[i]	3.373972e-18
@r2[i]	3.537727e-18
@r3[i]	1.637547e-19
@r4[i]	-7.08991e-19
@r5[i]	2.823391e-03
@r6[i]	5.749731e-19
@r7[i]	5.749731e-19
v1	0.000000e+00
v2	3.387204e-15
v3	1.078921e-14
v5	2.893565e-15
v6	8.853438e+00
v7	-1.17334e-15
v8	-1.77636e-15
v9	0.000000e+00

### 3.3 Exercise 3

In this section we used the results obtained in section 3.2 to determine the natural solution  $v_{6n}(t)$  in the interval  $[0, 20]ms$  using the boundary conditions  $V_6$  and  $V_8$ .

Figure 8 shows the plot of the required result that was obtained using the transient analysis.

Figure 8: Natural solution,  $v_{6n}(t)$  in  $V$  in the interval  $[0, 20]ms$

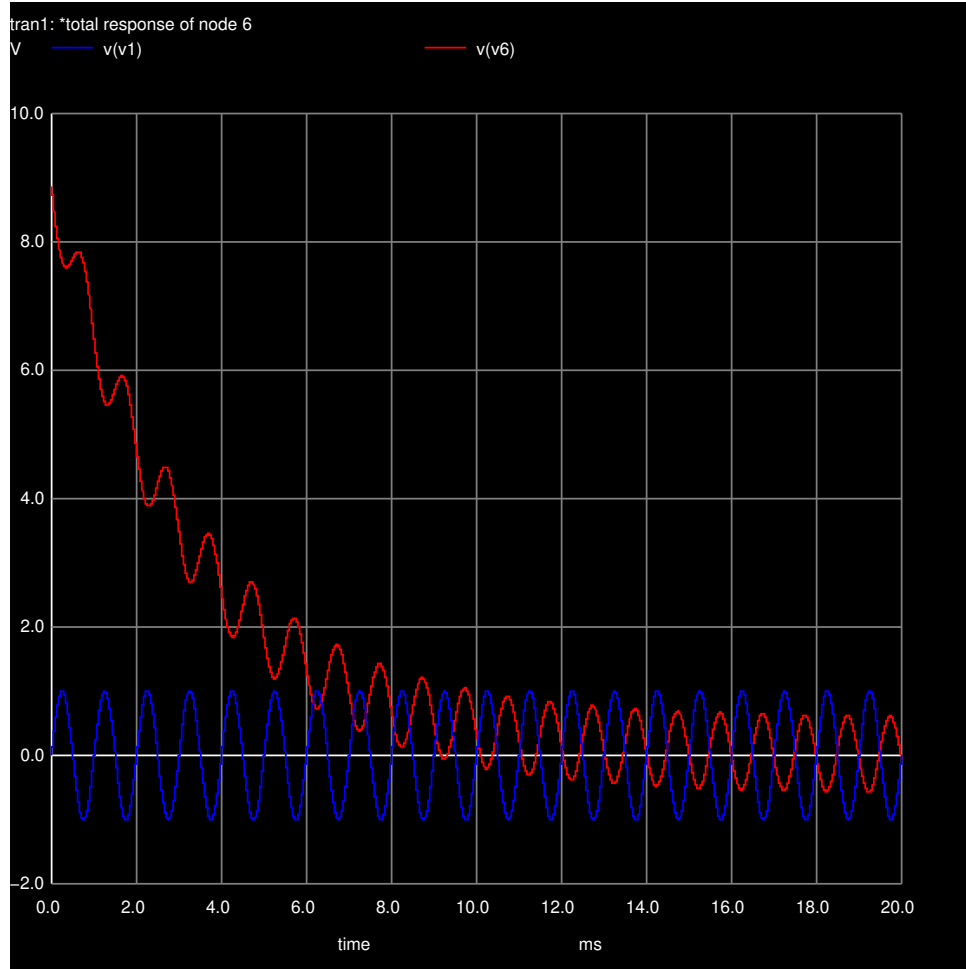


### 3.4 Exercise 4

In this section we are required to simulate the total response in node 6  $v_6(t)$  by repeating the procedure of 3.3 with the initially given  $v_s(t)$  (shown in 1, with a frequency of  $1000Hz$ ).

Figure 9 shows the plot of the required result that was obtained using the transient analysis as well as the stimulus (shown as  $v(V_1)$  since  $v_1(t) = v_s(t)$ )

Figure 9: Total response,  $v_6(t)$  in  $V$ , and stimulus  $v_s(t)$ , in  $V$  in the interval  $[0, 20]ms$



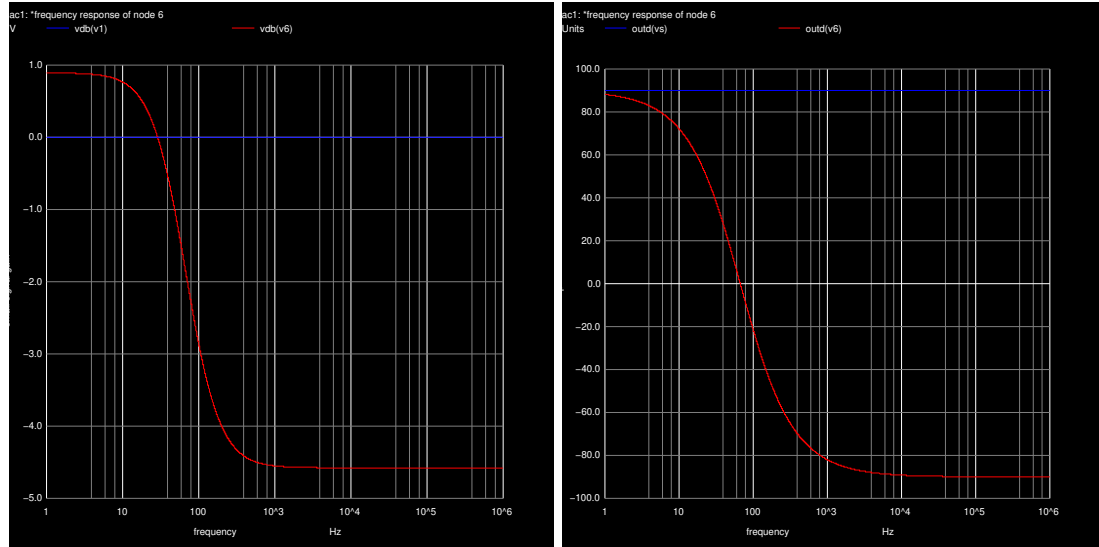
### 3.5 Exercise 5

In this section we are required to simulate the frequency response in node 6  $v_6(t)$  with the frequency in logscale, magnitude in  $dB$  and phase in degrees for a range of  $0.1Hz$  to  $1MHz$ .

Figure 10 shows the plot of the required result,  $v_6(f)$  as well as  $v_s(f)$ .

Since the source of frequency change is  $v_s$  itself, it is expected to not to show a frequency response since it changes alongside frequency (and in  $\log(1) = 0$ ), whereas  $v_6$  is dependant of the value that  $v_s$  takes.

Figure 10: Frequency response,  $v_6(f)$  in  $V$ , and  $v_s(f)$ , in  $V$ . Phase is in degrees and Magnitude in  $dB$



## 4 Conclusion

By analysing the circuit theoretically, with both the mesh and the node methods, and then simulating the circuit using Ngspice, we can verify that the values of the unknown components match almost perfectly and all approaches agree on the final currents' directions across the circuit's branches (which can be seen below in figure 11).

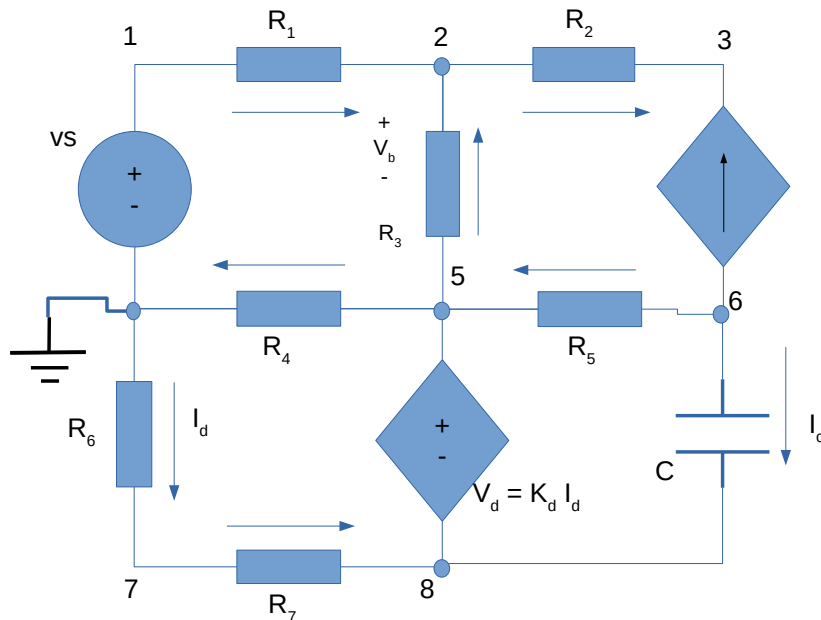


Figure 11: Representation of the final circuit with all the correct directions for the currents.

Some small discrepancies like the value of  $V_b$  obtained in section 3 differing from the ones found on sections ?? and ?? are due to the small number of decimal places considered by



Ngspice leading to slight inaccuracies. However, considering that the circuit complexity is still not considered, the differences are negligible.

In any case, the node analysis uses the Kirchhoff Current Law while the Mesh Analysis uses the Kirchhoff Voltage Law. This means that if a circuit contains more voltage sources than current sources, the mesh method is going to be more exact, as it is the other way around.

In this circuit, both types of sources have the same number of components; a fact that might help justify the accuracy of the results. Even more, it only includes linear components, making it so that the theoretical values are expected to be almost the same as the ones obtained in the simulation. Furthermore, as already mentioned, the low complexity of the circuit makes it that both methods are still extremely reliable.

All of this leads to the conclusion that the making of this laboratory assignment was coherent and that the main goal was attained: to achieve the circuit analysis through 3 different methods (mesh, nodal and simulated analysis).