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Contents

1	Hyperfine Splitting	2
2	Deuteron	3
3	Cross-section and Beam Intensity for an interaction	3
4	Elastic scattering, De-excitation, Fission	5

1 Hyperfine Splitting

Splitting of Na ground and excited states

we know,

$$\vec{F} = \vec{I} + \vec{J} \quad (1)$$

$$\Delta E = A \vec{I} \cdot \vec{J} \quad (2)$$

$$\Rightarrow \frac{A}{2} \left(|\vec{F}|^2 - |\vec{I}|^2 - |\vec{J}|^2 \right) \quad (3)$$

$$\Rightarrow \frac{A}{2} [F(F+1) - I(I+1) - J(J+1)] \quad (4)$$

For each \vec{F} there is different levels in the range

$$|I - J| \leq F \leq I + J \quad (5)$$

If $I \geq J$ there are $2J+1$ levels and if $J \geq I$ there are $2I+1$ levels.

Ground state of Na ($S_{\frac{1}{2}}$) has $I \geq J$ and $J = 1/2$. Therefore, $2J+1 = 2$ states.

Second excited state of Na ($P_{\frac{3}{2}}$) has $I \geq J$ and $J = 3/2$. Therefore, $2J+1 = 4$ states.

Constant of proportionality A

Ground state splitting,

$$h\Delta v = \frac{6.626 \times 10^{-34} \text{ Js} \times 1772 \times 10^6 \text{ X s}^{-1}}{1.6 \times 10^{-19} \frac{\text{J}}{\text{eV}}} = 7.33 \mu\text{eV} \quad (6)$$

$$\Delta E(F=2) - \Delta E(F=1) = h\Delta v \quad (7)$$

$$\Rightarrow \frac{A}{2} [2(3) - 1(2)] = 7.33 \mu\text{eV} \quad (8)$$

$$\Rightarrow 2A = 7.33 \mu\text{eV} \quad (9)$$

$$\Rightarrow A = 3.67 \mu\text{eV} \quad (10)$$

First excited state splitting,

$$h\Delta v = \frac{6.626 \times 10^{-34} \text{ Js} \times 192 \times 10^6 \text{ X s}^{-1}}{1.6 \times 10^{-19} \frac{\text{J}}{\text{eV}}} = 0.795 \mu\text{eV} \quad (11)$$

$$\Delta E(F=2) - \Delta E(F=1) = h\Delta v \quad (12)$$

$$\Rightarrow \frac{A}{2} [2(3) - 1(2)] = 0.795 \mu\text{eV} \quad (13)$$

$$\Rightarrow 2A = 0.795 \mu\text{eV} \quad (14)$$

$$\Rightarrow A = 0.397 \mu\text{eV} \quad (15)$$

Second excited state splitting, between F=0 and F=1,

$$h\Delta v = \frac{6.626 \times 10^{-34} \text{ Js} \times 17.1 \times 10^6 \text{ X s}^{-1}}{1.6 \times 10^{-19} \frac{\text{J}}{\text{eV}}} = 0.07 \mu\text{eV} \quad (16)$$

$$\Delta E(F=1) - \Delta E(F=0) = h\Delta v \quad (17)$$

$$\Rightarrow \frac{A}{2} [1(2) - 0(1)] = 0.07 \mu\text{eV} \quad (18)$$

$$\Rightarrow A = 0.07 \mu\text{eV} \quad (19)$$

Second excited state splitting, between F=1 and F=2,

$$h\Delta v = \frac{6.626 \times 10^{-34} \text{ Js} \times 36.6 \times 10^6 \text{ s}^{-1}}{1.6 \times 10^{-19} \frac{\text{J}}{\text{eV}}} = 0.152 \mu\text{eV} \quad (20)$$

$$\Delta E(F=2) - \Delta E(F=1) = h\Delta v \quad (21)$$

$$\Rightarrow \frac{A}{2}[2(3) - 1(2)] = 0.152 \mu\text{eV} \quad (22)$$

$$\Rightarrow 2A = 0.152 \mu\text{eV} \quad (23)$$

$$\Rightarrow A = 0.0757 \mu\text{eV} \quad (24)$$

Second excited state splitting, between F=2 and F=3,

$$h\Delta v = \frac{6.626 \times 10^{-34} \text{ Js} \times 60.9 \times 10^6 \text{ s}^{-1}}{1.6 \times 10^{-19} \frac{\text{J}}{\text{eV}}} = 0.252 \mu\text{eV} \quad (25)$$

$$\Delta E(F=3) - \Delta E(F=2) = h\Delta v \quad (26)$$

$$\Rightarrow \frac{A}{2}[3(4) - 2(3)] = 0.252 \mu\text{eV} \quad (27)$$

$$\Rightarrow 3A = 0.252 \mu\text{eV} \quad (28)$$

$$\Rightarrow A = 0.084 \mu\text{eV} \quad (29)$$

2 Deuteron

3 Cross-section and Beam Intensity for an interaction

Cross-section for an interaction

It is the measure of the probability of a collision taking place between particles. It is expressed as an area.

The total rate $W \propto NI$

where,

N = number of exposed targets

I = flux of incoming particles per unit area per unit time.

Therefore, $W = \sigma NI$

where σ is **cross-section** and the **constant of proportionality** with dimensions of area.

Beam Intensity

Assume a small length dx of solid perpendicular to the beam of area A . The change in intensity is $-dI$. This is equal to number of particles removed from the beam per unit area in length dx . Number of particles, N is

$$N = nAdx \because n \text{ is number of particles per unit volume}$$

$$W = \sigma_t IN = -AdI \quad (30)$$

$$W = \sigma_t I(nAdx) = -AdI \quad (31)$$

$$\Rightarrow \frac{dI}{I} = -n\sigma_t dx \quad (32)$$

$$\Rightarrow I(x) = I_0 e^{-n\sigma_t x} \quad (33)$$

Thickness of Lead required

Given,

$$I(d) = \frac{I_o}{1000} \quad (34)$$

$$\rho(Pb) = 11300 \text{kgm}^{-3} \quad (35)$$

$$m_{pb}(\text{mass of Pb}) = 207.21u \quad (36)$$

$$n = \frac{\rho}{m_{pb}} \quad (37)$$

from above 3 equations,

$$n = \frac{11300 \text{kgm}^{-3}}{207.21 \times 1.66 \times 10^{-27} \text{kg}} = 3.28 \times 10^{28} \text{m}^{-3} \quad (38)$$

$$\sigma_t = 2.6 \times 10^3 \text{barns} = 2.6 \times 10^{-25} \text{m}^2 \quad (39)$$

$$\frac{I(d)}{I_o} = e^{-n\sigma_t d} \quad (40)$$

$$10^{-3} = e^{-n\sigma_t d} \quad (41)$$

$$3 \ln(10) = 3.28 \times 10^{28} \times 2.6 \times 10^{-25} \times d \quad (42)$$

$$d = 0.81 \text{mm} \quad (43)$$

Thickness of Aluminum required

Given,

$$I(d) = \frac{I_o}{1000} \quad (44)$$

$$\rho(Al) = 2700 \text{kgm}^{-3} \quad (45)$$

$$m_{Al}(\text{mass of Al}) = 26.29u \quad (46)$$

$$n = \frac{\rho}{m_{Al}} \quad (47)$$

from above 3 equations,

$$n = \frac{2700 \text{kgm}^{-3}}{26.29 \times 1.66 \times 10^{-27} \text{kg}} = 6.18 \times 10^{28} \text{m}^{-3} \quad (48)$$

$$\sigma_t = 13 \text{barns} = 13 \times 10^{-28} \text{m}^2 \quad (49)$$

$$\frac{I(d)}{I_o} = e^{-n\sigma_t d} \quad (50)$$

$$10^{-3} = e^{-n\sigma_t d} \quad (51)$$

$$3 \ln(10) = 6.18 \times 10^{28} \times 13 \times 10^{-28} \times d \quad (52)$$

$$d = 85.98 \text{mm} \quad (53)$$

4 Elastic scattering, De-excitation, Fission

Attenuation rate

Given,

$$I_o = 10^5 s^{-1} \quad (54)$$

$$\rho x = 10^{-1} kg m^{-2} \quad (55)$$

$$\sigma_e = 20 mb \quad (56)$$

$$\sigma_c = 70 b \quad (57)$$

$$\sigma_f = 200 b \quad (58)$$

$$A = 235 \quad (59)$$

$$N_A = \text{Avogadro's Number} \quad (60)$$

$$I(x) = I_o e^{-n\sigma_t x} \quad (61)$$

$$n = \frac{\rho}{m_U} \quad (62)$$

$$m_U = \frac{A}{N_A \times 10^3} \text{ in Kg} = \frac{235}{6.023 \times 10^{26}} = 3.90 \times 10^{-25} kg \quad (63)$$

$$\sigma_t = \sigma_e + \sigma_c + \sigma_f = 270.02 \times 10^{-28} m^2 \quad (64)$$

$$nx = \frac{\rho x}{m_U} = \frac{10^{-1}}{3.90 \times 10^{-25}} m^{-2} = 2.56 \times 10^{23} m^{-2} \quad (65)$$

$$n\sigma_t x = 6.92 \times 10^{-3} \quad (66)$$

$$e^{-n\sigma_t x} = 0.9931 \quad (67)$$

Attenuation rate, $\frac{I(x)}{I_o} = 0.9931$

(68)

Number of fission reactions per second

Replacing σ_t with σ_f to get only Intensity decreased by fission reaction.

$$\frac{I_f(x)}{I_o} = e^{-n\sigma_f x} \quad (69)$$

$$\Rightarrow nx = 2.56 \times 10^{23} m^{-2} \text{ and } \sigma_f = 200 \times 10^{-28} m^2 \quad (70)$$

$$-n\sigma_f x = 5.12 \times 10^{-3} \quad (71)$$

$$e^{-n\sigma_f x} = 0.9948 \quad (72)$$

$$\frac{I_f(x)}{I_o} = 0.9948 \quad (73)$$

Intensity decreased by fission is equal to $I_o - I_f(x)$,

$$I_o - I_f(x) = I_o(1 - e^{-n\sigma_f x}) = 10^5(1 - 0.9948) = 510 s^{-1} \quad (74)$$

Number of fission reactions per second = $510 s^{-1}$

(75)

Elastic scattering

Attenuation due to elastic scattering,

$$\frac{I_e(x)}{I_o} = e^{-n\sigma_e x} \quad (76)$$

$$\Rightarrow nx = 2.56 \times 10^{23} m^{-2} \text{ and } \sigma_e = 20 \times 10^{-31} m^2 \quad (77)$$

$$-n\sigma_e x = 5.12 \times 10^{-7} \quad (78)$$

$$e^{-n\sigma_e x} = 0.999999488 \quad (79)$$

$$\frac{I_e(x)}{I_o} = 0.999999488 \quad (80)$$

Number of scattered per second = $I_o(1 - \frac{I_e(x)}{I_o}) = 5.1 \times 10^{-2} s^{-1}$.

Area of sphere at 10m = $400\pi m^2$

$$\text{Flux} = \frac{I}{A} = \frac{5.1 \times 10^{-2}}{400\pi} m^{-2} s^{-1} = 4.074 \times 10^{-5} m^{-2} s^{-1} \quad (81)$$

For gamma rays,

$$\frac{I_c(x)}{I_o} = e^{-n\sigma_c x} \quad (82)$$

$$\Rightarrow nx = 2.56 \times 10^{23} m^{-2} \text{ and } \sigma_c = 70 \times 10^{-28} m^2 \quad (83)$$

$$-n\sigma_c x = 1.792 \times 10^{-3} \quad (84)$$

$$e^{-n\sigma_c x} = 0.9982 \quad (85)$$

$$\frac{I_c(x)}{I_o} = 0.9982 \quad (86)$$

Number of scattered per second = $I_o(1 - \frac{I_c(x)}{I_o}) = 179 s^{-1}$.

Area of sphere at 10m = $400\pi m^2$

$$\text{Flux} = \frac{I}{A} = \frac{179}{400\pi} m^{-2} s^{-1} = 0.1424 m^{-2} s^{-1} \quad (87)$$